Pressure-Volume-Temperature Properties of Sulfur Dioxide

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PRESSURE-VOLUME-TEMPERATURE properties of sulfur dioxide were determined using a Burnett apparatus and a Beattie-type apparatus. The temperature range was 10° to 250° C. and the pressure range was 1 to 312 atm. Critical constants of sulfur dioxide were also determined. Vapor pressures and orthobaric densities were measured and correlated. Latent heats of vaporization were evaluated from the Clapeyron equation. Based on Hirth's (10) and Kang's work (13), smoothed compressibility factors and fugacity coefficients for gaseous sulfur dioxide were calculated for pressures up to 315 atm. over the temperature range from 10° to 250° C. Second virial coefficients were evaluated by Hirth from the low-pressure *P-V-T* data.

EXPERIMENTAL

Purity. The sulfur dioxide was supplied by the Tennessee Corp., Atlanta, Ga., with the specification of 99.9975% purity. Further purification was undertaken as suggested by Couch and others (7) and Vohra and Kobe (18). Samples of the purified sulfur dioxide were analyzed in a mass spectrometer. No foreign substance was found. It was concluded that the minimum purity was 99.998%.

Method and Apparatus. The Beattie-type apparatus is essentially the same as that used by Beattie (2). Apparatus, experimental procedures, and data treatment have been described (13). The design, construction, and calibration of the Burnett apparatus used by Hirth in this investigation are described by Silberberg, Kobe, and McKetta (16). Couch and others (7) have critically evaluated these two methods of data collection.

Reproducibility of Data. During the measurements of

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²Present address, Esso Research and Engineering Co., Florham Park, N. J. P-V-T data several different sizes of samples were chosen to provide some overlap in volume ranges. The agreement of the volume measurements in the overlapping area indicated an excellent reproducibility of data. The compressibility factors thus obtained were consistent and reproducible within $\pm 0.2\%$. The vapor pressure measurement reproducibility is estimated to be well within ± 0.01 atm. The agreement between Hirth's data and Kang's data is generally very good. Discrepancies are discussed later.

Experimental Data. By means of the Beattie-type apparatus the pressure-volume-temperature data of sulfur dioxide in the gaseous phase were measured at 50° , 75° , 100° , 125° , 150° , 157.5° , 175° , 200° , 225° , and 250° C. from 5 atm. to either the vapor pressure at the prevailing temperature or the maximum pressure of 312 atm. Below the critical temperature, which was determined to be 157.5° C. in this work, vapor pressures as well as specific volumes of both the saturated liquid and the saturated vapor were determined at 5° intervals above 50° C.

In the liquid phase, $P \cdot V \cdot T$ data were measured from the vapor pressures to about 312 atm. for five isotherms— 50°, 75°, 100°, 125°, and 150° C. In the course of determining the critical constants of sulfur dioxide, seven additional isotherms—157°, 157.2°, 157.3°, 157.35°, 157.4°, 157.45°, and 157.5° C.—were measured.

By means of the Burnett aparatus, compressibility factor isotherms were determined at intervals of 10° C. between 10° and 50° C. and of 25° C. between 75° and 200° C. At least two runs were made to define each isotherm. Below the critical point, pressures were measured ranging from atmospheric to just below the vapor pressure. Above the critical point the maximum pressure measured was 68 atm.

Hirth's and Kang's experimental compressibility data for gaseous sulfur dioxide are shown in Figures 1 and 2, respectively. The P-V-T data in the high-pressure region, presented partly in Table I, are shown in Figure 3. The P-V-T measurements in the critical region are presented in Table II and shown in Figure 4.



Figure 1. Compressibility factor of sulfur dioxide in the low-pressure region

³ Deceased.



Figure 2. Compressibility factors of sulfur dioxide



Figure 3. Pressure-volume isotherms for sulfur dioxide in the high-pressure region





Figure 4. Pressure-volume isotherms in the critical region of sulfur dioxide

DERIVED QUANTITIES

All of the work on the correlations and calculations was done by using an IBM 650 digital computer.

Smoothed Vapor Pressures. The vapor pressures measured by Kang in this work were correlated by the method of least squares into a Nernst-type equation after appropriate weighing factors were multiplied to the observed results. Equation 1 is the final form of the correlation for temperatures between 50° and 157.5° C.

 $\log P = 14.400840 - \frac{1437.1878}{T} - \frac{4.0200950 \log T}{+ 0.032898989 T}$ (1)

