# Latent Heats of Vaporization of Hydrocarbons

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> Latent heats of vaporization for different types of hydrocarbons were calculated using the rigorous Clapeyron equation, the Frost-Kalkwarf vapor pressure relationship, and experimental saturated vapor and liquid densities obtained from the literature. The calculated values ranged in temperature up to and including the critical point and were used to develop the relationship,  $\lambda = \lambda_o [1 - T_R]^{0.39}$  where  $\lambda_o$  is a constant for each hydrocarbon and represents the hypothetical latent heat of vaporization at  $T = 0^\circ$  K. For the hydrocarbons investigated,  $\lambda_o$  depended on molecular weight as follows:  $\lambda_o = 800 M^{0.72}$  where  $\lambda_o$  has the units B.t.u. per pound-mole. These relationships were used to calculate latent heats of vaporization, which, when compared with values obtained from the Clapeyron equation, produced an average deviation of 2.6% for 184 values representing 23 hydrocarbons. Values were also calculated and compared with calorimetric measurements presented in the literature for several hydrocarbons to produce an average deviation of 3.0% for 58 values representing nine hydrocarbons. Values for four of these hydrocarbons were not used in the development of the relationships of this study.

**A** NUMBER of methods are presented in the literature for the calculation of the latent heats of vaporization of substances in their saturated liquid state. In 1923, Kistiakowsky (7) presented the relationship

$$\lambda_b = T_b \left[ 8.75 + 4.576 \log T_b \right] \tag{1}$$

which permits the calculation of the latent heat of vaporization of nonpolar substances at their normal boiling point. Another relationship for establishing this value was proposed in 1954 by Riedel (15):

$$\lambda_b = T_b \ \frac{5 \log P_c - 2.17}{0.930 - T_b/T_c} \tag{2}$$

To predict heats of vaporization for temperatures below the normal boiling point, Othmer (13) utilizes water as a reference substance and presents the following relationship:

$$\frac{\lambda}{\lambda_{w}} = \frac{\log \frac{p_{2}}{p_{1}} \Delta z}{\log \frac{p_{w_{2}}}{p_{w_{1}}} \Delta z_{w}}$$
(3)

where  $\Delta z = z_v - z_l = [1 - P_R/T_R^3]^{1/2}$ . To cover the entire temperature range up to the critical point, Watson (20) proposed the relationship

$$\frac{\lambda}{\lambda'} = \left[\frac{1 - T_R}{1 - T'_R}\right]^{0.38} \tag{4}$$

where  $\lambda'$  is the latent heat of vaporization at  $T'_{k}$ . Equation 4 has the advantage over Equation 3 in that it does not require any vapor pressure data but does require a knowledge of a single latent heat of vaporization value. This value can be readily obtained through the use of Equation 1 or 2. Although the use of Equations 1 and 4 allows the calculation of latent heats of vaporization, a single relationship capable of predicting these values directly would be advantageous.

#### LATENT HEATS OF VAPORIZATION

To obtain latent heats of vaporization over a wide range of temperatures, the thermodynamically exact Clapeyron relationship

$$\frac{dP}{dT} = \frac{\lambda}{T(v_v - v_l)} \tag{5}$$

can be applied using vapor pressure data and saturated vapor and liquid densities. In order to express  $\lambda$  in terms of reduced variables, Equation 5 has been transformed to the following:

$$\lambda = z_c R T_c T_R [v_{R_i} - v_{R_i}] \frac{dP_R}{dT_R}$$
(6)

In this investigation the vapor pressure equation of Frost and Kalkwarf (4) has been used in reduced form to obtain the slopes,  $dP_R/dT_R$ , for temperatures ranging from the triple point to the critical point of a number of hydrocarbons including normal paraffins, olefins, diolefins, naphthenes, and aromatics. This reduced vapor pressure equation can be expressed as follows:

$$\ln P_{R} = \alpha + \frac{\beta}{T_{R}} + \gamma \ln T_{R} + \frac{27}{64} \frac{P_{R}}{T_{R}^{2}}$$
(7)

Equation 7 possesses the unique boundary condition that  $\alpha + \beta + 27/64 = 0$ . Upon differentiation, Equation 7 produces the slope in reduced variables as follows:

$$\frac{dP_R}{dT_R} = \frac{\frac{1}{T_R} \left[ \gamma - \frac{\beta}{T_R} - \frac{54}{64} \frac{P_R}{T_R^2} \right]}{\frac{1}{P_R} - \frac{27}{64} \frac{1}{T_R^2}}$$
(8)

Values of  $\beta$  and  $\gamma$  for the hydrocarbons considered in this investigation were obtained from the vapor pressure studies

