

- (7) Friedman, L., "The Determination of the Supercompressibility of Natural Gases," M.S. thesis in Petroleum Engineering, Texas A and M College, College Station, Tex., 1941.
- (8) Harper, R. C., Jr., "An Investigation of the Compressibility Factors of Gaseous Mixtures of Carbon Dioxide and Helium," Ph.D. dissertation in Chemistry, The University of Pennsylvania, Philadelphia, Pa., 1956.
- (9) Harper, R. C., Jr., Miller, J. G., *J. Chem. Phys.* **27**, 36-9 (1957).
- (10) International Critical Tables, Vol. I, pp. 395-402, McGraw-Hill, New York, 1926.
- (11) Keesom, W. H., "Helium," pp. 36-8, Elsevier Press, Amsterdam, 1942.
- (12) Kenney, J. F., Keeping, E. S., "Mathematics of Statistics," Part 2, pp. 207-11, Van Nostrand, New York, 1951.
- (13) Kramer, G. M., Miller, J. G., *J. Phys. Chem.* **61**, 785-88 (1957).
- (14) Liley, P. E., *J. Imp. Coll. Chem. Eng. Soc.* **7**, 69-85 (1953).
- (15) MacCormack, K. E., Schneider, W. G., *J. Chem. Phys.* **18**, 1269-72 (1950).
- (16) MacCormack, K. E., Schneider, W. G., *Ibid.*, **19**, 845-8 (1951).
- (17) Michels, A., Wouters, H., *Physica* **8**, 923-32 (1941).
- (18) Nicholson, G. A., Schneider, W. G., *Can. J. Chem.* **33**, 589-96 (1955).
- (19) Otto, J., "Handbuch der Experimentalphysik, Bd. VIII, Teil 2, 144 (1929).
- (20) Pfefferle, W. C., Jr., Ph.D. dissertation in Chemistry, The University of Pennsylvania, Philadelphia, Pa., 1952.
- (21) Pfefferle, W. C., Jr., Goff, J. A., Miller, J. G., *J. Chem. Phys.* **23**, 509-13 (1955).
- (22) Pfefferle, W. C., Jr., Miller, J. G., Univ. Penn. Thermodynamics Research Lab. Tech. Rept. June 1950.
- (23) Schneider, W. G., *Can. J. Research* **B37**, 339-52 (1949).
- (24) Schneider, W. G., Duffie, J. A. H., *J. Chem. Phys.* **17**, 751-54 (1949).
- (25) Stevens, A. B., Vance, H., *Oil Weekly* **106**, 21-26 (June 8, 1942).
- (26) Tanner, C. C., Masson, I., *Proc. Roy. Soc. (London)* **A126**, 268-88 (1929-30).
- (27) Wartel, W. S., "Compressibility Factor Determinations for Binary Gas Mixtures Containing Small Per Cents of One Component," Ph.D. dissertation in Chemistry, The University of Pennsylvania, Philadelphia, Pa., 1954.
- (28) Watson, G. M., others, *Ind. Eng. Chem.* **46**, 362-4 (1954).
- (29) Whalley, E., Lupien, Y., Schneider, W. G., *Can. J. Chem.* **31**, 722-33 (1953).
- (30) *Ibid.*, **33**, 633-6 (1955).
- (31) Wiebe, R., Gaddy, V. L., Heins, C., Jr., *J. Am. Chem. Soc.* **53**, 1721-25 (1931).
- (32) Yntema, J. L., Schneider, W. G., *J. Chem. Phys.* **18**, 641-6 (1950).
- (33) Zimmerman, R. H., Beitler, S. R., *Trans. Am. Soc. Mech. Engrs.* **74**, 945-51 (1952).

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## Compressibility of Isopentane with the Burnett Apparatus

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For the range in which modern compressibility data on isopentane at temperatures of interest are lacking, the Burnett method (5) is ideally suited. For complete and accurate establishment of the isotherms, the relatively low vapor pressures require an apparatus capable of accurate measurements at low as well as high pressures.

The Burnett apparatus constant,  $N$ , was determined by helium calibration to be 1.41507, and compressibility factor isotherms of gaseous isopentane, from 50° to 200°C. and at pressures up to 65 atm., were determined as described in the preceding article (17). Vapor pressures, saturated vapor densities, and second virial coefficients were also determined.

### EXPERIMENTAL

**Isopentane Purity.** The research grade isopentane was obtained from the Phillips Petroleum Co. The purity of this isopentane, based on a determination of the melting point, was stated to be 100%. Dissolved air was removed from the hydrocarbon by two condensations under vacuum conditions at dry ice temperatures. The high purity of the isopentane was confirmed by a traverse of the two-phase region at 175°C. The vapor pressure from 90% vapor to 10% vapor (by volume) did not vary by more than 0.01 atm.

### RESULTS

**Vapor Pressures.** Vapor pressures of isopentane were measured from 50° to 175°C. at 25°C. intervals, at least two measurements at each temperature. Separate charges of isopentane were used for each measurement. The observed vapor pressures were correlated and smoothed graphically by a residual technique and compared (Table I) with those values reported by Isaac, Li, and Canjar (6) and with values similarly smoothed from Young's data (20). The total maximum uncertainty in these vapor pressures including that portion corresponding to the temperature uncertainty, is estimated not to exceed 0.25%.

