# Thermodynamic Properties of 2-Propanol 

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The compressibility of gaseous 2-propanol was determined by the Burnett method at $25^{\circ}$ intervals from $100^{\circ}$ to $200^{\circ} \mathrm{C}$. From the experimental compressibility data, the deviations of the thermodynamic functions from ideal behavior as well as the fugacity coefficients for 2 -propanol were calculated.

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HERE has been an increasing need for accurate thermodynamic data because of the rising importance of high pressure and high temperature industrial processes. This type of data for the alcohols has been very sparse and the use of generalized correlations to estimate the properties of these highly polar compounds results in serious error. Data on the volumetric behavior of gaseous 2-propanol have been obtained (3) which permit accurate values of the thermodynamic properties to be calculated

## THERMODYNAMIC RELATIONS

The thermodynamic properties calculated from $P V T$ data are obtained in the form of deviations of these properties from ideal behavior. The thermodynamic properties of a substance in the ideal gas state may be calculated from heat capacity data using the methods of statistical mechanics. The deviations from ideal behavior of the thermodynamic properties are determined in dimensionless form as shown in Table I.

The derivation of the expressions relating the functions in Table I to the compressibility factor, pressure, and temperature has been presented in detail by Heichelheim and McKetta (2). The resulting relations are as follows:

$$
\begin{gather*}
\frac{P}{R T}\left(V-V^{*}\right)=Z-1  \tag{1}\\
\frac{\left(U-U^{*}\right)}{R T}=-T \int_{0}^{P} \frac{(\partial Z / \partial T)_{p}}{P} d P-(Z-1)  \tag{2}\\
\frac{\left(H-H^{*}\right)}{R T}=-T \int_{0}^{P} \frac{(\partial Z / \partial T)_{p}}{P} d P  \tag{3}\\
\frac{\left(S-S^{*}\right)}{R}=-T \int_{0}^{P} \frac{(\partial Z / \partial T)_{p}}{P} d P-\int^{P} \frac{(Z-1)}{P} d P  \tag{4}\\
\frac{\left(G-G^{*}\right)}{R T}=\int_{0}^{P} \frac{(Z-1)}{P} d P  \tag{5}\\
\frac{\left(A-A^{*}\right)}{R T}=\int_{0}^{P} \frac{(Z-1)}{P} d P-(Z-1) \tag{6}
\end{gather*}
$$

The fugacity coefficients may also be obtained from the experimental compressibility data by using the relation

$$
\begin{equation*}
\nu=\exp \int_{0}^{P} \frac{(Z-1)}{P} d P \tag{7}
\end{equation*}
$$

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## CALCULATIONS

Calculation of the values of the thermodynamic functions for 2 -propanol was done in several steps. First the measured compressibility factors were plotted $v s$. pressure on a large scale graph. Next a cross plot of the compressibility factors vs. temperature for constant values of pressure was made. These compressibility isobars were then fitted as polynomials in $T$ using a least squares procedure, and the resulting expressions were differentiated analytically to give values of $\partial Z / \partial T$ at various pressures. For each isotherm, the values of $(\partial Z / \partial T)_{P} / P$ were fitted to polynomials in $P$ by a least squares procedure, and the resulting expression was integrated analytically to provide values of

$$
\int_{0}^{P} \frac{(\partial Z / \partial T)_{P}}{P} d P
$$

at various pressures.
To determine the values of the integral used in the free energy calculations, the isothermal values of $(Z-1) / P$ were first calculated. These values were fitted to a polynomial in $P$, again using a least squares procedure, and the resulting expression was integrated analytically to provide values of

$$
\int_{0}^{P} \frac{(Z-1)}{P} d P
$$

Table I. Dimensionless Form of Thermodynamic Functions

| $\quad$ Function | Dimensionless Form |
| :--- | :---: |
|  |  |
| Volume | $P\left(V-V^{*}\right) / R T$ |
| Internal energy | $\left(U-U^{*}\right) / R T$ |
| Enthalpy | $\left(H-H^{*}\right) / R T$ |
| Entropy | $\left(S-S^{*}\right) / R$ |
| Gibbs free energy | $\left(G-G^{*}\right) / R T$ |
| Helmholtz free energy | $\left(A-A^{*}\right) / R T$ |

${ }^{\text {a* }}$ Indicates property of an ideal gas.