Table I. Experimental Pressure-Volume Isotherms for Liquid Sulfur Dioxide

Vol.,	Pressure,	Vol.,	Pressure,	Vol.,	Pressure,
Cc./G.	Atm.	Cc./G.	Atm.	Cc./G.	Atm.
Mass of	Sample =				
8.1841	Grams	Ma	ss of Sample	= 5.2040 C	rams
t = i	50° C.	t = 0	55° C.	t = 1	25° C.
0.7715	8.490	0.8515	21.320	0.9145	154.07
0.7704	9.981	0.8499	27.262	0.8915	206.71
0.7699 0.7679	12.039	0.8489	29.772	0.8808 0.8717	233.82
0.7641	50.998	t = 9	Э0° С.	0.8638	285.84
$0.7610 \\ 0.7573$	$75.845 \\ 101.58$	0 8654	23 227	0.8559	311.82
0.7536	127.67	0.8645	25.361	t = 1	30° C.
0.7499 0.7465	154.29 181.31	0.8631	28.959	1.0384	49.496
0.7430	207.15	t =	95° C.	1.0338	51.822
0.7399	233.75 260.58	0.8819	26.349	1.0290	54.369
0.7339	285.85	0.8809	28.144	t = 1	35° C.
0.7309	314.31	0.8799	31.399	1.0775	53.756
$t = \xi$	55° C.	t = 1	00° C.	1.0735	54.661
0.7795	10.320	0.8986	28.396	1.0707	00.042
0.7794	$12.043 \\ 14.074$	0.8967	31.265 34.302	t = 1	40° C.
0.1100	11.014	0.8881	49.118	1.1340	58.152
t = 6	60° C.	$0.8831 \\ 0.8763$	$59.430 \\ 75.694$	$1.1173 \\ 1.1065$	$59.412 \\ 62.088$
0.7891	12.050	0.8656	101.52	1.0973	64.696
0.7889 0.7885	$13.840 \\ 14.813$	0.8547 0.8480	128.26 155.91	t = 1	45° C.
0.7882	16.636	0.8407	180.47	1 1750	04.011
t = 6	5° C.	0.8341 0.8282	207.41 233.73	$1.1750 \\ 1.1573$	64.611 67.375
0.7000	10.050	0.8217	259.74	1.1431	69.989
0.7993	15.402	0.8169	285.89 313.78	t = 1	50° C.
0.7986	16.539	f 11	05° C	1 9745	69 909
0.1504	18.003	ι – Ι	JJ C.	1.2683	69.052
t = 7	0° C.	$0.9157 \\ 0.9138$	$31.139 \\ 33.007$	1.2539 1.2396	70.039 71.164
0.8114	14.578	0.9121	35.328	1.1950	76.561
$0.8109 \\ 0.8105$	$15.551 \\ 17.485$	t = 1	10° C.	1.0992 1.0500	101.51 127.82
		0.0004	04.140	1.0170	154.15
t = 1	5° C.	0.9364 0.9350	34.143 35.996	0.9915	207.31
0.8229	16.576	0.9316	39.494	0.9546	233.02
0.8223 0.8223	18.934	0.9290	42.000	0.9437	209.00
0.8220	21.920			Marrief	Q
0.8151	41.979	t = 1	15° C	8.6522	Grams
0.8085	75.882			t = 15	50° C.
		$0.9540 \\ 0.9528$	$37.011 \\ 38.232$	$1.2248 \\ 1.1583$	72.627 83.154
0.8024	102.12	0.9513	39.748	1.0980	101.96
0.7968	129.88 155.87	0.9903	41.444	1.0476	128.07 154.51
0.7868	181.60	t = 1	20° C.	0.9909	180.41
0.7779	233.59	0.9798	41.719	0.9535	233.57
0.7735 0.7698	259.26 286.36	$0.9788 \\ 0.9771$	$42.550 \\ 43.820$	0.9433 0.9268	259.55 285.67
0.7665	313.50	0.0111	10.020	0.9149	312.50
t = t	80° C.	t = 1	.25° C.	Mass of 8 184	Sample =
0.0055	10.005	1.0078	45.274	t = 1	.55° C.
0.8357 0.8350	18.325 20.162	1.0054 1.0021	46.381 49.166	1.4406 1.4301	74.859 74.911
0.8345	22.098	0.9949	54.132	1.4176	74.974
		0.9706	75.376	1.3525	76.393
		$0.9477 \\ 0.9294$	101.68 128.99	$1.3192 \\ 1.2944$	77.708 79.047

The observed vapor pressures and the smoothed results calculated from Equation 1 indicate that the maximum residual is about 0.02 atm., while the maximum deviation is within $\pm 0.05\%$. Hirth smoothed his vapor pressure data by means of pressure residuals. The maximum uncertainty of Hirth's smoothed vapor pressures is estimated to be 0.30% from 0° to 40° C. and 0.25% from 50° to 150° C. Both sets of smoothed data are tabulated in Table III.

Table IV compares the smoothed vapor pressures with the literature values for sulfur dioxide. Hellwig's results (8) agree within 0.5% with the smoothed vapor pressures in this work. The deviations between the reported values of Cardoso and Fiorentino (4) and the smoothed values in this work are generally less than 1%. Toriumi and Hara's data (18) are consistently lower. The International Critical Tables (11) give the least reliable vapor pressure data for sulfur dioxide. Riedel's vapor pressure at 50° C. (15) was extrapolated from his vapor pressure correlation.

Orthobaric Densities. Kang's observed orthobaric densities were smoothed by fitting them to Equations 2 and 3 by means of the method of the steepest descent.

