# Vapor Pressure of Propylene Oxide 

T. R. BOTT and H. N. SADLER<br>Chemical Engineering Department, University of Birmingham, Birmingham, England

The saturated vapor pressure of propylene oxide in the temperature range $20^{\circ}$ to $70^{\circ} \mathrm{C}$. has been determined. Between $40^{\circ}$ and $70^{\circ} \mathrm{C}$., the results are conelated by the equation

$$
\log P=7.658-\frac{1472}{T}
$$

$\mathbf{S}_{\text {aturated vapor pressures of propylene oxide }}$ at temperatures up to $48.5^{\circ} \mathrm{C}$. have been reported in the literature (2, 3, 4). The correlation up to a temperature of about $40^{\circ} \mathrm{C}$. given by Kireev and Popov (g) is:

$$
\begin{equation*}
\log P=-\frac{1722.73}{T}+8.48693 \tag{1}
\end{equation*}
$$

where $T=$ absolute temperature, ${ }^{\circ} \mathrm{K}$.
The increasing interest in this material has prompted the confirmation and extension of the data.

## APPARATUS AND EXPERIMENTAL METHOD

The apparatus, which is essentially a modified Reid vapor pressure apparatus (1) consisted of a $150-\mathrm{ml}$. chromiumplated brass cylindrical pressure vessel, immersed in a constant temperature bath. A mercury manometer was connected to the vessel by a flexible stainless steel tube. A "tee" junction in this line, having a valve with a connection to a vacuum pump via a cold trap (solid carbon dioxide), enabled the apparatus to be exhausted prior to the determination of vapor pressures.

The vessel and its contents of propylene oxide were held at constant temperature until equilibrium had been established when the level of mercury in the manometer was noted. Corrections were made for barometric pressure and the effects of liquid condensed in the manometer. Accuracy of pressure measurement was better than $0.25 \%$ while the temperature was recorded to $\pm 0.1^{\circ} \mathrm{C}$. The purity of the propylene oxide (I.C.I.Ltd., H.O.C. Division) is greater than $99.9 \%$.

## RESULTS

The results, given in Table I, when plotted graphically, gave a straight-line relationship up to approximately $40^{\circ} \mathrm{C}$. and a slightly different straight-line plot between $40^{\circ} \mathrm{C}$. and $70^{\circ} \mathrm{C}$.

| Table I. Saturated Vapor Pressure of Propylene Oxide at Different Temperatures |  |  |  |
| :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Temp., } \\ { }^{\circ} \mathrm{C} . \end{gathered}$ | Vapor Mm. Hg | $\begin{gathered} \text { Temp., } \\ { }^{\circ} \mathrm{C} . \end{gathered}$ | Vapor <br> Pressure <br> Mm. Hg |
| 19.0 | 416 | 50.2 | 1265 |
| 27.0 | 574 | 54.0 | 1452 |
| 36.3 | 806 | 59.2 | 1694 |
| 40.8 | 950 | 64.7 | 1994 |
| 46.8 | 1157 | 71.8 | 2403 |

The data obtained in the present work agree well with the data of Kireev and Popov in the range up to about $35^{\circ}$ to $40^{\circ} \mathrm{C}$.

The results presently reported in the range $40^{\circ}$ to $70^{\circ} \mathrm{C}$. are correlated by the following equation.

$$
\begin{equation*}
\log P=7.658-\frac{1472}{T} \tag{2}
\end{equation*}
$$

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# Phase Behavior in the Hydrogen-Cyclohexane System 

T. E. BERTY, H. H. REAMER, and B. H. SAGE

Chemical Engineering Laboratory, California Institute of Technology, Pasadena, Calif.

TTHERE HAS BEEN a gradual accumulation of information concerning the phase behavior of binary systems involving hydrogen and a paraffin hydrocarbon. However, data upon the hydrogen-cyclohexane system are limited. An experimental study involving measurements of the specific volume of three mixtures of hydrogen and cyclohexane at four temperatures between $100^{\circ}$ and $280^{\circ} \mathrm{F}$. was carried out at pressures as high
as 10,000 p.s.i.a. The composition of the coexisting gas phase in heterogeneous mixtures of hydrogen and cyclohexane was determined throughout the above-mentioned temperature and pressure interval. This binary system followed the trends of other hydrogen-paraffin hydrocarbon systems, and the critical pressure was above 10,000 p.s.i.a. for all of the temperatures investigated.


