### NOMENCLATURE

- $n_{25}$  = ethane-*n*-pentane system, mole fraction
- $n_{27}$  = ethane-*n*-heptane system, mole fraction
- *n*-pentane-*n*-heptane system, mole fraction  $n_{\rm M} =$
- $n_{257}$  = ethane-*n*-pentane-*n*-heptane system, mole fraction
- $P_{c}$ = critical pressure, p.s.i.a.
- = critical temperature,  $^{\circ}$  R. or  $^{\circ}$  F.  $T_{c}$  $T_c^{\prime}$
- = pseudocritical temperature, ° R.

### Subscripts

2, 5, 7 = specific components of mixture

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## **High Temperature Properties of Potassium**

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A virial equation of state for potassium with coefficients through the fourth virial is derived from PVT data covering a temperature range from 1600 $^\circ$  to 2525 $^\circ$  F. The equation is used thermodynamically to obtain superheat and saturation properties of the vapor. Values of the enthalpy, entropy, specific volume, and specific heat for some 200 selected states are tabulated in the temperature range from 1400 $^\circ$  to 2500° F., and in the pressure range from 2.9 to 499.3 p.s.i.a.

 $m \Gamma$ HE ALKALI METALS are being considered as thermodynamic working fluids in advanced power converters, and reliable values of their properties are required. The existing thermodynamic properties for alkali metal vapors have been calculated in most cases from spectroscopic data, vaporpressure data, and published thermodynamic functions. The agreement among the calculated properties for a given metal is poor and not acceptable. The principal objective at NRL was to determine experimentally for a wide temperature range the important thermodynamic properties of three metal vapors-sodium, potassium, and cesium. This was to be achieved by a thermodynamic reduction of pressure-volume-temperature data. The PVT measurements for each metal to 2500° F. have now been published. This article, the fourth in the series, describes the thermodynamic treatment of the potassium PVT data and presents the first thermodynamic properties of this metal derived directly from measured compressibilities.

### TREATMENT OF PVT DATA

Methods. Spectroscopic studies (4) have shown that the vapor of an alkali metal contains molecular species with two or more atoms. For a strongly associating vapor, such as that of potassium, the important properties-enthalpy, entropy, and specific heat-may be reduced from PVT data by either of two methods. In the first, the gas is treated as a monatomic assembly with all apparent imperfections given by a virial equation of state, and the thermodynamic quantities are obtained as corrections to those of the monatomic gas in terms of the virial coefficients. In the second method, equilibrium constants are derived for the molecular reactions by treating the gas as a mixture of molecular species, and the thermodynamic quantities are derived from the enthalpy changes associated with changes in the molecular composition of the vapor. The latter method, commonly called the quasichemical, generally assumes that all species behave as perfect gases.

While the two methods should be effectively equivalent from the standpoint of obtaining the three propertiesenthalpy, entropy, and specific heat-a higher degree of confidence was placed in the well-established thermodynamic relationships of the virial method. The virial equation of state for potassium with coefficients through the fourth virial was obtained from the raw PVT data and used to compute enthalpy, entropy, specific volume, and specific heat of potassium vapor.

Derivation of Virial Coefficients. The virial equation of state in the volume expansion form,

$$\frac{p\,\tilde{V}}{RT} = A + \frac{B}{\tilde{V}} + \frac{C}{\tilde{V}^2} + \frac{D}{\tilde{V}^3} + \dots$$
(1)

was chosen for this analysis, and the four coefficients are commonly called the first, second, third, and fourth virial. With this form of the equation, the first virial coefficient theoretically should be unity.

The virial coefficients are temperature-dependent and were derived graphically by plotting functions along constant temperature lines. Compressibility data at 50° temperature intervals were obtained from large-scale plots of the observed data for the nine experiments reported by Stone et al. (9). Virial coefficients were obtained from these data by a procedure similar to that devised by Hirschfelder, McClure, and Weeks (7). The second virial coefficient at each temperature was obtained as the  $\lim [(z-1)\bar{V}]_{(1/\bar{V}=0)}$ , the third virial as the lim  $Q_{(1/V \rightarrow 0)}$  where Q is defined as  $[(z-1)\tilde{V}-B]\tilde{V}$ , and the fourth virial as  $dQ/d(1/\tilde{V})$ .

It was noted from preliminary plots of z vs.  $1/\bar{V}$  for isotherms covering the temperature range that the deviations of observed compressibility factors from fitted curves were larger for the experiments at low pressures (up to 0.4%) than for those at high pressures (generally less than 0.2%). In addition, the magnitude and sign of the deviation for each experiment were relatively independent of temperature. This behavior can be explained. Nine experiments were used to generate the compressibility data for potassium (9). For each of these, pressure was observed as a function of temperature for a given weight of potassium vapor in a constant-volume chamber. Since the larger and principal uncertainties in the low-pressure experiments were generated in the measurement of two temperature-independent quantities (the volume of the chamber and the weight of potassium), the systematic deviations for these experiments were not unexpected.

A knowledge of this systematic behavior was used to help define the temperature dependency of the virial coefficients at lower temperatures. The procedure required the selection of a reference isotherm having the maximum pressure range of the observed compressibility factor in order to obtain the maximum definition of the virial coefficients. Accordingly, a reference temperature of 2450° F. was selected. The compressibility factor, z, at this temperature was plotted as a function of  $1/\tilde{V}$ , and the second virial coefficient was obtained as the  $\lim \left[ dz/d(1/\tilde{V}) \right]_{(1/\tilde{V}-0)}$ . Also,  $(z-1)\tilde{V}$  was plotted as a function of  $1/\tilde{V}$  and another value of B was obtained as the lim  $[(z-1)V]_{(1/V \rightarrow 0)}$ . The most consistent value of B obtained by both procedures was -18.447. Using the value, function Q was calculated and plotted against  $1/\tilde{V}$  (Figure 1) and the best linear curve was obtained by least squares, giving greater weight to the higher pressure data. From the deviation of an experimental Q at  $2450^{\circ}$  F. from the linear curve, the multiplying factor to z required to correct Q to the curve may be computed. Assuming the errors in the five low-pressure experiments to be largely systematic, adjusted compressibility quantities (identified as  $z^*$  or  $Q^*$ ) were derived for each experiment at all temperatures with the multiplying factor obtained at 2450° F.

Second virial coefficients were obtained from large-scale plots of  $(z - 1)\tilde{V}$  vs.  $1/\tilde{V}$  for isotherms at 50° intervals between 2000° and 2550° F. For the five low-pressure experiments, adjusted values,  $(z^* - 1)\tilde{V}$ , were included on each plot and were given weight in defining the intercepts at lower temperatures. Third and fourth virial coefficients were obtained by plotting the quantity Q vs.  $1/\tilde{V}$  for isotherms at 50° intervals between 2150° and 2550° F. The adjusted values of  $Q^*$  for the low-pressure experiments were, likewise, included on each plot and given weight in defining the intercepts and slopes at lower temperatures. Additional second virial coefficients in the lower temperature range from 1600° to 1950° F. were obtained by computing the average value of  $[(z - 1)\tilde{V} - C/\tilde{V} - D/\tilde{V}^2]$  for the lower pressure experiments on each isotherm. The values of C and D required for these calculations were obtained by extrapolation.