Table II. Experimental Pressure-Volume Isotherms in the Critical Regions of Sulfur Dioxide

Volume,	Pressure,	Volume,	Pressure,
Cc./G.	Atm.	Cc./G.	Atm.
	Mass of Sample	e = 2.8466 Grams	
t = 1	57° C.	t = 15'	7.3° C.
$\begin{array}{c} 2.4109\\ 2.3461\\ 2.2296\\ 2.2168\\ 2.1519\\ 2.0871\\ 1.9575\\ 1.8277\\ 1.6730\\ 1.6984\\ 1.6336\\ 1.5682 \end{array}$	$\begin{array}{c} 77.094\\ 77.136\\ 77.160\\ 77.179\\ 77.183\\ 77.182\\ 77.185\\ 77.185\\ 77.186\\ 77.186\\ 77.182\\ 77.256\\ 77.391\end{array}$	$\begin{array}{c} 2.3476\\ 2.3460\\ 2.2141\\ 2.0844\\ 1.9550\\ 1.8258\\ 1.7621\\ 1.6956\\ 1.6319\\ 1.5672 \end{array}$	$\begin{array}{c} 77.465\\ 77.470\\ 77.536\\ 77.556\\ 77.557\\ 77.557\\ 77.557\\ 77.639\\ 77.736\\ 77.862\end{array}$
t = 15	7.2° C.	t = 157	.35° C.
$\begin{array}{c} 2.3478\\ 2.2179\\ 2.1523\\ 2.0881\\ 2.0228\\ 2.0208\\ 1.8921\\ 1.7632\\ 1.6648\\ 1.6332\\ 1.5676\\ t=15\\ 2.3440\\ 2.2143\\ 2.0847\\ 2.0194\\ 1.9545\\ 1.8250\\ 1.8250\\ 1.7602\\ 1.7007\\ \end{array}$	$\begin{array}{c} 77.344\\ 77.416\\ 77.432\\ 77.435\\ 77.435\\ 77.435\\ 77.435\\ 77.435\\ 77.435\\ 77.435\\ 77.435\\ 77.436\\ 77.494\\ 77.546\\ 77.678\\ 77.678\\ 77.678\\ 77.682\\ 77.682\\ 77.682\\ 77.682\\ 77.683\\ 77.683\\ 77.683\\ 77.683\\ 77.716\\ 77.784\\ 77.784\\ 77.683\\ 77.683\\ 77.716\\ 77.784\\ 77.784\\ 77.784\\ 77.683\\ 77.716\\ 77.784\\ 77.784\\ 77.683\\ 77.716\\ 77.784$	2.3455 2.2158 2.1507 2.0860 2.0212 1.9566 1.8917 1.8269 1.7621 1.7080 1.6327 t = 157 2.3453 2.2156 2.0860 2.0212 1.9563 1.8915 1.8268 1.7620 1.7080	77.524 77.592 77.614 77.620 77.620 77.620 77.621 77.633 77.699 77.813 7.5° C. 77.686 77.744 77.782 77.799 77.804 77.815 77.837 77.876 77.876 77.919
t = 157	77.870 .45° C.	Mass of Sample	= 8.6522 Grams
2.3463 2.2159 2.0858 2.0211	77.631 77.693 77.740 77.747	2.3633 2.1393 1.6186	77.673 77.767 78.122
$\begin{array}{c} 1.9560 \\ 1.8907 \\ 1.8263 \\ 1.7611 \\ 1.6968 \\ 1.6327 \end{array}$	77.748 77.748 77.749 77.794 77.854 77.921		

Table III. Smoothed Vapor Pressure Orthobaric Density and Latent Heat of Vaporization Data for Sulfur Dioxide

	Vanor	Pressure	D	ensity, G./O	ΔH_{v} ,	
t	A	tm.	Va	apor	Liquid	Cal. per G.
° Ċ.	Kang	Hirth	Kang	Hirth	Kang	Kang
$10 \\ 20 \\ 30 \\ 40$		$2.268 \\ 3.260 \\ 4.556 \\ 6.218$		$\begin{array}{c} 0.00661 \\ 0.00930 \\ 0.01274 \\ 0.01715 \end{array}$		
50 55 60 65 70	8.484 9.683 11.010 12.474 14.085	8.302	$\begin{array}{c} 0.02336 \\ 0.02667 \\ 0.03029 \\ 0.03424 \\ 0.03858 \end{array}$	0.02264	$\begin{array}{c} 1.2970 \\ 1.2804 \\ 1.2635 \\ 1.2464 \\ 1.2289 \end{array}$	$74.81 \\ 74.08 \\ 73.23 \\ 72.26 \\ 71.16$
75 80 85 90 95	$\begin{array}{c} 15.853 \\ 17.787 \\ 19.898 \\ 22.198 \\ 24.696 \end{array}$	15.760	$\begin{array}{c} 0.04338 \\ 0.04868 \\ 0.05458 \\ 0.06117 \\ 0.06854 \end{array}$	0.04302	$\begin{array}{c} 1.2111 \\ 1.1928 \\ 1.1740 \\ 1.1546 \\ 1.1344 \end{array}$	$69.93 \\ 68.57 \\ 67.06 \\ 65.40 \\ 63.57$
100 105 110 115 120	27.406 30.337 33.503 36.916 40.589	27.425	0.07684 0.08623 0.09689 0.1091 0.1232	0.07798	$1.1134 \\ 1.0914 \\ 1.0682 \\ 1.0435 \\ 1.0170$	$61.57 \\ 59.38 \\ 56.98 \\ 54.34 \\ 51.45$
125 130 135 140 145	$\begin{array}{r} 44.534 \\ 48.767 \\ 53.299 \\ 58.147 \\ 63.324 \end{array}$	44.572	$\begin{array}{c} 0.1396 \\ 0.1589 \\ 0.1821 \\ 0.2107 \\ 0.2474 \end{array}$	0.1404	$\begin{array}{c} 0.9882 \\ 0.9566 \\ 0.9212 \\ 0.8805 \\ 0.8317 \end{array}$	$\begin{array}{r} 48.25 \\ 44.69 \\ 40.68 \\ 36.09 \\ 30.66 \end{array}$
150 155 157 157.5	68.845 74.727 77.807	68.824	$0.2980 \\ 0.3831 \\ 0.4571$	0.2903	$\begin{array}{c} 0.7691 \\ 0.6721 \\ 0.5933 \end{array}$	23.86 13.84

