

**Studies on Benzodiazepinooxazoles. II.<sup>1)</sup> Crystal and Molecular Structure of  
10-Bromo-2,3,5,6,7,11b-hexahydro-2-methyl-11b-phenylbenzo[6,7]-1,4-diazepino[5,4-b]oxazol-6-one, C<sub>18</sub>H<sub>17</sub>O<sub>2</sub>N<sub>2</sub>Br·C<sub>2</sub>H<sub>5</sub>OH**

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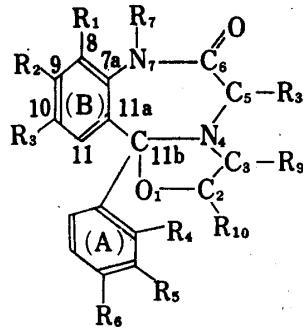
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The crystal structure of 10-bromo-2,3,5,6,7,11b-hexahydro-2-methyl-11b-phenylbenzo[6,7]-1,4-diazepino[5,4-b]oxazol-6-one, C<sub>18</sub>H<sub>17</sub>O<sub>2</sub>N<sub>2</sub>Br·C<sub>2</sub>H<sub>5</sub>OH, has been determined by the three dimensional Patterson method. This substance occurs as monoclinic crystals, space group P2<sub>1</sub>/c, with Z=4 in the unit cell dimensions a=16.34, b=8.88, c=13.89 Å, and β=102°. The block-diagonal least-squares refinements using 2780 reflections gave the final R=11.3%. The methyl and phenyl ring substituents are trans with respect to the plane of the oxazole ring.

### Introduction

In the preceding paper,<sup>1)</sup> the authors reported the synthesis and the pharmacology activity of benzo[6,7]-1,4-diazepino[5,4-b]oxazole derivatives and their analogues.

In these derivatives, compounds having substituents at 2- or 3-position can exist as two configurational isomers. The nuclear magnetic resonance (NMR) spectrum of 10-bromo-2,3,5,6,7,11b-hexahydro-2-methyl-11b-phenylbenzo[6,7]-1,4-diazepino[5,4-b]oxazol-6-one (R<sub>1</sub>=R<sub>4</sub>=R<sub>4</sub>=R<sub>5</sub>=R<sub>6</sub>=R<sub>7</sub>=R<sub>8</sub>=R<sub>9</sub>=H, R<sub>3</sub>=Br and R<sub>10</sub>=CH<sub>3</sub>) in deuteriochloroform showed two pairs of methyl protons at 1.25 (J=6.5 Hz) and 1.38 ppm (J=6.5 Hz) and two kinds of amino-protons at 8.32 and 8.53 ppm suggesting the existence of such isomers. After the compound was recrystallized from aqueous ethanol, the NMR spectrum of the crystals showed that the only one of the crystalline isomers had separated. Such crystals would be suitable for determining its structure and stereochemistry. The compound was labile in solution and a peak assigned to amino-proton splitted to the above values within a few minutes.



### Experimental

We have succeeded in obtaining crystals which belong to the monoclinic system by slow evaporation from 70% aqueous ethanol in the form of needles elongated along the c-axis. The crystals consisted of only one component isomer at the NMR level. The cell constants are determined by Weissenberg and oscillation photographs: a=16.34, b=8.88, c=13.89 Å, and β=102.0°. From the systematic absence of reflection, the space group was determined to be P2<sub>1</sub>/c. Intensity data are collected by an equi-inclination Weissenberg technique for the reflections of h0k to hk11. After several days under the X-ray beam the crystal turned opaque so that two crystals were used to take a total of 2780 independent reflections. They

- 1) This paper forms part II of a Series entitled "Anxiolytic Sedative". For previous paper, see Ref. 1. Part I: T. Miyadera, A. Terada, M. Fukunaga, Y. Kawano, T. Kamioka, C. Tamura, H. Takagi and R. Tachikawa, *J. Med. Chem.*, **14**, 520 (1971).
- 2) Location: No. 2-58, 1-Chome, Hiromachi, Shinagawa-ku, Tokyo.

were estimated by visual comparison of the calibrated standard film. Two sets of five multiple film were exposed until  $l=4$ , and one set of five for over  $l=5$ . The observed density was  $1.452 \text{ g cm}^{-3}$  measured by floatation method while the calculated value was  $1.451 \text{ g cm}^{-3}$  which was obtained by taking into account that four molecules of  $\text{C}_{18}\text{H}_{17}\text{O}_2\text{N}_2\text{Br} \cdot \text{C}_2\text{H}_5\text{OH}$  are contained in the unit cell dimensions. Lorentz and Polarization corrections were calculated but no absorption correction was made because of the small size of the crystals.

### Structure Analysis

The structure was determined by the three dimensional heavy atom method, using Sim's weighting scheme.<sup>3)</sup> The position of the bromine atom was readily obtained on the basis of the  $P2_1/c$  vector sets in the crystal. The first Fourier synthesis were calculated with phases derived from the contribution of the bromine atom alone ( $R=46.9\%$ ). The 22 peaks in the electron density map were corresponded to the proposed structure. The values of the temperature parameters in the early stages of structure factor calculation were used 3.5 for bromine and 4.0 for all light atoms. The whole atomic coordinates of the molecule were determined in the next cycle of Fourier calculation and refined by means of block diagonal least squares procedures. After 6 cycles of refinements with isotropic temperature parameters for whole atoms the R-factor reduced to 15%. At this stage the molecule of ethanol which is contained as the solvent of crystallization came out in the vacant areas of the molecular packing in the electron density map. In order to find out the positions of hydrogen atoms, the difference Fourier synthesis was computed. All hydrogen atoms were obtained around the expected positions.

By two more cycles of the block diagonal least squares refinements with anisotropic thermal parameters for bromine the R-factor decreased to 12.4%, further refinements with anisotropic thermal parameters for all atoms except hydrogen reduced the R to 11.3%. The final Fourier map and the bond distances and angles are shown in Fig. 1 and 3, and the bond distances and angles are shown in Fig. 2. The least squares planes for two benzene, oxazole, and diazepine ring systems are calculated as Fig. 4 which show the deviations of atomic coordinates from these planes. The final parameters of the atomic positions and the temperature factors are listed in Table I, and their standard deviations in Table II. The final values of  $F_0 - F_c$  are shown in Table III.

Fig. 1. The Final Electron Density Map Projected on the (010) Plane, Contours are Arbitrary in Equal Intervals except Bromine Atom

thermal parameters for all atoms except hydrogen reduced the R to 11.3%. The final Fourier map and the molecular packing diagram viewed along the b-axis are shown in Fig. 1 and 3, and the bond distances and angles are shown in Fig. 2. The least squares planes for two benzene, oxazole, and diazepine ring systems are calculated as Fig. 4 which show the deviations of atomic coordinates from these planes. The final parameters of the atomic positions and the temperature factors are listed in Table I, and their standard deviations in Table II. The final values of  $F_0 - F_c$  are shown in Table III.

