# Study of the U-Zr-O Ternary System\*

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In recent years, high-temperature interactions between UO<sub>2</sub> fuel and Zircaloy cladding have been studied to elucidate the fuel rod behavior under severe core damage conditions. Interfacial reaction of UO<sub>2</sub> with Zircaloy has been extensively investigated from kinetic points of view [1-3], and several analytical models have been proposed for the reaction [4--6].

For an understanding of the  $UO_2/Zircaloy$ chemical interaction, information is needed both on the reaction kinetics and on phase equilibria in a U-Zr-O ternary system. The UO<sub>2</sub>/Zircaloy interaction cannot be explained in terms of a pseudobinary UO<sub>2</sub>-Zr system, but should be treated as a ternary reaction in the U-Zr-O system.

The first study of phase relations in the U-Zr-O system was made by Saller et al. [7], and Politis [8] has proposed the isothermal sections at 1000, 1500 and 2000 °C. In our previous papers [9, 10], the isothermal section at 1000 °C has been reconstructed in the U-Zr-O system. Skokan and coworkers [11] have performed thermal analyses on the quasi-binary section between UO<sub>2</sub> and oxygen-saturated  $\alpha$ -Zr.

In order to interpret the chemical composition of the phases and the sequence of the reaction zone in the  $UO_2/Zircaloy$  chemical interaction, further investigation of phase equilibria is considered necessary. The purpose of the present study is to clarify whether or not the formation of a liquid phase can be caused by the reaction of Zr with  $UO_2$  at high temperatures and to examine the phase regions and boundaries in the U-Zr-O ternary system.

# Experimental

Powders of  $UO_2$  (O/U ratio = 2.16), Zr (99.9 wt.% purity) and ZrO<sub>2</sub> (99.9 wt.% purity) were used as starting materials. These powders were well ground and then mixed in the desired proportions. The mixtures with various compositions were pelletized,

The heated sample was powdered in a dry argonfilled glove box, and phases in the reaction products were identified by a computer-controlled X-ray diffractometer. Lattice parameters of the reaction products were evaluated from reflections according to Cohen's method.

Metallographic examination was also made for some of the samples with the aid of a scanning electron microscope (SEM) and an optical microscope. Compositions of reaction products were analysed by means of an energy dispersive X-ray analyser (EDXA).

#### **Results and Discussion**

The results for X-ray diffraction analysis of pellets of  $Zr/UO_2$  mixtures (samples A-Y) and  $Zr/ZrO_2/$ UO<sub>2</sub> mixtures (samples a-x) heated at 1400 °C are given in Fig. 1. No change with reaction period in the type and number of phases identified in the heated pellets was observed. All the results for X-ray diffraction analysis described in the present paper were



Fig. 1. Reaction products in Zr/UO<sub>2</sub> and Zr/ZrO<sub>2</sub>/UO<sub>2</sub> mixture pellets after heating at 1400 °C.

<sup>\*</sup>Paper presented at the Second International Conference on the Basic and Applied Chemistry of f-Transition (Lanthanide and Actinide) and Related Elements (2nd ICLA), Lisbon, Portugal, April 6-10, 1987. <sup>†</sup>Author to whom correspondence should be addressed.

obtained for samples with a 20-h reaction period. It is apparent from Fig. 1 that the type and number of phases are strongly dependent upon the composition of the sample.

For  $Zr/UO_2$  mixture pellets after heating at 1400 °C, only sample A was found to contain ZrO<sub>2</sub> in the reaction products. The X-ray diffraction pattern for sample **B** revealed that two phases  $(UO_2)$ and  $\alpha$ -Zr) existed in the reaction products. Three phases (UO<sub>2</sub>,  $\alpha$ -Zr and  $\alpha$ -U) were detected in the samples C-J with Zr contents of the samples from 20 to 66 at%. The reaction products for the samples **K**-**T** were composed of  $\alpha$ -U and/or UZr<sub>2</sub> in addition to  $\alpha$ -Zr, but UO<sub>2</sub> was not detected. The diffraction analysis for the samples U-Y showed that the reaction products consisted of  $\alpha$ -Zr and  $\beta$ -Zr. The  $\alpha$ -U,  $\beta$ -Zr and UZr<sub>2</sub> detected in the reaction products by X-ray diffraction analysis at room temperature are inferred to result from (U, Zr) liquid or solid solution at 1400 °C.

