

CeO₂-Promoted W-Mn/SiO₂ catalysts for conversion of methane to C₃–C₄ hydrocarbons at elevated pressure

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A CeO₂-doped Na-Mn-W/SiO₂ catalyst for oxidative conversion of methane has been studied in a micro-stainless-steel reactor under elevated pressure; a CH₄ conversion of 47.2% with a C₃–C₄ selectivity of 47.3% (C₂:C₃:C₄ = 1:1:3.3) was obtained at 983 K with 1.0×10^5 ml g⁻¹ h⁻¹ GHSV, CH₄/O₂ = 2.5 and *P* = 0.6 MPa.

In the last two decades, much attention has been paid to the conversion of methane under oxidative conditions into products with additional value.^{1–3} Recently, our work on the 2% Mn₂O₃–5% Na₂WO₄/SiO₂ catalyst showed that this catalyst had excellent activity for oxidative coupling of methane (OCM) under different reaction conditions including under elevated pressures, and was stable for long periods.^{3,4} In the OCM over the catalyst, we found that small amounts of C₃ and C₄ hydrocarbons were produced under different conditions, particularly at elevated pressures. On the other hand, Lunsford and coworkers,⁵ in particular, reported that C₃ and C₄ hydrocarbons were obtained from methane oxidation through a two-step reaction.

Here, the CeO₂ modified Mn₂O₃–Na₂WO₄/SiO₂ catalyst system was examined and found to have excellent performance in the conversion of methane to C₃–C₄ hydrocarbons under elevated pressure.

The CeO₂ modified 2% Mn₂O₃–5% Na₂WO₄/SiO₂ catalysts were prepared by the wet impregnation method. Silica particles were washed with water several times and dried and used as the stand-by material. The pretreated silica particles (40–60 mesh, surface area = 156 m² g⁻¹) were impregnated with aqueous solutions of Mn(NO₃)₂ (A.R.), Na₂WO₄·2H₂O (A.R.) and Ce(NO₃)₃·6H₂O in appropriate concentrations at 323 K. The catalysts were dried overnight at 373 K and calcined in air at 1123 K for 8 h (the surface area of the resulting catalyst was 6.8 m² g⁻¹). The catalytic runs were carried out in a continuous vertical-flow fixed-bed reactor comprising of a stainless-steel tube (I.D. = 8 mm). 0.4 g catalyst was loaded in the reactor while the remaining space of the reactor was filled with ceramic particles (40 mesh) so as to minimize the contribution due to any gas-phase reactions.

In all experiments, the reactant gases (without diluent) were co-fed into the reactor and their flow-rates were regulated with

mass flow controllers. A Ni/Cr–Ni/Al thermocouple was inserted into center of the reactor to monitor the temperature of the catalyst-bed and another thermocouple was positioned at the hottest part of the reactor to manipulate the furnace. The products were analyzed using three on-line gas chromatographs with TCD detectors (two GCs, one with a 5A molecular sieve column, for the separation and analysis of O₂, CH₄, CO and the other with a Poropak Q column for CH₄, CO₂, C₂H₄, C₂H₆) and in the third a GC FID detector with a Al₂O₃ capillary column (40.0 m) was used, with high-purity nitrogen as the carrier gas to separate C₃–C₄ hydrocarbons.

We examined the effects of several reaction conditions, such as temperature, pressure, GHSV and ratio of methane to oxygen on selectivity to C₃–C₄ hydrocarbons and conversion of methane. Based on the investigated effects of the operation conditions, all experiments were chosen under mild temperatures and high GHSVs. The results obtained over the CeO₂ doped Mn-W/SiO₂ catalyst at 983 K and 0.6 MPa with a range of GHSVs are presented in Table 1, where data were taken after 30 min of reaction. In the reaction of CeO₂ modified 2% Mn₂O₃–5% Na₂WO₄/SiO₂ catalysts for oxidative conversion of methane, it was found that a 16.5% yield of C₃–C₄ hydrocarbon with a 37.2% of CH₄ conversion could be obtained at a CH₄/O₂ ratio of 4 and 1.0×10^5 ml g⁻¹ h⁻¹ GHSV (run 6 in Table 1). Table 1 illustrates that CH₄ conversion and selectivity of C₃–C₄ hydrocarbons increases, with an increase of GHSV from 0.4×10^5 to 1.0×10^5 ml g⁻¹ h⁻¹, however, when the GHSV was increased from 1.0×10^5 to 2.0×10^5 ml g⁻¹ h⁻¹, CH₄ conversion and selectivity of C₄ hydrocarbon decreased, but C₃ selectivity still increased. Table 1 also shows that in terms of the conversion of methane to C₃–C₄ hydrocarbons the CeO₂ doped Mn-W/SiO₂ catalyst (Mn₂O₃–Na₂WO₄/SiO₂ with added CeO₂) have excellent catalytic activity. However, in other catalyst formulations, such as CeO₂ doped Mn/SiO₂, Na₂WO₄/SiO₂, Mn/SnO₂ and Na₂WO₄/CeO₂, only small amounts of C₃–C₄ were observed, which indicates a synergistic interaction Ce, Mn and W over the CeO₂ doped Mn-W/SiO₂ catalyst.

