Using a value of $z_{c}$ of 0.269 (12), reduced second virial coefficients were calculated from Equation 11 and compared with values read from the curve of Figure 5. The comparison is made in Table VIII. Above $T_{R}=0.7$, the agreement is within the experimental accuracy of the virial coefficients.

## NOMENCLATURE

$B=$ Second virial coefficient
$\mathcal{N}=$ Apparatus constant
$p=$ Absolute pressure
$R=$ Gas constant, 0.0820544 (liter) (atm.) / (g. mole) ( ${ }^{\circ} \mathrm{K}$.)
$\tau=$ Absolute temperature ( $T_{0}{ }^{\circ} \mathrm{C} .=273.16^{\circ} \mathrm{K}$.)
$T_{p}=$ Reduced temperature, $T / T_{r}$
$V=$ Molal volume
$z=$ Compressibility factor, $p V / R T$
$\alpha=$ Residual volume, $\frac{R T}{p}-V$
Subscripts:
$r, k=$ Number of the expansion
$c=$ Critical state
$0=$ Initial state of a run

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# Volumetric Behavior and Critical Constants of Isopentane 

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Serious disagreement in the volumetric properties of isopentane arose between the results of Isaac, Li , and Canjar (4) and those of Silberberg, McKetta, and Kobe (7). Deviations in the regions covered by both investigators ranged from 4.0 to $6.2 \%$. Values obtained by both groups differ from the work of Young ( 8 ) in 1894. The work of Isaac, Li, and Canjar was done in a variable-volume apparatus while that of Silberberg, McKetta, and Kobe (7) done in a Burnett apparatus. It was considered desirable to repeat the work in a variable volume apparatus. Because the critical constants have not been checked since the work of Young (9) in 1910, they were determined also.

## EXPERIMENTAL

Isopentane. The sample was taken from the cylinder used by Silberberg. Because the isopentane left in the Burnett apparatus at the conclusion of that work was transferred back to the cylinder, it is probable that some air leaked in during the process. The isopentane was frozen with liquid nitrogen and the permanent gases were evacuated. The sample was melted and the first $10 \%$ was evacuated; the sample was distilled into a second receiver, leaving the last $10 \%$ in the original flask. This operation was repeated several times. However, the behavior of the sample indicated that the isopentane was not as pure as desired. The vapor pressure of the liquid increased with decreasing vapor volume, and the isotherms in the critical region showed a slope instead of being flat. At $173^{\circ} \mathrm{C}$. the vapor pressure increased by 0.093 atm . when the vapor volume was reduced from $90 \%$ to $10 \%$. Silberberg ( 6 ) has observed about a $0.05-\mathrm{atm}$. increase under these same conditions.
Method and Apparatus. The apparatus used in this investigation is essentially that described by Beattie (2). Thermostat temperatures were controlled to $0.005^{\circ} \mathrm{C}$. by a platinum re-
sistance thermometer in conjunction with a photoelectric cell relay and a Mueller bridge. The actual thermostat temperatures were measured by the same platinum resistance thermometer. A known amount ( 2.8139 grams) of isopentane was charged to the $P-V-T$ bomb using a weighing bomb and charging union techniques described elsewhere (3).

In the determination of the critical constants, the usual pro-


Figure 1. Compressibility of isopentane


Figure 2. Isotherms of isopentane in the critical region
cedures for the determination of compressibility isotherms were followed. Such isotherms were determined below and above the critical temperature. Because of the impurities in the sample, the behavior of the piston gage was watched very carefully,

Table 1. Compressibility of Isopentane
( $175^{\circ}, 188.5^{\circ}$, and $200^{\circ} \mathrm{C}$. Isotherms)

| Sp. Vol., Pressure, Ml./G. Atm. | Sp. Vol., Mi./G. | Pressure, Atm. | Sp. Vol. <br> Ml./G. | Pressure, Atm. |
| :---: | :---: | :---: | :---: | :---: |
| $175^{\circ} \mathrm{C}$. | $188.5^{\circ} \mathrm{C}$. |  | $200^{\circ} \mathrm{C}$. |  |
| $17.042 \quad 20.850$ | 15.714 | 23.303 | 13.345 | 27.168 |
| $16.386 \quad 21.377$ | 14.921 | 24.069 | 12.019 | 28.860 |
| $15.726 \quad 21.896$ | 14.918 | 24.077 | 10.694 | 30.696 |
| $14.671 \quad 22.783$ | 12.015 | 27.176 | 9.3708 | 32.663 |
| $12.036 \quad 25.143$ | 10.695 | 28.731 | 6.7256 | 36.716 |
| $10.188 \quad 26.816$ | 9.3753 | 30.328 | 4.8744 | 39.186 |
| $9.9238 \quad 27.039$ | 8.0563 | 31.833 | 3.6866 | 41.407 |
| $9.3991 \quad 27.451$ | 6.7369 | 33.076 | 3.2724 | 43.707 |
| 8.8693 27.583 ${ }^{\text {a }}$ | 5.4177 | 33.804 | 2.9253 | 49.042 |
|  | 4.8901 | 33.932 | 2.7611 | 54.708 |
|  | 4.3627 | 34.009 | 2.6899 | 59.460 |
|  | 3.8353 | 34.100 | 2.5696 | 68.688 |
|  | 3.3082 | 34.694 | 2.4883 | 75.753 |
| ${ }^{\text {Q }}$ Vapor pressure. | 3.1762 | 35.168 | 2.3368 | 101.584 |
| Data above 65 atm . | 3.1060 | 35.559 | 2.2373 | 129.180 |
| are not shown in | 2.9752 | 36.774 | 2.1703 | 154.774 |
| Figure 1. | 2.8666 | 38.557 | 2.1182 | 181.981 |