All computations have been carried out with the CDC 3600 system at C. Itoh Electronic Computing Service Co., Ltd. using the set of programs registered as UNICS.

### Result and Discussion

The C15 methyl and C17 phenyl groups which are attached to the oxazole ring deviate 0.30 and  $-1.44 \text{ \AA}$  respectively from the five membered ring least squares plane. Therefore, the stereo-chemistry of the substituents on the oxazole ring is determined as *trans* for the methyl group and the benzene ring B. The planarity calculation of the C3, N4, C5 and C14, shows that the lone pair of the N4 atom is directed towards the same side of the C17 phenyl group that is the lone pair of nitrogen and phenyl group are *cis*. The least squares plane in the seven membered ring is constructed with four atoms of C14, N4, C6 and N7. The C12, C13 and C5 atoms in this ring deviate  $+0.88$ ,  $+0.81$  and  $+0.75 \text{ \AA}$  from this least squares plane respectively. The deviations of all plus signs indicate that the ring system takes a boat form, this is a common feature found in the compounds containing unsaturated seven membered rings, e.g., fulvane.<sup>4)</sup>

3) G.A. Sim, *Acta Cryst.*, **11**, 123 (1958).

4) R.E. Davio and A. Tulinsky, *J. Am. Chem. Soc.*, **88**, 4583 (1966); H. Shimanouchi, T. Hata and Y. Sasada, *Tetrahedron Letters*, **1968**, 3573.

TABLE I. Fractional Atomic Coordinates and Anisotropic Thermal Parameter. Anisotropic Temperature Factor:  $T = \exp[-(B_{11}h^2 + B_{22}k^2 + B_{33}l^2 + B_{12}hk + B_{13}hl + B_{23}kl)]$   
Each Thermal Parameter is multiplied by  $10^4$

Atom	X	Y	Z	B11	B22	B33	B12	B13	B23
O 1	.1412	.8894	.0525	19	55	15	0	0	14
C 2	.1561	1.0118	-.0110	34	66	36	3	-3	22
C 3	.2347	.9687	-.0411	26	81	21	0	2	12
N 4	.2830	.8990	.0529	20	52	8	-4	4	2
C 5	.3432	.7885	.0308	24	70	18	0	7	1
C 6	.4033	.7513	.1296	14	55	18	1	6	0
N 7	.3723	.6662	.1964	19	55	18	0	2	3
C 8	.2877	.4474	.2075	23	52	21	0	5	2
C 9	.2118	.3732	.1898	21	57	31	-2	3	-2
C10	.1422	.4504	.1427	18	65	17	-12	3	2
C11	.1442	.6033	.1152	16	58	11	-5	1	1
C12	.2202	.6792	.1326	21	44	12	-4	3	0
C13	.2926	.5986	.1776	15	57	7	-2	3	-4
C14	.2208	.8501	.1118	17	50	14	2	6	4
C15	.0811	1.0371	-.0956	30	142	42	3	0	25
O16	.4765	.7941	.1473	19	75	41	-3	4	10
C17	.2331	.9337	.2139	23	44	13	2	2	2
C18	.1675	.9422	.2659	31	74	31	-4	11	-2
C19	.1765	1.0170	.3570	37	102	36	2	15	-5
C20	.2526	1.0824	.3990	48	88	21	9	3	-7
C21	.3190	1.0764	.3487	35	60	26	4	-2	-2
C22	.3091	1.0031	.2571	24	69	18	3	1	-3
BR23	.0376	.3457	.1163	26	91	51	-29	-3	5
C24	.5253	.8476	.4091	36	108	45	-2	12	5
C25	.5509	.6844	.4192	28	99	48	4	7	-12
O26	.4806	.5906	.3836	22	69	32	3	1	0

TABLE II. Estimated Standard Deviations of the Fractional ( $\text{\AA}$ ) and Thermal Parameters.  
Each Thermal Parameter is multiplied by  $10^4$

Atom	X	Y	Z	B11	B22	B33	B12	B13	B23
O 1	.0061	.0057	.0065	2	7	4	3	2	3
O 2	.0111	.0104	.0119	4	13	8	6	4	7
O 3	.0100	.0095	.0105	3	11	7	5	3	6
N 4	.0073	.0068	.0076	2	8	5	3	2	4
O 5	.0095	.0090	.0102	3	11	6	4	3	6
O 6	.0083	.0080	.0098	3	9	6	4	3	5
N 7	.0074	.0070	.0081	2	8	5	3	2	5
O 8	.0092	.0084	.0101	3	10	6	4	3	5
O 9	.0094	.0086	.0107	3	10	7	4	3	6
O10	.0086	.0084	.0096	3	10	6	4	3	5
O11	.0084	.0081	.0092	3	9	6	4	3	5
O12	.0086	.0079	.0092	3	9	6	4	3	5
O13	.0082	.0079	.0090	3	9	5	4	3	5
O14	.0082	.0080	.0091	3	9	6	4	3	5
O15	.0119	.0125	.0132	4	17	9	7	4	9
O16	.0066	.0066	.0076	2	8	5	3	2	4
O17	.0090	.0079	.0094	3	9	6	4	3	5
O18	.0106	.0097	.0114	4	11	7	5	4	6
O19	.0119	.0111	.0125	4	14	7	5	4	8
O20	.0125	.0108	.0118	5	13	7	6	4	7
O21	.0109	.0093	.0110	4	11	7	5	4	6
O22	.0094	.0089	.0101	3	10	6	4	3	6
BR23	.0011	.0011	.0013	0	1	0	0	0	0
O24	.0125	.0117	.0134	5	15	9	6	4	8
O25	.0114	.0111	.0130	4	14	8	6	4	8
O26	.0066	.0066	.0073	2	8	5	3	2	4