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Table I. Comparison of Vapor Pressure Data

Temp., ° C.	Vapor Pressure, Atm.		
	Isaac, others (6)	Young (20)	This Work
50	...	2.022	2.025
75	...	3.954	3.983
100	...	7.031	7.106
125	11.881	11.621	11.787
150	18.474	18.171	18.449
175	27.590	27.171	27.556

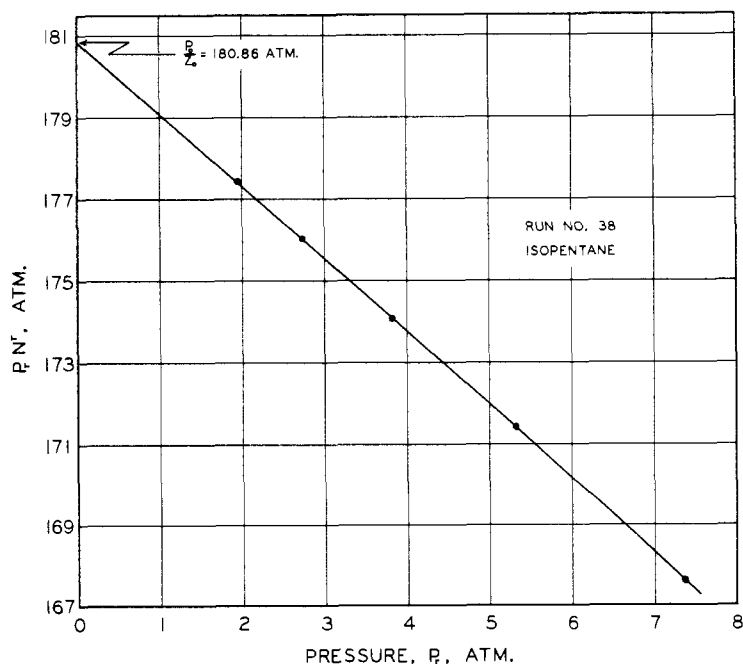


Figure 1. Graphical method to obtain  $p_0/z_0$

Table II. Isopentane Experimental Compressibility Data

Temp., °C.	Run No.	r	$\beta_r$ , Atm.	$z_r$	$\alpha_r$ , L./G. Mole	Temp., °C.	Run No.	r	$\beta_r$ , Atm.	$z_r$	$\alpha_r$ , L./G. Mole
50	19	0	1.4710	0.9462	0.9698	150	32	0	16.6955	0.7014	0.6210
		1	1.0557	0.9610	0.9796			1	13.1777	0.7834	0.5707
50	20	0	1.9920	0.9275	1.0002	150	33	0	15.6042	0.7287	0.6037
		1	1.3886	0.9482	0.9892			1	12.1613	0.8036	0.5607
		2	0.9966	0.9630	0.9845			2	9.1842	0.8588	0.5345
50	21	0	1.4569	0.9456	0.9901	175	34	0	27.2275	0.5160	0.6537
		1	1.0465	0.9612	0.9831			1	23.6530	0.6344	0.5684
75	22	0	3.9026	0.8842	0.8477	150	33	0	15.6042	0.7287	0.6037
		1	2.8681	0.9195	0.8018			1	12.1613	0.8036	0.5607
		2	2.0799	0.9436	0.7747			2	9.1842	0.8588	0.5345
		3	1.4956	0.9601	0.7622			3	6.7941	0.8990	0.5162
75	23	0	3.5131	0.8979	0.8302	175	34	0	27.2275	0.5160	0.6537
		1	2.5638	0.9272	0.8112			1	23.6530	0.6344	0.5684
		2	1.8527	0.9482	0.7988			2	19.2270	0.7297	0.5170
		3	1.3296	0.9629	0.7971			3	14.9542	0.8031	0.4842
75	24	0	3.1905	0.9090	0.8148	150	33	0	15.6042	0.7287	0.6037
		1	2.3200	0.9353	0.7967			1	12.1613	0.8036	0.5607
		2	1.6720	0.9539	0.7877			2	9.1842	0.8588	0.5345
		3	1.1979	0.9671	0.7846			3	6.7941	0.8990	0.5162
		4	0.9761	0.9789	0.6619			4	4.9541	0.9276	0.5074
		5	0.9761	0.9789	0.6619			5	3.5775	0.9479	0.5057
100	25	0	6.7037	0.8373	0.7431	175	34	0	27.2275	0.5160	0.6537
		1	5.0032	0.8843	0.7081			1	23.6530	0.6344	0.5684
		2	3.6705	0.9180	0.6840			2	19.2270	0.7297	0.5170
		3	2.6609	0.9418	0.6697			3	14.9542	0.8031	0.4842
		4	1.9142	0.9587	0.6606			4	11.2883	0.8579	0.4629
		5	1.3693	0.9704	0.6619			5	8.3498	0.8979	0.4497
100	26	0	5.8619	0.8614	0.7240	175	35	0	25.9482	0.5675	0.6129
		1	4.3363	0.9017	0.6941			1	21.8641	0.6767	0.5438
		2	3.1610	0.9301	0.6771			2	17.4135	0.7626	0.5013
		3	2.2816	0.9500	0.6710			3	13.3594	0.8279	0.4737
		4	1.6372	0.9647	0.6602			4	9.9905	0.8761	0.4561
100	27	0	6.9790	0.8292	0.7493	150	33	0	15.6042	0.7287	0.6037
		1	5.2320	0.8796	0.7046			1	12.1613	0.8036	0.5607
		2	3.8440	0.9145	0.6810			2	9.1842	0.8588	0.5345
		3	2.7904	0.9394	0.6650			3	6.7941	0.8990	0.5162
		4	2.0095	0.9573	0.6507			4	4.9541	0.9276	0.5074
		5	1.4378	0.9690	0.6602			5	3.5775	0.9479	0.5057
125	28	0	11.5851	0.7557	0.6889	175	36	0	27.4202	0.5059	0.6626
		1	8.9393	0.8251	0.6377			1	23.9751	0.6260	0.5736
		2	6.6990	0.8750	0.6096			2	19.5718	0.7231	0.5203
		3	4.9273	0.9107	0.5921			3	15.2642	0.7980	0.4866
		4	3.5786	0.9360	0.5843			4	11.5441	0.8541	0.4648
		5	2.5782	0.9542	0.5804			5	8.5514	0.8952	0.4507
		6	1.8470	0.9673	0.5782			6	6.2426	0.9248	0.4430
125	29	0	10.7907	0.7791	0.6688	188.5	41	0	38.3129	0.2089	0.7822
		1	8.2412	0.8420	0.6264			1	33.9477	0.2619	0.8236
		2	6.1383	0.8875	0.5988			2	33.6009	0.3669	0.7138
		3	4.4948	0.9196	0.5844			3	31.7303	0.4903	0.6085
		4	3.2556	0.9426	0.5760			4	27.7948	0.6077	0.5347
		5	2.3414	0.9593	0.5679			5	22.8396	0.7066	0.4866
		6	1.6752	0.9712	0.5617			6	17.9163	0.7844	0.4558
125	30	0	10.0148	0.7992	0.6550	150	31	0	18.0699	0.6618	0.6499
		1	7.5812	0.8561	0.6201			1	14.5502	0.7541	0.5868
		2	5.6167	0.8975	0.5962			2	11.2212	0.8229	0.5480
		3	4.0980	0.9266	0.5852			3	8.4143	0.8732	0.5233
		4	2.9616	0.9476	0.5780			4	6.1944	0.9096	0.5067
		5	2.1259	0.9626	0.5748			5	4.5045	0.9360	0.4933
		6	1.5186	0.9730	0.5809			6	3.2442	0.9540	0.4923
150	31	0	18.0699	0.6618	0.6499	188.5	42	0	36.2542	0.2073	0.8283
		1	14.5502	0.7541	0.5868			1	33.9211	0.2744	0.8103
		2	11.2212	0.8229	0.5480			2	33.4860	0.3834	0.6973
		3	8.4143	0.8732	0.5233			3	31.3051	0.5072	0.5963
		4	6.1944	0.9096	0.5067			4	27.1514	0.6224	0.5268
		5	4.5045	0.9360	0.4933			5	22.1453	0.7184	0.4817
		6	3.2442	0.9540	0.4923			6	17.2880	0.7936	0.4523
		7	2.3237	0.9669	0.4946			7	13.0913	0.8504	0.4329
188.5	43	0	34.5354	0.2156	0.8604	188.5	43	0	34.5354	0.2156	0.8604
		1	33.8613	0.2991	0.7841			1	33.8613	0.2991	0.7841
		2	33.1429	0.4142	0.6696			2	33.1429	0.4142	0.6696
		3	30.4021	0.5377	0.5760			3	30.4021	0.5377	0.5760
		4	25.9214	0.6487	0.5137			4	25.9214	0.6487	0.5137
5	20.8839	0.7396 <sup>b</sup>	.....	5	20.8839	0.7396 <sup>b</sup>	.....				