$$d = \left(\frac{d_t + d_s}{2}\right) = 0.52462015 + 1.1863691 \times 10^{-3}(t_c - t) + 6.9451764 \times 10^{-7}(t_c - t)^2$$
(2)

$$\Delta = \left(\frac{d_L - d_g}{2}\right) = 9.8206457 \times 10^{-2} (t_c - t)^{0.48013} - 3.7254523$$
$$\times 10^{-3} (t_c - t) + 6.0192965 \times 10^{-6} (t_c - t)^2 \tag{3}$$

During the equation fitting, suitable weighing factors were multiplied to the observed values, to obtain the correlations with the best fit to the experimental data. Table III lists the smoothed orthobaric densities. The deviations between the observed and the smoothed values are less than $\pm 0.37\%$. Hirth's molal volumes for the saturated vapor were obtained by extending his compressibility isotherms to the smoothed vapor pressures given in Table III. The maximum error in his smoothed values is estimated to be slightly greater than 0.55% at 150° C. but falls off to 0.1 to 0.3% at temperatures further from the initial temperature. Tables V and VI compare the smoothed saturated volumes of both liquid and vapor of sulfur dioxide with values reported in the literature. The saturated liquid specific volumes reported in International Critical Tables (11) are in close agreement with this work. There is a maximum deviation of 2.1% between Hellwig's saturated vapor specific volumes (8) and the smoothed results of this work. Riedel's (15) high specific volume of the saturated vapor at 50° C. again was an extrapolated value from his correlation. The saturated vapor specific volumes reported in International Critical Tables (11) are in complete disagreement with the smoothed results in this work.

Critical Constants. Figure 4 plots the pressure-volume isotherms in the critical region. The critical constants were determined graphically. Table VII presents the comparison with other experimental results in the literature. The agreement is good.

The critical volume, then, is 1.905 cc. per gram, and the critical compressibility factor is 0.2697.

Latent Heat of Vaporization. The latent heats of vaporization were evaluated by means of the Clapeyron equation,

$$\Delta H_{v} = T \left(V_{s} - V_{L} \right) \frac{dP}{dT}$$
(4)

using V_L taken from Table V, V_g from Table VI, and dP/dT from Equation 1. The calculated latent heats of vaporization of sulfur dioxide are presented in Table III. These were also correlated using Equation 5 for temperatures between 50° and 157.5° C.

$$\Delta H_v = 8.7759469 (t_c - t)^{0.49945} - 1.0021178 \times 10^{-2} (t_c - t) - 1.2866153 \times 10^{-3} (t_c - t)^2$$
(5)

The deviations between the values from Equation 5 and the values from the Clapeyron equation are less than 0.9%.

Smoothed Compressibility Factors. The volume residuals of gaseous sulfur dioxide were calculated from Hirth's compressibility data and the P-V-T data in Kang's work. Fourteen isotherms of volume residuals—10°, 20°, 30°, 40°, 50°, 75°, 100°, 125°, 150°, 157.5°, 175°, 200°, 225°, and 250° C.—were plotted vs. pressure on a large graph readable to ± 0.001 cc. per gram. Smooth curves were drawn through these points. The volume residuals read from the smoothed curves were regarded as the smoothed values. The smoothed compressibility factors of sulfur dioxide in this work were calculated with a high degree of accuracy from these smoothed volume residuals by using Equation 6.

$$Z = 1 - \gamma P / RT \tag{6}$$

The smoothed compressibility factors, thus obtained, are tabulated in Table VIII. The smoothed compressibility factors in Kang's work are in close agreement with Hirth's smoothed values. However, higher deviations (up to 0.37%) were found in the vicinity of the two-phase region and at high pressures. The maximum errors in Hirth's smoothed values are estimated to be less than 0.55% at 150° C., decreasing to 0.1 to 0.3% at temperatures further removed from the critical. Hellwig's experimental compressibility factors (8) are generally higher than Kang's smoothed results in this work. The maximum deviation is 1.87%.

Fugacity Coefficient. The fugacity coefficient, ν , is defined by Equation 7.

Table IV. Comparison of Smoothed Vapor Pressures with Literature Values for Sulfur Dioxide

Temp	Kang's (13)	Hirth	. (10)	Cardo	so (4)	I.C.T.	(11)	Torium	i (17)	Hellwi	g (8)	\mathbf{R} iedel	(15)
t, ° Č.	<i>P.</i> , Atm.	P	Dev.	P°	Dev."	\overline{P}	Dev.	P	Dev.	\overline{P}	Dev.	P	Dev.
$\frac{50}{75}$	$8.484 \\ 15.853$	$\frac{8.302}{15.760}$	$2.15 \\ 0.57$	$\frac{8.34}{15.87}$	$1.70 \\ -0.11$	$8.176 \\ 15.684$	$3.63 \\ 1.07$	8.35	1.58	$8.45 \\ 15.94$	$0.40 \\ -0.49$	8.583	-1.17
$100 \\ 125$	$27.406 \\ 44.534$	27.425 44.572	-0.09 -0.09	27.25	0.57 0.44	27.714	-1.12	27.25	0.57	27.45	-0.16		
150	68.845	68.824	0.03	68.40	0.65	68,405	0.64	68.20	0.94	$\frac{1}{68.75}$	0.14		

P = atmosphere.