**TABLE III. Observed and Calculated Structure Factors ( $\times 10^3$ )**

H	F0	FC	H	F0	FC	H	F0	FC	H	F0	FC	H	F0	FC	H	F0	FC	H	F0	FC				
K,L <sup>a</sup>	1	0	381	401	-16	240	187	13	385	397	-8	392	39	1	397	-682	2	209	-199	-2	697	-889		
1	6L2	667	1	521	530	15	347	322	14	230	424	-9	321	31	2	2110	-1428	3	378	-351	-3	267	219	
2	668	-720	2	575	590	17	346	60	15	71	75	-10	201	191	3	74	-801	4	173	149	-4	349	-343	
3	5b3	-603	3	362	431	19	170	-132	1	206	294	-12	208	183	5	603	-544	6	68	61	-6	82	-22	
4	6L2	667	4	214	234	20	145	-174	1	246	294	-12	208	183	5	453	-344	7	394	-365	-7	264	269	
5	6b8	-720	5	387	423	K,L <sup>a</sup>	2	423	434	-13	286	295	6	394	-365	7	221	185	-15	73	-56			
6	5b3	-603	6	405	-394	2	720	773	3	275	285	-14	108	119	8	422	366	8	112	90	-8	258	-251	
7	839	-903	7	276	-288	3	171	130	4	369	361	-16	68	72	9	215	169	10	192	191	-10	129	-126	
8	938	-1164	8	77	-75	4	1041	1113	5	273	246	-17	143	-145	10	625	585	10	343	345	-12	141	145	
9	764	-647	9	315	-436	5	1040	1114	6	378	395	-19	203	-219	11	195	174	11	309	285	-13	310	337	
10	6L2	667	10	249	-263	6	583	453	7	298	272	K,L <sup>a</sup>	5	1	22	488	397	12	269	225	-14	244	250	
11	6b8	-720	11	407	-422	7	842	616	8	197	139	-1	149	-167	13	443	421	13	221	185	-15	73	-56	
12	5b3	-603	12	224	-232	8	275	246	10	164	130	-2	198	-178	14	375	310	14	74	64	-16	130	133	
13	839	-903	13	296	-285	9	653	567	11	159	-112	-3	123	79	15	375	426	K,L <sup>a</sup>	8	2	-18	204	148	
14	938	-1164	14	292	-815	12	410	-345	12	291	-152	-4	171	-174	16	227	194	1	69	51	K,L <sup>a</sup>	4	2	
15	764	-647	15	77	-75	13	257	-194	13	194	-178	-6	268	-261	17	174	149	2	69	-45	0	197	-211	
16	801	-881	16	118	-134	14	309	-395	K,L <sup>a</sup>	9	1	7	302	319	18	139	111	3	124	-113	-1	668	-634	
17	767	-673	17	K,L <sup>a</sup>	7	15	117	-110	2	102	149	-8	53	2	K,L <sup>a</sup>	2	4	71	-83	-2	783	-816		
18	232	-234	18	223	-324	16	585	-477	3	111	-76	9	216	28	1	746	937	5	51	43	-3	162	-159	
19	55b	-45b	19	237	-229	17	275	-222	4	226	-190	-10	134	-12	2	212	136	6	129	26	-4	462	-442	
20	114	-56	20	3H7	-446	18	294	-213	5	187	-155	-11	298	323	3	219	190	7	136	108	-3	164	-127	
21	517	-402	21	244	-277	19	284	-170	7	200	-144	-12	206	189	4	108	-89	9	127	-110	-6	670	-617	
22	444	-407	22	140	-128	K,L <sup>a</sup>	3	1	8	195	-177	-13	230	214	5	982	891	10	229	-221	-7	755	-814	
23	84	65	23	263	-270	1	106	341	9	299	-286	-15	183	144	6	331	298	11	172	-133	-8	482	-409	
24	176	355	24	280	-315	2	224	414	10	184	-172	K,L <sup>a</sup>	6	1	7	390	364	12	87	71	-9	254	-245	
25	244	8	416	523	6	243	264	11	228	-242	0	50	-14	8	132	136	14	133	-119	-10	445	-393		
26	233	231	9	102	-66	4	126	34	12	119	-140	-1	180	-179	9	144	101	K,L <sup>a</sup>	9	2	-11	205	191	
27	87	103	10	104	99	5	82	24	K,L <sup>a</sup>	10	1	-2	48	-85	10	117	-73	1	175	-155	-12	82	-76	
28	619	800	11	206	179	7	858	-790	2	161	-63	-3	73	-51	11	185	151	3	298	-305	-13	199	200	
29	632	859	12	213	215	8	402	-517	3	123	-57	-12	117	-115	13	262	263	5	181	49	-15	74	-95	
30	1114	-1441	13	K,L <sup>a</sup>	9	9	562	-572	4	148	-121	-6	147	134	14	71	-71	6	119	-103	-17	195	169	
31	55b	-445	14	85	-64	10	551	-533	5	74	-51	-7	213	219	15	52	-59	7	147	-131	-18	238	209	
32	179	-203	15	128	-331	11	621	-451	6	70	44	-8	287	257	16	181	-168	8	143	-125	K,L <sup>a</sup>	5	2	
33	5b6	-584	16	247	227	12	423	-348	7	100	-61	-9	58	-71	17	210	-176	9	146	-146	0	757	787	
34	239	232	17	79	-449	13	275	-229	0	118	-131	-10	137	122	18	147	-121	10	93	127	-1	454	507	
35	713	976	18	98	-641	14	370	-320	K,L <sup>a</sup>	11	1	-11	248	29	K,L <sup>a</sup>	3	2	11	148	135	-2	971	1176	
36	113	-67	19	5	143	134	15	197	-129	2	128	121	-12	230	253	1	504	403	K,L <sup>a</sup>	10	2	-3	494	507
37	141	-130	20	159	126	16	154	121	K,L <sup>a</sup>	1	1	-13	139	147	2	284	-929	1	117	76	-6	238	206	
38	120	140	21	188	219	19	155	145	-1	309	-351	-14	228	234	3	168	135	3	70	91	-5	140	104	
39	415	349	22	92	69	K,L <sup>a</sup>	4	1	-2	444	-464	-15	168	173	4	346	-324	5	254	236	-6	72	31	
40	348	370	23	185	176	1	173	134	3	1043	-1359	-16	150	143	5	339	-264	6	247	333	-7	126	-124	
41	247	400	24	70	-52	2	280	-924	4	602	-624	-17	112	124	6	581	-529	7	285	230	-8	400	-353	
42	90	-85	25	K,L <sup>a</sup>	9	3	686	-741	-5	702	-651	K,L <sup>a</sup>	7	1	7	323	237	8	179	233	-9	413	369	
43	168	-151	26	168	-136	4	870	-941	-6	509	-500	0	324	-382	8	78	-48	9	94	129	-10	220	-209	
44	82	-56	27	204	-177	5	742	-663	-7	233	-260	-1	248	-243	9	111	59	K,L <sup>a</sup>	11	2	-11	431	-405	
45	97	-83	28	106	-69	7	332	-273	-6	95	-73	-2	516	-553	10	141	-113	1	268	327	-12	274	-278	
46	440	361	29	131	-131	10	96	57	-10	47	52	-4	390	-374	14	134	121	3	54	37	-14	493	-494	
47	308	-333	30	93	-75	11	246	-257	-11	242	-163	-3	394	-372	15	101	80	4	42	47	-15	166	-157	
48	443	-391	31	7	327	-337	12	144	116	-12	200	192	-6	458	-517	16	333	291	K,L <sup>a</sup>	3	2	-16	187	-189
49	195	-138	32	137	-147	14	244	-280	-13	405	494	-7	101	-15	K,L <sup>a</sup>	4	2	746	871	-17	131	-142		
50	489	-444	33	230	-249	14	341	439	-14	347	361	-9	214	-237	1	590	555	-5	656	591	-18	144	-135	
51	212	-175	34	168	-104	15	48	56	-17	178	180	-12	137	13	2	635	636	-4	141	106	K,L <sup>a</sup>	6	2	
52	223	-411	35	181	-165	17	142	161	-19	105	117	-14	217	213	4	361	288	6	659	608	-1	274	249	
53	153	-120	36	284	-283	18	284	263	-1	K,L <sup>a</sup>	7	-15	174	175	5	690	619	-7	993	975	-2	168	128	
54	211	-193	37	235	-215	K,L <sup>a</sup>	1	-1	103	197	-10	179	223	6	475	439	-1	1083	1072	-3	203	282		
55	60	74	38	178	-197	1	221	-184	-2	196	410	0	337	352	8	556	513	-10	201	204	-5	698	784	
56	131	-143	39	145	-124	1	156	99	-3	103	-74	0	337	352	9	526	481	-11	356	586	-6	477	552	
57	604	-672	40	132	122	4	279	247	-10	302	-404	-10	367	-377	17	124	-115	-3	82	-61	-15	262	-260	
58	1																							

