

Value-Based Multidisciplinary Techniques for Commercial Aircraft System Design

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A quantitative tool is presented to perform program-level valuation of commercial aircraft designs. The algorithm used expands on traditional net present value methods through the explicit consideration of market uncertainty and the ability of the firm to react to such uncertainty through real-time decision making throughout the course of the aircraft program. The algorithm links three separate models, performance, cost, and revenue, into a system-level analysis by viewing the firm as a decision-making agent facing continuous choices between several different operating modes. An optimization problem is set up and solved using a dynamic programming approach to find a set of operating mode decisions that maximizes the firm's expected value from the aircraft project. The result is a quantification of value that can be used to make program-level design trades and to gain insight into the effects of uncertainty on a particular aircraft design. Examples are drawn from the blended-wing-body aircraft concept to demonstrate the operation of the program valuation tool.

Introduction

TRADITIONAL methods for creating a commercial aircraft program typically consist of at least two distinct design efforts, the engineering development of the airframe itself and the strategic development of the aircraft program. The latter addresses questions such as which aircraft designs to invest in (product mix), how much production to plan for (sales volume), what prices and costs to expect (profitability), and how to plan for unforeseen market developments (flexibility).

In the past, the two elements of program design, engineering development and strategic development, have often been executed entirely separately from each other. Engineering and finance are often handled by different groups and at different times. When engineering and finance are uncoupled, a firm runs the risk of overlooking important interactions between the two. A design system that performs engineering and financial analysis simultaneously may improve on the efficiency and effectiveness of the traditional methods.

Numerous advances have been made in the application of multidisciplinary techniques to the engineering facet of aircraft development. The field of multidisciplinary design optimization (MDO) combines engineering disciplines, such as aerodynamics, structural dynamics, and controls, to provide a design framework that "coherently exploits the synergism of mutually interacting phenomena."¹ MDO has been implemented across a wide range of applications for aircraft design.^{1,2} Whereas multidisciplinary analysis and optimization has seen extensive use for technical design problems in aerospace, there has been less emphasis on applying these techniques to larger scope system design. Frameworks have been developed that include both engineering and cost elements for aircraft design^{3,4} and aircraft engine design.^{5,6} A common feature of those frameworks is that they use Monte Carlo simulation (MCS) to explore the impact of uncertainty on system design. Whereas MCS

provides a means to perform probabilistic analysis of a series of designs, it does not rigorously address the issue of real-time managerial decision making. Tools such as real options and game theory have been suggested as a means to incorporate decision making (for example, in Ref. 5) but do not appear to have been implemented as such.

The objective of this paper is to couple engineering and financial design, or, phrased differently, product and program design, to extract maximum value from the commercial aircraft design process. A multidisciplinary analysis is synthesized by creating three free-standing quantitative models, performance, cost, and revenue, and linking them to compute a measure of program value. Although the models are not high fidelity, their purposes are to establish a useful foundation for further study and to gain insight into the interactions between technical and program design.

To link the three models into an integrated multidisciplinary analysis tool, consideration must be given to the program structure, that is, the decision structure affecting product mix, design and production plans, and pricing strategy. With this element in place, the stage is set for a quantitative valuation of the program, which enables both technical and program-based trade studies to search for an optimal system design. This conceptual process is shown in Fig. 1. In this work, the valuation will be performed using a dynamic programming (DP) framework. The DP approach provides a quantitative measure of the program's net present value (NPV), while explicitly accounting for the effects of uncertainty and program flexibility by modeling the program as a series of decisions. This approach has been explored in finance literature as real options, for example, in Refs. 7 and 8. The algorithm results in a series of decision rules, which define the optimal decision strategy as a function of evolving and uncertain market conditions. This information could not be obtained using a MCS approach.

The next section summarizes the multidisciplinary approach taken to accomplish the objective by describing the three distinct models used to solve the problem: performance, cost, and revenue estimation. The following section describes the DP approach to link these models into one program value analysis tool, and two examples are given to demonstrate the operation of the valuation tool for analysis of a blended-wing-body (BWB) family of aircraft.⁹ Finally, the results are discussed, and conclusions are drawn.

Performance Model

The performance estimator is based on the WingMOD aircraft design tool. WingMOD is an MDO code that optimizes aircraft

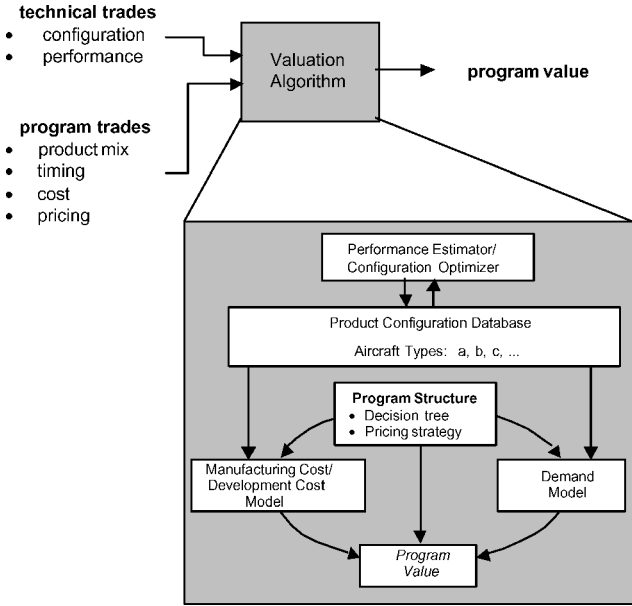
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Table 1 WingMOD outputs used as an input to the value framework

Output	Description
Maximum TOW	Gross vehicle weight at start of maximum range mission.
Design landing weight	Gross vehicle weight at end of maximum range mission.
Design range	Maximum range, specified as a constraint.
Seats	Number of passenger seats, specified as a constraint.
Weight breakdown	Estimates of weight for each primary component of the aircraft, summing to operating empty weight.
Structure: fuselage bays, inner wing, outer wing, etc.	Structural elements (spars, ribs, skin, etc.).
Propulsion	Structural weight broken down into a set of large parts, which together comprise the airframe.
Systems	Engines, nacelles, and supporting equipment.
	Onboard systems, for example, avionics, fuel, hydraulics.
Payloads	Seats, bag racks, cargo equipment, etc.

**Fig. 1 Value-based design process.**

wings and horizontal tails subject to a wide array of practical constraints.^{10,11} WingMOD uses low-fidelity analyses to analyze an aircraft quickly in over 20 design conditions that are needed to address issues from performance, aerodynamics, loads, weights, balance, stability, and control. The low computational cost of the simple analyses allows the examination of all of these issues in an optimization with over 100 design variables while achieving reasonable computation time.