The reaction products for sample **a** were composed of UO<sub>2</sub> and ZrO<sub>2</sub>. In the composition range for samples **b**-**j**, UO<sub>2</sub>,  $\alpha$ -Zr and ZrO<sub>2</sub> were identified in the reaction products. The X-ray diffraction patterns of samples **a**-**e** indicated that monoclinic ZrO<sub>2</sub> was involved in addition to the tetragonal phase. The monoclinic ZrO<sub>2</sub> is presumed to be a transformed phase based on the literature of UO<sub>2</sub>-ZrO<sub>2</sub> and Zr-O binary systems [12, 13], and the stable form ZrO<sub>2</sub> at 1400 °C seems to be tetragonal. UO<sub>2</sub> and  $\alpha$ -Zr were present in the reaction products of samples **k**-**o**. In the samples **p**, **q** and **r**, UO<sub>2</sub>,  $\alpha$ -Zr and  $\alpha$ -U were detected, while no formation of UO<sub>2</sub> was observed for the samples **s**-**x**.

The dependence of lattice parameters a and c, and axial ratio c/a on the Zr content of  $\alpha$ -Zr in the reaction products of the Zr/UO<sub>2</sub> mixture pellet is illustrated in Fig. 2. The lattice parameters for  $\alpha$ -Zr in the reaction products increased from a = 0.3233nm and c = 0.5149 nm for the starting Zr powder to the values of a = 0.3252 - 0.3246 nm and c = 0.5176 - 0.51760.5195 nm for samples C-V. The axial ratio c/a for  $\alpha$ -Zr was also larger than that before reaction (1.593). The extent of increase in the lattice parameters and axial ratio is found from this Figure to vary with the composition of the sample. Samples C-J, in which three phases of  $UO_2$ ,  $\alpha$ -Zr and  $\alpha$ -U were detected, showed nearly constant values of a = 0.3247 nm and c = 0.5194 nm. In this composition range, the c/aratio of 1.600 is also independent of the Zr content of the sample. Above a Zr content of 69 at%, the lattice parameter c decreased with increasing Zr content, whereas a more complicated change in the value of a was observed as the Zr content increased. The c/a ratio rapidly decreased from 1.600 to 1.593.

Figure 3 represents the variation of lattice parameters a and c, and axial ratio c/a with the Zr content of  $\alpha$ -Zr in Zr/ZrO<sub>2</sub>/UO<sub>2</sub> mixture pellets. The lattice



Fig. 2. Change in lattice parameters a and c, and axial ratio c/a with Zr content of  $\alpha$ -Zr in reaction products of the  $Zr/UO_2$  mixture pellet.



Fig. 3. Change in lattice parameters a and c, and axial ratio c/a with Zr content of  $\alpha$ -Zr in reaction products of the  $Zr/ZrO_2/UO_2$  mixture pellet.

parameters a and c and the axial ratio changed with Zr content in the range of 82-72 at% zirconium. The samples in which three phases (UO<sub>2</sub>,  $\alpha$ -Zr and  $\alpha$ -U) were detected revealed nearly constant a, c and c/a values, which were close to the data for the Zr/UO<sub>2</sub> pellets having UO<sub>2</sub> as one of the reaction products. In the composition range where two phases of UO<sub>2</sub> and  $\alpha$ -Zr coexisted, the lattice parameter c and the ratio c/a increased with decreasing Zr content, but the value of a decreased. There is no marked difference in values of a, c and c/a among the samples c-j with lower Zr content. The mean values of the lattice parameters and axial ratio were a = 0.3245 nm, c = 0.5200 nm, and c/a = 1.602.

