# Phase Equilibrium in the Ethylene-Water System

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The mutual solubilities of ethylene and water for the binary in the two-phase region were studied. Data were taken at temperatures of  $100^{\circ}$  to  $280^{\circ}$  F. at  $60^{\circ}$  intervals for the pressure range of 500 to 5000 p.s.i.a. This study was conducted to extend the available knowledge on the behavior of hydrocarbon-water binary systems. This information is of value in petrochemical and refining industries for use in the design of process dehydration units.

**B**RADBURY *et al.* (3) have reported data on the solubility of ethylene in water for temperatures to  $212^{\circ}$  F. and pressures to 7700 p.s.i.a. Diepen and Scheffer (7, 8) report *P* and *T* data and water composition in the vapor phase for pressures to 882 and 1500 p.s.i.a. for temperatures to 77° F. In this study the composition of water in the supercritical fluid phase and solubilities of ethylene in water are reported at temperatures of 100°,  $160^{\circ}$ ,  $220^{\circ}$ , and  $280^{\circ}$  F. and pressures to 5000 p.s.i.a.

The equipment used in this investigation has been described by Wehe (16, 17). A modified Meeco Model W water analyzer was used to determine the water content in the vapor phase. The sampling procedure has been described by Anthony (1). An absolute manometer and Orsat gas buret were used to determine the ethylene content of the water phase. This technique has been described by Wehe and McKetta (18). Chemical materials used were Phillips pure grade ethylene and deaerated distilled water.

The experimental technique used in determining the water content of the hydrocarbon vapor phase was tested by comparing data for the propylene-water, *n*-butane-water, and ethane-water throughout the anticipated temperature range with the data of Li (13), Wehe (17), and Reamer *et al.* (14, 15). These comparisons are shown in Table I. Agreement was believed to be within the accuracy of the literature values in all cases.

The sampling technique for the water phase was tested by comparing data for the ethane-water binary with the data of Culberson and McKetta (5) and the data for the ethylene-water binary with the data of Bradbury *et al.* (3). The agreement is considered good (Table II).

The effect of pressure on the water content of the vapor is shown in Figure 1. Graphically smoothed values for mutual solubilities of ethylene and water are tabulated in Table III. Figures 2 and 3 illustrate the effect of temperature and pressure on the solubility of ethylene in water for the binary. A minimum solubility exists for each isobar, and tends to occur at lower temperatures as the pressure is increased. This same effect was observed by Culberson and McKetta (5, 6) for ethane and methane solubilities in water.

The solubility of ethylene in water can be correlated with the following thermodynamic relation

$$\ln\left(\frac{f_H}{x_H}\right)_L = \frac{\vec{V}_H}{\vec{R}\vec{T}} P + \ln H' \tag{1}$$

where  $\ln H' = \ln H + \frac{\vec{V}_{H}P_{s}}{RT}$ .

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The assumptions implicit in Equation 1 are constant temperature, constant moles of water, and  $\overline{V}_H$  independent of pressure and of the change in composition of ethylene in water with pressure. The value of  $(f_H)_L$  at equilibrium is equal to  $(f_H)_v$ , which may be set equal to  $(X_H)_v(f_H^\circ)_v$ , provided the Lewis and Randal rule for ideal solutions applies to the vapor.

The fugacity of pure hydrocarbon vapor may be obtained from experimental data, from a generalized fugacity coefficient chart, or from an adequate equation of state. If, in addition, the values of Henry's law constant and of the partial molal volume of ethylene in the liquid are known, the solubility of ethylene in the liquid may be calculated from the above equation. This equation may also be used to extrapolate experimental solubility data at low pressures to theoretical solubilities at high pressures by treating the partial molal volume and the modified Henry's constant as empirical constants. The experimental data should form a straight line when plotted according to Equation 1.

Krichevsky and Kasarnovsky (10, 11) have derived and plotted Equation 1, to calculate solubilities of hydrogen and nitrogen in water, and Wiebe and Gaddy (19) calculated solubilities of carbon dioxide in water.

