# Table I: Densities of KOH Solutions

Temperature, °C.	Concn., Wt.% KOH	Number of Measurements	Density, G./Cc.
59.9	$6.17 \\ 11.50 \\ 20.90$	16 15	$1.0381 \pm 0.0001$ $1.0863 \pm 0.0002$ $1.1758 \pm 0.0002$
	27.80	10	$1.2448 \pm 0.0001$
	36.00 43.00	11 10	$1.3294 \pm 0.0002$ $1.4080 \pm 0.0001$
	47.20	10	$1.4560 \pm 0.0001$
79.9	50.37 6.17	10	$1.4957 \pm 0.0001$ $1.0269 \pm 0.0001$
	11.50	10	$1.0746 \pm 0.0001$
	20.90 27.80	9 10	$1.1652 \pm 0.0001$ $1.2329 \pm 0.0001$
	36.00	10	$1.3180 \pm 0.0001$
	$43.00 \\ 47.20$	9	$1.3973 \pm 0.0001$ $1.4442 \pm 0.0008$
99.2	50.37 36.0	10 14	$1.4848 \pm 0.0001$ $1.3073 \pm 0.0001$
00.2	43.0	14	$1.3858 \pm 0.0001$
	43.97 55.4	9 15	$1.3969 \pm 0.0001$ $1.5324 \pm 0.0001$
100 5	59.46	15	$1.5809 \pm 0.0001$
120.5	$55.4 \\ 59.46$	20 18	$1.5205 \pm 0.0001$ $1.5683 \pm 0.0001$
1.4.1	65.1	13	$1.6342 \pm 0.0001$
141	55.72	16	$1.4901 \pm 0.0001$ $1.5160 \pm 0.0001$
	59.71 65.1	10 10	$1.5622 \pm 0.0001$ $1.6268 \pm 0.0001$
161.4	64.68	16	$1.6086 \pm 0.0001$ $1.6086 \pm 0.0001$
	$72.25 \\ 77.1$	$\frac{16}{16}$	$1.7046 \pm 0.0001 \\ 1.7652 \pm 0.0001$

calculated by extrapolating values determined at lower temperatures using a power series in temperature for the volumetric expansion coefficient. Calibration of the plummet was repeated at frequent intervals during the measurements, and a small decrease in volume with time was observed at the higher temperatures. Solutions to be studied were maintained at the required temperature in an oil bath controlled to  $0.02^{\circ}$  C.

To prevent a rapid change in concentration by evaporation, an atmosphere of nitrogen presaturated with water vapor at a partial pressure equal to the equilibrium vapor pressure of the KOH solution was maintained over the surface of the sample studied. This was achieved by first passing the nitrogen stream through a series of presaturators containing pure water, and maintained at a temperature such that the vapor pressure of water was nearly equal to the known vapor pressure of the KOH solution (4) at the temperature under study. Final equilibration of the nitrogen stream was attained by passing it through a presaturator containing the KOH solution under study at the temperature of the density measurement. As a check against possible changes in concentration, a number of density measurements were made on the same sample and examined for any drift in density with time. At the higher temperatures, concentrations were determined by titration before and after an experiment.

## RESULTS

The measured densities are shown in Table I. The uncertainties listed are the standard deviations from the arithmetic mean. The analysis accuracy was estimated to be 0.2% of the concentration value.

The data at 59.9° and 79.9° C. may be compared with hydrometer readings (4); agreement between the two sets of data is within 0.07% for almost all points.

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# Vapor-Liquid Equilibria at 60° C. for *n*-Hexane–Alkyl Amines and 1-Hexene–Alkyl Amines

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**E**FFECTIVE separation of close boiling hydrocarbon mixtures often necessitates an uneconomical number of trays in a fractionator. An extractive distillation process may reduce the cost of the separation by changing the volatility characteristics of the mixture through the addition of a polar compound (solvent) to the hydrocarbon mixture. The solvent, if effective, will selectively interact with one or more of the hydrocarbon components. The solution complexities resulting from the interactions are difficult to define theoretically and quantitatively. This investigation is a por-

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tion of an experimental program at The University of Texas to determine the influence of various types of polar compounds in modifying the solution nonideality.

Binary vapor-liquid equilibrium data were determined at  $60^{\circ}$  C. for *n*-butylamine, diethylamine, *n*-hexylamine, di-*n*-propylamine, diisopropylamine, and triethylamine with each of the hydrocarbons, *n*-hexane and 1-hexene.