Reaction at 1400 °C resulted in a considerable expansion in the direction of the *c*-axis and only a slight change in the *a*-axis in  $\alpha$ -Zr. The lattice parameters of Zr and Zr-O solid solution,  $\alpha$ -Zr(O), are provided in the literature [14-16]. The incorporation of oxygen atoms into the  $\alpha$ -Zr lattice causes a marked increase in the value of c over the entire range of solid solubility. The value of a is less affected by the oxygen content but passes through a pronounced maximum at the composition of 20 at% oxygen. The changes in the lattice spacing after heating are considered to be closely related to oxygen dissolution in  $\alpha$ -Zr. The lattice parameters of  $\alpha$ -Zr in samples c-j containing  $ZrO_2$  as one of the reaction products indicated constant values irrespective of the sample composition and were in accord with those reported for  $\alpha$ -Zr(O) at the solubility limit of about 30 at% oxygen. Therefore, it can be concluded that in the samples  $c_{-j}$  with UO<sub>2</sub> and ZrO<sub>2</sub>  $\alpha$ -Zr may be saturated with oxygen. For the samples C-J and p-r which consisted of UO<sub>2</sub>,  $\alpha$ -Zr and  $\alpha$ -U,  $\alpha$ -Zr showed

nearly constant lattice parameters and axial ratio, which were lower than the reported values for oxygen-saturated  $\alpha$ -Zr(O). This suggests that  $\alpha$ -Zr coexisting with  $UO_2$  and  $\alpha$ -U has a constant oxygen content and may be unsaturated with oxygen. Assuming that the solubility of uranium in  $\alpha$ -Zr(O) is quite small and that dissolved uranium does not affect the lattice expansion of  $\alpha$ -Zr(O),  $\alpha$ -Zr in the reaction products for samples  $\mathbf{C}-\mathbf{J}$  and  $\mathbf{p}-\mathbf{r}$  may contain about 25 at% oxygen. However, in the composition range where no  $UO_2$  was formed in the reaction products, the a, c and c/a values of  $\alpha$ -Zr changed with the Zr content of the sample, and the values of c and c/awere lower than those for the samples C-J and p-r. These changes in the lattice parameters are attributed to the variation of oxygen content in α-Zr. In Zr-rich samples K-V and s-x, in which  $UO_2$  was not identified,  $\alpha$ -Zr appears to have various oxygen contents below 25 at% oxygen. From the results of phase identification and lattice parameter measurements, it was verified that the reduction of UO<sub>2</sub> by Zr produced uranium and that the type and number of phases thus formed were influenced by the composition of the sample.

Metallographic examination was carried out by means of SEM and optical microscopy for the Zr/ UO<sub>2</sub> samples F, G, L, Q, U, X and Y after heating at 1400 °C for 50 h. Typical results for SEM observation are shown in Fig. 4. The samples F and G in which three phases (UO<sub>2</sub>,  $\alpha$ -Zr and  $\alpha$ -U) were detected by the X-ray diffraction method were metallographically found to contain UO<sub>2</sub>,  $\alpha$ -Zr and metallic uranium. As evidenced by Fig. 4a, there exist large  $\alpha$ -Zr(O) particles, and small UO<sub>2</sub> particles are located in the metallic region. The EDXA analysis of the metallic



Fig. 4. Microstructures of  $Zr/UO_2$  mixture pellets after heating at 1400 °C: (a) sample G; (b) sample L; (c) sample Q; (d) sample Y.

region revealed that the U/(U + Zr) ratio of this region was 0.95-0.90. From the morphology of this U-rich phase, it was difficult to know whether at 1400 °C the phase is liquid or not. However, the result for EDXA analysis established that on the basis of the binary phase diagram of the U-Zr system [17], the U-rich phase should be a liquid rich in uranium at 1400 °C. The uranium content in the  $\alpha$ -Zr(O) particle was evident from EDXA analysis to be very low, and the uranium solubility in  $\alpha$ -Zr(O) can be estimated to be below 2 at%. The samples in this composition range seem to contain three phases  $(UO_2, \alpha$ -Zr(O) and liquid) at 1400 °C. Microstructures of samples L and Q are shown in Fig. 4b and c. In sample L, large  $\alpha$ -Zr(O) particles were surrounded by a U-rich region possessing a U/(U + Zr) ratio = 0.53. The micrograph of sample Q indicates that the U-rich region involves needlelike  $\alpha^\prime$  precipitates. The U-rich region in sample Q has a U/(U + Zr) ratio of 0.27. The structure of sample U is similar to that of sample **Q**. The value of U/(U + Zr) for the U-rich region is 0.08. For these samples, the U-rich region may exist as a  $(\gamma$ -U,  $\beta$ -Zr) solid solution at 1400 °C. In the composition range where no UO<sub>2</sub> was detected in the reaction products by X-ray analysis,  $\alpha$ -Zr(O) appears to coexist with  $(\gamma - U, \beta - Zr)$  solid solution with various uranium contents. As can be seen in Fig. 4d, a number of platelike  $\alpha'$  precipitates were formed in prior- $\beta$ -Zr matrix. This was a characteristic structure for Zr-rich samples X and Y. The  $\alpha'$  precipitates were