Table I. Comparison of Experimental and Literature Values of Vapor Phase Data

Expe	erimental	Data	Literature Values				
<i>T</i> , ° F.	Pres- sure, p.s.i.a.	Ун₂о	<i>T</i> , ° F.	Pres- sure, p.s.i.a.	<i>Ү</i> н₂о		
		Propylene-V	Water (13)				
160.0 160.2 159.9	178.2 181.7 177.8	0.02506 0.02456 0.02433 0.02370	$160.25 \\ 150.25 \\ 160.25 \\ 160.25 \\ 160.25 \\ 160.25 \\ 160.25 \\ 160.25 \\ 160.25 \\ 160.25 \\ 100.25 \\ 1$	187.67 187.67 187.67 187.67	0.02306 0.02306 0.02306 0.02306 0.02306		
n-But	ane–Wat	er Vapor in T	hree-Phase	Region	(15, 17)		
160	124.7 124.2 125.7 126.0	$\begin{array}{c} 0.0373\\ 0.0334\\ 0.0340\\ 0.0329\\ 0.0334\\ 0.0330\\ 0.0329\\ 0.0329\\ 0.0329\\ 0.0332 \end{array}$	160.0 160.0	125.4 124.9	0.0338 0.0351		
Ethane-Water $(14)$							
100.0 160.1 220.2 279.9	$372.1 \\ 434.2 \\ 1458.2 \\ 1566.2$	0.00267 0.01134 0.01322 0.0367	$100.0 \\ 160.0 \\ 220.0 \\ 280.0$		0.00279 0.01187 0.01396 0.0370		



Table II. Comparison of Ethane-Water and Ethylene-Water Liquid Phase Data with Literature

Table	III.	Smoothe	∍d Vo	lues	for	Mutual	So	lubilities	of	Ethyler	٦e
		and	Wat	er in	Va	por-Liqu	uid	Region			

	Mole Fraction Ethylene in Water $ imes$ 10 <sup>3</sup>						
Pressure.	T =	T =	T =	T =			
p.s.i.a.	100°F.	$1\overline{6}0^{\circ}$ F.	220° F.	$2\overline{80}^{\circ}$ F.			
200	0.838	0 585	0 567	0 545			
400	1 557	1 112	1 100	1 079			
500	1 875	1 344	1 346	1 320			
1000	2 955	2 355	2 281	2 455			
1500	3 351	2 858	2 941	3 352			
2000	3 574	3 159	3 351	3 970			
2500	3.732	3.369	3.628	4 435			
3000	3.830	3.545	3.872	4.836			
3500	3.905	3.702	4.107	5.105			
4000	3.954	3.840	4.333	5.535			
4500	3.982	3.961	4.545	5.852			
5000	3.999	4.085	4.751	6.180			
	Mole Fr	action Wate	er in Ethyle	ene $ imes$ 103			
200	5.126	25.22	86.36	252.53			
400	2.824	13.42	47.69	130.20			
500	2.400	11.18	39.20	107.00			
600	2.135	9.648	33.66	93.13			
800	1.821	7.763	26.64	71.60			
1000	1.661	6.675	22.60	60.03			
1500	1.519	5.452	17.59	45.89			
2000	1.535	5.037	15.47	38.62			
2500	1.543	4.909	14.37	34.93			
3000	1.550	4.910	13.83	32.59			
3000	1.007	4.909	13.50	31.01			
4000	1 561	4,900	13.32	29.94			
5000	1 563	4.900	13.18	29.08 29.08			
0000	1.000	4.300	10.10	23.00			



6.0

Figure 3. Effect of temperature on ethylene solubility for binary mixture

By use of experimental values of Henry's law constant and partial molal volumes of each gas in water, the solubility was calculated at pressures as high as 1000 atm. with excellent accuracy.

Kobayashi (9) plotted the solubilities of methane and other light hydrocarbons in water and Brooks (4) and Leland (12) plotted the solubility of 1-butene in water by use of Equation 1. Each of these investigators found that for the hydrocarbon systems, the experimental values showed considerable deviation from linearity as the pressures approached that of a phase change.

The solubility of ethylene in water was plotted according to Equation 1. This result is shown in Figure 4, and the values of  $\bar{V}_{II}$  and  $\ln H'$  are tabulated in Table IV. The values of the partial molal volumes and the modified Henry's constant were evaluated by two procedures. The first was to assume an ideal solution for the vapor. Therefore,  $(f_H)_L = (f_H)_v = (X_H)_v (f_H^\circ)_v$ . This method is the one used by Kobayashi (9), referred to here as the wet basis. The second procedure was to assume  $(X_H) = 1.0$ , and therefore  $(f_H)_v = (f_H^\circ)_v$ , referred to as the dry basis. The values of  $\overline{V}_{H}$  and ln H' were determined by the least squares method of curve fitting with the use of the raw experimental data and the graphically smoothed data. The Benedict-Webb-Rubin equation of state was used to calculate fugacities of hydrocarbons (2).