Fig. 1 shows the effects of CH₄/O₂ on CH₄ conversion and C₃–C₄ selectivities. With a decrease of CH₄/O₂, CH₄ conversion, C₃–C₄ yield and C₃–C₄ selectivities increase, whereas

Table 1 Performances of CeO₂–Mn₂O₃–Na₂WO₄/SiO₂ and other catalysts for the oxidative conversion of methane at elevated pressures^a

Cat.	10 ⁻⁵ GHSV/ml g ⁻¹ h ⁻¹	Conv. (%)	Selectivity (%)							
			C ₂	C ₂ =/C ₂ -	C ₃	C ₃ =/C ₃ -	C ₄	C ₄ =/C ₄ -	CO ₂	CO
A ^b	1.0	18.5	60.4	1.57	0	—	5.0	0	20.6	14.0
B ^c	1.0	23.3	62.2	1.85	2.6	0.23	0	—	21.4	15.2
C	1.0	32.1	34.2	1.40	4.5	0.41	19.5	4.11	20.5	21.3
D	0.4	22.4	49.6	1.14	11.1	0.13	3.4	0.28	20.6	15.3
D	0.5	20.3	32.3	2.09	13.0	0.14	16.0	6.45	19.4	19.1
D	1.0	37.2	29.4	2.18	16.4	0.18	28.0	5.20	10.6	15.6
D	1.5	30.7	30.8	2.61	19.2	0.10	8.2	4.94	13.6	28.2
D	2.0	30.0	27.2	3.15	23.3	0.10	7.3	0.82	17.0	25.2

^a Reaction conditions: CH₄/O₂ = 4, *P* = 0.6 MPa, *T* = 983 K. ^b SiO₂ non-treated. ^c SiO₂ treated by washing with water, A = 2% Mn₂O₃–5% Na₂WO₄/SiO₂, B = 2% Mn₂O₃–5% Na₂WO₄/SiO₂-treated, C = 5% CeO₂–2% Mn₂O₃–2.5% Na₄P₂O₇/SiO₂, D = 5% CeO₂–2% Mn₂O₃–5% Na₂WO₄/SiO₂.

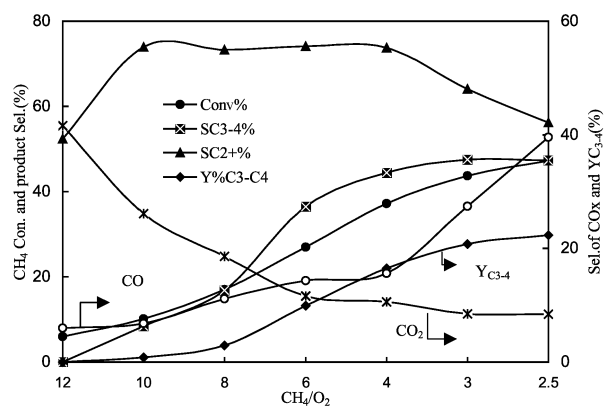


Fig. 1 Effect of CH_4/O_2 on the conversion of methane over 5% CeO_2 - Na_2WO_4 - $\text{Mn}_2\text{O}_3/\text{SiO}_2$: $T = 983 \text{ K}$, $\text{GHSV} = 1.0 \times 10^5 \text{ ml g}^{-1} \text{ h}^{-1}$, $P = 0.6 \text{ MPa}$.