		Critical Constants					<b>)</b> .	2	
			<u> </u>		ρ.,	Vapor Pressure Constants			Av.
	М	$Z_c$	<i>T</i> <sub>c</sub> , ° K.	$P_{ m c}$ , atm.	g./cc.	β	γ	LbMole	Dev. %
n-Paraffins									
Methane	16.04	0.289	191.1	45.8	0.162	-6.84018	-2.70212	5,400	3.93
Ethane	30.07	0.284	305.4	48.20	0.205	-8.07324	-3.60963	9,400	1.85
Propane	44.09	0.279	370.0	42.0	0.220	-8.88467	-4.24329	12,100	1.39
n-Butane	58.12	0.274	425.4	37.43	0.228	-9.57174	-4.80311	$14,\!650$	1.08
<i>n</i> -Pentane	72.15	0.269	469.8	33.31	0.232	-10.28884	-5.33564	16,900	2.23
n-Hexane	86.17	0.264	507.9	29.94	0.233	-11.01386	-5.90492	19,250	1.97
n-Heptane	100.20	0.260	540.6	26.95	0.235	-11.72872	-6.46159	$21,\!600$	1.07
n-Octane	114.22	0.255	569.4	24.64	0.233	-12.53570	-7.15220	22,700	5.27
<i>n</i> -Nonane	128.25	0.250	593.8	23.25	0.234	-13.18787	-7.59158	25,750	2.34
n-Decane	142.28	0.245	616.1	21.65	0.234	-13.95281	-8.21951	28,000	1.18
<i>n</i> -Undecane	156.30	0.240	636.0	20.27	0.233	-14.80003	-8.98351	30,200	0.83
n-Dodecane	170.33	0.235	653.9	19.06	0.232	-15.72640	-9.80767	32,800	2.53
Olefins									
Ethylene	28.05	0.284	283.1	50.5	0.215	-11.74860	-3.75709	8.600	4.85
Propylene	42.08	0.275	365.0	45.6	0.233	-9.99865	-4.26637	11,800	1.70
Diolefins									
1,3-But <b>a</b> diene	54.09	0.270	425.2	42.7	0.245	-9.48450	-4.71334	14,400	2.82
Naphthenes									
Cyclohexane	84.16	0.272	553.0	40.0	0.273	-10.04415	-5.26151	19,350	0.64
Aromatics									
Benzene	78.11	0.270	562.2	48.60	0.304	-10.06536	-5.28840	19.350	5.92
Toluene	92.13	0.271	593.5	41.56	0.290	-10.44129	-5.45371	21,200	2.86
Ethylbenzene	106.16	0.266	616.1	36.51	0.288	-11.18362	-6.05908	23,100	2.72
o-Xylene	106.16	0.268	632.1	36.83	0.281	-11.07859	-5.94175	23,100	3.01
<i>m</i> -Xylene	106.16	0.268	625.1	35.91	0.277	-11.04194	-5.91474	23.100	3.01
<i>p</i> -Xvlene	106.16	0.268	618.2	35.01	0.273	-11.09776	5.89868	23,100	3.30
<i>n</i> -Propylbenzene	120.19	0.262	638.8	32.0	0.28	-11.62240	-6.36370	24,700	2.63
		-							

Table I. Basic Constants for the Calculation of Latent Heats of Vaporization and the Resulting Deviations

of the saturated (18), unsaturated (17), naphthenic (14), and aromatic (1) hydrocarbons. These values with the critical constants of these hydrocarbons are summarized in Table I. The critical constants presented in Table I were obtained from the compilation of Kobe and Lynn (8) or were estimated by a group contribution method (19).

The use of Equations 7 and 8 at a fixed temperature  $T_R$  permits the calculation of  $dP_R/dT_R$ . The molar volumes

lation of  $dP_R/dT_R$ . The molar volumes and have slopes of 0.39. This slope is in close agreement

Table 11. Comparison of Latent Heats of Vaporizationfor n-Heptane Calculated with Clapeyron Equationand Equations 9 and 10