#### Abstract

Measurements of the composition of the coexisting phases in the hydrogen-cyclohexane system have been carried out at temperatures between $100^{\circ}$ and $280^{\circ}$ F. and at pressures up to 10,000 p.s.i.a. Limited measurements of the specific volume of the liquid phase were made throughout the above-mentioned temperature interval for three mixtures of hydrogen and cyclohexane. The experimental results are presented in tabular form, and the properties of the coexisting phases have been recorded


Studies of the phase behavior of the hydrogen-propane (4) and of the hydrogen- $n$-hexane system (6) are available. Benham, Katz, and Williams (2) reviewed the general characteristics of hydrogen-light hydrocarbon systems and presented a tentative method of predicting the phase behavior of such mixtures. Recently, data concerning the liquid-vapor equilibrium of the hydrogen-cyclohexane system became available at temperatures of $150^{\circ}$ and $250^{\circ} \mathrm{F}$. (11).

The volumetric behavior of cyclohexane is known (8), as is the vapor pressure (12). Likewise, the volumetric behavior of hydrogen has been established with a relatively high degree of accuracy (5, 12). As a result of the absence of data upon the volumetric or phase behavior of mixtures of hydrogen and cyclohexane, an investigation was started nearly a decade ago to establish the composition of the coexisting phases of mixtures of hydrogen and cyclohexane at pressures up to 10,000 p.s.i.a.

Table I. Experimental Volumetric Measurements
Pressure, Volume, Pressure, Volume, Pressure, Volume, Pressure, Volume, P.S.I.A. $\mathrm{Cu} . \mathrm{Ft} . / \mathrm{Lb} . \quad$ P.S.I.A. Cu . Ft./Lb. P.S.I.A. $\mathrm{Cu} . \mathrm{Ft} . / \mathrm{Lb} . \quad$ P.S.I.A. Cu . Ft./Lb

| $100^{\circ} \mathrm{F}$. |  |
| :---: | :---: |
| (1855) ${ }^{\text {a }}$ |  |
| 100.8 | 0.062144 |
| 1052.3 | 0.023090 |
| 1320.0 | 0.022119 |
| 1635.4 | 0.021538 |
| 1860.98 | 0.021177 |
| 2065.2 | 0.021037 |
| 2328.1 | 0.020983 |
| 2664.9 | 0.020924 |
| 3001.6 | 0.020813 |
| 4858.2 | 0.020390 |

Mole Fraction Hydrogen 0.0502

| (1610) |  | (1350) |  | (1080) |  |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 1339.7 | 0.022490 | 144.21 | 0.063821 | 189.8 | 0.062746 |
| 1461.0 | 0.022260 | 832.6 | 0.025540 | 851.6 | 0.026303 |
| 1501.8 | 0.022150 | 995.2 | 0.024467 | 1012.6 | 0.025064 |
| 1531.7 | 0.022000 | 1161.1 | 0.023657 | 1063.2 | 0.024760 |
| 1633.9 | 0.021922 | 1214.6 | 0.023492 | 1099.0 | 0.024483 |
| 2014.4 | 0.021802 | 1309.7 | 0.023151 | 1202.7 | 0.024349 |
| 3114.2 | 0.021508 | 1418.2 | 0.023031 | 1311.5 | 0.024270 |
| 4021.8 | 0.021419 | 1515.6 | 0.022980 | 1535.8 | 0.024154 |
| 4855.2 | 0.021338 | 1630.6 | 0.022915 | 1815.4 | 0.024015 |
|  |  | 2049.6 | 0.022783 | 2528.7 | 0.023697 |
| 933.9 | 0.02416 | 3018.1 | 0.022505 | 3484.5 | 0.023335 |
| 1077.1 | 0.023502 | 4074.9 | 0.022237 | 4635.5 | 0.02 .5021 |
| 1235.9 | 0.022943 | 4887.6 | 0.022099 |  |  |
| 1370.9 | 0.022504 |  |  |  |  |
| 1731.3 | 0.021927 |  |  |  |  |
| 1850.0 | 0.021892 |  |  |  |  |
| 1957.6 | 0.021842 |  |  |  |  |
| 2069.2 | 0.021792 |  |  |  |  |
| 2318.8 | 0.021764 |  |  |  |  |
| 2454.1 | 0.021719 |  |  |  |  |
| 2554.0 | 0.021657 |  |  |  |  |
| 3018.3 | 0.021485 |  |  |  |  |
| 3601.8 | 0.021375 |  |  |  |  |
| 4082.1 | 0.021385 |  |  |  |  |
| 4594.1 | 0.021332 |  |  |  |  |
| 4875.6 | 0.021325 |  |  |  |  |