^b Deviation, % = (smoothed vapor pressure – literature value) × 100/smoothed vapor pressure.

Temp.,	Smoothed	I.C.7	Γ. (11)	Caille	etet (3)	Hellwig (8)		Cardoso (5)	
t, ° Ċ.	V_L , Cc./G.	V_L	Dev.ª	V_L	Dev.	$\overline{V_L}$	Dev.		Dev.
50	0.7710	0.7722	-0.16	0.7740	-0.39	0.7750	-0.52		
75	0.8257	0.8254	0.04	0.8264	-0.08	0.8266	-0.11		
100	0.8981	0.8977	0.04	0.8981	0.00	0.9002	-0.23		
125	1.0119	1.0111	0.08	1.0103	0.16	1.0136	0.17		
150	1.3003	1.3038	-0.27	1.3179	-1.35	1.2783	1.59	1.1980	7.87
155	1.4880			1.5699	-5.99			1.3026	12.46

Deviation, % = (smoothed value – literature value) × 100/smoothed value.

Table VI. Comparison of Smoothed Saturated Vapor Specific Volumes with Literature Values for Sulfur Dioxide

Temp	Kang's (13)	Hirt	ch (8)	I.C.7	F. (11)	Hellw	vig (8)	Cardos	o (5)	Riedel	(15)
<i>t</i> , ° Ć.	V_{s} , Cc./G.	V_s	Dev.ª	V_s	Dev.	V_{s}	Dev.	V_{κ}	Dev.	V_{κ}	Dev.
50	42.812	44.215	-3.27	40.65	5.05	42.10	1.66			44.6	-4.18
75	23.054	23.242	-0.82	23.29	-1.02	22.83	0.97				
100	13.013	12.823	1.46	12.94	0.56	12.92	0.71				
125	7.1655	7.124	0.58	7.069	1.35	7.191	-1.35				
150	3.3553	3.445	-2.69	3.256	2.96	3.285	2.10	3.4352	2.38		

^a Deviation = (smoothed value - literature value) \times 100/smoothed value.



Figure 5. Fugacity coefficients for sulfur dioxide

$$\nu = \frac{f}{P} = e^{\left[-(1/RT) \int_{0}^{\mu} \gamma dP\right]}$$
(7)

In calculating the fugacity coefficients of sulfur dioxide, the smoothed volume residuals were first read from the smoothed curves. Then the integrand, $\int_{o}^{P} \gamma dP$, was evaluated numerically by using Weddle's rule. The fugacity coefficients, which were calculated from Equation 7, are presented in Figure 5.

Second Virial Coefficients. Hirth's experimental residual volume isotherms of sulfur dioxide appear in Figure 6. The experimental second virial coefficients, obtained by extrapo-

lation of the curves in Figure 6 to zero pressure, are presented in Table IX and plotted in Figure 7. Smoothed values of the second virial coefficient read from the curve in Figure 7 are also shown in Table IX. The smoothed second virial coefficients are estimated to have a maximum error of 0.020 liter per gram mole at 10° C., which decreases to 0.007 liter per gram mole at 200° C.

Second virial coefficients calculated from the low pressure measurements of Baume (1), Cawood and Patterson (6), Jacquerod and Scheurer (12), and Leduc (14) are shown in Figure 7 along with the values from the present work. The maximum deviation does not exceed 0.008 liter per gram

lable	VII. Critical Constant	ts for Sulfur Dioxide	
Investigators	t_c , ° C.	P_c , Atm.	d_c , G./Cc.
Cailletet and Mathias (3)	156.0		0.52
Cardoso and Fiorentino (4)	157.5 ± 0.05	77.79 ± 0.05	
Cardoso and Sorrentino (5)			0.524
Helllwig (8)	157.5 ± 0.05	77.803 ± 0.005	0.522
This work	$157.5~\pm~0.02$	77.808 ± 0.02	$0.525~\pm~0.001$