As detailed in Ref. 10, the WingMOD optimization framework takes a set of constraints representing mission requirements (range, payload capacity, cruise speed, approach speed, balance, etc.) and finds an optimal aerodynamic and structural configuration such that the resulting aircraft satisfies the constraints. In the valuation framework described here, the performance characteristics of the aircraft were assumed to be fixed, that is, WingMOD was run a priori to determine the minimum takeoff weight aircraft. Certain properties of the resulting design were then used as input to the value framework. These WingMOD outputs are summarized in Table 1.

Cost Model

The cost model has two components: manufacturing cost and development cost. Although detailed cost models are available publicly, such as the Aircraft Life Cycle Cost Analysis (ALCCA) code,¹² for this research, a simple cost model was developed. An important attribute of the cost model is that it should capture the effect of commonality between several different airframes; in general, both the

development cost and manufacturing cost of a new aircraft will depend on the aircraft's technical parameters and the technical parameters of other aircraft types that have already been designed or built.

The cost models used for this research are based on the decomposition of the aircraft into a set of components. A simple cost per pound estimation is applied at a component level and further modified with learning curve effects. The cost model parameters were derived from publicly available data and are published in detail in Refs. 13 and 14. A more detailed cost model could be linked to the valuation framework, provided commonality effects are captured.

Revenue Model

Given an aircraft design, a production rate, and a time horizon, the revenue model must provide the following three outputs: potential revenue cashflow for the current time period, the expected value of future revenue cashflows, and a measure of the uncertainty of the future cashflows. Furthermore, the model must demonstrate realistic sensitivities to changes in aircraft performance, for example, reduction in fuel burn, changes in the aircraft target market, for example, 100 vs 250 passengers, and changes in aircraft price charged, that is, demand price elasticity. To achieve this functionality, the model development is broken up into a static analysis and a dynamic analysis.

Static Demand Analysis

The static analysis estimates a baseline price and corresponding quantity demanded, along with an expected demand growth rate over the specified time horizon. Price is modeled as a function of several variables representing an aircraft's value to its operator, an airline. Several sets of variables and several functional forms were tested by applying the price model to 23 existing aircraft: 11 narrowbodies and 12 widebodies. The outputs generated by the price model were compared to best estimates for the actual sale prices for each of the aircraft, compiled from two sources.^{15,16} For each functional form tested, the function parameters were adjusted to minimize the mean squared error of estimated price.

The selected functions for narrowbody (NB) and widebody (WB) aircraft are shown next. Note that speed (or Mach number) is not one of the variables. No significant statistical relationship between price and speed was found in the range of available data. Thus,

$$\text{Price NB} = \left[0.735 \left(\frac{\text{Seats}}{\text{Seats}_{\text{ref}}} \right)^{1.910} + 0.427 \left(\frac{\text{Range}}{\text{Range}_{\text{ref}}} \right) \right] \text{Price}_{\text{ref}} - \Delta(\text{LC}) \quad (1)$$

$$\text{Price WB} = \left[0.508 \left(\frac{\text{Seats}}{\text{Seats}_{\text{ref}}} \right)^{2.760} + 0.697 \left(\frac{\text{Range}}{\text{Range}_{\text{ref}}} \right) \right] \text{Price}_{\text{ref}} - \Delta(\text{LC}) \quad (2)$$

where Seats is the passenger capacity, Range is the design range, and Seats_{ref}, Range_{ref}, and Price_{ref} are reference values of 419 seats, 8810 n miles, and \$148.7 million, respectively. $\Delta(\text{LC})$ is an increment in life cycle (LC) cost due to off-nominal cash airplane related operating costs (CAROC), which are equal to total operating costs less ownership costs. This term refers to the additional cost the operator incurs if the aircraft's CAROC is greater than the industry average CAROC for an aircraft of its size. It is a function of the difference between the aircraft's CAROC and the least-squares estimate for the CAROC of an aircraft with the same capacity. The prices generated by the preceding functions are compared to the best estimates of the actual aircraft prices in Fig. 2.

Whereas the aircraft seat count and range are provided by the outputs of the performance model, its CAROC must be estimated separately. For the example used, the assumption is made that fuel costs

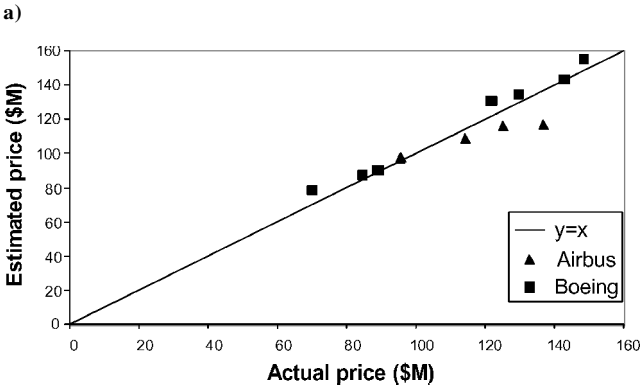
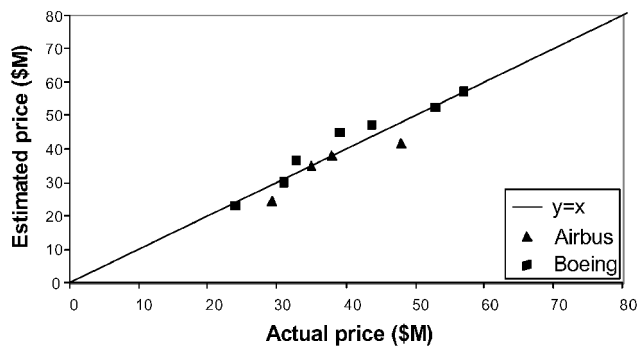


Fig. 2 Price model results: a) narrowbodies and b) widebodies.

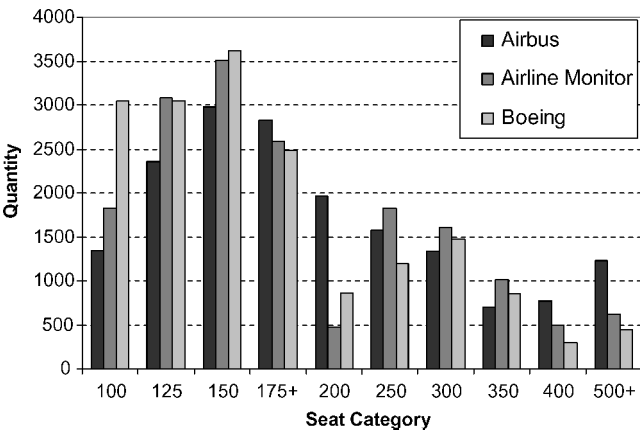


Fig. 3 Forecasted deliveries through 2019, 20-year gross demand.

for a reference mission (3000 n mile) represent 20% of CAROC. The figure of 20% is based on empirical data for several existing aircraft. Fuel burn is calculated using the Breguet range equation, and a fuel price of \$0.65 per gallon is used.