Figure 1 gives a plot of Q vs.  $1/\tilde{V}$  at  $2450^{\circ}$  F. for the several experiments which were effective in defining the higher virial coefficients. The vertical line for each Q represents the expected probable error in the quantity. Though the corresponding error in z is normally around 0.20%, that in Q becomes increasingly larger at low pressures (low values of  $1/\tilde{V}$ ) as z approaches unity. This figure may be used to illustrate the adjustment procedure, which was particularly helpful in defining the higher virial coefficients at lower temperatures where the definition provided by the higher pressure data is missing. For example, at 2200° F. the virials had to be determined from data corresponding to that for the five lower pressure experiments in Figure 1. Since errors are systematic with respect to the individual experiments, the relative point spread of the data for the five experiments at 2200° F. is the same as that shown at 2450° F. One could proceed at this temperature to weight the points and to



Figure 1. Plot of Q vs. 1/V for potassium at 2450° F.

define C and D by a least squares curve. However, when the adjusted values of  $(Q^*)$  are plotted, a linear curve is defined which is of somewhat lower slope than that obtained by the least squares fit. The curve with the lower slope should be more correct, since it incorporates information from the data at higher temperatures where greater definition is provided by the several experiments at higher pressures.

Virial Equation of State of Potassium. Since the virial coefficients are functions of equilibrium constants (17), it is not surprising that each coefficient can be represented for the full temperature range with simple exponential equations. The virial equation of state of potassium is

$$\frac{p\,\tilde{V}}{R\,T} = 1 + \frac{B}{\tilde{V}} + \frac{C}{\tilde{V}^2} + \frac{D}{\tilde{V}^3} \tag{2}$$

where

The log T term was included in the equation for the second virial coefficient, since this term can be derived directly from the relationship between the dimerization equilibrium constant and B (17).

The fit of the virial equation to observed data is shown graphically in Figure 2, where compressibility isotherms generated from Equation 2 are compared to experimental compressibilities at 100° intervals from 1600° to 2500° F. All the observed compressibility data for potassium as reported by Stone *et al.* (9) may be calculated from the virial equation with a standard per cent deviation of  $\pm 0.34$ .

The virial equation of state was effectively derived from experimental data over the temperature range from  $2000^{\circ}$ to  $2525^{\circ}$  F. Data were also obtained from  $1600^{\circ}$  to  $2000^{\circ}$  F., but the number of experimental points in this region did not permit one to obtain reliable coefficients by the graphical method. Consequently, before the virial equation was acceptable for calculations below  $2000^{\circ}$  F., it was necessary



Figure 2. Compressibility of potassium vapor at several temperatures

to determine its fit to the observed lower temperature data. At temperatures and pressures corresponding to observed low-temperature points, compressibility factors were calculated and compared to the observed values. The fit of the virial equation of state to the low-temperature data is illustrated in Figure 2, and found to be equivalent to that obtained at higher temperatures.

# FUNDAMENTAL PROPERTIES ON WHICH THERMODYNAMIC PROPERTIES ARE BASED

Saturation Pressure of Liquid Potassium. The vapor-pressure equation of Stone et al. (10) was chosen, since this equation,

$$\log p = 7.30625 - 8135.3/T - 0.53560 \log T \tag{3}$$

was based on experimentally determined data over the temperature range from the normal boiling point to  $2400^{\circ}$  F. and is in good agreement with the lower temperature work of Walling, Nuzum, and Lemmon (15) and Makansi *et al.* (8).

Specific Volume of Liquid Potassium. The specific volume of the condensed phase was obtained from the equation,

$$\frac{1}{v^{\prime}} \approx 52.768 - 7.4975 \times 10^{-3}t - 0.5255 \times 10^{-6}t^2 + 0.0498 \times 10^{-9}t^3$$
(4)

which was derived from the observed data of Stone *et al.* and other investigators (11). The error limit given for the equation was  $\pm 0.6\%$  for the full temperature range from the melting point to 2300° F.

Enthalpy and Entropy of Liquid Potassium. The thermodynamic properties presented in this report are based on the properties of the monomeric gas at 1 atm., but comparison calculations were made using the properties of the saturated liquid as a starting point. The enthalpy and



Figure 3. Specific heat of liquid potassium

entropy of the liquid (relative to the solid at  $0^{\circ}\,R.)$  were computed with

 $h_s^{l} = 87.8783 + 0.2022 t - 0.2177 \times 10^{-4} t^2 + 0.07741 \times 10^{-7} t^3$  (5)

 $s_s^l = 0.52298 \log T - 0.64848 \times 10^{-4} T +$ 

 $0.11589 \times 10^{-7} T^2 - 0.9646 \tag{6}$ 

The equations were derived directly from the work of Douglas *et al.* (2) and are based on their specific-heat equation for the solid and liquid over the temperature range from  $32^{\circ}$  to  $1472^{\circ}$  F. The enthalpy and entropy of solid potassium at  $32^{\circ}$  F. were taken from the work of Evans *et al.* (3).

The enthalpy and entropy equations were used well beyond the measured limit of the specific-heat data from which they were derived. The selection of the data of Douglas and the validity of the extrapolation of his equation are based on the following information. Three observations of the specific heat of potassium were made from heatcontent measurements at NRL in the temperature range from 1300° to 2100° F. The determinations were made in a copper-block calorimeter described by Walker. Grand, and Miller (13), and the probable error of each result is  $\pm 3\%$ . The three experimental points are compared to the data of Deem, Eldridge, and Lucks (1) and Douglas *et al.* (2) in Figure 3. The dashed curve above 1472 °F. represents a temperature extension of Douglas's data using his specificheat equation. The NRL data tend to verify this extension, while the smoothed data of Deem diverge at higher temperatures.

Enthalpy and Entropy of Vaporization of Potassium. The latent heat of vaporization was calculated with the equations,

$$\Delta h_v = J \, p_s [1274.6 / T_s - 0.036445] \left[ v_s^g - v_s^i \right] \tag{7}$$

which was derived from Equation 3 and the Clapeyron equation. The value of  $v_s^i$  at each temperature was obtained from Equation 4 and the value of  $v_s^a$  from the virial equation of state (Equation 2).

The corresponding entropy of vaporization at each saturation point was obtained by dividing the appropriate enthalpy change by the absolute temperature.

Enthalpy, Entropy, and Specific Heat of Monomeric Potassium Vapor. Relationships for these quantities in terms of temperature were derived from the tabulated properties of Evans *et al.* (3). The equations for the monomeric gas at 1 atm. (relative to the solid at  $0^{\circ}$  R.) are:

$$(h^{s})^{\circ} \approx 998.95 + 0.12700 \ T + 24.836 \ e^{-39.375 \cdot T}$$
 (8)

$$(s^s)^\circ = 0.18075 + 0.12700 \ln T + 0.7617 e^{-51.126.T}$$
 (9)

$$(c_p^s)^\circ = 0.12700 + 2.888 \ e^{-28.070.\ T}$$
 (10)

Enthalpy of Sublimation of Potassium at  $0^{\circ} R$ . The enthalpy of sublimation at  $0^{\circ} R$ . is needed to obtain Equation 8, and

its value is generally derived from vapor-pressure data. Evans analyzed the low-temperature vapor-pressure measurements existing at that time and selected a value of 21.70 mean kcal. per gram-atom which has been used in this analysis.

