# **Tetraalkylsilanes: A New Class of Wide Liquid Range Fluids**

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 $T_{\rm HE}$  ADVENT of new, higher performance jet aircraft has created a pressing need for heat-stable lubricants and fluids. High speed and high load operation of aircraft components have imposed upon the lubricant the additional burden of dissipating considerable amounts of frictional heat.

This laboratory began a general investigation of the synthesis and properties of tetraalkylsilanes in 1954. Although the materials are principally hydrocarbon in nature, the relatively simple synthetic methods available for producing a wide variety of pure, related materials allow a systematic study of the effect of molecular structure on such important fluid properties as liquid range, viscosity, volatility, and lubricity.

Low molecular weight tetraalkylsilanes have been known for many years (6) and have since been prepared by a variety of procedures (4, 6-8, 11). Some of the synthetic procedures reported in the literature for various tetraalkylsilanes are summarized below.

 $2 \operatorname{ZnR}_2 + \operatorname{SiCl}_4 \left[ \operatorname{or} \operatorname{Si}(\operatorname{OC}_2 \operatorname{H}_5)_4 \right] \to \operatorname{R}_4 \operatorname{Si}$ (1)

 $4 RMgX + SiCl_4 \longrightarrow R_4Si \qquad (2)$ 

 $RSiCl_3 + 3R'MgX \rightarrow RSiR'_3$  (3)

 $4 \operatorname{RLi} + \operatorname{SiCl}_{4} [\operatorname{or} \operatorname{Si}(\operatorname{OC}_{2}H_{5})_{4}] \rightarrow \operatorname{R}_{4}\operatorname{Si}$ (4)

 $R'Li + R_3SiH \rightarrow R_3SiR'$  (5)

Synthesis procedures and physical properties of high molecular weight, high boiling tetraalkylsilane fluids have been investigated in this laboratory as part of a general synthesis program (14, 16).

The general procedures for the synthesis of small quantities of various types of tetraalkylsilanes in this laboratory are:

 $R_{3}SiX + R'Li \longrightarrow R_{3}SiR' + LiX$ (9)

 $BrMg(CH_2)_5MgBr + SiCl_4 \rightarrow (CH_2)_5SiCl_2 + 2MgBrCl$  (10)

### $(CH_2)_5SiCl_2 + 2RLi \rightarrow (CH_2)_5SiR_2 + 2LiCl$

The alkyllithium procedure was preferred over other reported synthesis procedures because the organolithium intermediate is more reactive than the corresponding Grignard reagent and is easier to handle than the organozinc intermediates. Being more reactive, the organolithium intermediate produced tetraalkylsilanes in excellent yields (73 to 89%) and in purer quality than by the Grignard method. Since the Grignard reagent is not as reactive as the organolithium reagent, it is useful in the synthesis of partially alkylated chlorosilane intermediates as shown in Equations 7, 8, and 10, where complete alkylation is undesirable.

The preparation of larger quantities (1 to 15 gallons) of high molecular weight, high boiling tetraalkylsilane fluids was later reported by Harris and others (10). They preferred

the Grignard procedure because of the relatively lower cost of Grignard reagents to organolithium reagents. The various types of tetraalkylsilanes were prepared by the following procedures:

$4RMgX + SiCl_4$	$\rightarrow R_4Si$	+	4MgXCl	(11)
$RMgX + SiCl_4$	$\rightarrow \ RSiCl_3$	+	MgXCl	(12)
$3R'MgX + RSiCl_3$	$\rightarrow \ RSiR'_3$	+	3MgXCl	
$2RMgX + SiCl_4$	$\rightarrow \ R_2SiCl_2$	+	2MgXCl	(13)
$2R'MgX + R_2SiCl_2$	$\rightarrow R_2 Si R_2'$	+	2MgXCl	

Generally the Grignard route produced silanes containing various impurities as Si-H, Si-OH, and Si-O-Si-containing compounds. These impurities are due to the less reactive Grignard reagent which does not completely react with all the chlorosilane starting material. The unreacted chlorosilane in the work-up of the product yields the Si-OH type impurities which later can be converted partially to Si-O-Si type impurities through condensation. The Si-H type impurity is believed to be formed through some reductive action of the Grignard reagent on chlorosilanes or through thermal cleavage of the Si-C bond during distillation to yield an olefin and an Si-H compound.

$$\mathbf{R}_{3}\mathbf{SiCH}_{2}\mathbf{CH}_{2}\mathbf{R} \rightarrow \mathbf{R}_{3}\mathbf{SiH} + \mathbf{CH}_{2} = \mathbf{CHR}$$
(14)

Excess Grignard reagent is converted to a hydrocarbon during work-up of the reaction.