<sup>a</sup>From smoothed curve through data of Runs 41.

<sup>b</sup>From smoothed curve through data of Runs 41 and 42.

<sup>c</sup>From smoothed curve through data of Runs 41, 42, and 43.

<sup>d</sup>Read from smoothed curve through data of Runs 37 and 38.

Table II. (Continued)

Temp., °C.	Run No.	r	$p_r$ , Atm.	$z_r$	$\alpha_r$ , L./G. Mole	Temp., °C.	Run No.	r	$p_r$ , Atm.	$z_r$	$\alpha_r$ , L./G. Mole		
188.5	44	0	34.0915	0.2313	0.8542	200	39	4	28.9831	0.6426	0.4788		
		1	33.8175	0.3247	0.7565			5	23.3774	0.7334	0.4428		
		2	32.6845	0.4440	0.6444			6	18.1191	0.8044	0.4191		
		3	29.4211	0.5656 <sup>c</sup>	.....			7	13.6635	0.8584	0.4024		
200	37	0	60.5676	0.2982	0.4499			8	10.1039	0.8982	0.3912		
		1	41.0822	0.2863	0.6744			9	7.3681	0.9269	0.3852		
		2	38.5548	0.3802	0.6241			10	5.3244	0.9478	0.3806		
		3	35.4938	0.4952	0.5522			11	3.8206	0.9624	0.3821		
		4	30.8015	0.6082	0.4939			12	2.7304	0.9732	0.3811		
		5	25.2360	0.7051	0.4537			13	1.9449	0.9810	0.3793		
		6	19.7978	0.7827	0.4261			200	40	0	52.5919	0.2744	0.5356
		7	15.0493	0.8420	0.4076			1	40.5076	0.2991	0.6717		
		8	11.1952	0.8863	0.3943			2	38.1470	0.3985	0.6122		
		9	8.1971	0.9183	0.3870	3	34.8027	0.5145	0.5416				
		10	5.9394	0.9416	0.3817	4	29.9010	0.6255	0.4862				
		11	4.2724	0.9584	0.3780	5	24.3044	0.7195 <sup>d</sup>	.....				
		12	3.0572	0.9705	0.3746	200	40	0	44.2136	0.2634	0.6468		
		13	2.1788	0.9787	0.3795	1	39.5416	0.3333	0.6546				
14	1.5495	0.9850	0.3758	2	37.0562	0.4420	0.5846						
200	38	0	47.7420	0.2640	0.5985	3	33.0871	0.5585	0.5181				
		1	40.0533	0.3134	0.6655	4	27.7843	0.6636	0.4701				
		2	37.7035	0.4174	0.5999	5	22.1913	0.7500	0.4374				
		3	34.0849	0.5340	0.5308	6	17.0863	0.8172 <sup>d</sup>	.....				

**Compressibility.** The compressibility factor  $z$  is defined by the equation,  $z = pV/RT$  (Equation 1, 17). Compressibility factor isotherms of isopentane were determined from 50° to 200° C. at 25° C. intervals. Also, a critical region isotherm was determined at 188.5° C., slightly above the accepted value for the critical temperature,  $t_c = 187.8°$  C. (7, 12, 20). The experimental data are presented in Table II.

The data of the complete runs were treated graphically (17). A large-scale plot of the values of  $p_r N^r$  was used to determine the value of  $p_0/z_0$  for each run. On these plots, of which Figure 1 is typical, readings of the ordinates as precise as 0.01% were easily made, and abscissa scales commensurate with this precision on the ordinate were used. The compressibility factor  $z_r$  was then calculated as follows:

$$z_r = \frac{p_r N^r}{p_0/z_0} \quad (2)$$

The data of the incomplete runs at 188.5° and 200° C. were treated with Equation 9 of the preceding article (17). The values of  $z_k$  for the incomplete runs were read from large-scale plots with a precision of 0.0001.

The experimental compressibility factor isotherms are shown in Figure 2. At the lower pressures, these isotherms are consistent with respect to temperature to within 0.03%. Smoothed molal volumes and compressibility factors for each experimental temperature are presented in Table III. The molal volumes  $V$  were calculated from the graphically smoothed values of  $z$  (Equation 1, 17). The values for the saturated vapor in Table III were obtained by extrapolating the smoothed compressibility factor isotherms to the vapor pressures from this work shown in Table I.