TABLE III. (Continued)

M	F0	FC	M	F0	FC	M	F0	FC	M	F0	FC	M	F0	FC	M	F0	FC	M	F0	FC				
0	267	-299	2.	201	170	-2	88	-14	-6	100	97	12	270	-274	-16	154	-143	-4	78	-65	2	81	-73	
-1	201	-283	3	322	-244	-3	373	-354	-6	74	94	13	184	-182	-17	153	-155	-5	230	-206	3	326	-309	
-2	142	-115	4	331	267	-4	407	399	-10	23	21	14	102	105	-3	4	-6	109	-101	4	362	-303		
-3	164	-165	5	383	336	-5	290	328	K,L <sup>a</sup>	11	3	16	88	102	-1	233	-297	-7	303	-284	5	382	-378	
-4	129	-120	7	408	-363	-6	677	719	-2	58	-84	K,L <sup>a</sup>	6	4	-2	266	-221	-8	177	-169	6	165	-149	
-5	103	-150	8	202	164	-7	765	874	K,L <sup>a</sup>	0	4	0	317	-321	-3	426	-398	-9	166	-174	8	98	-88	
-6	103	-150	9	146	-150	-6	505	628	8	322	-299	1	617	-600	-4	93	-100	-11	215	-225	9	231	-196	
-7	103	108	10	84	-100	-9	427	459	9	237	416	2	383	-379	-5	375	-342	-12	117	-137	10	205	-162	
-8	K,L <sup>a</sup>	10	2	11	88	-75	-10	410	433	10	95	106	3	211	-210	-6	326	-340	K,L <sup>a</sup>	10	4	11	215	-209
-9	55	181	13	226	-229	-11	430	491	11	646	738	4	388	-405	-7	309	-307	-1	349	-334	12	201	-159	
-10	106	-62	14	125	-123	-12	475	597	12	3-3	361	5	583	-622	-8	236	-198	-2	118	146	15	44	-49	
-11	172	-153	15	185	-160	-13	358	396	13	309	327	0	72	48	-9	313	-288	-3	202	226	K,L <sup>a</sup>	7	3	
-12	208	-207	K,L <sup>a</sup>	6	3	-14	121	-141	14	435	499	7	126	103	-10	230	-228	-6	105	-59	0	317	285	
-13	177	-189	0	413	-416	-16	91	774	15	219	204	8	220	195	-11	119	4	K,L <sup>a</sup>	1	5	1	266	-299	
-14	193	-221	1	330	-381	K,L <sup>a</sup>	4	3	16	265	244	10	251	216	-13	222	-234	0	262	235	2	473	523	
-15	207	-290	3	109	-116	-1	R <sup>b</sup>	37	17	284	304	11	138	132	-14	75	66	1	222	255	4	87	-83	
-16	67	-99	4	246	-205	-2	301	-475	18	192	235	12	367	353	-15	153	174	2	81	-29	5	247	-223	
-17	61	-120	6	451	422	-3	394	-439	K,L <sup>a</sup>	1	4	13	299	259	-16	79	-91	3	157	-92	6	158	-119	
-18	169	-234	7	144	-131	-4	612	-628	0	290	-271	14	189	185	-17	110	-84	4	139	-87	8	262	-215	
-19	147	-245	8	147	-147	-5	684	-649	1	641	687	16	92	262	K,L <sup>a</sup>	4	4	5	408	362	9	322	-303	
-20	K,L <sup>a</sup>	11	2	10	285	302	-6	264	-274	2	361	-364	K,L <sup>a</sup>	7	4	-1	387	403	6	274	234	10	267	-232
-21	108	192	11	129	139	-8	310	-285	3	402	420	0	292	-290	-2	52	6	7	98	-118	11	252	-262	
-22	176	199	12	336	322	-2	297	198	4	703	704	1	230	100	-3	238	211	8	308	-287	12	184	-173	
-23	53	55	13	149	157	-10	244	296	5	347	314	2	141	165	-4	475	515	9	330	-316	13	249	-257	
-24	65	84	14	134	160	-11	246	194	6	507	590	5	409	468	-5	56	-50	10	341	-598	K,L <sup>a</sup>	8	3	
-25	65	-80	15	192	205	-12	144	148	7	702	792	4	73	71	-6	485	548	11	416	-477	0	376	-377	
-26	K,L <sup>a</sup>	1	3	16	127	150	-13	147	192	K,L <sup>a</sup>	630	637	0	191	163	-7	135	-79	14	232	-269	1	253	-274
-27	2326	1812	K,L <sup>a</sup>	7	3	-14	391	394	9	543	525	7	240	219	-8	284	-263	15	228	-235	2	184	-145	
-28	851	638	0	336	308	-15	278	274	10	341	348	8	135	110	-9	244	-235	16	116	-109	3	467	-443	
-29	860	785	1	260	271	-16	274	246	12	414	491	9	188	125	-10	347	-390	17	69	-73	4	232	-213	
-30	668	539	2	301	298	-18	101	78	14	244	205	10	156	13	-11	338	-364	K,L <sup>a</sup>	2	5	6	437	-407	
-31	869	799	3	161	140	-11	246	194	15	159	-129	14	110	-137	-12	200	-198	0	397	250	7	391	-341	
-32	959	880	4	613	603	-1	274	-270	16	179	-150	K,L <sup>a</sup>	4	4	-13	196	-166	1	359	-509	8	223	-202	
-33	15	11	5	402	505	-2	94	-60	17	126	-166	1	150	-135	-14	184	-170	2	718	-758	9	249	-226	
-34	198	-119	6	171	181	-3	249	184	16	73	83	121	2	110	-67	-15	154	-397	3	613	-707	10	99	-69
-35	411	-413	7	252	257	-4	497	-458	K,L <sup>a</sup>	2	4	9	198	-194	-16	386	-259	4	712	-814	11	149	-131	
-36	230	207	8	365	350	-5	177	164	0	704	694	8	202	-163	-17	220	-179	5	769	-959	K,L <sup>a</sup>	9	3	
-37	145	91	9	91	95	-6	104	-71	1	344	334	9	182	-185	-18	147	-110	6	383	-373	0	129	-130	
-38	162	-176	14	177	-198	-7	244	-218	2	263	-224	10	66	-65	K,L <sup>a</sup>	5	4	7	407	-353	1	226	-212	
-39	2/4	-276	K,L <sup>a</sup>	R	5	-8	240	-246	3	45	41	11	114	-117	-1	157	-143	8	423	-410	4	351	-314	
-40	143	-131	0	370	364	-9	210	167	4	693	535	K,L <sup>a</sup>	9	4	-2	284	239	9	494	-563	5	251	102	
-41	173	-173	1	122	104	-10	211	-211	5	61	541	1	70	75	-3	831	863	10	117	89	6	291	258	
-42	134	-167	2	154	166	-12	214	211	6	145	191	2	136	141	-4	459	448	11	234	-208	7	124	178	
-43	668	539	7	398	-372	-13	155	156	7	3	-44	3	110	75	-5	459	469	14	297	320	8	161	-125	
-44	630	698	8	306	-342	-10	119	116	8	264	-207	4	109	75	-6	467	485	15	224	233	9	160	-154	
-45	679	745	9	239	-211	-17	127	144	9	73	-89	5	170	122	-7	679	627	16	260	289	K,L <sup>a</sup>	10	5	
-46	766	542	10	353	-311	K,L <sup>a</sup>	6	5	11	403	-69	7	204	190	-8	814	591	17	115	167	1	125	108	
-47	632	594	11	268	-266	-1	104	-114	12	239	-231	9	174	289	-9	166	-153	18	134	250	2	121	89	
-48	759	-660	12	218	-254	-2	75	50	14	158	-114	10	105	123	-11	477	526	K,L <sup>a</sup>	3	5	3	116	76	
-49	351	-262	13	103	-14	3	226	-222	10	230	-233	8	40	-77	-2	298	-296	7	218	226	-6	208	-156	
-50	89	-74	14	201	177	-7	432	-459	11	123	121	8	424	215	-15	152	-164	1	331	-361	K,L <sup>a</sup>	1	5	
-51	953	-605	15	101	184	-6	256	-254	13	206	214	-10	404	475	-12	353	359	16	520	527	-8	651	655	
-52	556	-527	16	-1	584	584	-11	291	-292	17	52	-93	-12	554	675	-15	208	213	0	657	618	3	273	307
-53	344	-514	-2	119	149	-12	277	-311	K,L <sup>a</sup>	4	4	-13	340	384	-16	87	87	1	209	212	-4	198	183	
-54	300	-314	-3	448	-504	-13	149	-186	1	601	601	K,L <sup>a</sup>	1	4	-1	179	-150	3	348	313	-6	591	677	
-55	405	-414	-4	449	-481	-14	134	-150	2	502	525	-1	305	309	-2	169	-140	4	746	688	-7	1273	942	
-56	219	216	-5	303	-340	-15	47	-62	3	572	562	-2	887	-1023	-3	312	-285	5	196	175	-8	487	608	
-57	219	186	-6	202	-222	K,L <sup>a</sup>	-3	5	3	572	562	-2	887	-1023	-3	312	-285	5	196	175	-8	487	608	
-58	328																							