The virial equation of state and recent vapor-pressure measurements permit a more positive determination of the sublimation constant. As a check on the value reported by Evans, the vapor-pressure measurements of Stone *et al.* (10) were used to compute a new value. The heat of sublimation can be related to the saturation pressure, the virial coefficients, and the free-energy functions using the method outlined by Hicks (5), and the resulting relationship is

$$(\Delta H_{\theta}^{s})_{v} = -RT_{s} \left[ \frac{2B}{\tilde{V}_{s}} + \frac{3C}{2\tilde{V}_{s}^{2}} + \frac{4D}{3\tilde{V}_{s}^{3}} + \ln p_{s} - \ln \frac{p_{s}\tilde{V}_{s}}{RT_{s}} \right] - M_{1}T_{s} \left[ \frac{f^{\circ} - h_{\theta}}{T} \right]_{t}^{s}$$
(11)

The free-energy functions for the monomeric gas may be obtained from the data of Evans *et al.* (3) by using Equations 8 and 9. The free-energy functions for the liquid may be obtained from the heat-capacity data of Douglas *et al.* (2) by using Equations 5 and 6.

The functions for the liquid are accurately known to only 1500°F., but Stone *et al.* reported a number of vapor pressures at experimental temperatures below this value. Sublimation values were computed for these experimental pressures, and a value of 21.63 kcal. per gram atom (standard deviation 0.02) was obtained. Within experimental error this verifies the value of 21.70 obtained by Evans and used in this article.

**Specific Volume of Saturated and Superheated Vapor.** This property at all vapor states (Tables II and III) was computed from the virial equation of state.

Saturated specific volumes were directly observed by Stone *et al.* (9). A saturation value was obtained for each of nine *PVT* experiments by a short extrapolation of the superheated vapor curve to the true saturation curve. Specific volumes at temperatures corresponding to these extrapolated points were computed with the virial equation and exhibited an average deviation of only  $\pm 0.34\%$ . However, Stone has shown that pressures observed in the vicinity of the intersection of the saturated and superheated vapor curves may be expected to be low (9), and it is believed that saturated specific volumes obtained from the virial equation and the vapor-pressure equation are more reliable than those obtained at the intersection points.

# CALCULATION OF THERMODYNAMIC PROPERTIES OF POTASSIUM

**Basis.** The thermodynamic properties of potassium vapor were computed along constant temperature lines. Two computational paths exist for obtaining the properties. The starting point for a particular property along one path is the value of the property for the saturated liquid, and along the other path, the value of the property for the

Tabl	e I.	Comparison	of N	Aonomeric	Gas	and	Liquid	Path	Calculations
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(Virial method)

Temp	Pressure	Mon	omeric Gas	Path	Liquid Path				
° F.	P.S.I.A.	h*	S <sup>g</sup>	$C_p^{g}$	h®	S <sup>\$</sup>	$C_p^g$		
1600	29.39 14.70 2.94	$\begin{array}{c} 1211.6 \\ 1236.0 \\ 1255.6 \end{array}$	$1.095 \\ 1.140 \\ 1.230$	$\begin{array}{c} 0.260 \\ 0.193 \\ 0.140 \end{array}$	$1199.2 \\ 1223.5 \\ 1243.2$	$1.090 \\ 1.135 \\ 1.225$	$0.255 \\ 0.188 \\ 0.135$		
1800	73.48 14.70 2.94	$1213.3 \\ 1270.9 \\ 1282.9$	$1.054 \\ 1.156 \\ 1.242$	$\begin{array}{c} 0.287 \\ 0.160 \\ 0.134 \end{array}$	$1200.4 \\ 1258.0 \\ 1270.1$	$1.049 \\ 1.151 \\ 1.237$	$0.290 \\ 0.163 \\ 0.136$		
2000	$146.96 \\ 14.70 \\ 2.94$	$1219.4 \\ 1301.3 \\ 1309.3$	$1.026 \\ 1.169 \\ 1.253$	$\begin{array}{c} 0.290 \\ 0.146 \\ 0.131 \end{array}$	$1207.6 \\ 1289.5 \\ 1297.5$	$1.022 \\ 1.165 \\ 1.249$	$0.297 \\ 0.153 \\ 0.138$		
2200	249.83 146.96 14.70 2.94	$\begin{array}{c} 1231.0 \\ 1270.6 \\ 1329.6 \\ 1335.3 \end{array}$	$\begin{array}{c} 1.009 \\ 1.046 \\ 1.180 \\ 1.264 \end{array}$	$0.283 \\ 0.228 \\ 0.138 \\ 0.129$	$1220.2 \\ 1259.8 \\ 1318.9 \\ 1324.5$	$1.005 \\ 1.043 \\ 1.176 \\ 1.260$	$\begin{array}{c} 0.285 \\ 0.229 \\ 0.140 \\ 0.131 \end{array}$		
2400	$396.79 \\ 146.96 \\ 14.70 \\ 2.94$	$1240.1 \\ 1312.4 \\ 1356.9 \\ 1361.1$	0.993 1.062 1.190 1.273	0.293 0.193 0.134 0.129	$1227.4 \\ 1299.7 \\ 1344.2 \\ 1348.4$	0.989 1.057 1.186 1.269	$0.268 \\ 0.167 \\ 0.109 \\ 0.103$		

Table II. Saturation Properties of Potassium<sup>a</sup>

(Basis. h = 0 and s = 0 for solid potassium at  $0^{\circ} R$ )

t	$p_s$	U	$U_s^{g}$	$h^i$	$\Delta h_v$	$h_s^s$	$s^{\iota}$	$\Delta s_{v}$	$S_s^g$
1400.0	15.16	0.02417	30.9931	360.22	828.65	1188.87	0.6688	0.4456	1.1144
1500.0	24.64	0.02469	19.7806	380.05	813.06	1193.12	0.6792	0.4149	1.0941
1600.0	38.16	0.02523	13.2142	399.87	797.40	1197.28	0.6891	0.3871	1.0762
1700.0	56.69	0.02581	9.1829	419.62	781.93	1201.56	0.6984	0.3621	1.0604
1800.0	81.22	0.02641	6.6044	439.32	766.82	1206.14	0.7072	0.3393	1.0466
1900.0	112.76	0.02705	4.8944	459.05	752.06	1211.11	0.7157	0.3187	1.0344
2000.0	152.28	0.02772	3.7229	478.98	737.47	1216.45	0.7239	0.2998	1.0237
2100.0	200.72	0.02844	2.8962	499.37	722.68	1222.05	0.7319	0.2823	1.0143
2200.0	258.93	0.02919	2.2962	520.58	707.06	1227.64	0.7399	0.2658	1.0058
2300.0	327.66	0.02998	1.8487	543.07	689.69	1232.76	0.7481	0.2499	0.9980
2400.0	407.60	0.03083	1.5055	567.51	669.20	1236.71	0.7566	0.2340	0.9907
2500.0	499.30	0.03173	1.2328	595.08	643.12	1238.19	0.7659	0.2173	0.9832

<sup>a</sup> Values are given to more significant figures than the data warrant in order to retain precision in differences.