The values in Table III for the unsaturated vapor are considered to have the following maximum errors: pressure, 0.04%; absolute temperature, 0.02%; compressibility factor

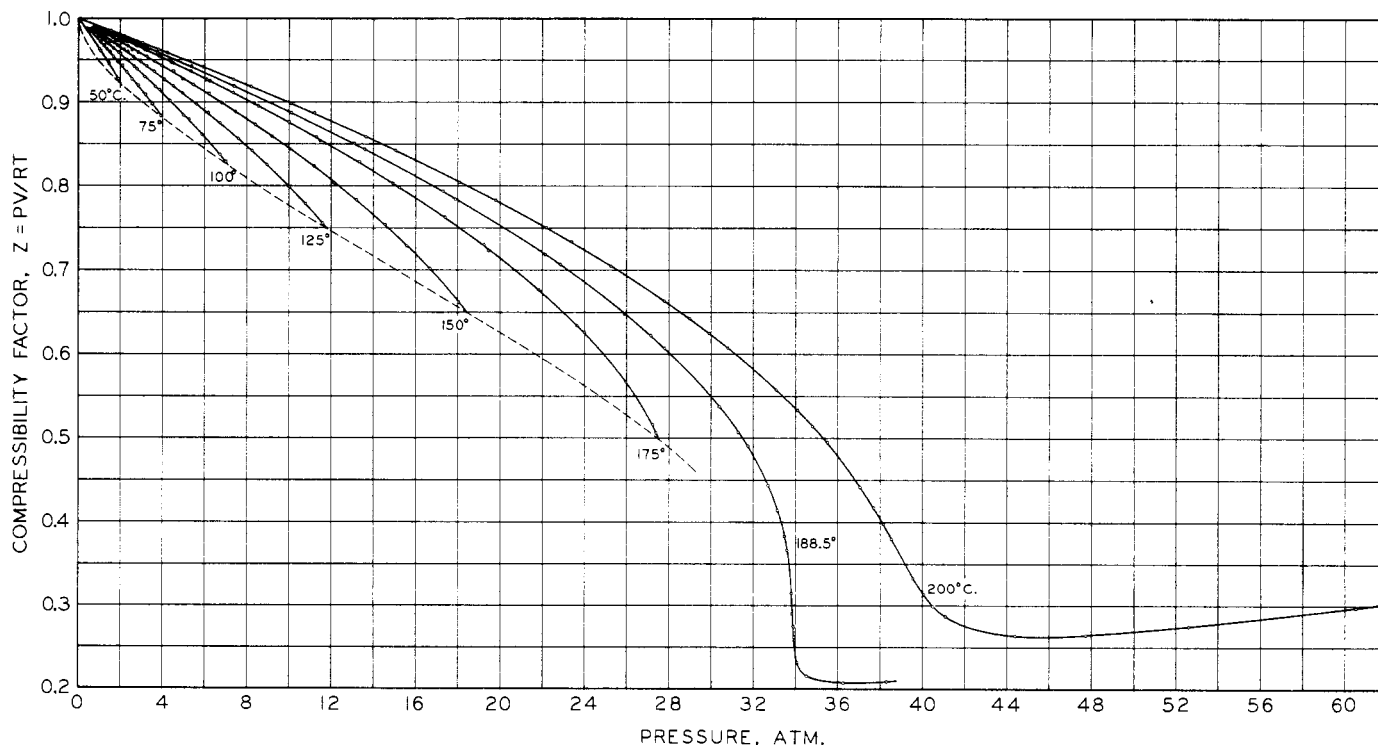


Figure 2. Experimental compressibility factor isotherms of isopentane

Table III. Isopentane Smoothed Compressibility Isotherms

Temp., °C.	Pressure, Atm.	Volume, L./G. Mole	$z = \frac{pV}{RT}$	
50	1	25.533	0.9629	
	2	12.233	0.9227	
	2.025 <sup>a</sup>	12.067 <sup>b</sup>	0.9216 <sup>b</sup>	
75	1	27.794	0.9729	
	2	13.496	0.9448	
	3	8.713	0.9150	
	3.983 <sup>a</sup>	6.324 <sup>b</sup>	0.8816 <sup>b</sup>	
100	1	29.955	0.9783	
	3	9.532	0.9339	
	5	5.418	0.8847	
	7	3.624	0.8285	
	7.106 <sup>a</sup>	3.556 <sup>b</sup>	0.8252 <sup>b</sup>	
125	1	32.099	0.9825	
	4	7.584	0.9286	
	7	4.054	0.8687	
	10	2.613	0.7997	
	11	2.296	0.7730	
	11.787 <sup>a</sup>	2.077 <sup>b</sup>	0.7494 <sup>b</sup>	
150	1	34.226	0.9857	
	5	6.440	0.9273	
	10	2.933	0.8448	
	15	1.721	0.7436	
	18	1.281	0.6641	
	18.449 <sup>a</sup>	1.222 <sup>b</sup>	0.6495 <sup>b</sup>	
175	1	36.340	0.9882	
	5	6.916	0.9403	
	10	3.220	0.8757	
	15	1.966	0.8020	
	20	1.315	0.7150	
	25	0.8789	0.5975	
	27	0.7168	0.5263	
	27.556 <sup>a</sup>	0.6646 <sup>b</sup>	0.4980 <sup>b</sup>	
	188.5	1	37.472	0.9892
		5	7.166	0.9458
		10	3.366	0.8886
		15	2.083	0.8250
		20	1.427	0.7536
25		1.011	0.6673	
30		0.6945	0.5500	
32		0.5668	0.4788	
33		0.4868	0.4241	
33.5		0.4325	0.3825	
33.6		0.4208	0.3732	
33.7		0.3934	0.3500	
33.8		0.3665	0.3270	
33.9		0.3157	0.2825	
34.0		0.2713	0.2435	
34.1		0.2566	0.2310	
34.2		0.2489	0.2247	
34.3		0.2439	0.2208	
34.4		0.2401	0.2180	
34.5		0.2374	0.2162	
35	0.2291	0.2117		
36	0.2187	0.2078		
37	0.2119	0.2070		
38	0.2075	0.2082		
200	1	38.444	0.9902	
	5	7.384	0.9509	
	10	3.492	0.8993	
	15	2.181	0.8426	
	20	1.514	0.7799	
	25	1.101	0.7090	
	30	0.8072	0.6237	
	35	0.5647	0.5091	
	38	0.4133	0.4045	
	39	0.3581	0.3597	
	40	0.3061	0.3154	
	41	0.2726	0.2879	
	42	0.2532	0.2739	
45	0.2266	0.2626		
50	0.2084	0.2684		
55	0.1984	0.2810		
60	0.1917	0.2963		

<sup>a</sup>Saturation pressure.