			Table	VIII. Smoo	thed Compre	essibility Fact	ors of Sulfu	Dioxide			
Р.			Ζ			P			Ζ		
Atm. 0.5 1 1.5 2 2.268° 2.5	10° C. 0.9889 0.9775 0.9657 0.9531 0.9459	20° C 0.9903 0.9806 0.9707 0.9607 0.9502	· 3 0. 0. 0. 0. 0.	0° C. 9917 9835 9751 9667 9582	40° C. 0.9928 0.9855 0.9782 0.9709 0.9635	Atm. 1 2 5 10 15	157.5° C. 0.9953 0.9906 0.9765 0.9528 0.9286	175° C. 0.9961 0.9922 0.9804 0.9605 0.9399	200° C. 0.9967 0.9934 0.9836 0.9671 0.9504	225° C. 0.9973 0.9946 0.9864 0.9728 0.9592	250° C. 0.9977 0.9954 0.9884 0.9769 0.9653
$3 \\ 3.260^{\circ} \\ 3.5 \\ 4 \\ 4.5$		0.9392 0.9330	0. 0. 0.	.9495 .9405 .9313	0.9560 0.9484 0.9406 0.9328	20 25 30 35 40	$\begin{array}{c} 0.9037\\ 0.8655\\ 0.8507\\ 0.8222\\ 0.7916 \end{array}$	$\begin{array}{c} 0.9185 \\ 0.8963 \\ 0.8732 \\ 0.8492 \\ 0.8243 \end{array}$	$0.9334 \\ 0.9157 \\ 0.8976 \\ 0.8791 \\ 0.8602$	$\begin{array}{c} 0.9454 \\ 0.9315 \\ 0.9173 \\ 0.9030 \\ 0.8883 \end{array}$	$\begin{array}{c} 0.9538 \\ 0.9422 \\ 0.9306 \\ 0.9191 \\ 0.9075 \end{array}$
$4.556^{\circ} \\ 5 \\ 5.5 \\ 6 \\ 6.218^{\circ}$			0.	9204	0.9248 0.9166 0.9080 0.9038	45 50 55 60 65	$\begin{array}{c} 0.7588 \\ 0.7241 \\ 0.6858 \\ 0.6435 \\ 0.5960 \end{array}$	$\begin{array}{c} 0.7983 \\ 0.7713 \\ 0.7429 \\ 0.7133 \\ 0.6820 \end{array}$	$\begin{array}{c} 0.8407 \\ 0.8208 \\ 0.8004 \\ 0.7795 \\ 0.7580 \end{array}$	$\begin{array}{c} 0.8734 \\ 0.8583 \\ 0.8429 \\ 0.8273 \\ 0.8115 \end{array}$	$0.8958 \\ 0.8840 \\ 0.8719 \\ 0.8597 \\ 0.8476$
-	50° C	75° C	2 100° C	125° C	150° C	70 75 80 85 90	$\begin{array}{c} 0.5359 \\ 0.4473 \\ 0.2062 \\ 0.1992 \\ 0.2050 \end{array}$	$\begin{array}{c} 0.6492 \\ 0.6127 \\ 0.5721 \\ 0.5255 \\ 0.4718 \end{array}$	$0.7360 \\ 0.7134 \\ 0.6900 \\ 0.6660 \\ 0.6412$	$\begin{array}{c} 0.7956 \\ 0.7794 \\ 0.7628 \\ 0.7464 \\ 0.7294 \end{array}$	0.8353 0.8231 0.8107 0.7984 0.7860
1 2 3 4 5 6 7	$\begin{array}{c} 0.9871 \\ 0.9742 \\ 0.9611 \\ 0.9478 \\ 0.9344 \\ 0.9207 \\ 0.9065 \end{array}$	0.9902 0.9804 0.9706 0.9606 0.9505 0.9403 0.9298	0.9925 0.9849 0.9773 0.9696 0.9619 0.9540 0.9460	0.9938 0.9877 0.9815 0.9752 0.9690 0.9627 0.9564	0.9951 0.9901 0.9852 0.9802 0.9752 0.9702 0.9652	95 100 105 110 115 120	0.2093 0.2145 0.2218 0.2310 0.2419 0.2477	$\begin{array}{c} 0.4093\\ 0.3470\\ 0.3074\\ 0.2922\\ 0.2856\\ 0.2849 \end{array}$	$\begin{array}{c} 0.6156\\ 0.5891\\ 0.5614\\ 0.5339\\ 0.5066\\ 0.4810 \end{array}$	$\begin{array}{c} 0.7123\\ 0.6952\\ 0.6780\\ 0.6607\\ 0.6435\\ 0.6264\end{array}$	$\begin{array}{c} 0.7737\\ 0.7612\\ 0.7487\\ 0.7365\\ 0.7242\\ 0.7121\end{array}$
$\overset{0}{8}$ 8.484 ^b 10 12 14 15.852 ^b	0.8906 0.8775	0.9191 0.8968 0.8731 0.8470	0.9379 0.9213 0.9042 0.8865	0.9500 0.9371 0.9240 0.9106	0.9601 0.9500 0.9398 0.9294	$125 \\ 130 \\ 135 \\ 140 \\ 145$	$\begin{array}{c} 0.2518 \\ 0.2564 \\ 0.2612 \\ 0.2684 \\ 0.2768 \end{array}$	0.2872 0.2910 0.2949 0.2984 0.3036	$\begin{array}{c} 0.4577\\ 0.4371\\ 0.4226\\ 0.4120\\ 0.4037\end{array}$	$\begin{array}{c} 0.6099 \\ 0.5939 \\ 0.5785 \\ 0.5643 \\ 0.5512 \end{array}$	$\begin{array}{c} 0.7003 \\ 0.6887 \\ 0.6776 \\ 0.6670 \\ 0.6564 \end{array}$