Detection of the silicon containing impurities is readily accomplished by infrared spectroscopy. Si-H compounds show a strong sharp band at 2100 cm.  $^{-1}$  and Si-O compounds have a strong broad band at 1055 to 1024 cm.  $^{-1}(2)$ .

Purification of a reaction product containing the above contaminants is difficult. Fractional distillation will often concentrate the hydrocarbon in early fractions and siloxanes in tail fractions. Hydrocarbons may also be removed by fractional crystallization. Current work at this laboratory indicates that column chromatography may be used for purification.

#### PROPERTIES

Viscosity and Pour Point. The alkyl groups in the three series prepared were varied from methyl to octadecyl. In the dodecyltri(alkyl)silanes, a minimum pour point below  $-76^{\circ}$  F. exists between dodecyltri(pentyl)silane and dodecyltri(heptyl)silane. The first nine members of the series all poured below  $-60^{\circ}$  F. The viscosities of the cyclopentamethylenedialkylsilanes were higher than those of the other two series with equivalent molecular weights. A minimum pour point of  $-35^{\circ}$  F. in the didodecyldialkylsilane series was observed for di(dodecyl)di(octyl)silane. The liquid properties of these three series are given in Tables I to II.

As insufficient quantities of the silanes were prepared in the laboratory for extensive evaluation studies, 11 silane fluids were obtained from commercial sources. The physical properties of these fluids are given in Table III and some general properties are given in Tables IV to V.

Viscosities and pour points of commercially prepared fluids were comparable to those obtained on laboratory samples. Cyclopentamethylene derivatives obtained from commercial sources were about 10% more viscous than

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Table I. Liquid Properties of Alkylsilanes

	Pour Point		Kinemetic Viscosity, Centistokes				
Alkyl	° F.	-65° F.	-40° F.	0° F.	100° F.	210° F.	400° F.
·		D	odecyltrialkylsila	nes			
$CH_3^a$	48				3.23	1.34	
$C_2H_5$	12			24.2	4.16	1.58	
$n - C_3 H_7$	-49		192.2	44.8	5.63	2.33	
$n-C_4H_9$	- 56		470.5	91.1	8.37	2.35	
$n-C_5H_{11}$	<-76	2720	671.2	123.0	10.49	2.80	0.87
$n-C_{6}H_{13}$	< -76	3465	875.5	160.8	13.23	3.35	0.99
$n - C_7 H_{15}$	< -76	5345	1294	225.8	16.44	3.90	1.21
$n - C_9 H_{19}$	-34.6			343.8	21.9	4.89	1.56
$n - C_{10}H_{21}$	8.6				27.0	5.66	1.57
$n-C_{11}H_{23}$	35.6				31.0	6.25	1.62
$n-C_{12}H_{25}$	55.4				35.1	6.96	1.84
$n - C_{14}H_{27}$	71.6				44.7	8.44	2.16
		Cyclopenta	amethylenedialky	lsilanes			
$C_{2}H_{5}^{b}$	<-60	9.93	5.98	3.35	1.22	0.68	
$n-C_3H_7$	<-60	26.6	12.24	4.95	1.50	0.77	
$n-C_4H_9$	<-60	131.2	41.6	11.61	2.28	0.97	
$n-C_5H_{11}$	<-60	314.4	91.1	21.0	3.17	1.22	
$n-C_{6}H_{13}$	< -60	553.0		32.7	4.31	1.50	
$n-C_7H_{15}$	<-60	1081.0	278.4	54.4	5.70	1.80	0.72
$n - C_8 H_{17}$	< -60	1739.5	418.3	82.8	7.26	2.19	0.81
$n-C_{9}H_{19}$	<-60	2751.8	630.4	108.1	9.16	2.56	0.89
$n - C_{10} H_{21}$	<-60	3870	829.4	138.2	11.42	2.90	1.02
$n-C_{11}H_{23}$	-26			199.4	13.90	3.42	1.09
$n - C_{12} H_{25}$	-31			428.5	16.92	4.00	1.28
$n - C_{14}H_{29}$	-12				23.9	5.25	1.51
$n-C_{16}H_{33}$	-1				31.5	6.37	1.81
$n - C_{18}H_{37}$	21				40.5	7.80	2.18
<sup>a</sup> Also reported (17).			<sup>b</sup> Also rep	orted (9).			

samples prepared in this laboratory. The average deviation of the 100° F. viscosity between commercial and laboratory samples was 2.5%. At 210° F. the average deviation was 5%. A comparison of pour points is possible for only two of the samples. Commercial samples which contained more siloxane contaminant than laboratory samples, as shown by infrared spectroscopy, possessed lower pour points. Completely symmetrical silanes tetradodecylsilane and tetraundecylsilane have the highest pour points. A small amount of a siloxane will drastically lower the pour point of the fluid and is believed to account for the discrepancies noted.