Quantity data are based on three distinct forecasts of quantities of aircraft to be delivered from 2000 through 2019 as released by The Boeing Company,¹⁷ Airbus,¹⁸ and the *Airline Monitor*.¹⁹ Each forecast has a different set of aircraft categories which comprise the global airline fleet. All three forecasts were recast into a single, consistent set of aircraft categories based on aircraft class (narrowbody or widebody) and seat count. Forecasted deliveries are assumed equivalent with quantities demanded at current market prices. The results are shown in Fig. 3. Depending on seat category, there is considerable variance between the three forecasts. This reflects differences in the forecasters' assumptions, methodology, and, to some extent, corporate strategy. Furthermore, the high variance reflects the high degree of uncertainty regarding future revenue cash flows.

For a given aircraft design, the quantity model proceeds as follows. Assign a given aircraft to a seat category; compute a 20-year gross demand for that category as the mean of the three forecasts;

assume a market share in that category; compute the 20-year quantity demanded as the market share multiplied by the 20-year gross demand; and compute the current annual quantity demanded by applying the expected annual demand growth rate. If several designs are considered for production simultaneously, fractions of seat category demands are assigned to each design, such that total quantity demanded will not exceed the product of market share and 20-year gross demand.

Dynamic Demand Analysis

The dynamic analysis aims to quantify the stochastic behavior of the market for commercial aircraft. It is observed that quantities of aircraft purchased fluctuate significantly from year to year and exhibit some cyclical properties. Thus, given a forecast for year 0, it is impossible to predict with certainty what the quantity of aircraft demanded will be in year 10. However, based on historical data, some representative characteristics were found to describe historical aircraft demand levels as geometric Brownian motions, not unlike stock prices. Therefore, the dynamic analysis uses an average annual growth rate of 4.43% and an average annual volatility of 45.57% for typical demand evolution patterns for widebody aircraft.

Dynamic Programming Formulation

The basic problem to be solved may be broken up into three parts: endogenous variables, those that are internal to the aircraft development process and may be controlled; exogenous variables, those that are external to the aircraft development process and may not be controlled; and a statement of the problem objective.

The endogenous variables constitute a set (or portfolio) of aircraft designs, any of which the producing firm may choose to develop and bring to market. To bring a concept to market, the firm must go through several phases: detail design, tooling and capital investment, testing, certification, and finally production. Each phase entails some required expenditure of time and money, and the firm may decide when to execute each phase. Each of the aircraft designs is defined by a set of component parts, for example, inner wing, outer wing, fuselage bay, etc., some of which may be common across several aircraft.

Given that an aircraft design is in production, the evolutions of sale price and quantity demanded are unaffected by any decisions made by the firm and are, thus, exogenous variables. Sale price evolves according to a steady growth rate, whereas quantity demanded evolves as a stochastic process, characterized by parameters such as drift rate and volatility. Each period that an aircraft design is in production, as many units are built and sold as are demanded, up to the maximum capacity of the plant.

Given the preceding endogenous and exogenous variables, the objective is to find a set of optimal decision rules governing which aircraft to design, which aircraft to produce, and when, as a function of the demand level and the aircraft built to date at any given time. Achieving this goal will necessarily yield the overall program value because program value is the objective function used to find the optimal decision rules.

General Theory

A stochastic DP problem may, in general, be framed in five parts:

- 1) State variables continuously evolve and completely define the problem at any point in time.

- 2) Control variables are set at any point in time by the decision maker and generally impact the evolution of the state variables.

- 3) Randomness is when one or more of the state variables is subject to random movements, and as such, involves a stochastic process.

- 4) The profit function is defined as follows. The goal of the DP method is to maximize some objective function, in this case the program value. The value is, in general, a function of certain profits incurred every period. These profits are functions of the state variables.

- 5) Dynamics represent the set of rules that govern the evolution of the state variables, including the effects of randomness, the effects of control variables, and any other relationships.

The problem is further defined by a time horizon (which may generally be finite or infinite) and a sequence of time periods of length Δt , which together comprise the time horizon. The objective, then, is to find the optimal vector of control variables as a function of time and state, such that the total value at the initial time is maximized. Equivalently, the objective may be stated recursively, as an expression for the value at any time t as

$$F_t(s_t) = \max_{u_t} \{ \pi_t(s_t, u_t) + [1/(1+r)] E_t[F_{t+1}(s_{t+1})] \} \quad (3)$$

where $F_t(s_t)$ is the value (objective function) at time t and state vector s_t , π_t is the profit in time period t as a function of the state vector s_t and the control vector u_t , r is some appropriate discount rate, and E_t is the expectation operator, providing in this case the expected value of F at time $t+1$, given the state s_t and control u_t at time t . Note that the expectation operation for next period is affected by the control decision and the state in this period.

Equation (3) is known as the Bellman equation and is based on Bellman's principle of optimality: "An optimal policy has the property that, whatever the initial action, the remaining choices constitute an optimal policy with respect to the subproblem starting at the state that results from the initial actions" (see Ref. 7). In other words, given that the optimal value problem is solved for time $t+1$ and onward, the action (choice of u) maximizing the sum of this period's profit flows and the expected future value is also the optimal action maximizing value for the entire problem for time t and onward.

The Bellman equation can, therefore, be solved recursively or, for a finite time horizon, iteratively. For a time horizon of T , this is done by first considering the end of the horizon, at time t_T . At this point, there are no future states and no future expected value of F . Therefore, the optimal control decisions u_{t_T} given the final state s_{t_T} are readily found. This process is repeated for all possible final values of the state vector s_{t_T} . Next, it is possible to take one step backward in time, to $t = t_{T-1}$. Now, Eq. (3) may be applied to find the optimal control decisions u_{t-1} because the expectation term $E[\dots]$, is easily calculated as the probability-weighted average of the possible future values of F_{t+1} . Again, the optimal control values u_{t-1} , are found for each possible value of s_{t-1} . At this point, the procedure is repeated by taking another backward timestep to $T-2$ and continuing to iterate until the initial time, $t=0$, is reached. Now, F_0 is known for all possible initial values of the state s_0 , and it is the optimal solution value.

Specific Application: Operating Modes

It is possible to extend the general DP framework presented to a specific application useful for the valuation of projects. The application is centered on the concept of operating modes, and has been demonstrated by several authors to be useful in modeling flexible manufacturing systems.^{8,20} Much of this description is based on their work.

Consider a hypothetical factory, which at the beginning of any time period may choose to produce output A or output B. Let the prices for which it can sell each of the outputs be different functions of a single random variable x , so that it may be more profitable in some situations to produce one output than the other. However, each time the factory switches production from A to B, or vice versa, a switching cost is incurred. Thus, it may not always be optimal simply to produce whichever output yields the higher profit flow in the current period. If there is a high probability of a switch back to the other output in the future, it may be preferable to choose the output with the lower profit this period.

