

Readers' Forum

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Comment on "Approximate Formula of Weak Oblique Shock Wave Angle"

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Introduction

IN Ref. 1 the authors describe two approximate formulas for evaluation of the wave angle β of an oblique shock wave in terms of the deflection angle θ and the upstream Mach number M_1 . These formulas are only valid for a limited range of deflection angles and upstream Mach numbers and are derived by the authors using the physically exact relations for a two-dimensional oblique shock wave in the form of Eq. (1), which was stated for the first time by Schubert² in 1943 as

$$\frac{\tan(\beta - \theta)}{\tan \beta} = \frac{(\gamma - 1)M_1^2 \sin^2 \beta + 2}{(\gamma + 1)M_1^2 \sin^2 \beta} \quad (1)$$

The disadvantage of Eq. (1) is the implicit relation between θ , β , and M_1 , which does not allow the wave angle β to be solved directly.

Nevertheless, the explicit and analytically exact expression for the wave angle β resulting from Eq. (1) was already derived in 1972 by the German mathematician Wellmann.³ By rewriting the more general form of Eq. (1)

$$\frac{\sin(\beta + \alpha) \sin(\beta - \alpha) \cos(\beta - \theta)}{\sin \beta \sin \theta} = \frac{\gamma + 1}{2} \quad (2)$$

$$\sin \alpha = 1/M_1 \quad (3)$$

in a cubic relation for $\tan \beta$, Wellmann obtained the following equation:

$$\begin{aligned} \tan \theta \left[\frac{\gamma - 1}{2} + \frac{\gamma + 1}{2} \tan^2 \alpha \right] \tan^3 \beta - \tan^2 \beta \\ + \tan \theta \left[\frac{\gamma + 1}{2} + \frac{\gamma + 3}{2} \tan^2 \alpha \right] \tan \beta + \tan^2 \alpha = 0 \end{aligned} \quad (4)$$

The solution of Eq. (4) is easily obtained and reads

$$\begin{aligned} \tan \beta = \frac{b + 9ac}{2(1 - 3ab)} \\ - \frac{d(27a^2c + 9ab - 2)}{6a(1 - 3ab)} \cdot \tan \left[\frac{n}{3} \pi + \frac{1}{3} \arctan \frac{1}{d} \right] \end{aligned} \quad (5)$$

$$n = 0, 1, -1$$

with

$$a = \left[\frac{\gamma - 1}{2} + \frac{\gamma + 1}{2} \tan^2 \alpha \right] \tan \theta$$

$$b = \left[\frac{\gamma + 1}{2} + \frac{\gamma + 3}{2} \tan^2 \alpha \right] \tan \theta$$

$$c = \tan^2 \alpha$$

$$d = \sqrt{\frac{4(1 - 3ab)^3}{(27a^2c + 9ab - 2)^2} - 1}$$

From Eq. (5), the following solutions for the wave angle β of a two-dimensional oblique shock wave can be obtained:

$n = 0$ the weak solution ($M_2 < 1$)

$n = 1$ the strong solution ($M_2 < 1$)

$n = -1$ a physically meaningless solution (decreasing entropy)

Since Eq. (5) represents the exact solution of Eq. (1) for the wave angle β of weak and strong oblique shocks in terms of the deflection angle θ and the upstream Mach number M_1 , no approximations to Eq. (1) are necessary any more.

Finally, it should be noted that Wellmann also derived explicit expressions for the maximum wave angle θ_m (i.e., the limiting wave angle for which the shock is attached) and the sonic wave angle θ_s (i.e., the wave angle for which $M_2 = 1$). The solutions are

$$\begin{aligned} \cos 2\theta_m = \frac{1}{\gamma} \left[\left(\frac{\gamma + 1}{2} - \cos 2\alpha \right) \right. \\ \left. - \sqrt{\gamma + 1} \cdot \sqrt{\left(\frac{\gamma + 1}{2} - \cos 2\alpha \right)^2 + \frac{\gamma}{4} (3 - \gamma)} \right] \end{aligned} \quad (6)$$

$$\begin{aligned} \sin^2 \theta_s = \frac{1}{2\gamma} \left[\left(\frac{\gamma - 3}{2} \sin^2 \alpha + \frac{\gamma + 1}{2} \right) \right. \\ \left. + \sqrt{4\gamma \sin^4 \alpha + \left(\frac{\gamma - 3}{2} \sin^2 \alpha + \frac{\gamma + 1}{2} \right)^2} \right] \end{aligned} \quad (7)$$

Furthermore, Wellmann derived a lot of useful explicit expressions for the evaluation of shock wave reflections at solid walls and freestream boundaries. For details see the original report, Ref. 3.

References

- ¹Dou, H. S., and Teng H. Y., "Approximate Formula of Weak Oblique Shock Wave Angle," *AIAA Journal*, Vol. 30, No. 3, 1992, pp. 837-839.
- ²Schubert, F., "Zur Theorie des stationären Verdichtungsstoßes," *Zeitschrift für Angewandte Mathematik und Mechanik*, Vol. 23, 1943, pp. 129-138.
- ³Wellmann, J., "Vereinfachung von Rechnungen am schiefen Verdichtungsstoß," *Deutsche Luft- und Raumfahrt*, Forschungsbericht 72-11, Deutsche Forschungs- und Versuchsanstalt für Luft- und Raumfahrt, Institut für Aerodynamik, Braunschweig, Germany, Jan. 1972.

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