Figure 4. Mollier diagram for potassium

monomeric gas. The two paths are interrelated to a temperature of 1500° F. by the third-law calculation of  $(\Delta H_{\delta})_{\nu}$ , but the monomeric gas path is preferred for calculations at higher temperatures for two reasons. First, the specific heat of the vapor and the relative values of both enthalpy and entropy are less dependent upon vaporization quantities. Secondly, the monomeric gas path does not require an extrapolation of the specific heat of the liquid above its measured limit of 1500° F., while the liquid path calculations are subject to considerable error from this standpoint.

Although the thermodynamic properties reported in this article are based on the monomeric gas path, properties by the other path at selected states are used as an internal consistency check. Therefore the thermodynamic relationships and the computational steps for both paths are included in this section. The relationships were derived by an extension of the method described by Hirschfelder (6).

Monomeric Gas Path. ENTHALPY, ENTROPY, AND SPECIFIC HEAT OF SATURATED AND SUPERHEATED VAPOR. These properties at all vapor states were computed along isotherms with the following equations:

$$h_{1}^{s} = (h^{s})^{\circ} + \frac{RT}{M_{1}} \left\{ \frac{1}{\tilde{V}} \left[ B - T\left(\frac{dB}{dT}\right) \right] + \frac{1}{\tilde{V}^{2}} \left[ C - \frac{T}{2} \left(\frac{dC}{dT}\right) \right] + \frac{1}{\tilde{V}^{3}} \left[ D - \frac{T}{3} \left(\frac{dD}{dT}\right) \right] \right\}$$
(12)

$$s_{i}^{s} = (s^{s})^{\circ} - \frac{R}{M_{1}} \left\{ \ln p - \ln \frac{p\tilde{V}}{RT} + \frac{B}{\tilde{V}} + \frac{T}{\tilde{V}} \left( \frac{dB}{dT} \right) + \frac{C}{2\tilde{V}^{2}} + \frac{T}{2\tilde{V}^{2}} \left( \frac{dC}{dT} \right) + \frac{D}{3\tilde{V}^{3}} + \frac{T}{3\tilde{V}^{3}} \left( \frac{dD}{dT} \right) \right\}$$
(13)

$$\begin{aligned} (c_{\beta}^{e})_{i} &= (c_{\beta}^{e})^{\circ} - \frac{R}{M_{i}} + \frac{R}{M_{i}} \\ &\left\{ \frac{\left[1 + \frac{1}{\bar{V}} \left(B + T \frac{dB}{dT}\right) + \frac{1}{\bar{V}^{2}} \left(C + T \frac{dC}{dT}\right) + \frac{1}{\bar{V}^{2}} \left(D + T \frac{dD}{dT}\right)\right]^{2}}{\left[1 + 2 \frac{B}{\bar{V}} + 3 \frac{C}{\bar{V}^{2}} + 4 \frac{D}{\bar{V}^{3}}\right]} \right\} - \\ &\frac{RT}{\bar{V}M_{i}} \left\{ \left(T \frac{d^{2}B}{dT^{2}} + 2 \frac{dB}{dT}\right) + \frac{1}{2\bar{V}} \left(T \frac{d^{2}C}{dT^{2}} + 2 \frac{dC}{dT}\right) + \frac{1}{3\bar{V}^{2}} \left(\frac{T}{c} \frac{d^{2}D}{dT^{2}} + 2 \frac{dD}{dT}\right) \right\} \quad (14) \end{aligned}$$

ENTHALPY AND ENTROPY OF CONDENSED PHASE. These properties (Table II) at each temperature were obtained by subtracting the enthalpy and entropy of vaporization from the corresponding properties of the saturated vapor.

Liquid Path. ENTHALPY, ENTROPY, AND SPECIFIC HEAT OF SATURATED VAPOR. The enthalpy and entropy of the saturated vapor at any given temperature were obtained by adding the enthalpy and entropy of vaporization to the corresponding properties of the saturated liquid.

The specific heat at saturation was obtained by numerically evaluating, at  $50^{\circ}$  intervals, the differential,

$$\left(c_{\rho}^{\delta}\right)_{s} = \lim\left[\left(\frac{\partial h^{\delta}}{\partial T}\right)_{\rho}\right]_{(T \to T,)} = \lim\left[\left(\frac{\Delta h^{\delta}}{\Delta T}\right)_{\rho}\right]_{(T \to T,)}$$
(15)

ENTHALPY, ENTROPY, AND SPECIFIC HEAT OF SUPER-HEATED VAPOR. With the saturated vapor state as a starting point, these properties in the superheat region were computed along constant temperature lines with the following equations:

$$h! = h! - \frac{RT}{M_1} \left\{ \frac{1}{\tilde{V}} \left[ B - T\left(\frac{dB}{dT}\right) \right] + \frac{1}{\tilde{V}^2} \left[ C - \frac{T}{2} \left(\frac{dC}{dT}\right) \right] + \frac{1}{\tilde{V}^3} \left[ D - \frac{T}{3} \left(\frac{dD}{dT}\right) \right] \right\}_{V_1}^{V_2}$$
(16)

$$s_{i}^{s} = s_{i}^{s} + \frac{R}{M_{1}} \left\{ \ln p - \ln \frac{p\bar{V}}{RT} + \frac{B}{\bar{V}} + \frac{T}{\bar{V}} \left( \frac{dB}{dT} \right) + \frac{C}{2\bar{V}^{2}} + \frac{T}{2\bar{V}^{2}} \left( \frac{dC}{dT} \right) + \frac{D}{3\bar{V}^{3}} + \frac{T}{3\bar{V}^{3}} \left( \frac{dD}{dT} \right) \right\} \frac{V}{V_{i}}$$
(17)

$$\begin{aligned} (c_{p}^{s})_{i} &= (c_{p}^{s})_{i} - \frac{R}{M_{i}} \\ &\{ \frac{\left[1 + \frac{1}{V} \left(B + T \frac{dB}{dT}\right) + \frac{1}{V^{2}} \left(C + T \frac{dC}{dT}\right) + \frac{1}{V^{3}} \left(D + T \frac{dD}{dT}\right)\right]^{2}_{V_{i}} \\ &\left[1 + 2 \frac{B}{V} + 3 \frac{C}{V^{2}} + 4 \frac{D}{V^{3}}\right] \\ &\frac{RT}{VM_{1}} \left\{ \left(T \frac{d^{2}B}{dT^{2}} + 2 \frac{dB}{dT}\right) + \frac{1}{2\tilde{V}} \left(T \frac{d^{2}C}{dT^{2}} + 2 \frac{dC}{dT}\right) + \frac{1}{3\tilde{V}^{2}} \left(T \frac{d^{2}D}{dT^{2}} + 2 \frac{dD}{dT}\right) \right\}^{V_{i}}_{V_{i}} \end{aligned}$$
(18)

Comparison of Two Computational Paths. Three properties-enthalpy, entropy, and specific heat-of the superheated vapor were computed by both paths, and values at selected states are compared in Table I. Properties as computed by the two paths exhibit rather good agreement in the temperature range from 1600° to 2200° F., and an internal consistency check of considerable importance is obtained. The basic property relationships, as well as the methods of calculation, are checked by this procedure. It is also interesting in this temperature range to compare values calculated for the specific heat of the liquid (monomeric gas path) with corresponding experimental values (liquid path). Values from the gas path may be obtained directly from  $h^i$  in Table II, and these show an average disagreement of only 2.1% (maximum of 3.2%) from those obtained by extending the experimental results of Douglas with his specific-heat equation. This extension to a degree (see Figure 3) is verified by several measurements at NRL.