Figure 1. Enthalpy deviation of 2-propanol
at various pressures. In all instances of polynomial fittings, the data were represented within the limits of their precision.

## RESULTS

The calculations were carried out with the aid of a CDC 1604 digital computer. The thermodynamic deviation functions and fugacity coefficients were calculated from the values of the integrals and are listed in Table II along with the values obtained for the integrals. The enthalpy,

Gibbs free energy, and entropy functions are shown in Figures 1, 2, and 3, and the fugacity coefficients in Figure 4.

Because of the method of computation, the thermodynamic deviation functions in Table II are internally consistent to 0.0001 ; however, they should be considered accurate to no more than 0.001 . The compressibility factor data from which the properties were calculated were estimated to be in error by less than $0.2 \%$ (3). Good accuracy in evaluating the integral

Table II. Thermodynamic Properties of 2-Propanol

| $\begin{gathered} \text { Temp., } \\ { }^{\circ} \mathrm{C} \mathrm{C}, \end{gathered}$ | $\begin{aligned} & \text { Press., } \\ & \text { Atm. } \end{aligned}$ | $z-1$ | $\int_{0}^{P} \frac{(Z-1)}{P} d$ | $\int^{P} \frac{(\partial Z / \partial T)_{p}}{P} d P$ | $\frac{U-U^{*}}{R T}$ | $\frac{H-H^{*}}{R T}$ | $\frac{A-A^{*}}{R T}$ | $\frac{G-G^{*}}{R T}$ | $\frac{S-S^{*}}{R}$ | Fugacity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 0 |  |  | - ${ }^{0}$ | ${ }^{0}$ | 0 | 0 | 0 | 0 | 1.0000 |
| 100 | 0.2 | $-0.0057$ | $-0.0059$ | ${ }^{0.0000735}$ | -0.0217 | $-0.0274$ | -0.0002 | -0.0059 | $-0.0215$ | 0.9941 |
| 100 | ${ }^{0.4}$ | ${ }^{-0.0113}$ | -0.0119 | 0.0001484 | $-0.0441$ | ${ }^{-0.0554}$ | $-0.0006$ | $-0.0119$ | $-0.0434$ | 0.9881 |
| 100 | 0.6 | $-0.0173$ | -0.0180 | ${ }^{0.00022248}$ | ${ }^{-0.0666}$ | -0.0839 | $-0.0007$ | -0.0180 | $-0.0659$ | 0.9821 |
| 100 | 0.8 | ${ }^{-0.0237}$ | $-0.0241$ | ${ }^{0.00033032}$ | $-0.0895$ | -0.1132 | ${ }^{-0.0004}$ | $-0.0241$ | -0.0891 | 0.9762 |
| 100 | 1.0 | -0.0304 | -0.0302 | 0.0003848 | -0.1132 | -0.1436 | 0.0002 | -0.0302 | -0.1134 | 0.9703 |
| 100 | 1.2 | $-0.0377$ | -0.0365 | ${ }^{0.0004705}$ | -0.1379 | -0.1756 | 0.0012 | -0.0365 | -0.1391 | 0.9642 |
| 100 100 | 1.4 | ${ }^{-0.0454}{ }^{-0.0550}$ | -0.0429 -0.0495 | ${ }_{0}^{0.00005622}$ | -0.1644 | -0.2098 -0.2478 | 0.0025 0.0055 | -0.0429 -0.0495 | -0.1668 -0.1983 | 0.9580 0.9517 |
| 100 | 1.7 | -0.0618 | $-0.0530$ | 0.0007222 | -0.2077 | -0.2695 | 0.0088 | $-0.0530$ | -0.2165 | 0.9484 |
| 100 | 1.8 | -0.0714 | -0.0568 | 0.0007886 | -0.2229 | -0.2943 | 0.0146 | -0.0568 | -0.2375 | 0.9448 |
| ${ }^{125}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1.0000 |