$(5290)^{a}$

| $(5290)$ |  |
| ---: | ---: |
| 118.0 | 0.120469 |
| 265.7 | 0.063455 |
| 1470.0 | 0.027009 |
| 1904.4 | 0.025104 |
| 2010.3 | 0.024766 |
| 3007.8 | 0.022867 |
| 3397.7 | 0.022339 |
| 3831.6 | 0.022010 |
| 4102.8 | 0.021778 |
| 4446.1 | 0.021598 |
| 4659.3 | 0.021555 |
| 4816.9 | 0.021423 |
| 4998.4 | 0.021376 |
| 5194.6 | 0.021248 |
| 5345.2 | 0.021130 |
| 5532.3 | 0.021056 |
| 6027.3 | 0.021090 |
| 7096.8 | 0.020947 |
| 7702.0 | 0.020966 |

Mole Fraction Hydrogen 0.1338

| $(4482)$ |  |  |  |
| ---: | ---: | ---: | ---: |
| 279.2 | 0.067259 | 349.8 | 0.063327 |
| 1637.8 | 0.027115 | 1203.3 | 0.031308 |
| 2639.7 | 0.024033 | 1464.3 | 0.029043 |
| 3535.3 | 0.022846 | 2027.0 | 0.026311 |
| 3738.6 | 0.022659 | 2662.2 | 0.024602 |
| 3912.9 | 0.022498 | 3038.7 | 0.023901 |
| 4012.7 | 0.022399 | 3243.3 | 0.023575 |
| 4112.2 | 0.022327 | 3406.0 | 0.023384 |
| 4209.1 | 0.022242 | 3512.1 | 0.023297 |
| 4329.0 | 0.022187 | 3623.3 | 0.023183 |
| 4516.0 | 0.022086 | 3763.1 | 0.023115 |
| 4985.7 | 0.022019 | 3886.6 | 0.023088 |
| 5990.1 | 0.021867 | 4161.4 | 0.023012 |
| 6921.7 | 0.021734 | 4988.9 | 0.022830 |
| 7479.1 | 0.021665 | 6094.5 | 0.022636 |
|  |  | 7099.1 | 0.022470 |
|  |  | 7415.9 | 0.022374 |

(3010)

| 1021.0 | 0.035382 |
| :--- | :--- |
| 1436.3 | 0.030509 |
| 1923.9 | 0.027575 |
| 2332.1 | 0.026069 |
| 2504.8 | 0.025569 |
| 2618.1 | 0.025261 |
| 2717.7 | 0.025061 |
| 2822.2 | 0.024847 |
| 3033.2 | 0.024548 |
| 3228.5 | 0.024455 |
| 3408.3 | 0.024377 |
| 3508.1 | 0.024317 |
| 4035.1 | 0.024138 |
| 5133.8 | 0.023771 |
| 5970.3 | 0.023543 |
| 7010.3 | 0.023299 |

in the temperature interval between $100^{\circ}$ and $280^{\circ} \mathrm{F}$. In addition, a limited study of the volumetric behavior of mixtures of hydrogen and cyclohexane in the liquid phase has been made. This latter work was carried out within the composition interval between pure cyclohexane and 0.022 mole fraction hydrogen. The latter data were employed to establish the bubble-point pressures of these mixtures throughout the above-described range of temperature and pressure.