<sup>b</sup>Saturated vapor.

and molal volume, 0.20% each. The uncertainty in the latter two is somewhat larger because of the uncertainty in the vapor pressures.

**Other Investigations.** The physical properties of isopentane have been investigated for over 90 years. Its normal boiling point was measured as early as 1864 (19), and its critical constants were first reported in 1883 (11). Comprehensive studies of the volumetric behavior of isopentane have been reported by Young (19, 20), Young and Thomas (21), Bridgman (4), and Isaac, Li, and Canjar (6). A study of the 200°C. isotherm by Kobe and Vohra appears in the following article (8). The work by Bridgman, at 0°, 50°, and 95° C. and pressures of 500 to 9000 kg. per sq. cm., was exclusively a study of the liquid phase, so no comparison with the present work is possible.

Young investigated isopentane at temperatures from -30° to 280° C. and at pressures from near atmospheric to 72.5 atm. (19). Critical constants were determined as well as vapor pressures from -30° C. to the critical temperature and orthobaric volumes from 10° C. to the critical temperature. Measurements on the gas phase were reported from 30° to 280° C. at intervals of 10° C. except in the critical region where the isotherms were spaced much more closely.

Young's data were smoothed as residual volumes and are compared in Table IV as molal volumes at selected pressures

Table IV. Comparison with Molal Volumes of Young

Temp., °C.	Pressure, Atm.	Molal Volume, Liters/G. Mole		Dev., %
		Young (19)	This Work	
50	1	25.532	25.533	0.00
	2	12.224	12.233	-0.07
75	1	27.716	27.794	-0.28
	2	13.430	13.496	-0.49
	3	8.660	8.713	-0.61
100	1	29.885	29.955	-0.23
	3	9.480	9.532	-0.54
	5	5.382	5.418	-0.66
	7	3.590	3.624	-0.94
125	1	32.030	32.099	-0.21
	4	7.540	7.584	-0.58
	7	4.019	4.054	-0.86
	10	2.577	2.613	-1.38
	11	2.262	2.296	-1.48
150	1	34.158	34.226	-0.20
	5	6.395	6.440	-0.70
	10	2.896	2.933	-1.26
	15	1.692	1.721	-1.68
	18	1.254	1.281	-2.11
175	1	36.258	36.340	-0.23
	5	6.864	6.916	-0.75
	10	3.185	3.220	-1.09
	15	1.938	1.966	-1.42
	20	1.292	1.315	-1.75
	25	0.8564	0.8789	-2.56
	27	0.6880	0.7168	-4.02
200	1	38.354	38.444	-0.23
	5	7.324	7.384	-0.81
	10	3.444	3.492	-1.37
	20	1.488	1.514	-1.72
	30	0.7847	0.8072	-2.79
	35	0.5382	0.5647	-4.69
	40	0.2767	0.3061	-9.60
	45	0.2209	0.2266	-2.52
	50	0.2052	0.2084	-1.54
	60	0.1900	0.1917	-0.89

Table V. Comparison of Compressibility Factors at 1 Atm.

Temp., °C.	$z = pV/RT$		Deviation, %
	Young, Thomas (21)	This Work	
50	0.9628	0.9629	- 0.01
100	0.9756	0.9783	- 0.28
150	0.9870	0.9857	+ 0.13

with the results of the present work. The deviation between the two sets of volumes is consistent in its direction and increases very rapidly with pressure both at 175° and 200° C. This behavior suggests a systematic deviation in the pressure scales of the two investigations, a possibility which is also supported by the deviation in vapor pressures shown in Table I. In addition, Young's vapor pressures of normal pentane (20) are consistently lower than the values reported by Beattie, Levine, and Douslin (2), Li and Canjar (10), and Sage and Lacey (13, 14, 15). In fact, it appears to be generally true that the vapor pressures determined by Young in his numerous studies are consistently lower than those reported in more modern investigations.

In contrast, the saturated vapor volumes reported by Young (19, 20) at 50°, 100°, and 150° C. are higher by 0.35%, 0.43%, and 1.22%, respectively, than the values found in the present work. As the saturated vapor state is a univariant one, Young's saturated vapor volumes would be independent of any error in pressure measurement. Consequently, the possibility is suggested that Young's volume measurements may also have contained considerable error.

The low-pressure investigation of Young and Thomas (27) extended from 10.75° to 150° C. and from 60 to 825 mm. of mercury. The data reported at 50°, 100°, 150° C. were graphi-

cally smoothed as compressibility factor isotherms to compare them with the results of the present work (Table V).

Isaac, Li, and Canjar studied the compressibility of isopentane from 100° to 300° C. and from 100 to 200 atm. (6). The only gas-phase measurements made below the critical temperature were made in the vicinity of saturation. The comparison between the data at 175° and 200° C. and those of the present work is shown in Table VI. A detailed comparison made of the data of Isaac, Li, and Canjar (6) and of Young (19) revealed that above 100° C. the molal volumes of Isaac, Li, and Canjar are lower than those reported by Young except from about 36 to 43 atm. at 200° C. Young's molal volumes are, in turn, consistently lower than those of the present work.

Using a sample of the same isopentane as in the present work, Kobe and Vohra (8) determined the 200° C. compressibility factor isotherm in a conventional variable-volume type apparatus. Pressures ranged up to approximately 65 atm. At no pressure did the discrepancy between the compressibility factors so obtained and those of the present work exceed 0.20% and at most pressures agreement was to within 0.10%.