| 125 | 0.5 | -0.0111 | -0.0118 | 0.0001342 | -0.0423 | -0.0534 | $-0.0007$ | -0.0118 | -0.0417 | 0.9883 |
| 125 | 1.0 | -0.0228 | -0.0232 | 0.0002752 | -0.0868 | -0.1096 | -0.0004 | -0.0232 | -0.0864 | 0.9771 |
| 125 | 1.5 | -0.0349 | -0.0348 | ${ }^{0.0004253}$ | ${ }^{-0.1344}$ | ${ }^{-0.1693}$ | 0.0001 | -0.0348 | -0.1345 | 0.9658 |
| 125 | 2.0 | -0.0478 | $-0.0466$ | ${ }^{0.0005872}$ | -0.1860 | -0.2338 | 0.0012 | $-0.0466$ | -0.1872 | 0.9545 |
| 125 | 2.5 | -0.0618 | $-0.0586$ | 0.0007651 | -0.2428 | $-0.3046$ | 0.0032 | $-0.0586$ | -0.2460 | 0.9430 |
| 125 125 | ${ }_{3.5}^{3.0}$ | ${ }^{-0.0765}$ | ${ }^{-0.0712}$ | 0.0009655 0.0012000 | -0.3079 -0.3846 | -0.3844 -0.4778 | 0.0053 0.0090 | ${ }_{-0}^{-0.0712}$ | -0.3132 -0.3935 | 0.9313 0.9192 |
| 125 | 3.8 | -0.1047 | -0.0923 | 0.0013644 | ${ }_{-0.4385}$ | ${ }_{-0.5432}$ | 0.0124 | ${ }_{-0.0923}$ | -0.4509 | 0.9118 |
| 125 | 4.0 | -0.1140 | -0.0979 | 0.0014873 | -0.4782 | -0.5922 | 0.0161 | $-0.0979$ | -0.4943 | 0.9068 |
| 125 | 4.1 | -0.1202 | -0.1008 | 0.0015535 | -0.4983 | -0.6185 | 0.00194 | $-0.1008$ | -0.5177 | 0.9041 |
| 125 | 4.2 | -0.1294 | -0.1038 | 0.0016232 | -0.5169 | $-0.6463$ | 0.0256 | -0.1038 | $-0.5425$ | 0.9014 |
| 125 | 4.3 | -0.1510 | -0.1070 | 0.0016969 | $-0.5385$ | -0.6756 | 0.0440 | -0.1070 | $-0.5686$ | 0.8985 |
| 150 150 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 1.0000 |
|  | 1.0 | -0.0164 | -0.0167 | ${ }^{0.0001818}$ | ${ }^{-0.0605}$ | -0.0769 | -0.0003 | -0.0167 | -0.0602 | 0.9834 |
| 150 | 3.0 | ${ }_{-0.0519}$ | ${ }_{-0.0505}$ | 0.0006033 | ${ }_{-0.2034}$ | -0.2553 | ${ }_{0} .0014$ | -0.0505 | -0.2048 | ${ }_{0}$ |
| 150 | 4.0 | -0.0708 | -0.0681 | 0.0008519 | -0.2897 | -0.3605 | 0.0027 | -0.0681 | $-0.2924$ | 0.9342 |
| 150 | 5.0 | ${ }^{-0.0910}$ | ${ }^{-0.0861}$ | 0.0011319 | $-0.3879$ | $-0.4789$ | ${ }^{0.0049}$ | -0.0861 | $-0.3929$ | 0.9175 |
| 150 | 6.0 | -0.1130 | -0.1047 | 0.0014474 | -0.4994 | -0.6124 | 0.0083 | $-0.1047$ | -0.5078 | 0.9006 |
| 150 | 7.0 | -0.1374 | -0.1240 | 0.0018029 | ${ }^{-0.6255}$ | $-0.7629$ | 0.0134 | $-0.1240$ | $-0.6389$ | 0.8834 |
| 150 150 | 7.5 | -0.1509 -0.1661 | -0.1339 | 0.0019974 0.0022042 | -0.6943 | -0.8452 -0.9327 | ${ }_{0}^{0.0270}$ | -0.1339 -0.1441 | -0.7113 | 0.8747 0.8658 |
| 150 | 8.5 | -0.1850 | -0.1546 | 0.0024245 | -0.8409 | -1.0259 | 0.0304 | ${ }_{-0.1546}$ | ${ }_{-0.8713}$ | ${ }_{0.8567}$ |
| 175 | 0 | 0 |  | 0 |  | 0 | 0 | 0 |  | 1.0000 |
| 175 | 1.0 | -0.0127 | -0.0129 | 0.0001165 | -0.0395 | -0.0522 | -0.0002 | -0.0129 | -0.0393 | 0.9871 |
| 175 175 | ${ }_{3.0}^{2.0}$ | ${ }_{-0}^{-0.02391}$ | - ${ }^{-0.0256}$ | 0.0002349 0.0003562 | ${ }_{-0}^{-0.0795}$ | ${ }_{-0}^{-0.1053}$ | 0.0002 0.0007 | -0.0256 | -0.0797 -0.1213 | ${ }^{0.9747}$ |