## METHODS AND APPARATUS

The equipment employed in determining the volumetric behavior of this system has been described ( 9 ). In principle, it consists of a stainless steel cylinder in which the hydrocarbon and hydrogen were confined over mercury. Mechanical agitation within the chamber was provided and this chamber was immersed in an agitated oil bath. The samples were withdrawn from the gas phase under isobaric, isothermal conditions, and the quantity of cyclohexane present was determined by partial condensation techniques (7). A description of the apparatus used for the gas phase withdrawals is available (10).

Determination of the compositions of the liquid phase by direct analysis was not attempted because of the relatively small amount of hydrogen present in the liquid phase at the lower pressures. For this reason, the discontinuous change in slope of the specific volume-pressure diagram was employed as a means of determining the bubble-point pressure for a system
of known composition. The equipment employed for these measurements has been described (9). In principle, this equipment was similar to that used for confining the samples for the composition of the coexisting phases. Gravimetric techniques were employed for the introduction of the cyclohexane, and the quantity so introduced was also established from limited volumetric measurements upon the pure cyclohexane. Hydrogen was introduced utilizing volumetric methods to establish the quantity so introduced. The quantity of cyclohexane employed probably was known within $0.15 \%$, while the quantity of hydrogen was known within $0.25 \%$ of the total quantity added. Mechanical agitation was provided to permit the attainment of physical equilibrium.

The pressures for both the composition of the coexisting gas phase and the volumetric measurements were determined by means of a balance involving a piston-cylinder combination (9). Calibration of this instrument over a period of two decades against the vapor pressure of carbon dioxide at the ice point (3) has indicated a probable uncertainty in the measured values of the pressure of $0.15 \%$ or 0.1 p.s.i., whichever is the larger measure of uncertainty. Temperature was determined by means of a strain-free platinum resistance thermometer. Its indications were compared against those of a similar instrument calibrated by the National Bureau of Standards. The temperature for both the gas-phase composition and volumetric measurements was known relative to the international platinum scale within $0.02^{\circ} \mathrm{F}$. throughout the temperature interval between $100^{\circ}$ and $280^{\circ} \mathrm{F}$.