	$\lambda$ , B.t.u./		
$T_R$	Clapeyron	Eq. 9, 10	Deviations, $\%$
0.650	14,300	14,475	-1.23
0.700	13,400	13,631	-1.73
0.750	12,580	12,695	-0.92
0.800	11,460	11,637	-1.55
0.825	10,930	11,046	-1.07
0.850	10,290	10,402	-1.09
0.875	9,623	9,688	-0.68
0.900	8,802	8,880	-0.90
0.925	7,823	7,938	-1.48
0.950	6,718	6,777	-0.88
0.975	5,106	5,171	-1.29
1.000	0	0	0.00
			1.07



of the saturated vapor and liquid states reported by Brad-

ford (2) were used in Equation 6 to obtain values of  $\lambda$  ranging from the triple point to the critical temperature

of each hydrocarbon. The resulting values of  $\lambda$  were related to the variable  $1 - T_R$  on log-log coordinates to produce

for each hydrocarbon the essentially linear relationships

presented in Figure 1. These relationships are nearly parallel

with the value of 0.38 reported by Watson (20). The straight lines of Figure 1 suggest a relationship of the form

$$\lambda = \lambda_0 [1 - T_R]^{0.39} \tag{9}$$

where  $\lambda_0$  is a hypothetical latent heat of vaporization at  $T = 0^{\circ}$  K. Values of  $\lambda_0$  were obtained from Figure 1, are summarized in Table I, and are plotted against molecular weight in Figure 2 to produce the analytical expression

$$\lambda_0 = 800 \ M^{0.72} \tag{10}$$

Equation 10 represents the behavior of hydrocarbons of all types including n-paraffins above methane, olefins, diolefins, naphthenes, and aromatics.

Equations 9 and 10 have been developed from basic physical data for hydrocarbons, and thus, their application should not be extended to other types of substances. Further work in this area should be carried out before any generalizations can be drawn.



Figure 2. Linear relationship between log  $\lambda_0$  and log M for the hydrocarbons investigated

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\lambda$ , B.t.u./LbMole			Aole		$\lambda$ , B.t.u./LbMole			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	<i>T</i> , ° K.	Exptl.	Calcd.	Deviation, %	$T, \circ K.$	Exptl.	Calcd.	Deviation, %	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1-Butene (9); $T_c = 419.6^{\circ}$ K.			K.		Cyclohexane (10); $T_c = 553.0^\circ$ K.			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	311.0	8350	8590	-2.87	311.0	13,832	14,100	-1.94	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	327.6	7857	8052	-2.48	327.6	13,462	13,713	-1.87	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	344.3	7295	7455	-2.19	344.3	13,076	13,309	-1.78	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	361.0	6593	6756	-2.47	361.0	12,585	12,883	-2.37	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	377.6	5806	5926	-2.07	377.6	12,215	12,436	-1.81	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					394.3	11.721	11,960	-2.04	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				2.42	411.0	11.263	11.454	-1.70	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		2-Butene (6)	; $T_c = 430.0^\circ$	K.	444.3	10,673	10,909	-2.21	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	311.0	8834	8819	0.18				1 96	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	327.6	8368	8317	0.60		<b></b> (	_		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	344.3	7815	7764	0.65		n-Hexane (5)	; $T_c = 507.9^\circ$	K.	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	361.0	7230	7141	1.02	311.0	13,191	13.681	-3.71	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	377.6	6478	6418	0.92	327.6	12,731	13,217	-3.82	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	394.3	5483	5539	-1.02	344.3	12,315	19,217	-3.34	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	001.0	0100	0000	1.02	361.0	11 777	12,127	-3.63	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				0.77	377.6	11 262	11 644	-0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		1-Pentene (1	6) $\cdot T_{1} = 474^{\circ}$	к	394 3	10.679	11,044	-0.00	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		1 1 01100110 (1	07, 17 - 111		411.0	10,075	10.277	-3.37	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	284.0	11 201	11.040	E 00	411.0	0.242	0.641	-3.08	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	298.2	10.958	11,545	-0.83	427.0	0,040	9,041	-3.19	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	303.1	10,555	11,093	-0.80	444.5	0,000	0,000	-3.17	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	000.1	10,040	11,404	-5.76				3.41	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				5.79		n-Octane (12	$T_c = 569.4$	° K	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 1	Act hul 9 huton	(1c) T	<b>7</b> 0.00 <b>1</b> 7	311.0	17,456	17,820	-2.09	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2-1	vietnyi-z-butene	$= (10); 1_c = 4$	70.0° K.	327.6	16,981	17,363	-2.25	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					344.3	16,415	16.885	-2.87	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	289.9	11,835	11.740	0.80	361.0	15,858	16,388	-3.34	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	298.2	11,642	11.527	0.99	377.6	15,368	15,863	-3.22	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	311.7	11.317	11.163	1.36	394.3	14,749	15,310	-3.81	
1.0511,0511,0511,0511,10-2.98 $n$ -Pentane (11); $T_c = 469.8^{\circ}$ K.427.613,69314,101-2.98311.011,06611,413-3.14444.313,02913,429-3.07327.610,59510,930-3.16344.320,50520,420-2.13361.09,5849,848-2.75361.019,93320,138-1.56377.68,9829,241-2.78377.619,31319,616-1.57394.38,3168,540-2.70394.318,77519,068-1.03411.07,5377,749-2.81411.018,11218,497-0.67444.36,5716,805-3.55427.617,42617,895-2.693.001.69-2.19-2.19-2.19-2.19-2.19		,	,•		411.0	14,361	14 726	-2.54	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				1.05	427.6	13 693	14 101	-2.98	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		n Dontono (11	). T 400.0	• <b>V</b>	444.3	13,029	13 429	-3.07	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		<i>n</i> -rentane (11	); $I_c = 469.8$	° K.		10,020	10,120	2.01	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	311.0	11.066	11 413	-314		» D	. T 010 10	2.31	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	327.6	10,595	10,930	-3.14		n-Decane (3)	); $I_c = 616.1$	'n.	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	344.3	10,100	10,000	-3.08	344.3	20,505	20,420	-2.13	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	361.0	9.584	9 848	-2.75	361.0	19,933	20,138	-1.56	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	377.6	8,982	9.241	-2.78	377.6	19,313	19,616	-1.57	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	394.3	8,316	8,540	-2.70	394.3	18,775	19,068	-1.03	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	411.0	7.537	7 749	-2.81	411.0	18,112	18,497	-0.67	
444.3     16,890     17,259     -2.19       3.00     1.69	444.3	6.571	6.805	-3.55	427.6	17,426	17,895	-2.69	
3.00		0,012	0,000	0.00	444.3	16,890	17,259	-2.19	
				3.00				1.69	