This example lends itself well to the DP formulation. In this case, the control variable u_t is the choice of output, or operating mode, for the period beginning at time t : A or B. The state vector s_t consists of two elements, the random variable x and the operating mode from last period m_t . The operating mode m will have one of two possible values, for example, 0 or 1, representing output A and B. Depending on the value of m_t , the control variable choice u_t may result in payment of a switching cost. Specifically, the Bellman

equation may be rewritten for this example as

$$F_t(x_t, m_t) = \max_{u_t} \{ \pi_t(x_t, u_t) - I(m_t, u_t) + [1/(1+r)] E_t[F_{t+1}(x_{t+1}, u_t)] \} \quad (4)$$

Note that the state vector s has been separated into its two components, the random variable x and last period's operating mode m . Here, the profit function term from Eq. (3) has been replaced by the difference between a profit flow and $I(m_t, u_t)$, the switching cost from mode m to mode u . This will equal zero if $m_t = u_t$ and there is in fact no switch made and will be nonzero otherwise. Note also that the future value F_{t+1} (for which the expectation is found) is a function of the future random variable x_{t+1} and of the current control decision u_t because u_t will become the operating mode from last period m_{t+1} at time $t+1$. In other words, $m_{t+1} = u_t$ because as soon as the control decision u_t is made, the mode in which next period will be entered, m_{t+1} , is set. As before, this equation can be solved iteratively by starting at the final time period and working backward.

One additional point regarding Eq. (4) bears discussion: the selection of an appropriate discount rate r . This is a nontrivial task; in fact, the selection of a discount rate is traditionally one of the most difficult and sensitive steps in capital budgeting. For an in-depth discussion of discounting as it applies to this valuation technique, refer to Ref. 13.

Applying DP to the Aircraft Design Problem

The described DP approach is adapted here to solve the problem of optimal decision making in managing an aircraft program. The aircraft program valuation algorithm is briefly overviewed here in the context of the five parts that frame a DP problem:

- 1) For each new aircraft design being simultaneously considered, two state variables exist: quantity demanded, which evolves stochastically, and the "operating mode from last period" (as introduced earlier) for that aircraft.
- 2) For each aircraft design, one control variable exists: the choice of operating mode for the current period.
- 3) For each aircraft design, one state variable exists with random characteristics: the quantity demanded. It evolves from a given initial value as a stochastic process.
- 4) The profit function during each period is the sum of profits associated with the operating modes for each aircraft, less any switching costs incurred during that period. For production operating modes, the profits are simply revenues less recurring costs; however, other modes exist for which the profit functions represent nonrecurring costs.

- 5) There are two types of state variables in this formulation: quantity demanded, which evolves as a stochastic process, and operating mode, which evolves as dictated by the control variables (operating mode decisions). This defines the dynamics.

Given this framework, it is useful to consider the impact of various parameters on computation time. To solve the problem iteratively as just described, the algorithm must evaluate each possible combination of control variables for each possible state vector, and it must repeat this process for each time step in the problem's time horizon, starting at the final time $t = t_T$ and ending at $t = 0$. Therefore, at the most general level, computation time scales linearly with the time horizon and exponentially with the number of state variables. The time horizon, as defined in this application, is 30 years, which is a typical valuation time frame for an aircraft program. For purposes of simplicity and computation time constraints, the time period length Δt was selected to be one year. For the same purposes, the maximum number of aircraft designs to be simultaneously considered by the algorithm was set to two.

Connection to Operating Modes

Whereas the operating modes introduced earlier were simply modes of production, this formulation extends the operating mode framework to represent each phase of the life cycle of an aircraft program. The purpose of this extension is to model the significant time and investment required to develop an aircraft, before any sales

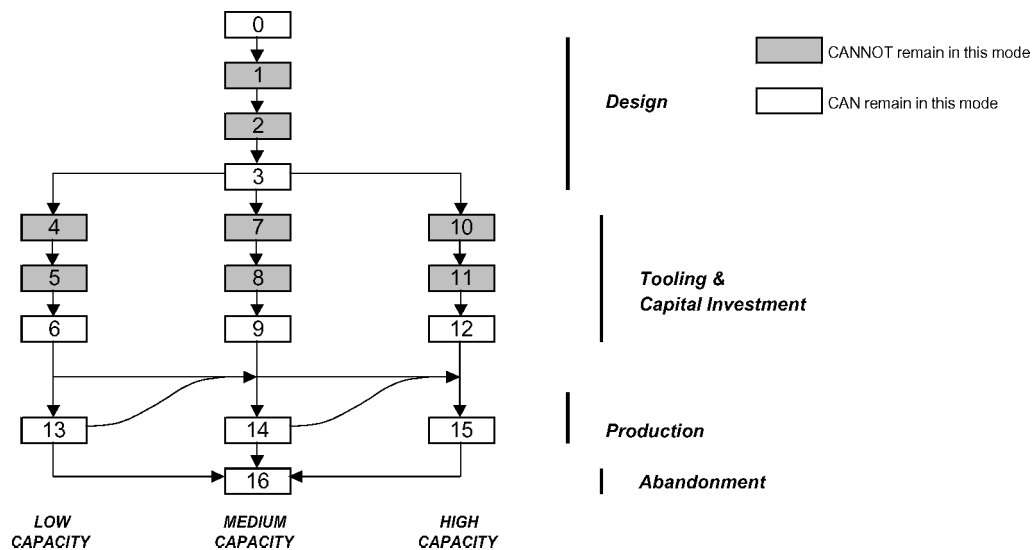


Fig. 4 Operating mode framework for a single aircraft.

are made. Therefore, the nonrecurring development process, which may last as many as six years, is represented as a chain of operating modes. Clearly, none of these modes entails a positive profit flow. Rather, each has some negative profit associated with the nonrecurring investment for that particular phase of the aircraft development cycle. The only incentive for the firm, and the optimizer, to enter one of these modes is the opportunity it creates to switch to the following development mode in the following period, and, so on, until the production mode is reached. A graphical representation of the operating modes for a single aircraft design is shown in Fig. 4. The diagram is similar in concept to a Markov chain, where the arrows represent possible transitions between modes. In fact, the arrows connecting the modes represent switching costs that are finite; if two modes are not connected by an arrow, the associated switching cost is infinite.