TABLE III. (Continued)

H	F <sub>U</sub>	F <sub>L</sub>	H	F <sub>U</sub>	F <sub>C</sub>																			
-1	170	-109	4	308	287	K,L <sup>a</sup>	8	8	-10	105	190	9	373	367	-2	303	-262	16	205	-323	K,L <sup>a</sup>	0	0	
-2	110	84	5	352	331	2	240	-194	-11	226	185	10	190	145	-3	82	-65	K,L <sup>a</sup>	1	8	-4	241	249	
-3	264	-279	6	360	349	3	-114	-95	-12	235	239	12	195	-162	-4	335	-323	0	394	556	-6	146	-126	
-4	232	-231	7	334	250	4	80	94	-13	305	334	14	167	-13	-5	346	-341	1	189	-147	-7	374	-340	
-5	554	-580	9	138	-138	5	156	141	-14	328	402	15	186	-195	-6	282	-245	2	191	160	-8	325	-296	
-6	365	-349	10	395	-471	6	77	-54	-15	105	155	16	190	-269	-7	381	-381	3	220	-183	-9	347	-326	
-7	421	-451	12	285	-267	K,L <sup>a</sup>	9	6	K,L <sup>a</sup>	6	0	K,L <sup>a</sup>	4	7	8	708	-709	4	473	-457	-10	579	-566	
-8	437	-481	13	305	-314	1	181	151	-1	347	-332	0	410	45	-9	473	-549	5	321	-315	-11	709	-687	
-9	204	-190	14	247	-250	2	128	189	-2	459	-391	1	170	151	-10	425	-445	7	291	-299	-12	94	-50	
-10	198	-177	15	282	-303	3	216	197	-3	177	-204	2	485	475	-11	308	-273	8	632	-660	-13	134	-122	
-11	120	-95	16	143	-163	4	146	159	-4	592	-519	3	139	112	-12	157	-125	9	376	-489	-14	472	-418	
-12	160	-95	17	126	-147	6	149	162	-5	568	-515	4	185	114	-13	246	-235	10	211	-189	K,L <sup>a</sup>	1	8	
-13	179	-167	18	161	-177	7	146	134	-6	259	-221	5	200	-213	-14	121	84	11	181	-153	-1	67	-30	
-14	91	93	K,L <sup>a</sup>	7	6	7	146	134	-7	3	381	9	477	-469	-16	121	79	12	305	-320	-2	487	960	
-15	117	141	0	163	-107	9	44	4	-7	3	381	9	477	-469	-16	121	79	12	305	-320	-2	484	382	
-16	145	120	1	103	-65	K,L <sup>a</sup>	10	6	-8	124	107	10	195	179	K,L <sup>a</sup>	4	7	14	144	-128	-3	484	-326	
-17	180	-137	3	218	-194	0	83	81	-9	340	-334	11	278	-29	-1	406	394	15	159	-146	-4	861	971	
-18	318	-236	4	191	-174	3	141	166	-10	321	-312	12	343	319	-2	263	230	K,L <sup>a</sup>	2	8	-5	77	-21	
-19	410	383	5	420	-411	K,L <sup>a</sup>	0	4	-13	178	124	14	149	-123	-4	376	383	2	305	-284	-7	306	-332	
-20	106	-91	6	88	-83	-3	726	-704	-14	179	155	K,L <sup>a</sup>	5	7	5	384	374	3	328	-462	-8	375	415	
-21	408	393	7	66	-44	-4	345	-371	-16	208	224	0	217	189	-7	102	-24	4	381	-379	-9	282	-233	
-22	177	-151	8	212	-233	-5	705	-661	-17	103	195	5	104	85	-8	187	162	5	278	-219	-12	116	85	
-23	368	-370	10	127	-120	6	624	-631	K,L <sup>a</sup>	7	0	4	240	-223	-9	108	-93	6	282	240	-13	282	-263	
-24	327	-364	11	287	-274	-7	672	-612	-21	101	101	5	333	-335	-10	241	-264	8	117	-120	-14	103	85	
-25	259	-236	13	115	-95	-8	545	-512	-2	256	267	6	112	-114	-11	168	-154	11	149	151	-15	201	-180	
-26	261	-252	14	112	114	-9	507	-421	-4	254	-242	7	198	154	-12	293	-276	12	105	110	-16	337	-299	
-27	159	-135	16	106	109	-10	470	-438	-6	135	-97	8	216	24	-13	302	-334	13	231	226	K,L <sup>a</sup>	2	8	
-28	214	-221	17	64	81	-11	115	-65	-7	108	-174	13	150	135	-14	151	-129	15	69	72	-1	277	-231	