**Second Virial Coefficients.** Three types of expansions are commonly employed for the representation of volumetric behavior of a gas.

$$z = 1 + Bp + Cp^2 + \dots \quad (4)$$

$$z = 1 + \frac{B'}{V} + \frac{C'}{V^2} + \dots \quad (5)$$

$$pV = RT + B''p + C''p^2 + \dots \quad (6)$$

Table VI. Comparison with Molal Volumes of Isaac and Others

Temp., °C.	Pressure, atm.	Volume, Liters/G. Mole		Deviation, %
		Isaac, others (6)	This Work	
175	26.600	0.7091	0.7511	-5.59
	26.807	0.6935	0.7335	-5.45
	26.988	0.6779	0.7181	-5.60
	27.201	0.6622	0.6991	-5.28
	27.382	0.6466	0.6824	-5.25
	27.500	0.6310	0.6672	-5.22
200	31.004	0.7096	0.7566	-6.21
	33.070	0.6156	0.6566	-6.24
	34.894	0.5372	0.5700	-5.75
	36.643	0.4587	0.4847	-5.36
	38.255	0.3797	0.3995	-4.96
	39.757	0.3016	0.3170	-4.86
	40.919	0.2623	0.2748	-4.55
	44.096	0.2231	0.2324	-4.00

Table VII. Second Virial Coefficients of Isopentane

Temp., °C.	-B, Liters/G. Mole	
	Experimental	Smoothed
0	...	1.367
25	...	1.150
50	0.960	0.946
75	0.763	0.772
100	0.645	0.648
125	0.570	0.567
150	0.494	0.496
175	0.434	0.435
188.5	0.407	0.403
200	0.376	0.377

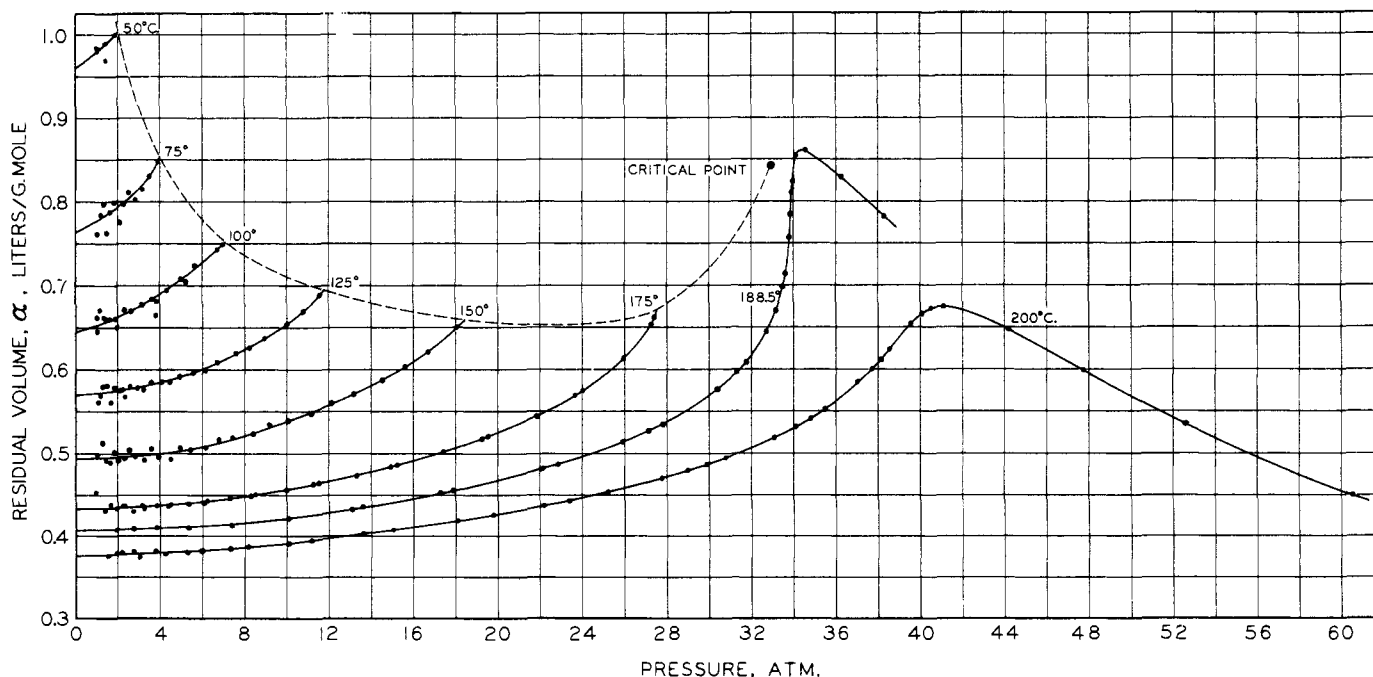


Figure 3. Reduced volume isotherms of isopentane

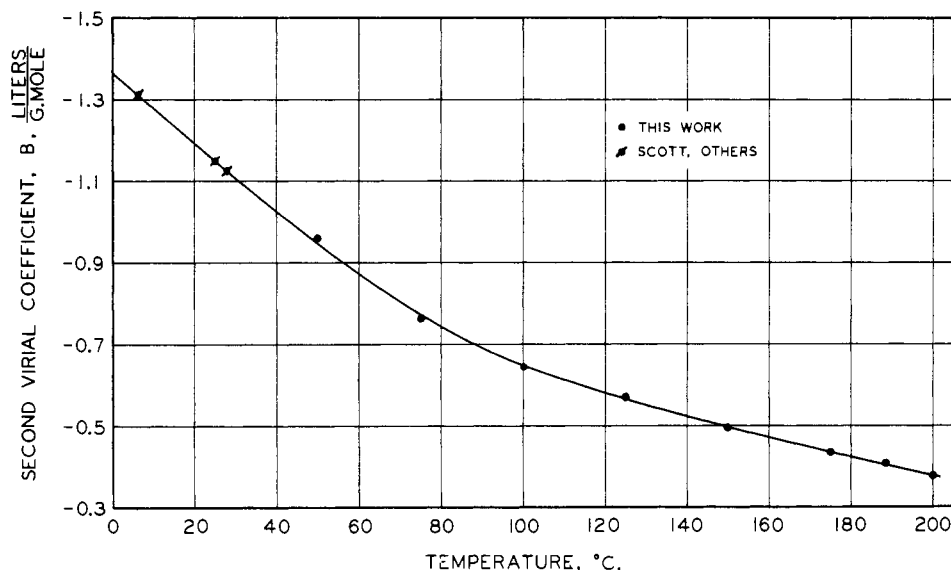


Figure 4. Experimental second virial coefficients of isopentane

For the case in which all three series are infinite,

$$B' = B'' = BRT \quad (7)$$

Because the second virial coefficient is a property of the gas and not of the particular equation selected to describe the behavior of that gas, symbol  $B$  is assigned to the second virial coefficient. In such a case, the units of the coefficient indicate with which equation it may be employed.