Mode 0 represents the initial conditions: the firm is waiting to invest. Modes 1–3 represent roughly the first half of the development effort, primarily detailed design. Note that several operating modes are shaded. The shading indicates an infinite cost not to switch to a different mode. In other words, it is impossible to remain in a shaded mode for more than one period. Thus, once the firm commits to a detail design effort, it is assumed impractical to stop halfway through. However, it is possible to stop before the second half of development, here, mostly tooling and capital investment, begins. Once this development stage is initiated, a capacity choice must be made: a low, medium or high capacity production line. This determines the maximum demand level that may be satisfied with sales every period. Once the capacity choice is made, the firm must continue to switch modes annually until it reaches mode 6, 9, or 12, at which point it is ready to enter production. Recall that each time period has a duration of one year; therefore, if the firm does not wait midway through the development process, an aircraft design takes six years to bring to market. (The six-year baseline duration may be altered, as discussed later.) The production modes are 13, 14, and 15, corresponding to a low-, medium-, and high-capacity line. Note that each mode will produce exactly as many units as demanded each period, up to a maximum that depends on the mode. The actual values for maximum capacity are parameters and easily changed. While in production (or waiting to enter production), it is possible to invest in additional tooling and expand the capacity of the production line. However, it is assumed impossible to reduce capacity, that is, the scrapping of tools has little to no salvage value, due to the high specificity of the tools to their product. Finally, an abandonment mode exists to model any salvage value associated with permanently shutting down the program. If the salvage value is positive, the switching costs to enter mode 16 will be negative. The determination of switching costs is based on the adaptation of the development cost and manufacturing cost models to the operating mode framework.

The development cost model generates a time profile of the nonrecurring expenses associated with the development of a given new aircraft design. Because of the inclusion of two aircraft designs in the valuation algorithm, the switching cost calculation proceeds as follows for each of the two aircraft designs. The sequential switching costs from mode 0 through mode 9 (medium production rate) are calculated by discretizing the nonrecurring cost time profile into one-year segments. This discretization is done as a step function of the operating mode of the other aircraft design: If the other aircraft has not yet been fully developed, the baseline nonrecurring cost profile is used. However, if the other aircraft has already been fully developed, the nonrecurring cost profile is calculated with any commonality effects included. Specifically, if the aircraft share any common components, the development cost and time are both reduced to reflect the savings resulting from a preexisting design. If the commonality effects are significant enough to result in a cost profile shorter than six years, one or more development modes are skipped. Finally, once medium capacity development process switching costs have been defined, the switching costs corresponding to the tooling/capital investment part of the development process are scaled by a low-capacity and a high-capacity scaling factor to find the switching costs corresponding to the low- and high-capacity decisions.

As with development cost, to account for two aircraft designs present in the valuation, the switching costs associated with manufacturing are found for each aircraft as functions of the operating mode of the other aircraft. Switching costs associated with manufacturing have two components. The first component is switching from a ready-to-produce mode (6, 9, or 12) into the corresponding production mode (13, 14, or 15, respectively). The second component is switching from one production line capacity to another. Both of these components are sometimes involved in a single switch, for example, 6 to 14 or 6 to 15; however, they are calculated separately and simply added together as necessary.

The costs of switching production line capacity are calculated as the product of a scaling factor (which is greater than one and represents the additional costs incurred due to disruption of a preexisting production line) and the cumulative difference in cash outflows between the two development processes associated with the production capacities in question. For example, the cost to switch from low to medium capacity (involved in either a 6 to 14 switch or a 13 to 14 switch) equals the difference in total development cost between low-capacity development (3, 4, 5, and 6) and medium-capacity development (3, 7, 8, and 9).

The other component of manufacturing-related switching costs is the initial switch into one of the three production modes (13, 14, or 15). For any given aircraft, the unit cost will generally fall as production starts and continues to fall due to the learning curve effect.

Eventually, it is reasonable to assume that unit cost approaches an asymptote and stabilizes at the long-run marginal cost. To model the effect of the learning curve exactly with DP would be impossible, because knowledge of unit cost requires a knowledge of how many units have been built to date. This information is not part of the state vector. One possibility would be to include units built to date as an additional state variable, but because computation time grows exponentially with the number of state variables, as noted earlier, the exercise would be impractical for even two aircraft. Therefore, once in a production mode, all aircraft are assumed to be produced at their long-run marginal cost.

To account for this discrepancy, the switching cost to enter production is set equal to the total extra cost expected to be incurred during the production run of the aircraft over and above the long-run marginal cost. Because this extra cost will be incurred gradually and with certainty over time, the risk-free rate is used to find the expected present value of these cash flows, assuming a production rate equal to baseline demand.

The entire described process, for both development cost and manufacturing cost, is conducted for both aircraft designs, resulting in a set of switching costs for each that is a function of the operating mode of the other. To use the symbology introduced earlier, the process finds the switching costs $I(m_i, u_i | m_j)$ for each aircraft i , where the other aircraft is j , for each prior operating mode m_i and control variable decision u_i . Then, the switching cost from any operating mode vector $[m_1, m_2]$ to $[u_1, u_2]$ is simply equal to the sum of $I(m_1, u_1 | m_2)$ and $I(m_2, u_2 | m_1)$. This set of data is stored in the switching cost matrix.

Stochastic Process Dynamics

A crucial component of the algorithm is the model describing the nature of the unpredictable behavior of the stochastic process representing the development of the market for commercial aircraft. The annual quantity demanded is represented as a stochastic variable that evolves according to a random walk, modeled as a binomial tree process. Each time period, the variable may either increase or decrease by a specified amount with a certain associated probability. Thus, if there are two such variables, representing the evolution of the market for two distinct aircraft, there are four possible outcomes each time period. A transition probability matrix is constructed linking possible initial states to final states in this framework. These transition probabilities are used to find the expected future value of the project as a probability-weighted average, expressed as the expectation term $E[\dots]$ in Eq. (4).

Examples

The examples presented here illustrate the mechanics of the algorithm and highlight its distinguishing features. The first considers design of a single aircraft and presents two illustrations: a simulation run to demonstrate the decision rules arrived at by the optimizer and a connection to the NPV technique. The second example considers the design of a family of two aircraft sharing common components and demonstrates how the tool can be used to determine the value of commonality.