The viscosity index (1) of the silanes in Table IV ranged from 124 to 155. Diphenyldi(dodecyl)silane possessed the lowest viscosity index, completely symmetrical silanes possessed intermediate values, and mixed symmetrical silanes possessed values ranging from 152 to 155.

High temperature viscosities were measured using the

	Pour	Kine	matic Viscos	ity, Centist	okes
Alkyl	Point, ° F.	0° F.	100° F.	210° F.	400° F.
$CH_3$	75		9.96	2.95	1.03
$C_2H_5$	68		11.28	3.19	1.06
$n-C_3H_7$	41		14.76	3.68	1.10
n-C₄H₃	39		17.27	4.08	1.16
$n \cdot C_5 H_{11}$	30	• • •	18.77	4.29	1.23
$n - C_6 H_{13}$	7		21.22	4.72	1.42
$n - C_7 H_{15}$	-9	355.8	21.91	4.86	1.43
$n-C_8H_{17}$	-35	407.8	24.80	5.36	1.57
$n - C_9 H_{19}$	-8		25.70	5.49	1.59
$n - C_{10}H_{21}$	9		29.50	6.10	1.66
$n - C_{11}H_{23}$	28		32.10	6.68	1.75
$n - C_{12}H_{25}$	55		35.10	6.96	1.84
$n - C_{14}H_{29}$	54		41.80	8.14	2.11
$n - C_{18}H_{37}$	54		47.40	8.90	2.34

Cannon-Fenske viscometer immersed in a well-stirred silicone oil bath. At 700° F. the temperature of the bath was controlled to  $\pm 1.0^{\circ}$  F. The viscometer constant was corrected for the thermal expansion of fluid. The kinetic energy coefficient was not evaluated. At 700° F., the viscosity of the higher molecular weight silanes shown in

	Table III.	Physical	Properties	of Commer	rcially F	Prepared	Silanes
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Silane	Boiling Point, ° C./Mm. Hg	Refractive Index, $n_{ m D}^{25}$	Density, 25°/4° C.
$(C_6H_5)_2Si(C_{12}H_{25})_2^a$	237-243/0.035	1.5060	0.905
$(C_{12}H_{25})_4Si^{\alpha}$	280/0.13	1.4622	0.8276
$C_{18}H_{37}Si(C_8H_{17})_3^b$	208/0.075	1.4620	0.834
$C_{18}H_{37}Si(C_{10}H_{21})_3^b$	255/0.06	1.4649	0.8357
$C_{12}H_{25}Si(C_{10}H_{21})_3^{\circ}$	200/0.10	1.4608	0.8220
$(C_{12}H_{25})_{2}Si(C_{8}H_{17})_{2}^{b}$	170/0.075	1.4601	0.8191
$C_{12}H_{25}Si(C_6H_{13})_3^{b}$	165/0.06	1.4558	0.814
$C_{12}H_{25}Si(C_5H_{11})_3^{b}$	148/0.06	1.4543	0.812
$C_5H_{10}Si(C_8H_{17})_2^{b}$	140/0.1	1.4631	0.8344
$C_5H_{10}Si(C_{10}H_{21})_2^{b}$	160/0.1	1.4649	0.8637
${}^{a}_{b}$ Metal and Thermit Cor	p. val Comp		

Table IV ranged from 0.62 to 0.66 cs. The viscosity of the lighter silanes was not measured above  $400^{\circ}$  F. because of their volatility.

Thermal Stability. Tetraalkylsilanes show good resistance to thermal degradation up to temperatures of  $700^{\circ}$  F. After exposure at  $700^{\circ}$  F. for 9 hours in sealed borosilicate glass ampoules, the silanes exhibited minor changes in viscosity of 4 to 6%.

The temperature where decomposition reactions are detectable is about  $600^{\circ}$  F. This value was obtained from a

discontinuity occurring in a plot of the log of the vapor pressure vs. the reciprocal of the absolute temperature (Figure 1).

Vapor pressure was determined in an isoteniscope of the Smith and Menzies design (15). Blake and coworkers (3) have reported  $660^{\circ}$  to  $670^{\circ}$  F. as the thermal decomposition point based on the isothermal rate of pressure rise in a similar apparatus.