The data were curve-fitted on the dry basis for engineering purposes. Very often when the solubility of a hydrocarbon in the liquid phase is desired an engineer does not know the water concentration in the vapor phase. Therefore, Equation 1 or Figure 4 would be more applicable for design calculations. The ethane solubilities reported by Culberson and McKetta (5) were also used to evaluate the values of  $\overline{V}_{II}$  and  $\ln H'$ for ethane over the pressure range of 500 to 5000 p.s.i.a. with both procedures by the method of least squares. These values are compared to those reported by Kobavashi (9) in Table IV. Kobayashi plotted the ethanewater data over the pressure range of 500 to 10,000 p.s.i.a. However, by use of the values calculated in this work on the dry or wet basis, the solubility of ethane in water at 10,000 p.s.i.a. was predicted to within 25% of Culberson's data for all temperatures as shown in Table IV.

Thermodynamically and graphically smoothed values of ethylene dissolved in water for the binary are tabulated in Table V. Experimental data for the ethylene water system are shown in Table VI.

Table	١٧.	Modified	Henry's Law	<sup>7</sup> Constants	and	Partial	Molal
		Volumes	of Dissolved	Gases for	Bina	ries	

		100° F.	160° F.	220° F.	280° F.			
		E	Sthane					
$\mathrm{DB}^{a}$	$ar{V}$ ln $H'$	$0.8258 \\ 13.2852$	0.7573 13.7819	$0.7473 \\ 13.8785$	0.8543 13.7511			
WB	$ar{V}$ ln $H'$	$\begin{array}{c}0.8271\\13.2840\end{array}$	$0.7608 \\ 13.7778$	0.7641 13.8605	$0.9966 \\ 13.6637$			
Lit. (9)	$ar{ abla}$ ln $H'$	0.849 13.3113	$\begin{array}{c}0.858\\13.7489\end{array}$	0.917 13.8088	$1.021 \\ 13.6591$			
Comp	Comparison of predicted and experimental values at 10,000 p.s.i.a.							
DB	$X_{ ext{caled}}$ , $X_{ ext{exptl.}}$ (5)	$0.00134 \\ 0.00113$	$0.00146 \\ 0.00123$	$0.00144 \\ 0.00150$	0.00254 0.00206			
WB	$X_{ ext{caled.}} \ X_{ ext{exptl.}(\delta)}$	$0.00134 \\ 0.00113$	0.00145 0.00122	0.00194 0.00150	0.00230 0.00206			
		$\mathbf{E}^{i}$	thylene					
Raw DE WI	data $\vec{V}$ $\ln H'$ $\vec{V}$ $\ln H'$	$0.8448 \\ 12.1814 \\ 0.8454 \\ 12.1796$	$0.8275 \\ 12.5588 \\ 0.8310 \\ 12.5513$	0.7428 12.7415 0.7834 12.7099	$0.6361 \\ 12.7550 \\ 0.7855 \\ 12.6504$			
Smoo DE	thed data 3 $\overline{V}$ ln $H'$	$0.7911 \\ 12.2170$	$0.7567 \\ 12.6208$	0.8800 12.6926	$\begin{array}{c} 0.7435\\ 12.7088 \end{array}$			
WI	$egin{array}{c} ar{V} \ \ln H' \end{array}$	0.7931 12.2145	$0.7654 \\ 12.6111$	$\begin{array}{c} 0.9240 \\ 12.6567 \end{array}$	0.8894 12.6084			
DB	$\ln\left(\frac{f_v}{X}\right)$	$\Big)_{HC} = \frac{\vec{V}}{RT}$	$P + \ln H'$					

WB. 
$$\ln\left(\frac{T_{Iv}}{X}\right)_{HC} = \frac{v}{RT}P + \ln H'$$

<sup>a</sup> DB, dry basis.

WB, wet basis.