| Table I. Experimental Volumetric Measurements (Continued) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pressure, P.S.I.A. | Volume, $\mathrm{Cu} . \mathrm{Ft} . / \mathrm{Lb}$. | Pressure, P.S.I.A. | Volume, Cu. Ft./Lb. | Pressure, P.S.I.A. | Volume, $\mathrm{Cu} . \mathrm{Ft} . / \mathrm{Lb}$ | Pressure, P.S.I.A. | Volume, Cu. Ft./Lb. |
| $100^{\circ} \mathrm{F}$. |  | $160^{\circ} \mathrm{F}$. |  | $220^{\circ} \mathrm{F}$. |  | $280^{\circ} \mathrm{F}$. |  |
| Mole Fraction Hydrogen 0.2203 |  |  |  |  |  |  |  |
| $(9520)^{\text {a }}$ |  | (7769) |  | (6605) |  | (5610) |  |
| 473.4 | 0.063006 | 446.2 | 0.072015 | 600.2 | 0.063497 | 543.6 | 0.062498 |
| 1431.7 | 0.033810 | 1316.3 | 0.037015 | 1688.1 | 0.034654 | 698.0 | 0.049446 |
| 5328.2 | 0.023215 | 2336.4 | 0.029254 | 2733.1 | 0.028751 | 1429.1 | 0.039512 |
| 6270.3 | 0.022606 | 4420.9 | 0.024573 | 3759.0 | 0.026193 | 2356.8 | 0.031399 |
| 6752.9 | 0.022362 | 5616.1 | 0.023525 | 4741.0 | 0.024777 | 3415.6 | 0.027646 |
| 7185.6 | 0.022224 | 6461.0 | 0.023010 | 5544.0 | 0.023996 | 4379.3 | 0.025823 |
| 7609.6 | 0.022071 | 7082.4 | 0.022703 | 6015.1 | 0.023713 | 5242.9 | 0.024825 |
| 8056.1 | 0.021931 | 7489.2 | 0.022520 | 6432.5 | 0.023501 | 5353.1 | 0.024770 |
| 8318.4 | 0.021816 | 7726.9 | 0.022453 | 6547.9 | 0.023460 | 5427.0 | 0.024698 |
| 8546.7 | 0.021802 | 7843.4 | 0.022412 | 6629.9 | 0.023416 | 5496.9 | 0.024651 |
| 8707.5 | 0.021780 | 7900.1 | 0.022406 | 6850.1 | 0.023375 | 5597.1 | 0.024582 |
| 8809.3 | 0.021738 | 8015.2 | 0.022368 | 6946.4 | 0.023360 | 5908.3 | 0.024537 |
| 8932.6 | 0.021712 | 8155.9 | 0.022354 | 7088.7 | 0.023320 | 7074.5 | 0.024212 |
| 9402.3 | 0.021606 | 8315.5 | 0.022333 | 7276.3 | 0.023273 | 4082.5 | 0.026257 |
| 9545.5 | 0.021568 | 8586.2 | 0.022284 | 8162.5 | 0.023137 | 4607.8 | 0.025505 |
| 9770.9 | 0.021540 | 9034.0 | 0.022229 | 9097.4 | 0.022978 | 4884.7 | 0.025127 |
| 9938.3 | 0.021536 | 9133.4 | 0.022215 | 9559.1 | 0.022939 | 5029.3 | 0.024952 |
| 475.2 | 0.063198 | 9617.0 | 0.022144 | 9807.0 | 0.022901 | 5107.3 | 0.024905 |
| 655.6 | 0.050915 | 9711.0 | 0.022149 |  |  | 6121.3 | 0.024467 |
| 4214.3 | 0.024124 |  |  |  |  | 7234.5 | 0.024191 |
| 6227.5 | 0.022615 |  |  |  |  | 8001.3 | 0.023983 |
| 7181.3 | 0.022235 |  |  |  |  | 9010.8 | 0. 123792 |
| 8149.2 | 0.021890 |  |  |  |  | 9282.4 | 0.023755 |
| 8676.3 | 0.021775 |  |  |  |  |  |  |
| 8968.4 | 0.021690 |  |  |  |  |  |  |
| 9024.1 | 0.021668 |  |  |  |  |  |  |
| 9153.8 | 0.021616 |  |  |  |  |  |  |
| 9259.4 | 0.021547 |  |  |  |  |  |  |
| 9301.8 | 0.021552 |  |  |  |  |  |  |
| 9421.5 | 0.021484 |  |  |  |  |  |  |
| 9440.4 | 0.021473 |  |  |  |  |  |  |
| 9575.2 | 0.021461 |  |  |  |  |  |  |
| 9887.8 | 0.021422 |  |  |  |  |  |  |
| 9958.4 | 0.021415 |  |  |  |  |  |  |
| ${ }^{\text {a }}$ Values in parentheses represent bubble-point pressures expressed in p.s.i.a. |  |  |  |  |  |  |  |



Figure 1. Experimental volumetric measurements at $220^{\circ} \mathrm{F}$.

The investigation was not extended to higher temperatures because of thermal rearrangement of the cyclohexane at temperatures significantly in excess of $280^{\circ} \mathrm{F}$. This occurred at a sufficiently rapid rate as to render either volumetric or phase composition measurements of questionable accuracy. It was not feasible to extend the measurements to lower temperatures because of the proximity of the freezing point of cyclohexane (1).
The analytical techniques yielded a reproducibility of the order of 0.0002 mole fraction and the uncertainty in measurement appears to be of the order of 0.001 mole fraction. Throughout the range of temperatures and pressures covered in this investigation, the volumetric measurements in the liquid phase are believed to involve uncertainties of the order of $0.02 \%$ and the bubble-point pressures were established with a precision of 0.5 p.s.i.