Three different aircraft designs are used, all based upon the BWB concept. Table 2 summarizes the key characteristics of the designs. The example designs are purely hypothetical and significantly simplified. They do not represent actual current BWB configurations. Three different airframes are possible: one large, 747-class vehicle (BWB-450), and two smaller, 250-passenger class designs. One of the smaller designs, the BWB-250C, shares 39.7% of its parts, by weight, with the BWB-450. The other has no commonality with

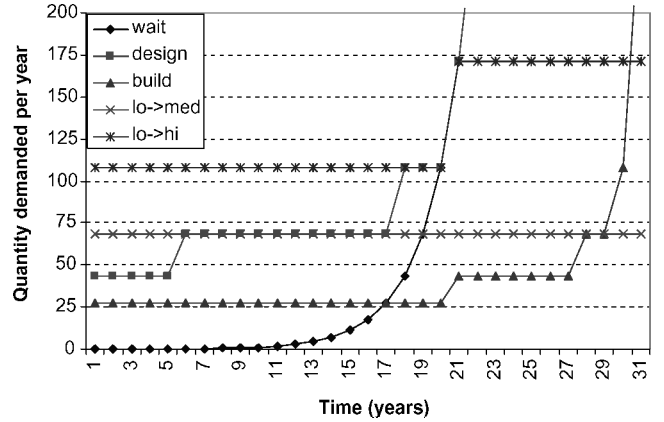


Fig. 5 Decision rules for BWB-250C.

the BWB-450, being a point design, optimized without consideration for commonality. Note that the point design results in a lighter airframe because the commonality constraint placed on the BWB-250C results in a weight penalty. Specifically, the BWB-250C uses the same wing as the BWB-450 to save on development cost, but an individually optimized design for the BWB-250 would not need as much wing area.

Single Aircraft Valuation

The DP algorithm was applied for valuation of the BWB-250C and resulted in a set of decision rules, which are shown in Fig. 5. These decision rules represent the optimal decision strategy identified by the algorithm. For each control variable (in this case, there is only one, the next period operating mode decision), the decision rules specify the optimal value to which the variable should be set, as a function of time and of all of the state variables. In other words, given how long the program has been ongoing, the operating mode from last period, and the current market conditions (quantity demanded), the decision rule specifies what the operating mode should be for the next period. Figure 5 shows, as a function of time, the minimum value of the demand index for which it is optimal to make certain program-related decisions, namely, wait, design (enter mode 1 from mode 0), build (enter mode 13, 14, or 15 from mode 6, 9, or 12), switch from low- to medium-capacity production (enter 14 from 13), and switch from low- to high-capacity production (enter 15 from 13).

Figure 6 shows a simulation run, which represents a sample path of demand through time, a scenario constructed using a random number generator to approximate the stochastic behavior of demand. Figure 6a shows the random evolution of annual quantity demanded over time: This is a sample path of the underlying stochastic process. Also shown is the optimizer's real-time strategy in response to the evolution of demand using the decision rules shown in Fig. 5. Thus, at the beginning of the simulation, demand is at its baseline static forecast quantity, as calculated by the revenue model. This demand level, which happens to be 28 units per year, is insufficient for the firm to commit to developing the BWB (according to the optimal strategy). However, in year 3, demand increases as the result of a random fluctuation, and the choice is made to invest in nonrecurring development for the aircraft. The investment choice is made because the new level of demand is greater than the threshold level corresponding to the design decision at time $t = 3$ in the optimizer's solution. Recall that once the initial design operating mode is entered, the firm is committed to the first phase of the development process, until halfway through development, immediately before tooling. In this simulation run, demand falls immediately after design is started, but increases again when the halfway point is reached. Development is, therefore, continued, until time $t = 9$, when the operating mode is 6 (end of development). At this point in time, demand is low, and the production decision is deferred.

However, one year later, at time $t = 10$, demand increases past the threshold value for the build decision, and production is entered.

Table 2 BWB example key characteristics

Design	Seat count	Range, n mile	Gross TOW (normalized)	Commonality (by weight), %
BWB-450	475	8550	1	N/A
BWB-250C	272	8550	0.756	39.7
BWB-250P	272	8550	0.624	0

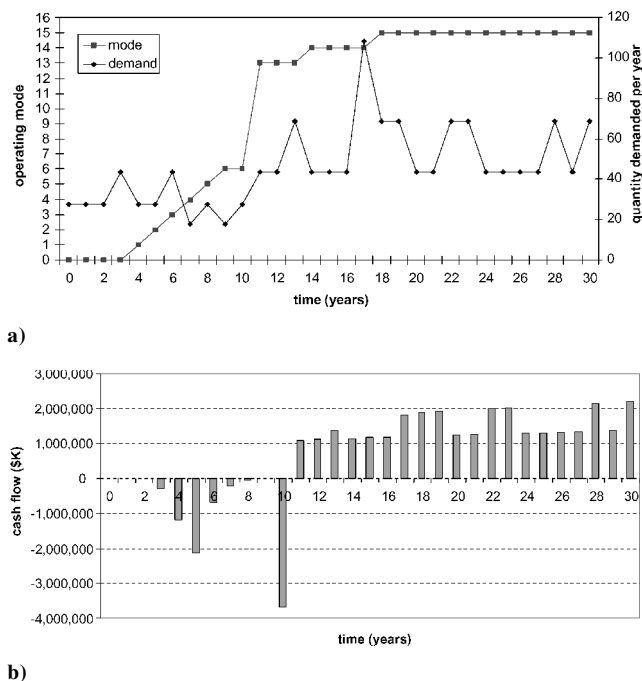


Fig. 6 Simulation run for BWB-250C: a) quantity demanded per year and resulting choice of operating mode and b) associated cash flows.

Figure 6b shows the cash flows associated with the decisions made each year. Years 2–8 demonstrate the familiar bell-curve shape of a typical development effort. Year 10 shows why the optimizer chooses to wait at all before going into production: The switching cost to enter production is on the order of \$4 billion. This switching cost is the algorithm's way of handling the learning curve effect: the \$4 billion switching cost here is the present value of all of the projected future costs in excess of long-run marginal cost for BWB production.

Once production is entered, after year 10, all units are produced at their long-run marginal cost. (In reality, the \$4 billion would be distributed over the entire production run, with more weight on the early years.) The cash flows from production, in years 11–30, continue to fluctuate as a function of demand and gradually creep upward with inflation. Return to Fig. 6a: The optimizer can be observed to respond to demand spikes in year 13 and then 17 by making incremental investments in tooling to expand the capacity of the production line, first to a medium and then to a high level. In this simulation run, the high production capacity was put to good use only in year 17 because demand never reached that level again. However, the decision to enter high capacity production was optimal at that time because the demand spike indicated a higher expected future demand. The CPU time for this simulation run was approximately 0.01 s on a 700-MHz AMD Athlon processor. In comparison, the stochastic optimization to determine the decision rules took approximately 690 s of CPU time.

The preceding simulation run is just one of millions of possible paths that can be taken by demand through time, but it effectively illustrates the decision-making element of the solution to the program valuation problem. The actual expected program value corresponding to the DP solution is computed as \$2.26 billion. However, the magnitude of this value depends strongly on the assumptions used in the underlying models and is not as important as the dynamics and approach illustrated by the valuation process. To further interrogate the value behavior of the system, one could conceive of using MCS to run a series of simulations using the optimal decision rules, such as the simulation shown in Fig. 6. If an appropriate discount rate is chosen, the mean NPV calculated by MCS should be equal to the expected program value computed by the DP algorithm. The choice of discount rate along with the possible estimation and interpretation of variance results are important issues that are the subject of ongoing research.