-29	63	-72	K,L <sup>a</sup>	3	0	-12	244	227	-9	246	-229	14	120	147	-15	149	-108	K,L <sup>a</sup>	3	8	-4	183	-168	
-30	353	364	-13	103	-94	-10	208	-213	K,L <sup>a</sup>	6	7	-16	182	-167	0	93	-64	-6	320	335	-10	282	-257	
-31	79	47	1	310	-285	14	205	177	-11	243	-227	2	259	252	-17	102	-182	1	301	-239	-7	110	129	
-32	112	97	2	324	334	-15	240	210	-1	149	-100	5	118	-79	K,L <sup>a</sup>	5	7	2	99	77	-8	187	177	
-33	245	228	3	163	-142	K,L <sup>a</sup>	1	4	-15	74	49	6	171	-102	-1	125	-94	3	185	116	-9	86	37	
-34	242	-212	4	584	477	-1	604	524	K,L <sup>a</sup>	8	0	6	123	-80	-4	104	78	4	193	-154	-10	90	-57	
-35	117	61	5	247	197	-2	923	980	-1	80	29	10	141	-123	-6	399	436	5	213	-190	-11	244	234	
-36	311	316	6	201	154	-3	444	423	-2	202	164	12	176	-116	-7	183	161	6	220	211	-12	225	224	
-37	220	-213	8	224	227	-4	320	-405	-3	114	-107	16	151	-173	-9	189	-189	7	218	203	-15	106	83	
-38	557	9	9	223	-207	-5	580	-563	-4	61	-80	K,L <sup>a</sup>	7	7	11	146	-131	8	423	-427	-16	282	-257	
-39	129	-135	11	111	-91	-6	244	236	-6	114	-125	2	436	-401	-14	122	86	9	236	-214	K,L <sup>a</sup>	3	8	
-40	243	-233	15	95	-75	-7	227	-217	-8	141	-132	3	273	-251	-16	182	-166	12	174	-140	-1	279	252	
-41	234	-257	16	152	-164	-9	624	-624	-9	135	-104	4	311	-305	-17	162	-175	13	92	-88	-2	94	-46	
-42	212	-231	K,L <sup>a</sup>	4	0	-10	373	-416	-10	104	-157	5	305	-295	K,L <sup>a</sup>	6	7	14	78	-73	-3	236	180	
-43	322	320	-11	294	-278	-13	135	-193	-13	230	-235	2	174	144	-15	158	-158	1	348	340	-7	225	217	
-44	440	434	2	86	-70	-13	341	-462	K,L <sup>a</sup>	9	6	8	350	-321	-4	336	333	1	348	340	-7	225	217	
-45	298	302	3	471	-451	-14	196	-181	-1	216	259	11	113	-125	-5	242	270	2	407	-407	-8	257	130	
-46	419	456	4	348	-304	-15	207	-203	-2	216	222	K,L <sup>a</sup>	8	7	7	344	-79	3	427	-443	-9	137	-130	
-47	180	178	5	228	-193	K,L <sup>a</sup>	2	6	-4	108	751	0	500	-545	-10	122	148	4	466	-484	-10	335	336	
-48	274	300	6	396	-381	-1	455	444	-6	146	122	1	171	-144	-13	159	-126	5	304	-268	-11	210	179	
-49	375	395	7	383	-351	-2	119	105	-10	139	-149	2	123	-74	-15	98	-154	6	212	202	-12	121	-83	
-50	240	-201	8	104	-61	-4	49	102	-11	47	-75	4	120	-8	-16	101	-194	9	138	-124	-13	104	-65	
-51	100	134	9	326	-335	-5	841	829	-10	203	199	1	104	-75	-17	116	-90	10	108	95	K,L <sup>a</sup>	4	8	
-52	171	177	10	453	-497	-6	203	-190	-11	104	170	6	109	75	K,L <sup>a</sup>	7	7	11	73	73	-1	395	-367	
-53	177	177	11	0	597	-644	-14	180	-164	0	425	-371	4	283	-280	-9	369	367	3	423	440	-11	267	275
-54	61	62	12	255	-569	-17	210	-179	1	209	-230	2	268	275	-10	208	-172	11	312	332	-2	222	228	
-55	180	152	13	620	-707	K,L <sup>a</sup>	3	6	2	292	-216	6	98	124	-12	209	225	5	218	194	-14	285	178	
-56	308	359	14	176	-171	-1	248	201	3	675	-681	K,L <sup>a</sup>	10	/	-13	251	265	6	347	403	-15	187	197	
-57	219	187	15	124	-147	-2	608	554	4	200	-280	0	77	85	-14	124	132	7	343	346	-16	187	133	
-58	294	216	16	146	-117	-4	74	-59	5	320	-301	2</												

TABLE III. (Continued)