Values for the specific heat of the liquid when computed from the monomeric gas path are completely independent of the other path, and the agreement between the calculated and observed values increases the degree of confidence which can be placed in the relative values of enthalpy and entropy for the vapor at all saturation and superheat states.

## THERMODYNAMIC PROPERTIES OF POTASSIUM AND DISCUSSION

Saturation and superheat properties from  $1400^{\circ}$  to  $2500^{\circ}$  F. are presented in Tables II and III, and the thermal properties from  $1200^{\circ}$  to  $2500^{\circ}$  F. for both wet and dry vapors are presented graphically in a Mollier chart (Figure 4). Properties of potassium vapor have been included in the tables and in the Mollier diagram for states outside the measured limits of the basic data. For example, superheat properties for states at pressures below 2.3 and above 27.4 atm. required for their computation short extrapolations of the virial equation. Likewise, vaporization and saturation properties at states below 1399° and above 2393° F. (the limits of the saturation data) required short extrapolations of the vapor-pressure equation. The properties computed by extending the basic relationships may be of reduced accuracy.

The properties of potassium in this article were compared to those in two recent publications (14), (16). The results generated in these studies were not based directly on measured PVT data; the properties reported by Walling (14) were deduced principally from saturation pressures, and those by Weatherford (16) were computed from published thermodynamic functions of the monomeric and

### Table III. Thermodynamic Properties of Potassium Vapor in the Superheat Region<sup>a</sup>

(Basis: h = 0 and s = 0 for solid potassium at  $0^{\circ} R$ )