The residual volume  $\alpha$  is defined by the following relation:

$$\alpha = \frac{RT}{p} - V = \frac{RT}{p}(1 - z) \quad (8)$$

Residual volumes of isopentane were calculated from each experimental compressibility measurement (Figure 3). Equations 4, 5, and 6 show that

$$\text{Limit}_{p \rightarrow 0} \alpha = -BRT = -B' = -B'' \quad (9)$$

The second virial coefficients of isopentane were therefore determined from the zero-pressure intercepts of the isotherms of Figure 3.

The experimental second virial coefficients are presented in Table VII and are correlated graphically in Figure 4 with the values reported by Scott and others (16). Also included in Table VII are the smoothed values read from the curve of Figure 4. It is believed that the errors in these smoothed values do not exceed 0.030 liters per gram mole at 50°C. decreasing to 0.015 liters per gram mole at 200°C.

The experimental second virial coefficients of isopentane were also correlated on a reduced basis with the coefficients of normal pentane and neopentane reported by Beattie and coworkers (1, 3). The critical constants employed were those selected by Rossini and others (12). The correlation is shown in Figure 5.

According to the Berthelot equation of state, the second virial

coefficient may be expressed as

$$B = \frac{9}{128} \frac{RT_c}{p_c} \left( 1 - \frac{6}{T_R^2} \right) \quad (10)$$

Lambert and others (9) compared experimental second virial coefficients of many organic vapors, including hydrocarbons, with values calculated from Equation 10 and found that, for the nonpolar compounds, the equation represented the data within their experimental accuracy. For the purposes of correlation as  $B/V_c$ , Equation 10 may be written as

$$\frac{B}{V_c} = \frac{9}{128} \frac{1}{z_c} \left( 1 - \frac{6}{T_R^2} \right) \quad (11)$$

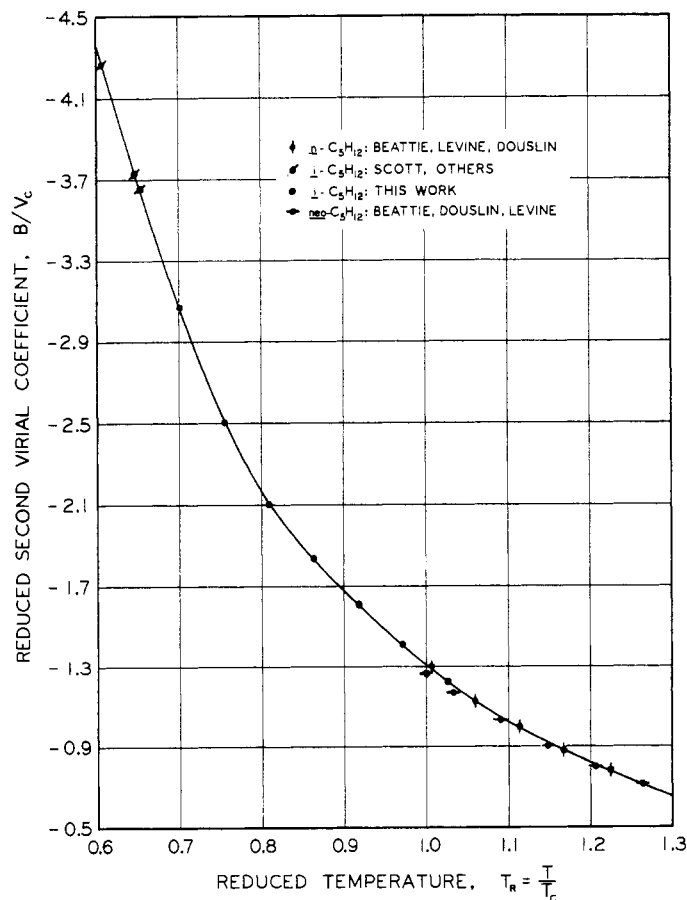


Figure 5. Experimental second virial coefficients vs. reduced temperature

Table VIII. Comparison of Experimental and Calculated Reduced Second Virial Coefficients

$T_R$	$-B/V_c$	
	Smoothed Experimental	Berthelot Equation
0.6	4.37	4.10
0.7	3.08	2.94
0.8	2.16	2.19
0.9	1.68	1.68
1.0	1.31	1.30
1.1	1.02	1.04
1.2	0.82	0.83
1.3	0.65	0.66

Using a value of  $z_c$  of 0.269 (12), reduced second virial coefficients were calculated from Equation 11 and compared with values read from the curve of Figure 5. The comparison is made in Table VIII. Above  $T_R = 0.7$ , the agreement is within the experimental accuracy of the virial coefficients.

#### NOMENCLATURE

$B$  = Second virial coefficient  
 $N$  = Apparatus constant  
 $p$  = Absolute pressure  
 $R$  = Gas constant, 0.0820544 (liter) (atm.) / (g. mole) ( $^{\circ}\text{K}.$ )  
 $T$  = Absolute temperature ( $T_{0^{\circ}\text{C.}} = 273.16^{\circ}\text{K}.$ )  
 $T_R$  = Reduced temperature,  $T/T_c$   
 $V$  = Molal volume  
 $z$  = Compressibility factor,  $pV/RT$   
 $\alpha$  = Residual volume,  $\frac{RT}{p} - V$

#### Subscripts:

$r, k$  = Number of the expansion  
 $c$  = Critical state  
 $0$  = Initial state of a run

#### LITERATURE CITED

- (1) Beattie, J. A., Douslin, D. R., Levine, S. W., *J. Chem. Phys.* **20**, 1619-20 (1952).
- (2) Beattie, J. A., Levine, S. W., Douslin, D. R., *J. Am. Chem. Soc.* **73**, 4431-2 (1951).
- (3) *Ibid.*, **74**, 4778-9 (1952).