## MATERIALS

The cyclohexane was obtained as research grade from the Phillips Petroleum Co., which reported it to contain less than 0.0006 mole fraction of impurities. The hydrocarbon was dried over metallic sodium and solidified at liquid nitrogen temperatures and maintained at a relatively high vacuum for an extended period to aid in the removal of noncondensable gases. The specific weight at $77^{\circ} \mathrm{F}$. and atomospheric pressure was 48.307 pounds per cubic foot for an air-free sample as compared with a value of 48.311 pounds per cubic foot reported (1) for an air-saturated sample at the same temperature. The index of refraction relative to the $D$-lines of sodium at $77^{\circ} \mathrm{F}$. was 1.42355 as compared with a value of 1.42354 reported for an airsaturated sample (1). The material used in this investigation contained less than 0.002 mole fraction of impurities and these impurities are probably hydrocarbons containing six carbon atoms per molecule.
The hydrogen, obtained from a commerical manufacturer who had prepared it by electrolytic techniques, was reported to contain 0.00002 mole fraction of oxygen and 0.001 mole fraction of materials other than hydrogen and water. The gas was passed through a coil immersed in liquid nitrogen, through a chamber containing platinum wire heated to approximately $800^{\circ} \mathrm{F}$., and again through a second coil immersed in liquid nitrogen. This treatment was followed by contact with anhydrous calcium sulfate and activated charcoal at pressures in excess of 500 p.s.i. A mass spectrographic analysis of the purified hydrogen indicated it to contain less than 0.0014 mole fraction of materials other than hydrogen.


Figure 2. Pressure-composition diagram for bubble point

## EXPERIMENTAL RESULTS

Measurements of the volumetric behavior of three mixtures of hydrogen and cyclohexane were made at pressures up to $10,000 \mathrm{p}$.s.i.a. A sample of the experimental results at $220^{\circ} \mathrm{F}$. is presented in Figure 1. The information shown in this figure is typical of that obtained at the other three temperatures investigated. The corresponding values of the specific volume of cyclohexane have been included. Results of these volumetric measurements are recorded in Table I for each of the three mixtures investigated experimentally. The bubble-point pressures obtained from the isothermal discontinuities are also included in this table.
Figure 2 shows the bubble-point pressure of the hydrogencyclohexane system as a function of mole fraction hydrogen for temperatures between $100^{\circ}$ and $280^{\circ} \mathrm{F}$. The corresponding values from the work of Thompson and Edmister (11) have been included. The curvature shown in Figure 2 for the $150^{\circ} \mathrm{F}$. isotherm results from following the experimental points of Thompson. The experimentally determined compositions of the dew-point gas are set forth in Table II for each temperature of measurement.

| Table II. Composition of Gas Phase in Heterogeneous System |  |  |  |
| :---: | :---: | :---: | :---: |
| Pressure, | Mole Fraction | Pressure, | Mole Fraction |
| P.S.I.A | Hydrogen | P.S.I.A. | Hydrogen |
| $100^{\circ} \mathrm{F}$ |  | $220^{\circ} \mathrm{F}$ |  |
| 30.0 | 0.9113 | 249.5 | 0.8742 |
| 81.3 | 0.9585 | 507.4 | 0.9341 |
| 249.3 | 0.9852 | 1004.0 | 0.9626 |
| 898.4 | 0.9952 | 2012.5 | 0.9762 |
| 2740.7 | 0.9958 | 2725.8 | 0.9799 |
| 3292.8 | 0.9966 | 4318.5 | 0.9823 |
| 5470.2 | 0.9976 | 6086.5 | 0.9836 |
| 7857.9 | 0.9957 | 8157.8 | 0.9834 |
|  | $160^{\circ} \mathrm{F}$. |  | $280^{\circ} \mathrm{F}$. |
| 205.8 | 0.9433 | 779.2 | 0.8993 |
| 450.3 | 0.9717 | 1604.4 | 0.9420 |
| 986.4 | 0.9850 | 3063.8 | 0.9606 |
| 1989.8 | 0.9900 | 6154.2 | 0.9680 |
| 1993.0 | 0.9901 | 7158.9 | 0.9681 |
| 4030.7 | 0.9917 | 9531.7 | 0.9684 |
| 6146.9 | 0.9920 |  |  |
| 9280.0 | 0.9920 |  |  |