Table II. Isotherms in the Critical Region of Isopentane

| Density, <br> G. Mi . |  | Temperature, ${ }^{\circ} \mathrm{C}$. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 187 | 187.5 | 187.7 | 187.75 | 187.8 | 187.85 |
|  |  | Pressure, Normal Atm. |  |  |  |  |  |
| 0.1680 | 5.953 | 33.029 | 33.216 | 33.289 |  |  |  |
| 0.1758 | 5.689 | 33.122 | 33.317 | 33.396 |  | 33.439 |  |
| 0.1799 | 5.558 | 33.158 |  |  |  |  |  |
| 0.1843 | 5.425 | 33.186 | 33.383 | 33.470 |  | 33.518 | 33.538 |
| 0.1937 | 5.162 | 33.218 | 33.426 | 33.526 |  | 33.574 | 33.602 |
| 0.1989 | 5.028 |  | 33.457 |  |  | 33.594 |  |
| 0.2042 | 4.898 | 33.237 | 33.471 | 33.566 | 33.542 | 33.612 | 33.639 |
| 0.2099 | 4.764 |  | 33.478 | 33.575 |  | 33.627 |  |
| 0.2158 | 4.634 | 33.245 |  | 33.588 | 33.614 | 33.636 | 33.669 |
| 0.2222 | 4.500 |  | 33.495 | 33.597 | 33.626 | 33.648 | 33.679 |
| 0.2288 | 4.370 | 33.249 |  | 33.607 | 33.633 | 33.658 | 33.688 |
| 0.2361 | 4.235 |  | 33.512 | 33.614 | 33.643 | 33.668 | 33.701 |
| 0.2435 | 4.106 | 33.257 |  | 33.618 | 33.649 | 33.680 | 33.715 |
| 0.2518 | 3.972 |  | 33.527 | 33.635 | 33.667 | 33.091 | 33.730 |
| 0.2603 | 3.842 | 33.273 | 33.540 | 33.653 | 33.685 | 33.712 |  |
| 0.2697 | 3.708 |  | 33.571 | 33.684 |  | 33.745 | 33.783 |
| 0.2794 | 3.579 | 33.307 | 33.623 |  |  |  |  |
| 0.2857 | 3.500 | 33.367 |  |  |  |  |  |
| 0.2904 | 3.444 |  | 33.737 |  |  |  |  |
| 0.2924 | 3.420 | 33.443 |  |  |  |  |  |
| 0.3016 | 3.315 | 33.624 |  |  |  |  |  |

Table III. Comparison of the Critical Constants of Isopentane

| Source | $t_{c},{ }^{\circ} \mathrm{C}$ | $p_{c}$, Atm. | $d_{c}, \mathrm{G} . / \mathrm{Ml}$ |  |
| :--- | :---: | :---: | :---: | :---: |
| This work | $187.8 \pm 0.05$ | $33.66 \pm 0.05$ | $0.236 \pm 0.005$ |  |
| Pawlewski (5) | 194.8 |  |  |  |
| Altschul (7) | 187.1 | 33.3 | 0.2343 |  |
| Young (9) | 187.8 | 32.9 | 0.0 |  |

particularly near the saturated vapor and liquid states. Entrance into the two phase region was marked by a slow fall of the piston caused by addition of a 1 -gram weight to the pan.

Experimental Data. Table I presents compressibility data for $175^{\circ}, 188.5^{\circ}$, and $200^{\circ} \mathrm{C}$. isotherms. These data are compared with those of others ( 4,7 ) in Figure 1.

The results of the measurements of the compressibility of isopentane in the critical region are given in Table II. These isotherms are plotted in Figure 2, and the critical constants derived from the plot are compared with the results of other workers in Table III. The agreement of the authors' values of critical temperature and critical volume with those of Young (9) is striking.

## DISCUSSION

Compressibility data obtained at $175^{\circ}, 188.5^{\circ}$, and $200^{\circ} \mathrm{C}$. agree with those of Silberberg and coworkers (7) within $0.2 \%$, which is claimed to be the experimental accuracy, except in high density region of $188.5^{\circ} \mathrm{C}$. where the effect of impurities is pronounced. Even in this region maximum deviation is less than $1.0 \%$.

Because of an additional source of error in the critical region, introduced by the impurities, it is hard to estimate the magnitude of uncertainties in the critical constants. Nevertheless, the values presented in Table III were chosen after a realistic evaluation of these uncertainties.

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