CO_2 selectivity decreases significantly and CO selectivity increases sharply, but the total CO_x selectivity decreases slightly. This implies, at least partly, that the origin of CO_x is mainly from the oxidation of CH_4 at this rather high temperature (983 K), pressure and GHSV over CeO_2 modified Mn_2O_3 - $\text{Na}_2\text{WO}_4/\text{SiO}_2$ catalyst. An increase in oxygen pressure results in a marked shift to higher molecular weight products. A 22.3% yield of C_3 - C_4 with 47.2% of CH_4 conversion and 47.3% of C_3 - C_4 selectivity was obtained at $\text{CH}_4/\text{O}_2 = 2.5$. Additionally, it is found that higher temperatures do not favor the formation of C_3 - C_4 hydrocarbons.

The addition of CeO_2 to the Mn-W/ SiO_2 catalysts on the conversion of methane to C_3 - C_4 hydrocarbons at elevated pressures led to significant effects. Fig. 2 shows the effects of CeO_2 loading on CH_4 conversion and C_3 - C_4 selectivities for the reaction. With CeO_2 loading increased from 0 to 5%, CH_4 conversion and C_3 - C_4 yield increases. Further CeO_2 loading from 5 to 20% led to a slight decrease in CH_4 conversion and C_3 - C_4 yield. The performances of catalyst depend on the loading of CeO_2 and the most suitable amount of CeO_2 is 1-5%. We found that other metal oxide doped 2% Mn_2O_3 -5% $\text{Na}_2\text{WO}_4/\text{SiO}_2$ catalysts also exhibit good conversions of methane to C_3 - C_4 hydrocarbons, for example, on a 8% SnO_2 promoted Na-Mn-W/ SiO_2 catalyst, a CH_4 conversion of 29.7% with a C_3 - C_4 selectivity of 42.0% was attained at a pressure of 0.6 MPa and 1013 K.

By investigating all these results, it is concluded that the CeO_2 promoted Na-Mn-W/ SiO_2 catalysts not only exhibit

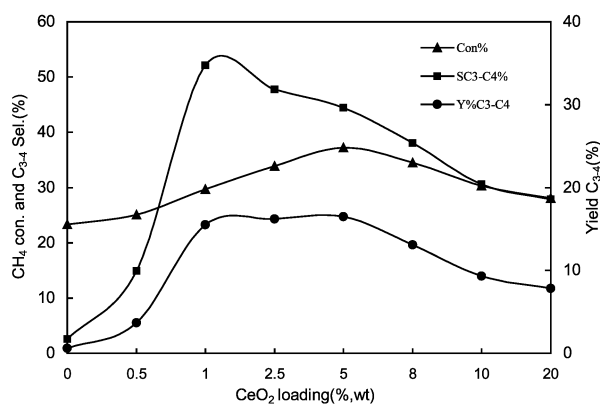


Fig. 2 Effect of CeO_2 loading on the conversion of methane over CeO_2 - Na_2WO_4 - $\text{Mn}_2\text{O}_3/\text{SiO}_2$: $T = 983 \text{ K}$, $\text{GHSV} = 1.0 \times 10^5 \text{ ml g}^{-1} \text{ h}^{-1}$, $\text{CH}_4/\text{O}_2 = 4$, $P = 0.6 \text{ MPa}$.

excellent performance for conversion of methane to C_3 - C_4 hydrocarbons at elevated pressure but also show excellent behavior for the oxidative coupling of methane: at $1.5 \times 10^5 \text{ ml g}^{-1} \text{ h}^{-1}$ GHSV and 993 K with a CH_4/O_2 ratio of 6, a 23.0% CH_4 conversion with 84.7% C_{2+} selectivity was achieved. On the basis of the above results, we propose that high GHSV, low CH_4/O_2 ratio, low temperature and elevated pressure favor the output of C_3 - C_4 hydrocarbons. We consider that C_3 or C_4 hydrocarbons are formed by oxidative dehydrogenation and oxidative re-coupling of C_2H_4 and/or C_2H_6 (containing CH_4) in the gas phase and the partial pressure of oxygen in the gas phase plays an important role in the implementation of the reaction.⁶

Further experiments are currently being carried out in our laboratory to confirm these deductions through catalyst characterization and to explain the nature of the CeO_2 promoted Mn-W/ SiO_2 catalysts under elevated pressure.

Notes and references

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