Table III. Some Properties of the Coexisting Phases

| Pressure, P.S.I.A. | Mole Fraction Hydrogen |  | Equilibrium Ratio |  | Volume Cu. Ft./Lb. Mole Bubble Point |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dew point | Bubble point | Hydrogen | Cyclohexane |  |
|  | $100^{\circ} \mathrm{F}$. |  |  |  |  |
| $3.2{ }^{\text {a }}$ | 0.0000 | 0.0000 |  | 1.00000 | 1.775 |
| 500 | 0.9921 | 0.0135 | 73.58 | 0.00800 | $1.748^{\text {b }}$ |
| 1000 | 0.9949 | 0.0269 | 37.00 | 0.00526 | 1.724 |
| 1500 | 0.9964 | 0.0400 | 24.89 | 0.00373 | 1.700 |
| 2000 | 0.9969 | 0.0530 | 18.80 | 0.00330 | 1.678 |
| 2500 | 0.9970 | 0.0658 | 15.16 | 0.00320 | 1.656 |
| 3000 | 0.9971 | 0.0784 | 12.72 | 0.00313 | 1.635 |
| 3500 | 0.9972 | 0.0906 | 11.00 | 0.00302 | 1.615 |
| 4000 | 0.9973 | 0.1028 | 9.703 | 0.00300 | 1.598 |
| 4500 | 0.9973 | 0.1145 | 8.711 | 0.00309 | 1.578 |
| 5000 | 0.9972 | 0.1260 | 7.914 | 0.00324 | 1.560 |
| 6000 | 0.9970 | 0.1480 | 6.736 | 0.00348 | 1.525 |
| 7000 | 0.9967 | 0.1692 | 5.891 | 0.00401 | 1.492 |
| 8000 | 0.9960 | 0.1893 | 5.261 | 0.00496 | 1.462 |
|  | $160^{\circ} \mathrm{F}$. |  |  |  |  |
| $10.9{ }^{\text {a }}$ | 0.0000 | 0.0000 |  | 1.0000 | 1.851 |
| 500 | 0.9734 | 0.0157 | 61.97 | 0.0270 | $1.821^{\text {b }}$ |
| 1000 | 0.9851 | 0.0316 | 32.00 | 0.0153 | 1.791 |
| 1500 | 0.9888 | 0.0473 | 20.91 | 0.0119 | 1.762 |
| 2000 | 0.9903 | 0.0627 | 15.80 | 0.0104 | 1.735 |
| 2500 | 0.9912 | 0.0774 | 12.80 | 0.00956 | 1.709 |
| 3000 | 0.9915 | 0.0927 | 10.70 | 0.00933 | 1.683 |
| 3500 | 0.9919 | 0.1068 | 9.286 | 0.00911 | 1.660 |
| 4000 | 0.9920 | 0.1215 | 8.163 | 0.00912 | 1.635 |
| 4500 | 0.9920 | 0.1357 | 7.311 | 0.00924 | 1.613 |
| 5000 | 0.9920 | 0.1494 | 6.639 | 0.00944 | 1.591 |
| 6000 | 0.9920 | 0.1760 | 5.637 | 0.00972 | 1.550 |
| 7000 | 0.9919 | 0.2020 | 4.910 | 0.00102 | 1.511 |
| 8000 | 0.9918 | 0.2273 | 4.374 | 0.0106 | 1.47 |
| 9000 | 0.9917 | 0.2520 | 3.936 | 0.0111 |  |
|  | $220^{\circ} \mathrm{F}$. |  |  |  |  |
| $28.4{ }^{\text {a }}$ | 0.0000 | 0.0000 |  | 1.0000 | 1.945 |
| 1500 | 0.9350 | 0.0189 | 49.42 | 0.0662 | $1.906^{\text {b }}$ |
| 1000 | 0.9622 | 0.0384 | 25.18 | 0.0393 | 1.868 |
| 500 | 0.9716 | 0.0574 | 16.93 | 0.0301 | 1.832 |
| 2000 | 0.9763 | 0.0760 | 12.84 | 0.0257 | 1.797 |
| 2500 | 0.9789 | 0.0941 | 10.40 | 0.0233 | 1.764 |
| 3000 | 0.9804 | 0.1119 | 8.762 | 0.0221 | 1.733 |
| 3500 | 0.9815 | 0.1281 | 7.660 | 0.0212 | 1.704 |
| 4000 | 0.9822 | 0.1446 | 6.792 | 0.0208 | 1.676 |
| 4500 | 0.9827 | 0.1599 | 6.144 | 0.0206 | 1.649 |
| 5000 | 0.9830 | 0.1758 | 5.593 | 0.0207 | 1.623 |
| 6000 | 0.9832 | 0.2058 | 4.777 | 0.0211 | 1.574 |
| 7000 | 0.9834 | 0.2362 | 4.163 | 0.0217 | 1.53 |
| 8000 | 0.9835 | 0.2644 | 3.719 | 0.0225 | 1.53 |
| 9000 | 0.9832 | ... | ... | ... | ... |
|  | $280^{\circ} \mathrm{F}$. |  |  |  |  |
| $62.0{ }^{\text {a }}$ | 0.0000 | 0.0000 |  | 1.000 | 2.055 |
| 500 | 0.8582 | 0.0224 | 38.26 | 0.145 | 2.0096 |
| 1000 | 0.9196 | 0.0466 | 19.61 | 0.0843 | 1.962 |
| 1500 | 0.9402 | 0.0697 | 13.48 | 0.0643 | 1.917 |
| 2000 | 0.9503 | 0.0914 | 10.41 | 0.0547 | 1.873 |
| 2500 | 0.9564 | 0.1118 | 8.556 | 0.0491 | 1.834 |
| 3000 | 0.9603 | 0.1340 | 7.248 | 0.0458 | 1.793 |
| 3500 | 0.9630 | 0.1505 | 6.400 | 0.0435 | 1.759 |
| 4000 | 0.9651 | 0.1673 | 5.721 | 0.0419 | 1.725 |
| 4500 | 0.9664 | 0.1858 | 5.202 | 0.0412 | 1.691 |
| 5000 | 0.9673 | 0.2020 | 4.789 | 0.0410 | 1.659 |
| 6000 | 0.9681 | 0.2343 | 4.148 | 0.0417 | 1.598 |
| 7000 | 0.9681 | 0.2652 | 3.633 | 0.0434 | 1.55 |
| 8000 | 0.9683 | 0.2919 | 3.244 | 0.0442 | , |
| 9000 | 0.9684 | - |  | . | $\ldots$ |