**Oxidative Stability.** Uninhibited silane fluids showed only moderate resistance, at  $500^{\circ}$  F., to oxidation in the presence of metal catalysts which included copper, aluminum, silver, steel, and titanium. Although metal corrosion was not observed, considerable darkening of the fluid occurred as well as neutralization number changes of 1 to 3 and viscosity increases of 25 to 50% have been observed as shown in Table VI. The procedure used was a small scale modification of the apparatus described in MIL-L-9236 (13).

Some success in the inhibition of the oxidation of silanes was reported by Cole (5) using organoselenium compounds. However, these materials were corrosive to copper and silver.

The lack of a suitable oxidation inhibitor restricts considerably the use of silane fluids where a severe thermaloxidative environment exists.

**Flammability.** The silanes exhibit very high flash and fire points. Even the light cyclopentamethylenedioctylsilane has a flash point of  $380^{\circ}$  F. The other fluids possessed flash points up to  $555^{\circ}$  F. The autogenous ignition temperatures ranged from  $610^{\circ}$  to  $775^{\circ}$  F. ASTM D 9252 and D 286-30 procedures were used (1).

**Lubricity.** The ability of the silanes to lubricate sliding surfaces in plane contact was investigated in the 4-ball wear machine (12). The effect of varying speed, load, and temperature was studied. The resulting data are given in

Table VII. At low loads, up to 10 kg., effective thin film lubrication is provided by the fluids. At 40-kg. load, however, the wear scars exceed 1.0 mm. in diameter and are elongated, indicating that seizure and tearing of the wearing surfaces occurred. At 400° F. and 10-kg. load, the border line between film collapse and thin film lubrication is



#### Table IV. General Properties of Commercially Prepared Silanes

Laboratory Tests	$(C_{12}H_{25})_4Si$	$(C_6H_5)_2Si (C_{12}H_{25})_2$	${ m C_{18}H_{37}Si} \ ({ m C_8H_{17}})_3$	$C_{18}H_{37}Si$ ( $C_{10}H_{21}$ ) <sub>3</sub>	$(C_{10}H_{25})_2$ Si $(C_{12}H_{25})_2$	$\begin{array}{c} (C_{12}H_{25})  _2Si \\ (C_8H_{17})  _2 \end{array}$	$(C_{11}H_{23})_4Si$
Spontaneous ignition							
temp., ° F.	775	690	790	750	750	750	760
Flash point. ° F.	555	530	520	545	535	520	545
Fire point. ° F.	625	580	590	595	575	565	600
Pour point, ° F.	20	-25	-30	-20	-35	-45	0
Viscosity, centistokes							
0° F.		1024.9	516.9	689.1	665.1	442.8	
100° F.	34.58	37.2	27.5	33. <del>9</del>	26.4	23.1	29.26
210° F.	6.37	6.2	5.76	6.8	5.6	5.0	6.11
400° F.	1.66	1.6	1.58	1.79	1.56	1.41	1.57
550° F.	0.90	0.91	0.90	0.95	0.91	0.89	0.95
700° F.	0.63	0.65	0.66	0.69	0.64	0.63	0.62
ASTM slope 210/100° F.	0.66	0.69	0.62	0.62	0.61	0.66	0.62
Viscosity index	139	124	154	152	154	155	148
Thermal stability, 700° F.,							
cosity change at 210° F.	-6.9 %	-8.1%	-5.03%	-6.0%	-5.7	-4.0%	-5.7%
Neut. No. change	0.09	0.07	0.0	0.0	0.0	0.0	0.0
Appearance after test	No change	No change	No change	No change	No change	No change	No change

#### Table V. General Properties of Commercially Prepared Silanes

Test	$C_{12}H_{25}Si(C_6H_{13})_3$	$C_{12}H_{25}Si(C_5H_{11})_3$	$C_5H_{10}Si(C_{10}H_{21})_2$	$C_5H_{10}Si(C_8H_{17})_2$
Flash point, ° F.	435	395	450	380
Fire point, ° F.	465	425	490	415
Pour point, ° F.	- 85	- 85	- 70	- 85
Spontaneous ignition temp., ° F.	665	650	700	610
Viscosity, centistokes				
-65° F.	5463.4	3158.4	8987.7	2317.8
-40° F.			1743.2	546.3
100° F.	14.34	10.95	15.0	8.5
210° F.	3.65	2.73	3.7	2.4
400° F.	0.84	0.89	1.08	0.80