| 175 | 4.0 | -0.0527 | ${ }_{-0.0514}$ | 0.0004821 | ${ }_{-0.1633}$ | -0.2160 | 0.0013 | ${ }_{-0.0514}$ | ${ }_{-0.1646}$ | 0.9499 |
| 175 | 5.0 | -0.0669 | -0.0647 | 0.0006144 | -0.2084 | -0.2753 | 0.0022 | -0.0647 | -0.2106 | 0.9373 |
| 175 | 6.0 | -0.0816 | -0.0782 | 0.0007559 | -0.2571 | -0.3387 | 0.0034 | -0.0782 | -0.2606 | 0.9248 |
| 175 | 7.0 | ${ }^{-0.0969}$ | -0.0919 | ${ }^{0.00099094}$ | -0.3107 | -0.4076 | ${ }^{0.0050}$ | -0.0919 | -0.3157 | 0.9122 |
| 175 | ${ }_{9}^{8.0}$ | -0.1130 -0.1297 | -0.1058 | ${ }^{0.0010785}$ | ${ }^{-0.3703}$ | ${ }^{-0.4833}$ | ${ }^{0} 0.0072$ | -0.1058 | -0.318 | 0.8996 |
| 175 | 10.0 | ${ }_{-0.1472}$ | ${ }_{-0.1344}$ | ${ }_{0} .0014781$ | ${ }_{-0.5152}$ | -0.6624 | 0.0128 | ${ }_{-0.1344}$ | ${ }^{-0.5488}$ | ${ }_{0} .8874$ |
| 175 | 11.0 | $-0.1656$ | -0.1493 | 0.0017162 | -0.6035 | -0.7691 | 0.0163 | ${ }_{-0.1493}$ | ${ }^{-0.6198}$ | 0.8613 |
| 175 | ${ }^{12.0}$ | $-0.1851$ | -0.1645 | 0.0019847 | -0.7043 | ${ }^{-0.8894}$ | 0.0206 | -0.1645 | -0.7249 | 0.8483 |
| 175 | 13.0 14.0 | -0.2062 -0.2296 -0.250 | -0.1801 -0.1961 | ${ }_{0}^{0.00228888}$ | ${ }_{-0.8186}^{-0.9468}$ | ${ }_{-1.0248}^{-1.1744}$ | ${ }^{0.0261}$ | ${ }^{-0.1801}$ | -0.8447 | 0.8352 |
| 175 | 15.0 | -0.2587 | -0.2129 |  |  |  | ${ }_{0} 0.0458$ | ${ }_{-0.2129}$ | -0.9802 | $\begin{aligned} & 0.8219 \\ & 0.8082 \end{aligned}$ |
| 200 |  |  |  |  |  |  | 0 |  |  | 1.0000 |
| 200 | 2.0 | ${ }^{-0.0206}$ | -0.0205 | ${ }^{0.0001533}$ | -0.0520 | -0.0726 | 0.0001 | -0.0205 | -0.0502 | 0.979 |
| 200 | 4.0 | $-0.0416$ | -0.0411 | ${ }^{0.00003085}$ | -0.1044 | $-0.1460$ | 0.0005 | -0.0411 | -0.1049 | 0.9597 |
| ${ }_{200}^{200}$ | ${ }_{8.0}^{6.0}$ | ${ }^{-0.0632}$ -0.0860 | ${ }_{-}^{-0.0621}$ | ${ }^{0.00004671}$ | -0.1578 | ${ }_{-0.2210}^{0.0285}$ | 0.0011 | ${ }_{-0}^{0.0621}$ | -0.1589 | 0.9398 |
| 200 | 10.0 | ${ }^{-0.1103}$ | ${ }_{-0.1057}$ | 0.0008021 | ${ }_{-0.2692}$ | -0.3795 | ${ }_{0} 0.0046$ | ${ }_{-0.1057}$ | ${ }_{-0.2739}$ | 0.8997 |
| 200 | 12.0 | -0.1356 | -0.1282 | 0.0009839 | -0.3299 | $-0.0074$ | 0.0074 | -0.1282 | -0.3373 | 0.8796 |
| 200 | 14.0 | -0.1627 | -0.1514 | 0.0011795 | -0.3954 | -0.5581 | 0.0113 | -0.1514 | -0.4067 | 0.8595 |
| 200 | 16.0 18.0 | ${ }^{-0.1818}$ | ${ }^{-0.1752}$ |  |  |  | 0.0166 | ${ }_{-0.1752}$ |  | 0.8393 |
| 200 | 20.0 | -0.2571 | -0.2250 |  |  |  | 0.0321 | ${ }_{-0.2250}$ |  | ${ }_{0} .8985$ |
| 200 | ${ }_{22}^{22.0}$ | $-0.2949$ | ${ }_{-0}-0.2513$ |  |  |  | 0.0436 | $-0.2513$ |  | 0.7778 |
| 200 | 24.0 | $-0.3383$ | -0.2787 |  |  |  | 0.0596 | $-0.2787$ |  | 0.756 |