Table III. Calculated and Experimental Latent Heats of Vaporization for Several Hydrocarbons

## COMPARISON OF CALCULATED AND EXPERIMENTAL VALUES

Equations 9 and 10 were used to calculate latent heats of vaporization for the hydrocarbons used to develop these relationships. These calculated values were compared with the ones from the Clapeyron equation to obtain for each hydrocarbon the average deviation presented in Table I. Maximum deviations are encountered with ethylene, benzene, and *n*-octane, while minimum deviations occur with cyclohexane, n-heptane, and n-undecane. For n-heptane, the deviations are presented in Table II for the temperature range  $0.65 \leq T_R \leq 1.00$ . The average deviation for *n*-heptane was 1.07% and the over-all average deviation for the 23 hydrocarbons used in this study was 2.6%.

Calorimetric measurements presented in the literature for a number of hydrocarbons were compared with corresponding values obtained from Equations 9 and 10. Table III presents calculated and experimental latent heats of vaporization for nine hydrocarbons along with their resulting deviations. n-Pentane, cyclohexane, n-hexane, n-octane, and n-decane were five of the 23 original hydrocarbons used for the development of Equations 9 and 10. The average deviations for these five hydrocarbons ranged from 1.69% for *n*-decane to 3.41% for *n*-hexane. The remaining four hydrocarbons were butenes and pentenes which were not included in the development of the basic relationships. The average deviation for the nine hydrocarbons was 3.0%.

# NOMENCLATURE

- M =molecular weight
- vapor pressure = pP
- = pressure, atm.
- $P_{c}$ = critical pressure, atm.
- $P_R$ = reduced pressure,  $P/P_c$
- R = gas constant, 82.055 atm. cc./g.-mole ° K.
- Т = temperature, °K.
- Т = normal boiling point, °K.
- $\hat{T}_c$ = critical temperature, ° K.
- $T_R$ = reduced temperature,  $T/T_{c}$
- = molar volume, cc./g.-mole υ
- $v_c$ = critical volume, cc./g.-mole
- molar volume for saturated liquid, cc./g.-mole  $v_i =$
- $v_v =$ molar volume for saturated vapor, cc./g.-mole
- $v_R$  = reduced volume for saturated liquid state,  $v_l/v_c$
- $v_{R_i}$ = reduced volume for saturated vapor state,  $v_v/v_c$

- $z_c$  = critical compressibility factor,  $P_c v_c / RT_c$
- = compressibility factor for saturated vapor, Pv/RTΖ.
- compressibility factor for saturated liquid, Pv/RT= Z

## **Greek Letters**

- $\alpha,\beta,\gamma$  = constants, Equation 7
  - latent heat of vaporization, B.t.u./lb.-mole λ =
  - $\lambda_b$ = latent heat of vaporization at the normal boiling point, cal./g.-mole
  - $\lambda_0 =$ hypothetical latent heat of vaporization at 0° K., B.t.u./ lb.-mole
  - latent heat of vaporization of water, Equation 3  $\lambda_{w}$ =
  - = critical density, g./cc.  $\rho_c$

## Subscript

w = water

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- RECEIVED for review March 13, 1967. Accepted April 10, 1967.