- (4) Bridgman, P. W., *Proc. Am. Acad. Arts Sci.* **66**, 185-233 (1930-1).
- (5) Burnett, E. S., *J. Appl. Mechanics* **58**, A136-40 (1936).
- (6) Isaac, R., Li, K., Canjar, L. N., *Ind. Eng. Chem.* **46**, 199-201 (1954).
- (7) Kobe, K. A., Lynn, R. E., Jr., *Chem. Revs.* **52**, 117-236 (1953).
- (8) Kobe, K. A., Vohra, S. P., *J. CHEM. ENG. DATA* **4**, 329 (1959).
- (9) Lambert, J. D., others, *Proc. Roy. Soc. (London)* **A196**, 113-25 (1949).
- (10) Li, K., Canjar, L. N., *Chem. Eng. Progr. Symposium Ser.* **49**, No. 7, 147-9 (1953).
- (11) Pawlewski, B., *Ber.* **16**, 2633-6 (1883).
- (12) Rossini, F. D., others, "Selected Values of Physical and Thermodynamic Properties of Hydrocarbons and Related Compounds," p. 327, Carnegie Press, Pittsburgh, 1953.
- (13) Sage, B. H., Lacey, W. N., *Ind. Eng. Chem.* **34**, 730-7 (1942).
- (14) Sage, B. H., Lacey, W. N., "Thermodynamic Properties of Hydrocarbons," pp. 70-82, Am. Petroleum Inst., New York, 1950.
- (15) Sage, B. H., California Institute of Technology, personal communication Dec. 21, 1956.
- (16) Scott, D. W., others, *J. Am. Chem. Soc.* **73**, 1707-12 (1951).
- (17) Silberberg, I. H., Kobe, K. A., McKetta, J. J., *J. CHEM. ENG. DATA* **4**, 314 (1959).
- (18) Warren, C. M., *Mem. Am. Acad. Arts Sci.* **9**, 156-176 (1867-73).
- (19) Young, S., *Proc. Phys. Soc. (London)* **13**, 602-57 (1894).
- (20) Young, S., *Sci. Proc. Roy. Dublin Soc.* **12**, 374-443 (1909-10).
- (21) Young, S., Thomas, G. L., *Proc. Phys. Soc. (London)* **13**, 658-65 (1895).

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## Volumetric Behavior and Critical Constants of Isopentane

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Serious disagreement in the volumetric properties of isopentane arose between the results of Isaac, Li, and Canjar (4) and those of Silberberg, McKetta, and Kobe (7). Deviations in the regions covered by both investigators ranged from 4.0 to 6.2%. Values obtained by both groups differ from the work of Young (8) in 1894. The work of Isaac, Li, and Canjar was done in a variable-volume apparatus while that of Silberberg, McKetta, and Kobe (7) done in a Burnett apparatus. It was considered desirable to repeat the work in a variable volume apparatus. Because the critical constants have not been checked since the work of Young (9) in 1910, they were determined also.

#### EXPERIMENTAL

**Isopentane.** The sample was taken from the cylinder used by Silberberg. Because the isopentane left in the Burnett apparatus at the conclusion of that work was transferred back to the cylinder, it is probable that some air leaked in during the process. The isopentane was frozen with liquid nitrogen and the permanent gases were evacuated. The sample was melted and the first 10% was evacuated; the sample was distilled into a second receiver, leaving the last 10% in the original flask. This operation was repeated several times. However, the behavior of the sample indicated that the isopentane was not as pure as desired. The vapor pressure of the liquid increased with decreasing vapor volume, and the isotherms in the critical region showed a slope instead of being flat. At 173°C. the vapor pressure increased by 0.093 atm. when the vapor volume was reduced from 90% to 10%. Silberberg (6) has observed about a 0.05-atm. increase under these same conditions.

**Method and Apparatus.** The apparatus used in this investigation is essentially that described by Beattie (2). Thermostat temperatures were controlled to 0.005°C. by a platinum re-

sistance thermometer in conjunction with a photoelectric cell relay and a Mueller bridge. The actual thermostat temperatures were measured by the same platinum resistance thermometer. A known amount (2.8139 grams) of isopentane was charged to the  $P$ - $V$ - $T$  bomb using a weighing bomb and charging union techniques described elsewhere (3).

In the determination of the critical constants, the usual pro-

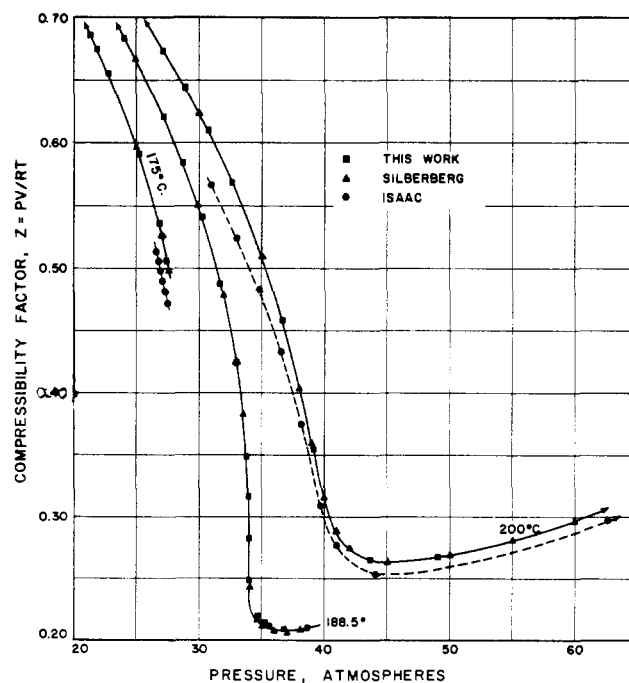


Figure 1. Compressibility of isopentane

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