Figure 2. Gibbs free energy deviation of 2-propanol


Figure 3. Entropy deviation of 2-propanol

$$
\int_{0}^{P} \frac{Z-1}{P} d P
$$

should have allowed no more than $1 \%$ error in the Gibbs free energy function. The Helmholtz free energy function should be somewhat more accurate because of the cancellation effect of errors in $Z-1$. As a result of the differentiation, evaluation of the integral

$$
\int_{0}^{P} \frac{(\partial Z / \partial T)_{P}}{P} d P
$$

was subject to greater uncertainties. The error in the internal energy and enthalpy functions is therefore estimated not to exceed $2 \%$. The entropy function consequently may be in error by as much as $3 \%$. The minimum accuracy of the fugacity coefficient $f / P$ should be $0.3 \%$.


Figure 4. Fugacity coefficients of 2-propanol

Calculation of the thermodynamic properties of 2 -propanol vapor from the data of Table II requires only the corresponding properties of the ideal gas state. Green has computed the ideal gas constant pressure heat capacity, enthalpy, Gibbs free energy, and entropy from $0^{\circ}$ to $1000^{\circ}$ K.(1).

## NOMENCLATURE

| $A$ | $=$ Helmholtz free energy |
| ---: | :--- |
| $f$ | $=$ fugacity |
| $G$ | $=$ Gibbs free energy |
| $H$ | $=$ enthalpy |
| $P$ | $=$ pressure |
| $R$ | $=$ gas constant |
| $S$ | $=$ entropy |
| $T$ | $=$ absolute temperature |
| $U$ | $=$ internal energy |
| $V$ | $=$ molal volume |
| $Z$ | $=$ compressibility factor, $P V / R T$ |
| $v$ | $=$ fugacity coefficient, $f / P$ |

## Superscripts

* = property of ideal gas state


## literature cited

(1) Green, J.H.S., Trans. Faraday Soc. 59, 1559 (1963).
(2) Heichelheim, H.R., McKetta, J.J., Chem. Eng. Progr. Symp. Ser. 59, No. 44, 23 (1963).
(3) Moreland, M.P., McKetta, J.J., Silberberg, I.H., J. Chem. Eng. Data 12, 329 (1967).
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