

Removal of the secular term gives

$$2\tau_2 A'_1 = -\sigma_1 B_1 - \sigma_2 B_1 (A_1^2 + B_1^2) \quad (14)$$

$$2\tau_2 B'_1 = \sigma_1 A_1 + \sigma_2 A_1 (A_1^2 + B_1^2) \quad (15)$$

This system has the first integral

$$A_1^2 + B_1^2 = k^2 = \text{constant} \quad (16)$$

The solutions of Eqs. (14) and (15) are

$$A_1 = a \cos \theta_1 - b \sin \theta_1 \quad (17)$$

$$B_1 = a \sin \theta_1 + b \cos \theta_1 \quad (18)$$

where a and b are constants of integration and

$$\sigma = [\sigma_1 + \sigma_2 k^2] / 2\tau_2 \quad (19)$$

Note that the final solution of ψ is independent of the value of τ_2 ; hence τ_2 can be set equal to unity.

References

- ¹Hablani, H.B. and Shrivastava, S.K., "Analytical Solution for Planar Librations of a Gravity Stabilized Satellite," *Journal of Spacecraft and Rockets*, Vol. 14, Feb. 1977, pp. 126-128.
- ²Nayfeh, A.M., *Perturbation Methods*, John Wiley, New York, 1973.
- ³Beletskii, V.V., *Motion of an Artificial Satellite About Its Center of Mass*, NASA TTF-429, 1966.

Reply by Authors to K.T. Alfried

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WE thank K.T. Alfried for his comments on our Note.¹ The following points were raised in his comments:

1) Alfried points out that our series solution, Eq. (23) in Ref. 1, is not uniformly valid. After examining $\psi_j(\theta)$ ($j=0,1,2$), it is evident that for all values of θ the term $e^j \psi_j(\theta)$ is a small correction to $e^{j-1} \psi_{j-1}(\theta)$ and that the coefficient of e^j is bounded. Thus, contrary to the comment, we fail to see any nonuniformity in Eq. (23). The equation can even furnish uniformly valid eccentricity-induced oscillations.

2) The simultaneous presence of e^2 in both amplitude and frequency in Eq. (23) led us to comment that the solution was up to fourth order in eccentricity. However, we now recognize that, in fact, it is up to second order only. To establish relations of A_j , B_j ($j=1,2$) with Θ_j , the uniformity conditions are derived from third- and fourth-order equations, respectively. This we incorrectly stated as having obtained the response up to fourth order in e . In the multiple scales

method, to fully determine response up to a certain order of a small parameter, one needs to consider equations of higher order. Thus we are obliged to include equations of third order, even though response obtained was up to second order only. This supports the linearizability of Eq. (1). Further, Beletskii² has given solution of the *linear* equation for *nonzero* initial conditions of $O(1)$ using the method of Krylov-Bogolyubov. After some algebra we observe a similarity between this solution and Eq. (23), except for a few additional terms of first and second order in the latter equation. For the initial conditions and parameters of Figs. 1a and 1b of Ref. 1, the two solutions closely agree with each other and differ from the numerical response by the same amount. However, for the particulars of Fig. 1c, the Krylov-Bogolyubov method fares better. Of course, if we selected a nonlinear equation to obtain the response up to the same order it would, in principle, be more accurate than the linear response. However, in a linear regime there would be no benefits. Thus we assert that within the *linear range* of pitch angle the response recorded in Ref. 1 is correct and uniformly valid. The response arrived at by Alfried is confined to the eccentricity-induced oscillations and is thus restrictive, although it includes nonlinearity and is expected to fare well even in the nonlinear regime.

3) Regarding resonance, a glance at any linear solution such as Eq. (23)¹ instantly reflects such points. Besides, analyses which cover these resonances are well documented (e.g., Ref. 2). As such we felt that they did not warrant any discussion.

References

- ¹Hablani, H.B. and Shrivastava, S.K., "Analytical Solution for Planar Librations of a Gravity Stabilized Satellite," *Journal of Spacecraft and Rockets*, Vol. 14, Feb. 1977, pp. 126-128.
- ²Beletskii, V.V., *Motion of an Artificial Satellite About Its Center of Mass*, NASA TTF-429, 1966, pp. 32-58.

Errata

Local Analytical Solution for Compressible Turbulent Boundary Layers

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[JSR 14, 219-223 (1977)]

EQUATION (19) should read as

$$C = 0.0176 \left(\frac{T_{\text{ref}}}{T_e} \right)^{-1+\omega_i} \left(\frac{T_e}{T_0} \right)^{-\left(\frac{1}{\gamma-1} - \omega \right)_i} \left(\frac{\rho_0 \mu_e}{\rho_e \mu_0} \right)^{-i}$$

Received Sept. 19, 1977.

Index categories: Boundary Layers and Convective Heat Transfer - Turbulent; Nozzle and Channel Flow; Launch Vehicle Systems (including Ground Support).

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Received May 2, 1977.

Index category: Spacecraft Dynamics and Control.

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