15.853 16 18 20 22 24 26		0.0190	0.8682 0.8492 0.8292 0.8077 0.7849 0.7608	0.8970 0.8830 0.8687 0.8539 0.8388 0.8232	$\begin{array}{c} 0.9188 \\ 0.9081 \\ 0.8973 \\ 0.8862 \\ 0.8749 \\ 0.8634 \end{array}$	150 155 160 165 170 175	$\begin{array}{c} 0.2869 \\ 0.2983 \\ 0.3104 \\ 0.3178 \\ 0.3224 \\ 0.3278 \end{array}$	$\begin{array}{c} 0.3102 \\ 0.3187 \\ 0.3276 \\ 0.3344 \\ 0.3403 \\ 0.3457 \end{array}$	$\begin{array}{c} 0.3985\\ 0.3946\\ 0.3927\\ 0.3931\\ 0.3952\\ 0.3980 \end{array}$	$\begin{array}{c} 0.5395 \\ 0.5287 \\ 0.5198 \\ 0.5121 \\ 0.5060 \\ 0.5014 \end{array}$	$\begin{array}{c} 0.6461 \\ 0.6364 \\ 0.6274 \\ 0.6191 \\ 0.6116 \\ 0.6052 \end{array}$
27.406° 28 30 32 34 36	, ⁶	0.7462 0.7462 0.790 0.790 0.777 0.755	0.8070 0.7902 0.7723 0.7536 0.7339	0.8515 0.8394 0.8269 0.8141 0.8009	180 185 190 195 200	$\begin{array}{c} 0.3340 \\ 0.3405 \\ 0.3478 \\ 0.3551 \\ 0.3631 \end{array}$	$\begin{array}{c} 0.3510 \\ 0.3572 \\ 0.3633 \\ 0.3694 \\ 0.3766 \end{array}$	$\begin{array}{c} 0.4011 \\ 0.4055 \\ 0.4090 \\ 0.4134 \\ 0.4182 \end{array}$	$\begin{array}{c} 0.4976 \\ 0.4953 \\ 0.4944 \\ 0.4942 \\ 0.4947 \end{array}$	$\begin{array}{c} 0.5993 \\ 0.5941 \\ 0.5894 \\ 0.5850 \\ 0.5818 \end{array}$	
38 40 42 44 44.534 ^b				$\begin{array}{c} 0.7130 \\ 0.6905 \\ 0.6659 \\ 0.6391 \\ 0.6258 \end{array}$	0.7875 0.7737 0.7597 0.7451	205 210 215 220 225	$\begin{array}{c} 0.3711 \\ 0.3789 \\ 0.3872 \\ 0.3946 \\ 0.4020 \end{array}$	$\begin{array}{c} 0.3843 \\ 0.3925 \\ 0.3998 \\ 0.4069 \\ 0.4140 \end{array}$	$\begin{array}{c} 0.4223 \\ 0.4272 \\ 0.4320 \\ 0.4370 \\ 0.4428 \end{array}$	$\begin{array}{c} 0.4959 \\ 0.4973 \\ 0.4992 \\ 0.5014 \\ 0.5049 \end{array}$	$\begin{array}{c} 0.5790 \\ 0.5772 \\ 0.5761 \\ 0.5755 \\ 0.5760 \end{array}$
46 48 50 52 54 56					$\begin{array}{c} 0.7300 \\ 0.7144 \\ 0.6981 \\ 0.6809 \\ 0.6628 \\ 0.6634 \end{array}$	$230 \\ 235 \\ 240 \\ 245 \\ 250$	$\begin{array}{c} 0.4089 \\ 0.4154 \\ 0.4224 \\ 0.4292 \\ 0.4362 \end{array}$	$0.4206 \\ 0.4272 \\ 0.4345 \\ 0.4417 \\ 0.4477$	$0.4485 \\ 0.4544 \\ 0.4598 \\ 0.4654 \\ 0.4711$	$\begin{array}{c} 0.5076 \\ 0.5114 \\ 0.5154 \\ 0.5193 \\ 0.5235 \end{array}$	$\begin{array}{c} 0.5764 \\ 0.5777 \\ 0.5785 \\ 0.5804 \\ 0.5822 \end{array}$
58 60 62 64 66					$\begin{array}{c} 0.6434 \\ 0.6226 \\ 0.6002 \\ 0.5758 \\ 0.5488 \\ 0.5150 \end{array}$	255 260 265 270 275	$\begin{array}{c} 0.4434 \\ 0.4519 \\ 0.4587 \\ 0.4659 \\ 0.4730 \end{array}$	$\begin{array}{c} 0.4546 \\ 0.4612 \\ 0.4678 \\ 0.4746 \\ 0.4811 \end{array}$	$\begin{array}{c} 0.4775 \\ 0.4837 \\ 0.4900 \\ 0.4954 \\ 0.5017 \end{array}$	$\begin{array}{c} 0.5278 \\ 0.5324 \\ 0.5373 \\ 0.5421 \\ 0.5472 \end{array}$	$\begin{array}{c} 0.5844 \\ 0.5871 \\ 0.5898 \\ 0.5930 \\ 0.5961 \end{array}$
68 68.845 [*]					0.4712 0.4262	280 285 290 295 300	$\begin{array}{c} 0.4799 \\ 0.4869 \\ 0.4941 \\ 0.5013 \\ 0.5086 \end{array}$	0.4839 0.4959 0.5032 0.5101 0.5170	$\begin{array}{c} 0.5077 \\ 0.5142 \\ 0.5209 \\ 0.5276 \\ 0.5342 \end{array}$	$\begin{array}{c} 0.5524 \\ 0.5576 \\ 0.5627 \\ 0.5685 \\ 0.5740 \end{array}$	$\begin{array}{c} 0.5597 \\ 0.6036 \\ 0.6074 \\ 0.6110 \\ 0.6148 \end{array}$
^a Vapor pres ^b Vapor pres	ssures deter ssures deter	mined by Hi mined by Ka	rth (10). ang.			305 310 315	$\begin{array}{c} 0.5157 \\ 0.5230 \\ 0.5307 \end{array}$	$\begin{array}{c} 0.5236 \\ 0.5298 \\ 0.5362 \end{array}$	$\begin{array}{c} 0.5415 \\ 0.5488 \\ 0.5565 \end{array}$	$\begin{array}{c} 0.5792 \\ 0.5844 \\ 0.5891 \end{array}$	$\begin{array}{c} 0.6185 \\ 0.6224 \\ 0.6260 \end{array}$