H	FL	FC	H	FO	FC	H	FO	FC	H	FO	FC												
-12	163	-169	7	230	230	-10	250	-241	K,L*	0	10	8	147	-141	-10	252	-239	8	441	-426	-5	173	186
-14	220	-223	8	179	172	-11	212	-225	6	587	-715	9	197	-214	-11	124	145	10	73	-57	-6	244	-246
K,L*	8	8	9	144	-114	-12	124	-134	7	348	-366	10	134	-165	-15	175	175	11	227	-237	-7	66	-51
-3	129	120	11	66	79	-13	167	-218	8	167	-205	K,L*	7	10	K,L*	5	10	12	142	-172	-8	69	-82
-4	129	105	12	54	51	-14	172	-122	9	297	-356	1	130	-97	-1	263	234	K,L*	3	11	-9	289	182
-5	128	125	K,L*	6	9	-15	208	-223	10	509	-503	2	179	-137	-2	213	173	0	213	199	-10	94	-86
-8	76	50	1	194	-155	-16	154	-169	12	179	-173	3	145	-169	-3	273	249	2	168	-178	-11	185	-188
-9	91	-82	3	272	-236	-17	198	-225	13	63	-104	4	63	25	-5	66	58	3	398	-433	-12	198	-212
-10	65	96	4	163	-146	K,L*	4	9	K,L*	1	10	5	211	-229	-6	67	-64	4	351	-351	-13	391	-366
K,L*	9	8	5	147	-169	-1	257	246	0	148	-126	7	142	-112	-7	257	-275	5	416	-441	-14	195	-130
-2	59	152	6	96	-82	-2	217	170	1	473	-361	8	96	64	-8	141	-146	6	148	-127	-13	198	-169
-3	167	136	7	224	-204	-3	130	69	2	434	-467	K,L*	8	10	-9	295	-300	7	149	-136	-16	160	-175
-4	148	48	9	58	-57	-4	157	170	3	322	-416	1	152	125	-10	313	-312	8	243	-233	K,L*	3	11
-5	145	161	10	150	-139	-5	150	139	4	248	-274	2	103	81	-11	259	-238	9	391	-453	-1	189	-63
-7	249	265	11	74	-91	-6	243	239	5	214	-237	J	214	-207	-12	70	-65	10	68	-74	-2	118	183
-8	149	110	K,L*	7	9	-7	453	429	6	125	-13n	5	82	74	-13	252	-244	11	71	-57	-3	243	293
-9	115	143	0	154	-184	-8	427	384	7	274	-286	6	72	88	-14	149	-163	12	41	-33	-5	190	154
K,L*	1	9	1	220	-185	-9	141	115	8	70	-47	K,L*	9	10	-15	53	-58	K,L*	4	11	-6	935	936
0	401	-393	2	297	-289	-10	214	219	9	139	136	1	119	-150	-16	83	-85	0	268	-245	-7	311	334
1	501	-530	3	187	-165	-11	112	-114	10	71	72	2	65	-85	K,L*	6	10	1	398	-445	-8	281	222
2	129	99	7	110	117	-14	70	71	12	140	167	K,L*	0	10	-1	177	140	2	325	-329	-9	184	204
3	181	-187	8	115	104	-18	11H	-126	13	52	17U	4	677	635	-2	329	304	3	188	130	-10	165	151
4	257	-231	9	53	67	K,L*	3	9	14	171	261	5	521	532	-3	177	168	4	101	-77	-11	293	270
5	141	82	10	57	92	-1	10H	155	K,L*	2	1U	6	368	359	-4	166	139	5	136	-85	-12	116	85
6	99	83	K,L*	8	9	-2	24H	-242	0	171	-132	-7	238	-230	-5	300	313	7	81	66	K,L*	6	11
7	323	-331	0	66	-35	-4	158	-175	1	177	82	-8	307	285	-6	276	259	8	76	63	-1	98	-86
9	510	458	1	198	186	-7	404	389	2	80	81	9	275	226	-7	241	229	9	135	150	-2	119	-127
10	442	401	2	224	225	-8	144	109	3	58	-31	-10	452	376	-8	115	68	10	141	151	-15	127	136
12	181	157	3	190	191	-10	201	-194	4	112	106	-12	259	-232	-11	81	82	11	93	130	-4	97	-93
13	181	180	4	70	92	-11	115	103	6	96	81	-13	122	120	-12	109	-107	K,L*	5	11	-6	143	-124
14	62	83	5	181	194	-12	112	97	7	98	106	K,L*	1	10	-13	158	-159	0	280	233	-7	96	-76
15	97	76	6	179	185	-13	216	187	8	106	187	-1	225	-242	-14	60	-73	1	119	89	-10	326	359
K,L*	2	9	7	204	229	-14	155	159	10	130	106	2	234	-206	-15	37	-31	2	226	-202	-11	234	241
0	164	132	K,L*	9	9	-15	58	65	11	142	131	5	229	-213	K,L*	7	10	3	102	-76	-14	137	129
1	122	70	0	87	76	-16	50	-71	13	6	70	-4	127	-102	-1	223	-184	4	102	86	-15	127	136
2	239	225	2	146	126	K,L*	6	9	K,L*	3	1U	-5	402	440	-2	71	-42	5	147	110	-16	120	109
3	366	344	3	155	161	-1	14H	-133	0	412	-355	-6	143	-115	-4	223	181	6	78	98	K,L*	9	11
4	263	252	4	75	95	-2	122	93	1	82	-34	-7	158	143	-5	124	100	7	104	112	-1	81	44
5	614	702	K,L*	1	9	-3	139	-96	2	270	-231	-8	250	242	-6	130	96	8	66	-50	-2	246	-266
6	536	572	-1	264	-215	-4	96	-64	3	01	-35	-9	540	512	-7	160	135	9	124	-92	-3	131	-70
7	436	469	-2	358	-287	-5	147	140	4	137	-143	-10	167	143	-8	66	-44	K,L*	6	11	-5	243	-229
8	216	194	-3	363	-289	-6	333	337	8	157	-13V	-11	206	163	-9	173	156	1	228	-169	-6	182	163
9	114	85	-4	70	76	-7	141	149	9	131	106	-12	224	207	-10	135	124	2	198	-137	-7	162	151
11	310	294	-5	301	-24H	-9	144	146	12	91	-94	-13	272	243	-8	96	111	5	203	-173	-10	117	99
14	65	-82	-6	228	-197	-11	98	117	13	68	12U	K,L*	2	10	-12	69	-45	7	61	55	-13	70	67
15	65	-166	-7	162	-130	-12	93	103	K,L*	4	1U	-1	406	-362	-13	125	125	8	143	135	-14	43	64
K,L*	3	9	-8	66	-70	-13	170	184	0	269	-305	-2	77	55	K,L*	0	10	K,L*	7	11	-15	120	139
0	552	574	-9	157	-121	-14	94	122	1	02	34	-3	185	-173	-1	94	-72	0	93	73	K,L*	6	11
1	475	510	-11	259	248	-15	190	154	2	233	192	-4	79	32	-4	61	-38	1	139	96	-1	83	-68
2	411	376	-12	266	263	K,L*	9	4	63	-61	-5	150	-145	-5	60	51	2	72	68	-2	171	-149	
3	220	211	-13	206	200	-1	147	-153	5	85	-22	-6	360	-323	-6	72	91	3	167	168	-4	250	-234
4	60	-51	-14	121	114	-2	203	-262	6	224	19U	-7	254	-249	-8	123	127	4	243	246	-5	166	-133
5	129	-93	K,L*	2	9	-3	342	-317	7	344	363	-11	66	60	-9	113	138	5	108	81	-8	225	-211
6	78	67	-1	109	77	-4	314	-303	8	193	185	-12	206	183	K,L*	9	10	6	188	209	-13	69	81
7	163	-148	-2	298	209	-5	87	68	9	180	174	-13	87	-91	-1	106	-122	7	62	109	-14	54	81
8	240	-218	-3	119	67	-6	180	-93	10	223	230	-14	167	161	-2	43	-47	K,L*	8	11	K,L*	7	11
9	87	-97	-4	517	-520	-7	128	-126	11	142	125	-15	66	77	-3	52	-50	0	249	275	-1	112	-76
10	460	-421	-5	635	-754	-11	160	173	12	135	135	K,L*	3	10	-5	49	-55	1	206	223	-2	113	-77
11	254	-252	-6	432	-441	-12	68	70	K,L*	5	1U	-1	205	179	-6	36	25	2	52	70	-4	76	66
12	274	-284	-7	185	-182	-13	59	58	0	109	165	-3	306	-263	-7	36	49	3	98	-61	-5	144	-114
13	203	-229	-8	56	-61	-14	204	234															