Fig. 5. Isothermal section of the U–Zr–O ternary system at 1400  $^{\circ}$ C.

introduced during cooling. Since no  $\alpha$ -Zr(O) islands (as observed in the samples L, Q and U) were formed, these samples are considered to consist of a  $\beta$ -Zr single phase at 1400 °C.

Figure 5 shows the isothermal section of the U-Zr-O ternary system at 1400 °C proposed from the present results for  $Zr/UO_2$  and  $Zr/ZrO_2/UO_2$  reaction experiments. The phase relationships which differ from those obtained at lower temperatures [7-10]are essentially consistent with Politis's results at 1500 ℃ [8]. In the isothermal section at 1400 ℃, there exists the characteristic triangle of  $UO_2$  +  $\alpha$ -Zr(O) + L (L = liquid). Compositions of UO<sub>2</sub>,  $\alpha$ -Zr(O) and liquid have to be thermodynamically fixed in this three-phase region. Actually, experimental results of lattice spacing for  $\alpha$ -Zr in this phase region are in agreement with the phase rule. The solubilities of oxygen and uranium in  $\alpha$ -Zr(O) are about 25 and 2 at%, respectively. The UO<sub>2</sub> takes little Zr into solution at 1400 °C, as can be predicted by the  $UO_2$ --ZrO<sub>2</sub> pseudo-binary phase diagram [12]. Although the composition of the liquid phase in equilibrium with  $\alpha$ -Zr(O) and UO<sub>2</sub> was not determined precisely, it will contain about 10 at% Zr. This three-phase region may be adjacent to two-phase regions of UO<sub>2</sub> + L,  $\alpha$ -Zr(O) + L, and UO<sub>2</sub> +  $\alpha$ -Zr(O). In the two-phase region of  $UO_2 + \alpha - Zr(O)$ , the  $\alpha$ -Zr(O) in equilibrium with UO<sub>2</sub> possesses an oxygen content ranging from 25 to 30 at%.

Compositions for samples with higher oxygen content are expected to lie in the three-phase region of UO<sub>2</sub>, tetragonal  $ZrO_2$  and  $\alpha$ -Zr(O). In the twophase region of  $\alpha$ -Zr(O) and ( $\gamma$ -U,  $\beta$ -Zr), the lattice parameters of  $\alpha$ -Zt vary with composition. The results for X-ray diffraction analysis of  $\alpha$ -Zr in this region allow us to draw isoparametric lines. Tentative isoparametric lines which correspond to tie lines are shown in the isothermal section. In the binary Zr-O system,  $\beta$ -Zr with 6 at% oxygen content can equilibrate with 14 at% oxygen  $\alpha$ -Zr(O) [13]. The conjugate phase of  $\alpha$ -Zr(O) with an oxygen content of about 15 at% is likely to be a ( $\gamma$ -U,  $\beta$ -Zr) solid solution with a limited U concentration range of 0-10 at%. The compositions of  $(\gamma - U, \beta - Zr)$  in equilibrium with  $\alpha$ -Zr(O) estimated from isoparametric lines agree with the results obtained by EDXA analysis of the  $Zr/UO_2$  mixture pellets.

# Conclusions

The isothermal section at 1400 °C was proposed for the U-Zr-O ternary system. The liquid phase was confirmed to exist in the isothermal section at 1400 °C. It should be noted that at 1400 °C UO<sub>2</sub> can equilibrate with  $\alpha$ -Zr(O) of oxygen content between 25 and 30 at%. Zirconium can reduce UO<sub>2</sub>, and may produce liquid uranium as long as the oxygen content of Zr reaches about 25 at%. However, above the oxygen content of 25 at% Zr cannot continue the oxygen absorption from  $UO_2$ .

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