р	$v^s$	z	h*	S <sup>#</sup>	C <sup>8</sup> <sub>P</sub>	p	$U^{\mathcal{S}}$	z	$h^s$	S <sup>\$</sup>	$C_p^{g}$
		(at 1400°)	F.)					(at 2000° I	E. Cont.)		
$15.16 \\ 14.70 \\ 11.76 \\ 8.82 \\ 5.88 \\ 2.94$	$\begin{array}{c} 30.9931\\ 32.0491\\ 40.7307\\ 55.2017\\ 84.1450\\ 170.9752 \end{array}$	0.92035 0.92276 0.93818 0.95363 0.96909 0.98455	$\begin{array}{c} 1188.87\\ 1190.30\\ 1199.36\\ 1208.38\\ 1217.35\\ 1226.27 \end{array}$	$\begin{array}{c} 1.11443\\ 1.11664\\ 1.13207\\ 1.15075\\ 1.17538\\ 1.21460\end{array}$	$\begin{array}{c} 0.2840 \\ 0.2789 \\ 0.2473 \\ 0.2163 \\ 0.1859 \\ 0.1561 \end{array}$	$73.48 \\ 58.78 \\ 44.09 \\ 29.39 \\ 14.70 \\ 11.76 \\ 8.82 \\ 5.98 \\ 14.70 \\ 1.76 \\ 11.76 \\ 11.76 \\ 11.76 \\ 10.78 \\$	$\begin{array}{c} 8.4217\\ 10.7088\\ 14.5276\\ 22.1749\\ 45.1353\\ 56.6180\\ 75.7569\\ 114.0364\end{array}$	0.91665 0.93247 0.94874 0.96544 0.98254 0.98601 0.98948 0.92298	1262.80 1272.15 1281.70 1291.43 1301.31 1303.31 1305.31	1.07521 1.08950 1.10713 1.13081 1.16916 1.18113 1.19638 1.21761	$\begin{array}{c} 0.2166\\ 0.1997\\ 0.1821\\ 0.1641\\ 0.1457\\ 0.1420\\ 0.1383\\ 0.1245\end{array}$
		(at 1500°	F.)			2.94	228.8781	0.99298 0.99648	1307.31	1.25346	$0.1345 \\ 0.1308$
24.64 14.70	$\begin{array}{c} 19.7806 \\ 34.5370 \\ \end{array}$	806 0. <b>9</b> 0620 370 0.94365	$1193.12 \\ 1215.24$	1.09411 1.12972	$0.2936 \\ 0.2249$			(at 2100°	<b>F</b> .)		
11.76 8.82 5.88 2.94	43.6836 58.9304 89.4273 180.9234	0.95485 0.96609 0.97737 0.98867	$1221.78 \\ 1228.31 \\ 1234.83 \\ 1241.34$	$1.14382 \\ 1.16119 \\ 1.18454 \\ 1.22250$	$0.2049 \\ 0.1851 \\ 0.1655 \\ 0.1461$	200.72 191.05 176.35 161.66	2.8962 3.0691 3.3685 3.7232	$0.82747 \\ 0.83460 \\ 0.84555 \\ 0.85671$	1222.05 1226.33 1232.93 1239.65	1.01427 1.01802 1.02402 1.03041	$0.2907 \\ 0.2843 \\ 0.2746 \\ 0.2647$
		(at 1600°	F.)			$146.96 \\ 132.26$	$4.1500 \\ 4.6733$	$0.86812 \\ 0.87982$	$1246.53 \\ 1253.56$	$1.03727 \\ 1.04469$	$0.2545 \\ 0.2438$
$\begin{array}{c} 38.16\\ 29.39\\ 14.70\\ 11.76\\ 8.82\\ 5.88\\ 2.94 \end{array}$	$\begin{array}{c} 13.2142 \\ 17.6188 \\ 36.8319 \\ 46.4452 \\ 62.4699 \\ 94.5227 \\ 190.6872 \end{array}$	0.89203 0.91605 0.95750 0.96593 0.97440 0.98290 0.99144	1197.28 1211.64 1236.01 1240.91 1245.81 1250.72 1255.62	$\begin{array}{c} 1.07620\\ 1.09517\\ 1.14006\\ 1.15334\\ 1.16991\\ 1.19245\\ 1.22961 \end{array}$	$\begin{array}{c} 0.2999\\ 0.2602\\ 0.1931\\ 0.1797\\ 0.1664\\ 0.1532\\ 0.1401 \end{array}$	$117.57 \\ 102.87 \\ 88.18 \\ 73.48 \\ 58.78 \\ 44.09 \\ 29.39 \\ 14.70 \\ 11.76 \\ 8.82$	5.3293 6.1750 7.3053 8.8911 11.2738 15.2503 23.2108 47.1065 59.0565 78.9739	0.89184 0.90419 0.91689 0.92993 0.94332 0.95703 0.97106 0.98539 0.98829 0.98829	$\begin{array}{c} 1260.76\\ 1268.14\\ 1275.68\\ 1283.38\\ 1291.24\\ 1299.25\\ 1307.39\\ 1315.66\\ 1317.62\\ 1319.00\\ \end{array}$	1.05281 1.06178 1.07186 1.08342 1.09711 1.11413 1.13717 1.17488 1.18671 1.20183	0.2327 0.2210 0.2088 0.1962 0.1830 0.1695 0.1556 0.1415 0.1386 0.1357
		(at 1700°	<b>F</b> .)			5.88 2.94	118.8100 238.3209	0.99412 0.99706	$1320.67 \\ 1322.35$	$1.22294 \\ 1.25865$	$0.1328 \\ 0.1299$
56.69 44.09 29.39 14.70	9.1829 12.1516 18.8544 39.0051	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	878181201.56903821217.02934901235.47967041254.25	$1.06043 \\ 1.07897 \\ 1.10647 \\ 1.14871$	$\begin{array}{c} 0.3028 \\ 0.2651 \\ 0.2196 \\ 0.1733 \end{array}$			(at 2200°	<b>F</b> .)		
$11.76 \\ 8.82 \\ 5.88 \\ 2.94$	49.0857 65.8890 99.4983 200.3319		$\begin{array}{c} 0.1640 \\ 0.1547 \\ 0.1455 \\ 0.1362 \end{array}$	$\begin{array}{c} 258.93 \\ 249.83 \\ 235.14 \\ 220.44 \\ 205.74 \end{array}$	$\begin{array}{c} 2.2962 \\ 2.3966 \\ 2.5752 \\ 2.7775 \\ 3.0090 \end{array}$	$\begin{array}{c} 0.81446 \\ 0.82022 \\ 0.82948 \\ 0.83875 \\ 0.84807 \end{array}$	$1227.64 \\1230.99 \\1236.43 \\1241.91 \\1247.45$	$\begin{array}{c} 1.00579 \\ 1.00853 \\ 1.01312 \\ 1.01791 \\ 1.02295 \end{array}$	$\begin{array}{c} 0.2883 \\ 0.2832 \\ 0.2752 \\ 0.2675 \\ 0.2599 \end{array}$		
		(at 1800°	<b>F</b> .)			191.05 176.35	3.2765 3.5892 2.9596	0.85751 0.86709 0.87686	1253.08 1258.80 1264.64	1.02828 1.03394 1.03998	$0.2522 \\ 0.2444 \\ 0.2364$
$\begin{array}{c} 81.22\\ 73.48\\ 58.78\\ 44.09\\ 29.39\\ 14.70\\ 11.76\\ 8.82\\ 5.88\\ 2.94 \end{array}$	$\begin{array}{c} 6.6044\\ 7.3986\\ 9.4908\\ 12.9912\\ 20.0101\\ 41.0980\\ 51.6461\\ 69.2279\\ 104.3940\\ 209.8969 \end{array}$	0.86487 0.87657 0.89956 0.92350 0.94830 0.97384 0.97902 0.98423 0.98947 0.99472 (at 1900°	1206.14 1213.27 1227.16 1241.43 1256.03 1270.89 1273.88 1276.89 1279.90 1282.91 F.)	$\begin{array}{c} 1.04659\\ 1.05417\\ 1.07039\\ 1.09003\\ 1.11578\\ 1.15625\\ 1.15864\\ 1.18432\\ 1.20598\\ 1.24226\end{array}$	$\begin{array}{c} 0.3024\\ 0.2873\\ 0.2574\\ 0.2260\\ 0.1935\\ 0.1604\\ 0.1537\\ 0.1470\\ 0.1404\\ 0.1337\end{array}$	$161.66\\146.96\\132.26\\117.57\\102.87\\88.18\\73.48\\58.78\\44.09\\29.39\\14.70\\11.76\\8.82\\5.88$	$\begin{array}{c} 3.5350\\ 4.4051\\ 4.9509\\ 5.6346\\ 6.5154\\ 7.6920\\ 9.3417\\ 11.8194\\ 15.9531\\ 24.2262\\ 49.0571\\ 61.4741\\ 82.1699\\ 123.5626\end{array}$	$\begin{array}{c} 0.8668_{\rm 5}\\ 0.89704\\ 0.90748\\ 0.91818\\ 0.92913\\ 0.94033\\ 0.95179\\ 0.96350\\ 0.97544\\ 0.98761\\ 0.99007\\ 0.99254\\ 0.99502 \end{array}$	$1204.04\\1270.59\\1276.66\\1282.86\\1289.19\\1295.64\\1302.22\\1308.91\\1315.71\\1322.63\\1329.64\\1331.05\\1332.47\\1333.89$	$\begin{array}{c} 1.03336\\ 1.04649\\ 1.05355\\ 1.06128\\ 1.06985\\ 1.07951\\ 1.09064\\ 1.10388\\ 1.12044\\ 1.14302\\ 1.18024\\ 1.19198\\ 1.20700\\ 1.22800\\ \end{array}$	$\begin{array}{c} 0.2364\\ 0.2280\\ 0.2194\\ 0.2011\\ 0.1914\\ 0.1814\\ 0.1710\\ 0.1604\\ 0.1495\\ 0.1384\\ 0.1361\\ 0.1339\\ 0.1316\end{array}$
$112.76 \\ 102.87$	4.8944 5.4367	0.85213 0.86357	1211.11 1218 10	1.03443 1.04139	$0.2994 \\ 0.2867$	2.94	247.7427	0.99751	1335.31	1.26362	0.1293
88.18 73.48 58.78 44.09 29.39 14.70 11.76 8.82 5.88 2.94	$\begin{array}{c} 6.4719\\ 7.9273\\ 10.1178\\ 13.7780\\ 21.1116\\ 43.1360\\ 54.1514\\ 72.5119\\ 109.2347\\ 219.4070 \end{array}$	$\begin{array}{c} 0.88114\\ 0.89940\\ 0.91834\\ 0.93792\\ 0.95810\\ 0.97881\\ 0.98302\\ 0.98724\\ 0.99147\\ 0.99573 \end{array}$	1228.78 1239.78 1251.08 1262.65 1274.45 1286.46 1288.88 1291.31 1293.75 1296.19	$\begin{array}{c} 1.05275\\ 1.05275\\ 1.06566\\ 1.08075\\ 1.09922\\ 1.12376\\ 1.16299\\ 1.17514\\ 1.19057\\ 1.21198\\ 1.24801 \end{array}$	$\begin{array}{c} 0.2667\\ 0.2455\\ 0.2232\\ 0.2000\\ 0.1761\\ 0.1517\\ 0.1468\\ 0.1419\\ 0.1369\\ 0.1320 \end{array}$	327.66 323.31 308.62 293.92 279.22 264.53 249.83 235.14 220.44	$\begin{array}{c} 1.8487\\ 1.8796\\ 1.9899\\ 2.1107\\ 2.2438\\ 2.3916\\ 2.5567\\ 2.7425\\ 2.9532\end{array}$	(at 2300) 0.79977 0.80232 0.81078 0.81905 0.82718 0.83525 0.84330 0.85137 0.85950	<sup>2</sup> F.) 1232.76 1234.18 1238.94 1243.64 1248.32 1253.00 1257.70 1262.45 1267.24	$\begin{array}{c} 0.99802\\ 0.99908\\ 1.00271\\ 1.00644\\ 1.01028\\ 1.01426\\ 1.01426\\ 1.01840\\ 1.02272\\ 1.02727\\ 1.02727\end{array}$	0.2905 0.2878 0.2796 0.2722 0.2654 0.2589 0.2527 0.2465 0.2404
		(at 2000°	<b>F</b> .)			205.74 191.05 176.25	3.1944 3.4732 3.7000	0.86771 0.87604 0.88451	$1272.10 \\ 1277.03 \\ 1282.05$	1.03205 1.03712 1.04252	0.2343
152.28 146.96 132.26 117.57 102.87 88.18	3.7229 3.8799 4.3800 5.0075 5.8172 6.9006	$\begin{array}{c} 0.83980\\ 0.84460\\ 0.85812\\ 0.87205\\ 0.88644\\ 0.90131 \end{array}$	$\begin{array}{c} 1216.45\\ 1219.38\\ 1227.61\\ 1236.06\\ 1244.74\\ 1253.66\end{array}$	$\begin{array}{r} 1.02372 \\ 1.02644 \\ 1.03435 \\ 1.04296 \\ 1.05245 \\ 1.06308 \end{array}$	$\begin{array}{c} 0.2950 \\ 0.2903 \\ 0.2770 \\ 0.2631 \\ 0.2484 \\ 0.2329 \end{array}$	$1633 \\161.66 \\146.96 \\132.26 \\117.57 \\102.87 \\88.18$	4.1847 4.6484 5.2162 5.9272 6.8427 8.0650	$\begin{array}{c} 0.89312\\ 0.90191\\ 0.91087\\ 0.92001\\ 0.92935\\ 0.93888\end{array}$	$1287.15 \\1292.35 \\1297.64 \\1303.03 \\1308.52 \\1314.10$	$1.04232 \\ 1.04830 \\ 1.05453 \\ 1.06130 \\ 1.06873 \\ 1.07699 \\ 1.08633$	0.2150 0.2082 0.2011 0.1938 0.1863 0.1784