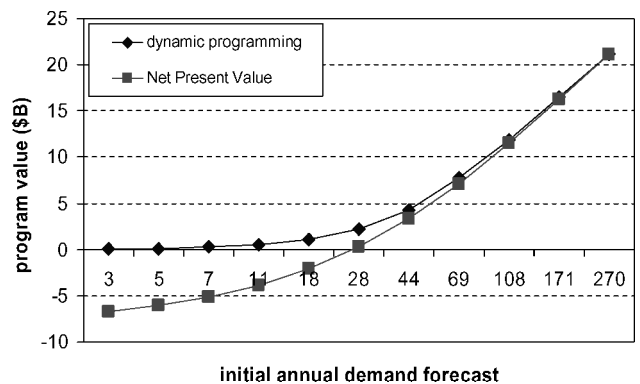


Fig. 7 BWB-250C program value as a function of baseline demand.

Connection to NPV

There is one primary conceptual difference between the DP approach used in this work and traditional project valuation approach of NPV: DP takes into account managerial flexibility, that is, decision making in real time. NPV analysis assumes a fixed schedule of actions and cash flows, and uncertainty regarding the magnitude of those cash flows is accounted for by appropriate selection of a discount rate. However, there is no uncertainty regarding which operating mode the firm is using at any time; these decisions are made *ex ante*. Therefore, if the ability to make decisions is removed from the DP tool, it should reduce to a traditional NPV analysis. In other words, the switching costs between operating modes must be adjusted such that the optimizer has only one choice with a finite switching cost for any given operating mode. Refer to Fig. 4: The only finite cost path through the modes is now set as 0–1–2–3–10–11–12–15. This assumes an irreversible commitment, as of time 0, to design, tooling, and high capacity production. Now, as the optimizer solves the problem, it is forced to make the same decisions regardless of the demand level. As a result, it is possible to generate negative program values, just as it is routine to find that a project has a negative NPV.

Figure 7 shows program value for the single aircraft case as a function of the initial annual demand forecast. This demand level is a strong function of the characteristics of the aircraft, specifically, the range and seat count, but is also dependent on the current condition of the market and the resulting expectations and needs of the airlines. Thus, in Fig. 7, the sensitivity of the program's success to the current condition of the market is considered. Demand is expressed as the number of aircraft per year that are demanded in year 1 of the analysis. This initial quantity is the starting point for the evolution of demand according to a stochastic process over the time horizon of the problem.

Figure 7 shows two plots of value on the same set of axes: dynamic programming and NPV. The former shows the output of the algorithm as it finds the value of the program using DP to account for managerial flexibility. The latter is the NPV case described earlier, where flexibility is removed from the program. As the initial demand forecast increases, expected program value increases. If the forecast is very small, the value of the program with no flexibility is negative, that is, the aircraft is developed, the nonrecurring cost is incurred, but few if any units are sold. However, the value with flexibility for low demand indices is zero; if no sales are expected, no investment is made in developing the aircraft.

As the demand index increases, the no-flexibility program value quickly approaches value with flexibility. However, for small or marginal demand index numbers, there is a significant difference between the two valuations—one that may mean the difference between keeping a program and scrapping it. At the baseline initial demand of 28 aircraft per year, the value with flexibility, \$2.26B, is almost seven times the value without flexibility, \$325M.

Aircraft Family Valuation

Using the DP method, the three aircraft designs listed in Table 2 are evaluated in several different combinations to find program

Table 3 Key input parameters for all test cases

Parameter	Value
Number of periods	30
Timestep per period	1 year
Risk-free rate r_f	5.5%
Annual aircraft price inflation	1.2%
Annual aircraft demand volatility	19.6%

Table 4 Intermediate results: cost and demand characteristics for BWB family

Design	Baseline quantity demanded, units/yr	Long-run marginal cost, \$ millions	Baseline price, \$ millions
BWB-450	16.7	139.0	195.0
BWB-250C	27.6	93.8	116.1
BWB-250P	27.6	84.9	142.2

Table 5 Final results: program value for BWB family

Program	Value
BWB-450, \$ billion	5.95
BWB-250C, \$ billion	2.26
BWB-250P, \$ billion	14.62
BWB-450 plus BWB-250C, \$ billion	8.21
BWB-450 and BWB-250C, \$ billion	8.95
Commonality premium, %	9

value. First, each of the designs is evaluated on an individual basis, as though it is the only design option available to the firm. Then, the BWB-450 and BWB-250C are evaluated simultaneously, to investigate any synergies that may exist as a result of commonality. Finally, the BWB-450 and BWB-250P are also evaluated simultaneously. The key input parameters used for all test cases are listed in Table 3.

The intermediate results of the test runs described are summarized in Table 4. These represent the primary outputs of the models described in this paper: cost characteristics and demand characteristics based on a particular airframe and its performance. It can be seen that there is greater annual demand for the smaller capacity aircraft than for the larger BWB-450. Note that quantity demanded is modeled as independent of operating characteristics; rather, the quantity estimator considers only the size class of the aircraft. However, the price estimator distinguishes between all three vehicles. The baseline price is expectedly high for the BWB-450, as it is a much larger aircraft. However, although the two smaller aircraft have identical seat counts, the BWB-250P is significantly higher priced. This effect is due to its lighter weight, which results in significantly reduced fuel burn and, therefore, a lower operating cost.

Predictably, long-run marginal cost (LRMC) scales with the vehicles' weight. For this example, the LRMC is defined as the marginal cost of unit 100, produced without any commonality effects. Thus, because the point-designed BWB-250P is lighter than the derivative BWB-250C, its long-run cost of production is smaller. However, commonality should result in a reduced development cost and a reduced learning effort for the BWB-250C. That is, the marginal cost should reach LRMC faster.

Table 5 shows the final results of this example: the program values resulting from the several different combinations of designs evaluated. The first result to consider is the extremely high program value found for the BWB-250P. Although it is probably too high to be realistic, it highlights the key design issues in this example: A considerable sacrifice was made in the 250-passenger class aircraft design to accommodate commonality. A modest increase in empty weight translated to a medium increase in takeoff weight (TOW), which translated to a significant difference in fuel burn and operating cost and an even greater difference in market price. The sensitivity of price to operating cost is difficult to observe in practice, and these results suggest that it is overestimated by this pricing

model. However, this snowballing phenomenon underscores the importance of considering the downstream effects of a design change on program value.