		Table VI. Oxid	ative Stability of	<sup>:</sup> Commercially F	Prepared Silanes		
Laboratory Tests	$(\mathrm{C}_{12}\mathrm{H}_{25})_4\mathrm{Si}$	$(C_6H_5)_2Si$ $(C_{12}H_{25})_2$	${{ m C}_{18}}{ m H}_{37}{ m Si} \ ({ m C}_8{ m H}_{17})_3$	${}^{C_{18}H_{37}Si}_{(C_{10}H_{21})_3}$	$C_{12}H_{25}Si$ ( $C_{10}H_{21}$ ) <sub>3</sub>	$(C_{12}H_{25})_{2}Si$ $(C_{8}H_{17})_{2}$	(C <sub>11</sub> H <sub>23</sub> )₄Si
	Oxida	ation-Corrosion, 5	00° F., 24 Hr., 5 L	Liters Air/Hr., Wi	t. Change, Mg./Sq	. Cm.	
Copper			0.104	0.056	0.114	0.064	0.072
Aluminum	0.02	0.06	0.032	0.016	0.016	0.0	0.088
Silver	0.14	0.04	0.048	0.024	0.032	0.009	0.184
Titanium	0.06	0.0	0.0	0.0	0.0	0.006	0.136
Steel	0.06	0.08	0.018	0.104	0.104	0.152	0.0
			Appearance	e of Metals			
Copper			Slight	Stain	Slight corresion	Tarnish	Tamish
Aluminum	No change	No change	No change	No change	No change	No change	No change
Silver	Tarnish	Tarnish	Stain	Stain	Tarnish	Tarnish	Coated
Titanium	Tarnish	Slight ta <del>m</del> ish	Tarnish	Tarnish	Tarnish	Tarnish	Tarnish
Steel	Dark stain	Slight tarnish	Slight	Slight	Slight	Slight	Coated
Appearance of			corrobion	corrosion	corrosion	conosion	
oil after test	Solid	Black,	Dark green.	Dark green,	Green-brown,	Green-brown,	Black,
% vis change at 9	210° F	48.3	47.5	22.0	10 SOITUS	24.9	45.7
Neut. No. change		0.0	1.0	00.0	20.0	15	40.7
% evaporation los	28 	-6.7	-5.8	-5.8	-10.8	-6.6	-5.0

approached. Perhaps there is some contribution to film strength by lubricant viscosity. Increasing the running speed of the machine to 1200 r.p.m. at 40-kg. load results in drastic wearing of the stationary M-10 bearings. A common antiwear agent, tricresyl phosphate, adequately reduced wear at 167° F., but at 400° F. it was not very effective. The M-10 steel bearings are, however, more difficult to lubricate by chemically active agents.

## CONCLUSIONS

Tetraalkysilanes may be conveniently prepared in a wide range of molecular weights and structures. Optimum physical properties are reached in the molecular weight region of 600. Completely symmetrical substitution yields silanes of too high a pour point to be of practical value in

Table VII. Four-Ball Wear Machine Data on

Octadecyltridecylsilane

	Load, Kg. <sup>a</sup>				
	4	10	40		
Conditions	Av. Wear S	Scar Diam	eter, Mm		
167° F., 1200 r.p.m., SAE 52100 bear	ings				
Silane	0.39	0.39	0.97		
Silane, 3% TCP		0.31	0.51		
400° F., 600 r.p.m., M-10 bearings					
Silane	0.42	0.58	1.34		
Silane, 3% TCP			1.22		
400° F., 1200 r.p.m., M-10 bearings					
Silane		0.87	3.75		
Silane, 3% TCP			1.41		
<sup>a</sup> Running time, 2 hr.					

fluid applications. The cyclopentamethylenedialkylsilanes require very long alkyl chains to reduce volatility, thus resulting in high pour point compounds. The didodecyldialkylsilanes possess the lowest pour points of the three series studied in the molecular weight region of interest.

There is little difference in the oxidative, thermal, and lubricating character of the silanes. Oxidative resistance and additive susceptibility at 500° F. are poor. Thermal degradation is first observed at 600° F. It is not yet clear whether the Si-C bond cleavage or the C-C bond cleavage is the predominant degradation reaction. Silane fluids provide effective thin film lubrication under moderate operating conditions. At high speed and high load conditions, film collapse occurs and antiwear agents are required.

Additional structural modification may bring about improved low temperature properties in high molecular weight silanes.

# ACKNOWLEDGMENT

The authors acknowledge the assistance of the Lubricants Branch, Materials Central, Wright Air Development Division, in the determination of many physical properties reported.

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RECEIVED for review March 8, 1960. Accepted August 23, 1960.