(Continued on page 467)

### Table III. Thermodynamic Properties of Potassium Vapor in the Superheat<sup>a</sup> Region (Continued)

(Basis: h = 0 and s = 0 for solid cesium at  $0^{\circ}$  R.)

р	U <sub>s</sub>	z	h	54	C <sub>P</sub>	р	U <sup>d</sup>	z	h	s#	C <sup>d</sup> <sub>P</sub>			
		(at 2300°	F. cont.)			(at 2400° F. cont.)								
73.48 58.78 44.09	9.7782 12.3505 16.6409	$0.94860 \\ 0.95852 \\ 0.96862$	$\begin{array}{r} 1319.77 \\ 1325.54 \\ 1331.40 \end{array}$	1.09712 1.11002 1.12623	$\begin{array}{c} 0.1704 \\ 0.1621 \\ 0.1536 \end{array}$	5.88 2.94	133.0243 266.5427	0.99629 0.99814	13 <b>6</b> 0.04 1361.10	1.237 <b>48</b> 1.27 <b>29</b> 7	0.1 <b>30</b> 1 0.1 <b>286</b>			
29.39 14.70 11.76	25.2264 50.9920 63.8762	0.97890 0.98937 0.99148	1337.33 1343.35 1344.57	1.14845 1.18530 1.19697	$0.1450 \\ 0.1361 \\ 0.1343$			(at 2500°	<b>F</b> .)					
8.82 5.88	85.3503 128.2995	0.99360 0.99573	1345.78 1347.00	1.21191 1.23284	0.1325 0.1307	499.30 484.97	$1.2328 \\ 1.2850$	0.75775 0.76719	1238.19 1242.94	0.98323 0.98596	$\begin{array}{c} 0.3312 \\ 0.3145 \end{array}$			
2.94	257.1488	0.99786	1348.22	1.26839	0.1289	470.27 455.58 440.88	$1.3406 \\ 1.3987 \\ 1.4598$	0.77612 0.78444 0.79229	$1247.49 \\ 1251.80 \\ 1255.92$	0.98870 0.99142 0.99412	0.3006 0.2893 0.2797			
		(at 2400°	<b>F</b> .)			426.18 411.49	1.5244 1.5929	0.79975 0.80690	1259.88 1263.73	0.99683 0.99957	0.2714 0.2642			
407.60	1.5055 1.5590	$0.78181 \\ 0.78815$	1236.71 1240.07	0.99066	0.3013	396.79 382.10 367.40	$1.6661 \\ 1.7444 \\ 1.8287$	$0.81381 \\ 0.82052 \\ 0.82708$	$\begin{array}{r} 1267.49 \\ 1271.18 \\ 1274.83 \end{array}$	1.00233 1.00515 1.00802	0.2578 0.2520 0.2467			
382.10 367.40	1.6359 1.7182	0.79639 0.80429	1244.50 1248.81	0.99597 0.99907	$0.2838 \\ 0.2756$	352.70 338.01	1.9197 2.0185	0.83353 0.83989	1278.44 1282.04	1.01096 1.01399	0.2418 0.2372			
352.70 338.01 323 31	$1.8068 \\ 1.9025 \\ 2.0066$	0.81191 0.81932 0.82659	$1253.02 \\ 1257.16 \\ 1261.26$	1.00222 1.00543 1.00873	$0.2683 \\ 0.2618 \\ 0.2558$	323.31 308.62 203.02	2.1261 2.2438 2.3734	0.84620 0.85247 0.85874	1285.63 1289.23 1292.84	1.01710 1.02033 1.02367	0.2328			
308.62 293.92	2.0000 2.1204 2.2454	0.83376 0.84086	1265.34 1269.42	1.01211 1.01562	0.2502 0.2449	279.22 264.53	2.5165 2.6757	0.86502 0.87133	$1292.04 \\1296.47 \\1300.13$	1.02307 1.02714 1.03076	0.2203 0.2163			
279.22 264.53 249.83	2.3835 2.5369 2.7084	0.84793 0.85501 0.86211	$1273.51 \\ 1277.63 \\ 1281.77$	1.01925 1.02302 1.02697	$0.2398 \\ 0.2348 \\ 0.2298$	249.83 235.14 220.44	2.8538 3.0543	0.87768 0.88409 0.89057	$1303.83 \\ 1307.57 \\ 1311.36$	1.03455 1.03853 1.04272	0.2122			
235.14 220.44	2.9016 3.1208	0.86927 0.87649	1285.97 1290.21	1.02037 1.03110 1.03544	0.2249 0.2199	220.44 205.74 191.05	3.5421 3.8428	0.89713 0.90377	1315.19 1319.08	1.04714 1.05185	0.1996			
205.74 191.05 176.35	3.3716 3.6614 4.0000	0.88380 0.89122 0.89874	1294.51 1298.87 1203.20	1.04003 1.04490 1.05009	$0.2148 \\ 0.2096 \\ 0.2042$	176.35 161.66 146.96	4.1940 4.6097 5.1090	$0.91051 \\ 0.91734 \\ 0.92429$	$1323.02 \\ 1327.02 \\ 1221.08$	1.05687 1.06226 1.06809	0.1908			
161.66 146.96	4.4008 4.8824	0.90640 0.91418	1307.80 1312.38	1.05565 1.06166	0.1988 0.1931	132.26 117.57	5.7200 6.4846	0.92429 0.93134 0.93851	1335.20 1339.37	1.00805 1.07445 1.08145	0.1766 0.1716			
132.26 117.57 102.87	5.4720 6.2098 7 1596	$0.92211 \\ 0.93018 \\ 0.93839$	$1317.03 \\ 1321.75 \\ 1326.55$	$1.06820 \\ 1.07539 \\ 1.08341$	$0.1873 \\ 0.1813 \\ 0.1751$	$102.87 \\ 88.18 \\ 73.48$	7.4684 8.7813 10.6207	0.94580 0.95319 0.96071	$1343.61 \\ 1347.91 \\ 1352.26$	1.08927 1.09816 1.10850	0.1665 0.1613 0.1559			
88.18 73.48	8.4273 10.2037	0.94676 0.95527	1331.43 1336.38	1.09250 1.10304	0.1687 0.1622	58.78 44.09	13.3813 17.9845	0.96834 0.97609	$1356.68 \\ 1361.14$	1.12092 1.13664	0.1504 0.1447			
58.78 44.09 29.39	$12.8703 \\ 17.3172 \\ 26.2148$	0.96393 0.97274 0.98169	$1341.40 \\ 1346.49 \\ 1351.65$	1.11567 1.13161 1.15354	$0.1554 \\ 0.1486 \\ 0.1416$	29.39 14.70 11.76	27.1940 54.8286 68.6468	0.98395 0.99192	$1365.67 \\ 1370.25 \\ 1371.17$	$1.15836 \\ 1.19471 \\ 1.20627$	0.1390			
$14.70 \\ 11.76$	52.9150 66.2662	0.99078 0.99261	1356.87 1357.93	1.19011 1.20172	$0.1344 \\ 0.1330$	8.82 5.88	91.6776 137.7397	0.99514 0.99676	1372.09 1373.02	1.22112 1.24194	0.1308			
8.82	88.5186	0.99445	1358.98	1.21661	0.1315	2.94	275.9272	0.99838	1373.94	1.27739	0.1284			