The other side of the coin is the value benefit gained by commonality: a savings in development and manufacturing costs. This is reflected in the existence of a commonality premium, albeit a modest one in this example. The value of the program with both designs (BWB-450 and BWB-250C) considered simultaneously is greater than the sum of the values of their individual programs. The program value of the BWB-450 and BWB-250P considered simultaneously is not shown, inasmuch as it would be identical to the sum of their individual values, because there is no interaction between those two aircraft. It would, however, be interesting to consider interactions in program value arising not from physical commonality but from market effects, for example, complements or substitutes.

Within the framework of flexibility and decision making used by the DP algorithm, the choice to use commonality may be framed using real options. When the firm develops the BWB-450, it acquires an option to develop the BWB-250C for a reduced cost and at a time of its choosing. The penalty paid, that is, the price of the option, is the present value of additional profits the firm would receive had it instead developed the BWB-250P as a point design to maximize its performance. From a program flexibility standpoint, the firm still has an option to develop a second aircraft even if there is no commonality. In such a case, the exercise price of the option is simply higher by the amount of cost savings from commonality.

The conclusion of this example, therefore, is not that commonality is not justifiable. Rather, for commonality to be justifiable, the benefits must outweigh the costs. The benefits include the development and manufacturing cost savings gained if the derivative aircraft is in fact built. The costs include any additional design or manufacturing costs as a result of commonality, but most important, any resulting performance penalty on the aircraft. This performance penalty must be translated into an opportunity cost: the revenues foregone by not selling a higher-performance aircraft. The set of aircraft designs used in this example, with the baseline parameters specified, did not indicate a higher program value for commonality because the opportunity cost of lost revenues was very high.

Conclusions

An aircraft program valuation tool is presented, which combines performance, cost, and revenue models and a DP algorithm to measure the value of a set of aircraft designs to a firm. The value measurement is not based on any technical characteristics per se, or any static forecast of cost and revenue, but on an analysis of an uncertain future, assuming that value-maximizing decisions are made by management as time goes on and uncertainty is resolved. The approach, which parallels real options analysis, provides additional insight over traditional valuation techniques by its attempt to quantify the value created by flexibility. Flexibility is modeled and addressed by the DP operating modes formulation, which is an explicit method of formalizing and discretizing the decision-making process that is continuously ongoing for any project at any firm. Two of the method's distinguishing features are the combination of economic analysis with engineering analysis and the explicit consideration of management's ability to make and defer decisions in real time in response to unfolding market conditions.

One important question that has not been addressed here is the impact on the results of uncertainty in the cost and performance estimates. Although it is possible to think of adding cost or one performance metric as an additional stochastic variable, the computational demands of the DP algorithm make this approach very challenging, if not impossible. One could conceive of a two-step process, where the DP approach is used to first determine a set of decision rules and then a more traditional MCS is subsequently applied to determine the effect of additional uncertainty on the valuation results. These extensions are the subject of ongoing research.

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References

- ¹Zang, T. A., and Green, L. L., "Multidisciplinary Design Optimization Techniques: Implications and Opportunities for Fluid Dynamics Research," AIAA Paper 99-3798, June–July 1999.
- ²Kroo, I., "MDO Applications in Preliminary Design: Status and Directions," AIAA Paper 97-1408, April 1997.
- ³Kirby, M. R., and Mavris, D. N., "Forecasting Technology Uncertainty in Preliminary Aircraft Design," Society of Automotive Engineers, SAE Paper 1999-01-5631, Oct. 1999.
- ⁴Mavris, D. N., DeLaurentis, D. A., Bandte, O., and Hale, M. A., "A Stochastic Approach to Multi-Disciplinary Aircraft Analysis and Design," AIAA Paper 98-0912, Jan. 1998.
- ⁵Mavris, D. N., and Birney, M., "Formulation of a Stochastic, Physics-Based Strategic Business Decision Making Environment," AIAA Paper 2002-5850, Oct. 2002.
- ⁶Younghans, J. L., Luffy, R. J., Brewer, J. T., and Wallace, D. R., "An Integrated Probabilistic Approach to Advanced Commercial Engine Cycle Definition," 14th International Symposium on Air Breathing Engines, IS-ABE Paper 99-7194, Sept. 1999.
- ⁷Dixit, A. K., and Pindyck, R. S., *Investment Under Uncertainty*, Princeton Univ. Press, Princeton, NJ, 1994.
- ⁸Trigeorgis, L., *Real Options: Managerial Flexibility and Strategy in Resource Allocation*, MIT Press, Cambridge, MA, 2000.
- ⁹Liebeck, R. H., Page, M. A., Rawdon, B. K., "Blended-Wing-Body Subsonic Commercial Transport," AIAA Paper 98-0438, Jan. 1998.
- ¹⁰Wakayama, S., "Blended-Wing-Body Optimization Problem Setup," AIAA Paper 2000-4740, Sept. 2000.
- ¹¹Wakayama, S., "Lifting Surface Design Using Multidisciplinary Optimization," Ph.D. Dissertation, Dept. of Aeronautics and Astronautics, Stanford Univ., Stanford, CA, Dec. 1994.
- ¹²Mavris, D. M., Nottingham, C. R., and Bandte, O., "The Impact of Supportability on the Economic Viability of a High Speed Civil Transport," 1st Joint International Conf. of the International Society of Parametric Analysts and the Society of Cost Estimating and Analysis, June 1998, URL: <http://www.asdl.gatech.edu/>.
- ¹³Markish, J., "Valuation Techniques for Commercial Aircraft Program Design," S. M. Thesis, Dept. of Aeronautics and Astronautics, Massachusetts Inst. of Technology, Cambridge, MA, June 2002.
- ¹⁴Markish, J., and Willcox, K., "Multidisciplinary Techniques for Commercial Aircraft System Design," AIAA Paper 2002-5612, Sept. 2002.
- ¹⁵"Aircraft Value News," *Aviation Newsletter*, Vol. 10, Nos. 1–25, 2001, URL: <http://www.aviationtoday.com/catalog.htm>.
- ¹⁶"World Jet Airplane Database—List and Realized Prices of New Commercial Aircraft," *The Airline Monitor*, Vol. 13, No 12, ESG Aviation Services, Ponte Vedra Beach, FL, May 2001.
- ¹⁷*Boeing Current Market Outlook*, edited by T. Meskill, The Boeing Co., Seattle, WA, 2000, Appendix B, p. 42.
- ¹⁸"Detailed Passenger Fleet Results," *Airbus Global Market Forecast, 2000–2019*, Airbus SAS, 1999, Appendix G, p. 74.
- ¹⁹"Projected Jet Airplane Deliveries—2000 to 2020," *The Airline Monitor*, Vol. 13, No. 2, ESG Aviation Services, Ponte Vedra Beach, FL, July 2000, pp. 10, 11.
- ²⁰Kulatilaka, N., "Valuing the Flexibility of Flexible Manufacturing Systems," *IEEE Transactions on Engineering Management*, Vol. 35, No. 4, 1998, pp. 250–257.

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