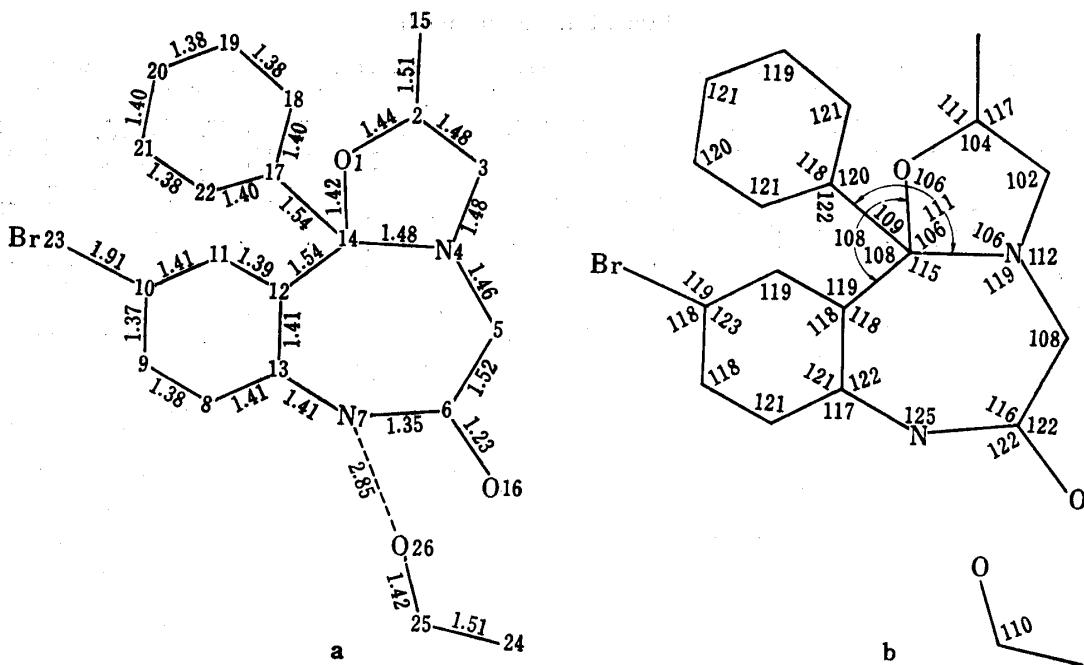


Fig. 2. (a) Bond Distances (b) Bond Angles

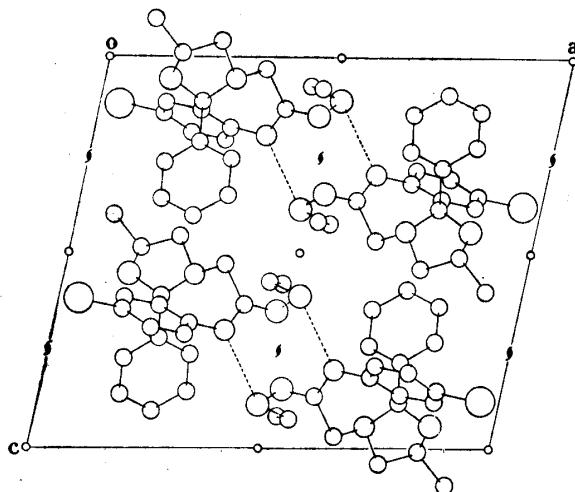


Fig. 3. The Crystal Structure as Viewed along the b Axis

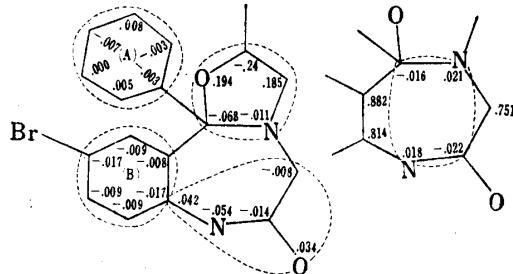


Fig. 4. Deviation in Ångstrom Units from Least-Squares Planes

saturated carbon atoms in a pyramidal form. The bond lengths of C3-N4, C5-N4 and C14-N4 are normal, and their values are 1.48, 1.46 and 1.48 Å. The angles of C3-N4-C14, C3-N4-C5 and C5-N4-C14 are 106.2, 111.5 and 118.6° respectively. On the other hand, the N7 atom is bonded to a carbonyl group and a benzene ring; the bond lengths of C6-N7 and C13-N7, 1.35 and 1.41 Å respectively are shorter than the normal C-N single bond of 1.47 Å. Shorter carbon-nitrogen bond lengths have been pointed out by Karle<sup>6)</sup> such that nitrogen atoms adjacent to C=S, C=O, and C=C bonds, tend to be in a planar configuration with short C-N bond lengths of in the range 1.34—1.40 Å. The bond angle for C6-N7-C13 is 125.3°. Several molecules containing such systems have usually larger bond angles, some examples of these compounds are shown in Table IV. The value of the mean bond lengths of the benzene rings is 1.39 Å which is normal. The deviations of the atoms from the benzene least squares planes are within 0.01 Å for benzene ring A and 0.02 Å for ring B. The intermolecular contacts within 3.7 Å are given in Table V. They are

within the range of normal van der Waals radii. Intermolecular hydrogen bonds are observed in N7...O26=2.85 Å and O26...O16=2.78 Å.

TABLE IV. Comparison of Csp<sup>3</sup>-N-Csp<sup>3</sup> Bond Angles

Compound	Angle	Reference
	125.3	This work
	128.4	H. Ringertz (1966) <sup>a</sup>
	127.5	
	127.6	B.F. Pedersen (1967) <sup>b</sup>
	124.5	F. Hanic (1966) <sup>c</sup>
	1; 120.6 2; 126.3	K. Hoogsteen (1963) <sup>d</sup>

a) H. Ringertz, *Acta Cryst.*, **20**, 983 (1966)  
 c) F. Hanic, *Acta Cryst.*, **21**, 332 (1966)

b) B.F. Pederson, *Acta Chem. Scand.*, **21**, 1415 (1967)  
 d) K. Hoogsteen, *Acta Cryst.*, **16**, 28 (1963)

TABLE V. Intermolecular Contacts within 3.7 Å

O 26...O 26(I)	3.47	C 21...C 9(III)	3.61
N 4...C 25(II)	3.67	C 22...C 9(III)	3.68
C 6...O 26(II)	3.58	C 25...O 16(IV)	3.54
O 16...C 25(II)	3.58	O 26...C 5(IV)	3.46

I: 1-x, 1-y, 1-z  
 II: 1-x, 1/2+y, 1/2-z

III: x, 3/1+y, z  
 IV: x, 3/2-y, 1/2+z