<sup>o</sup> Values are given to more significant figures than the data warrant in order to retain precision in differences.

dimeric vapors. If the NRL data are taken arbitrarily as a reference and the property changes from  $p_s$  to 0.2 atm. compared at each temperature, the enthalpy changes reported by Walling are 17 to 95% high and the entropy changes are 2 to 14% high. Similarly, the enthalpy changes reported by Weatherford are 28 to 40% low, and the entropy changes are 5 to 8% low. Specific heats and specific volumes of potassium vapor were tabulated by Walling, and these values also are in considerable disagreement with those of NRL.

In the existing compilations of properties for potassium, the reported values can be no better than the accuracy of the assumptions which made the calculations possible. The properties reported in this paper are based on measured compressibilities. They have been evaluated by several tests for internal consistency, and it is believed that they will be satisfactory for any type of calculation now required for the design of systems using potassium as heat-transfer or working fluid.

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### NOMENCLATURE

- = second virial coefficient, cu. ft./ mole В
- third virial coefficient, (cu. ft.) $^{2}/(mole)^{2}$ C=
- fourth virial coefficient,  $(cu. ft.)^3/(mole)^3$ D =
- specific heat at constant pressure, B.t.u./lb.-° F.
- $c_p = f =$ = free energy, B.t.u./lb.
- h = enthalpy per unit mass, B.t.u./lb.
- enthalpy change per unit mass, B.t.u./lb.  $\Delta h =$
- $\Delta h_v =$ enthalpy change upon vaporization of a unit mass of equilibrium vapor, B.t.u./lb.

- $\Delta H_{\nu}$  = enthalpy change upon vaporization of a mole of equilibrium vapor, B.t.u./lb.-mole
  - J =any unit conversion
- $M_1$  = molecular weight of monomeric species
- $_Q^p$ = absolute pressure, p.s.i.
- = a defined function,  $[(z-1)\tilde{V}-B]\tilde{V}$
- $\dot{R} = gas constant$
- s Ξ entropy per unit mass, B.t.u./lb.-° F.
- $\Delta s_{\nu} =$ entropy change upon vaporization of a unit mass of equilibrium vapor, B.t.u./lb.-° F.
- T =absolute temperature, ° R.
- temperature, ° F. =
- Ũ = molal volume (per formula weight of monomer), cu. ft./lb.mole
- v =specific volume, cu. ft./lb.
- compressibility factor,  $p \tilde{V}/RT$ z =

### Subscripts

- i =quantity at any state
- 0 = quantity at 0° R.
- p = constant pressure change
- s = quantity at saturation

### **Superscripts**

- g = quantity in gas state
- = quantity in liquid state
- = standard state, 1 atm. for gas

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## High-Temperature Properties of Sodium

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A virial equation of state for sodium with coefficients through the fourth virial is derived from PVT data covering a temperature range from 1750 $^\circ$  to 2525 $^\circ$  F. Exact thermodynamic relations involving the virial and vapor-pressure equations are used to generate saturation and superheat properties of the vapor. Values of enthalpy, entropy, specific heat, and specific volume are tabulated for some 140 selected vapor states in the temperature range from 1650° to 2550° F. and in the pressure range from 2.9 to 358.7 p.s.i.a. The thermal properties for a somewhat greater temperature range from 1400° to 2500° F. are presented as a Mollier chart.

THE existing thermodynamic properties of alkali metal vapors have for the most part been obtained by estimating imperfections from spectroscopic data. The properties so obtained are of questionable accuracy, and there is a need for an increased reliability for the evaluation of the metal vapors as working fluids in turbines and other power cycles. To meet this need, reliable thermodynamic properties of sodium, potassium, and cesium are being generated from sets of experimentally determined properties-pressurevolume-temperature, vapor pressure, and liquid density. These properties for all three metals have been reported by Stone et al. (10, 11, 12), and those for potassium have been reduced thermodynamically to yield a consistent body of vapor properties—enthalpy, entropy, specific heat, and specific volume (3). This article describes a similar reduction of the measured properties of sodium.

TREATMENT OF PVT DATA AND THE VIRIAL EQUATION OF STATE

The major imperfections in sodium vapor at the temperatures and pressures involved in this study stem from the existence of molecular species with two or more atoms (5). These species are present in such abundance that an equation of state of the quasichemical type (involving equilibrium constants) could have been used to represent the PVTdata. However, the virial equation was preferred over the quasichemical types since the thermodynamic relationships based on it are believed to be better established.

The PVT data of Stone and coworkers (10) were fitted by the graphical method described for potassium (3) and the resulting virial equation of state is