mole, which is considered excellent for second virial coefficients.

Second virial coefficients computed from the Berthelot relation using Kang's critical constants are presented in Table IX, as well as second virial coefficients calculated by the Stockmayer potential function (9) for polar gases. The parameters used were $t^* = 0.6$, $e/k = 455^\circ$ K., and $b_o = 0.03029$ liter per gram mole. The maximum difference between the values calculated by the Stockmayer potential and those of this work is 0.007 liter per gram mole.

Table IX. Second	Virial	Coefficients	ot	Sultur	Dioxide
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Temp		-B, Liters	s/G. Mole	
° C.	Exptl.	Smoothed	Berthelot	Stockmayer
10	0.5000	0.503	0.412	0.5000
20	0.4520	0.448	0.382	0.4447
30	0.4040	0.404	0.355	0.4026
40	0.3675	0.366	0.330	0.3654
50	0.3328	0.334	0.309	0.3331
75	0.2790	0.276	0.262	0.2718
100	0.2325	0.234	0.255	0.2272
125	0.2010	0.199	0.192	0.1934
150	0.1711	0.170	0.167	0.1672
175	0.1441	0.145	0.145	0.1463
200	0.1258	0.124	0.126	0.1293
° From equa	ation. $B = \frac{9}{12}$	$\frac{RT_c}{8P_c} \left[1 - \frac{6}{T_c} \right]$	<u>2</u>].	
[°] Parameter	$t^* = 0.6, e$	$/k = 455^{\circ} \text{ K.},$	$b_{\circ} = 0.03029$) liter/g. mole

NOMENCLATURE

- В = second virial coefficients
- parameter in Stockmayer potential function b. =
- = critical density, g./cc. d.
- density of saturated vapor, g./cc. d, =
- d_L = density of saturated liquid, g./cc.
- parameter in Stockmayer potential function e/k =
- f = fugacity
- latent heat of vaporization $\Delta H_i =$
- Ρ = absolute pressure
- P_{c} critical pressure, atm. =
- R = gas constant
- Т absolute temperature =
- temperature, ° C. = t
- +* = parameter in Stockmayer potential function
- T_{c} Ŧ critical temperature, ° K.
- critical temperature, ° C. = t.
- T_r = reduced temperature
- V = volume
- V_{e} = specific volume of saturated vapor, cc./g.
- specific volume of saturated liquid, cc./g. V_L Ŧ
- Ż compressibility factor, PV/RT=
- volume residual, RT/P Vγ =
- fugacity coefficient, f/P=

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LITERATURE CITED

- Baume, G., J. chim. phys. 6, 1 (1908). (1)
- (2)
- Beattie, J.A., Proc. Am. Acad. Arts Sci. 69, 389 (1934). Cailletet, L., Mathias, E., Compt. rend. 104, 1563 (1887). (3)
- Cardoso, E., Fiorentino, U., J. chim. phys. 23, 841 (1926). (4)(5)Ibid., 24, 81 (1927).
- (6)
- Cawood, W., Patterson, H.S., J. Chem. Soc. 1933, p. 619. (7)Couch, E.J., Hirth, L.J., Kobe, K.A., J. CHEM. ENG. DATA 6,229 (1961).
- Hellwig, L.R., "Pressure-Volume-Temperature Properties of (8)Sulfur Dioxide," Ph.D. dissertation in chemical engineering, University of Texas, Austin, Tex., 1955.
- Hirschfelder, J.O., Curtiss, C.F., Bird, R.B., "Molecular (9)



Figure 6. Experimental residual volume isotherms for sulfur dioxide



Figure 7. Second virial coefficients for sulfur dioxide

- Theory of Gases," pp. 211-20, Wiley, New York, 1954. Hirth, L.J., "Gas Compressibility of Nitrous Oxide and of Sulfur Dioxide by the Burnett Method," Ph.D. dissertation (10)in chemical engineering, University of Texas, Austin, Tex., 1958.
- International Critical Tables, Vol. III, p. 236, McGraw-Hill, (11)New York, 1928.
- Jacquerod, A., Scheurer, O., Compt. rend. 140, 1384 (1905). (12)
- Kang, T.L., "Thermodynamic Properties of Sulfur Dioxide," (13)
- Ph.D. dissertation in chemical engineering, University of Texas, Austin Tex., 1960.
- Leduc, A., Sacerdote, P., Compt. rend. 125, 297 (1897). (14)
- (15) Riedel, L., Bull. Intern. Inst. Refrig. 20, No. 4, Annex No. 5, B1 (1939).
- Silberberg, I.H., Kobe, K.A., McKetta, J.J., J. CHEM. ENG. (16)DATA 4, 314-23 (1959).
- Toriumi, T., Hara, R., J. Soc. Chem. Ind. (Japan) 47, 502 (17)(1944).
- (18)Vohra, P.S., Kobe, K.A., J. CHEM. ENG. DATA 4, 329-30 (1959).

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