- Vapor pressure of cyclohexane.
${ }^{\text {b }}$ Bubble-point volumes are estimated and subject to larger uncertainties.


Figure 3. Composition of coexisting gas phase


Figure 4. Equilibrium ratios for hydrogen and cyclohexane

Figure 3 depicts the experimentally determined composition of the coexisting gas phase in samples of heterogeneous mixtures of hydrogen and cyclohexane. A number of duplicate measurements were made, and these yielded a degree of agreement which would not permit the points to be differentiated from those shown on the diagram. The standard error of estimate of the experimental points from the smooth curves was 0.0007 mole fraction, assuming all of the uncertainty in the composition and none in the measured values of pressure and temperature. Following conventional smoothing techniques, the compositions
of the coexisting phases in the hydrogen-cyclohexane system have been evaluated and are presented for even values of pressure and temperature in Table III. Included also are the equilibrium ratios for hydrogen and cyclohexane. As a result of the number of significant figures reported for dew-point gas compositions, some discrepancies in the tabulated values of the equilibrium ratio for cyclohexane, computed from the compositions, may exist. In the upper part of Figure 4 is shown the product of the pressure and the equilibrium ratio, $P K_{k}$, for hydrogen in the hydrogen-cyclohexane system. These data were compared with similar information based upon the measurements of Thompson and Edmister (11) and a comparison has been indicated in the upper part of Figure 4. The quantity $P y_{j} / P^{\prime \prime}{ }_{j}$ has been used to portray the phase behavior of cyclohexane and is shown in the lower part of Figure 4. In this expression $P$ is the pressure, $y_{j}$ is the mole fraction of cyclohexane in the gas phase, and $P^{\prime \prime}{ }_{j}$ is the vapor pressure of cyclohexane. In the case of relatively nonvolatile materials such a function yields a smaller variation with respect to state than the use of the more conventional equilibrium ratio. In the lower part of Figure 4 the measurements of Thompson and Edmister (11) are shown for comparison.

The current measurements and those of Thompson and Edmister (11) appear to agree within an uncertainty in mole fraction of approximately 0.0066 in the gas phase and 0.0083 in the liquid phase for temperatures of $150^{\circ}$ and $250^{\circ} \mathrm{F}$. The current investigation extended over a sufficiently limited range of temperatures so as not to permit the evaluation of the behavior at higher temperatures approaching the critical state of cyclohexane.

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