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Table V. Comparison of Thermodynamic and Graphically Smoothed Values for Ethylene-Water Binary Mole Fraction of Ethvlene in Water Phase  $\times 10^3$ 

						· · · · · · · · · · · · · · · · · · ·		
D	100° F.		160° F.		200° F.		280° F.	
p.s.i.a.	$X (GS)^a$	X (TS)	X (GS)	X (TS)	$\overline{X (GS)}$	X (TS)	$\overline{X}$ (GS)	X (TS)
$\begin{array}{c} 400\\ 500\\ 1000\\ 2000\\ 2500\\ 3000\\ 3500\\ 4000\\ 4500 \end{array}$	$\begin{array}{c} 1.557\\ 1.875\\ 2.955\\ 3.574\\ 3.732\\ 3.830\\ 3.905\\ 3.954\\ 3.982\end{array}$	1.680 1.993 3.012 3.526 3.657 3.769 3.867 3.956 4.038	1.112 1.344 2.355 3.159 3.367 3.545 3.702 3.840 3.961	$1,208 \\ 1,454 \\ 2,389 \\ 3,244 \\ 3,455 \\ 3,619 \\ 3,759 \\ 3,882 \\ 3,993 \\ \end{cases}$	$\begin{array}{c} 1.100\\ 1.346\\ 2.281\\ 3.351\\ 3.628\\ 3.872\\ 4.107\\ 4.333\\ 4.545\end{array}$	1.039 1.261 2.173 3.254 3.575 3.826 4.034 4.214 4.214	$\begin{array}{c} 1.079\\ 1.320\\ 2.455\\ 3.970\\ 4.435\\ 4.836\\ 5.195\\ 5.535\\ 5.852\end{array}$	$\begin{array}{c} 1.061 \\ 1.295 \\ 2.300 \\ 3.669 \\ 4.136 \\ 4.516 \\ 4.836 \\ 5.113 \\ 5.360 \end{array}$
5000	3.999	4.114	4.085	4,095	4.751	4.520	6.180	5.584

<sup>a</sup> GS, graphically smooth data.

TS, thermodynamically smooth data from Equation 1 on dry basis.

## Table VI. Experimental Data on Ethylene-Water Binary

		Analysis, Mole Fractio		
		Water in HC	C₂H₄ in water	
Temp	Pressure.	vapor	phase	
° F.	p.s.i.a.	$\times$ 10 <sup>3</sup>	$\times 10^{3}$	
160.0	517.7	10.955	1,555	
160.1	1074.7	6.352	2.319	
160.0	1501.2	5.374	2.921	
159.9	2007.2	5.086	3.209	
159.9	2887.2	4.971	4.134	
99.9	497.2	2.363	2.012	
99.9	1012.2	1.416	3.146	
100.0	1483.2	1.495	3.388	
100.1	2075.2	1.533	3.685	
100.1	3067.2	1.579	3.720	
100.1	4029.7	1.622	3.855	
100.1	4724.2	1.545	4.125	
160.1	4989.2	5.115	4.124	
160.1	4289.7	5.110	3.945	
160.0	4079.7	No vapor	3,826	
		sample taken		
160.0	3064.7	5.124	3.576	
219.9	4099.7	13.24	4.589	
220.2	3144.7	13.71	3.937	
219.9	2102.2	14.86	3,368	
219.9	1526.2	17.26	3.010	
220.0	1018.2	22.79	2.240	
220.1	534.2	37.37	1,329	
279.7	616.7	95.98	1.540	
279.8	1032.2	60.77	2.475	
280.2	1499.2	51.89	3.264	
280.1	2018.2	38.25	4.019	
280.0	3002.2	32.93	4.728	
279.9	4005.2	30.47	5.602	
279.8	3874.7	29.83	5.631	
280.0	1339.2	48.66	No liquid	
			sample	
			taken	
279.9	1556.2	44.43	3.375	
279.8	529.7	10.18	1.329	
100.1	513.2	2.347	1.907	
100.1	1002.2	1.542	2.854	
99.9	1000.2	1.485	2.854	
100.1	1000.2	1.532	3.134	

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### NOMENCLATURE

f =fugacity

- $f_i^{\circ}$  = fugacity of pure component *i* at temperature and pressure of system
  - = partial molal volume of component i in water phase
- P =pressure
- H = Henry's constant
- H'= modified Henry's constant as defined by Equation 1
- T= temperature
- X = mole fraction of hydrocarbon in water
- $(X_i)_v$ , Y = mole fractions in vapor phase

## Subscripts

- v = vapori = component i
- H = hydrocarbon
- L =water-rich liquid phase of system
- vapor pressure of solvent (water) at temperature s =

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