#### EXPERIMENTAL

Materials. All materials used for the experimental work were checked for purity by a Beckman GC-2 gas chroma-

Binary vapor-liquid equilibrium data are reported at  $60^{\circ}$  C. for *n*-butylamine, diethylamine, *n*-hexylamine, di-*n*-propylamine, diisopropylamine, and triethylamine with each of the hydrocarbons, *n*-hexane and 1-hexene. The *n*-butylamine was the most effective solvent in modifying the volatility of *n*-hexane relative to 1-hexene. The terminal binary hydrocarbon activity coefficient ratios produced by the various amines were: *n*-butylamine-1.23, *n*-hexylamine-1.18, diethylamine-1.14, di-*n*-propylamine-1.10, diisopropylamine-1.07, and triethylamine-1.03.

tograph, and a Bausch and Lomb precision refractometer. The normal boiling point was also used as an indication of the purity of the lower boiling materials. Table I summarizes the measured and reported values. Disagreement among some published literature values for the amines suggest that some properties, particularly refractive indices, have not been well established.

The two hydrocarbons used in this study, *n*-hexane and 1-hexene, were pure grade chemicals obtained from the Phillips Petroleum Co. The guaranteed minimum purities were 99 mole %, and, consequently, they were used without further purification.

The amines, supplied by the Union Carbide Chemicals Corp., were purified by chemical treatment and subsequent distillation. The liquid amines were in contact with potassium hydroxide pellets for a minimum of three days with intermittent agitation. The supernatant liquid was then drained off and distilled over reagent grade calcium oxide in a 35-plate Oldershaw column. The heartcut of the overhead product was used as the purified product. This procedure is similar to that used by Wiberg (12). The chromatograms of the purified materials indicated purities no lower than 99.3% after treatment.

The amines used in this study are members of either the  $C_4$  or  $C_6$  isomeric series and are primary,  $RNH_2$ , secondary,  $R_2NH$ , or tertiary,  $R_3N$ , where R is a saturated radical. These are listed below.

Compound	Type C₄ Series	Structure
<i>n</i> -Butylamine Diethylamine	Primary Secondary	$\begin{array}{c} CH_3(CH_2)_3NH_2\\ (CH_3CH_2)_2NH \end{array}$
	C <sub>6</sub> Series	
<i>n</i> -Hexylamine Di- <i>n</i> -propylamine Diisopropylamine Triethylamine	Primary Secondary Secondary Tertiary	$\begin{array}{l} CH_{3}(CH_{2})_{5}NH_{2}\\ (CH_{3}CH_{2}CH_{2})_{2}NH\\ [(CH_{3})_{2}CH]_{2}NH\\ (C_{2}H_{5})_{3}N\end{array}$

The principal difference between the normal primary and secondary amines in either series is chemical rather than physical, in that both compounds have identical molecular weights and similar structures but differ in the number of hydrogen atoms attached to the nitrogen atom. Triethylamine is characterized by having no hydrogen atoms bonded to the nitrogen atom.



Table I. C	Comparison	of	Measured	Properties	with	Literature	Values
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	Molecular	Normal Bo	iling Point	Refractive Index $(n_{\rm D})$ at 20° C.		
Compound	Weight	Experimental	Literature	Experimental	Literature	
n-Hexane	86.2	68.78	68.74	1.37492	1.37486	
1-Hexene	84.2	63.51	63.49	1.38792	1.38786	
<i>n</i> -Butylamine	73.1	77.5	77.8	1.4009	.1.40086	
Diethylamine	73.1	55.33	55.5	1.38477	1.3850	
n-Hexylamine	101.2		132.7	1.41842	1.4190	
Di-n-propylamine	101.2		109.2	1.4040	1.4042	
Diisopropylamine	101.2	83.3	83.5	1.39146	1.3912	
Triethylamine	101.2	89.45	89.35	1.4013	1.4010	

<sup>a</sup> (1, 2, 9, 11).

	$n$ -Butylan $A_{12} =$	nine (1) and $n$ - 0.7842, $A_{21} = 0$	Hexane (2) 0.6023			Di-n-propylan $A_{12} =$	mine (1) and $n$ 0.760, $A_{21} = 1$ .	-Hexane (2) 0774	
$\boldsymbol{x}_1$	$y_1$	<i>P</i> , Mm.	$\gamma_1$	$\gamma_2$	$x_1$	${\mathcal Y}_1$	<i>P</i> , Mm.	$\gamma_1$	$oldsymbol{\gamma}{}_2$
0.128	0.149	601.8	1.659	1.023	0.114	0.036	526.1	1.159	1.002
0.218	0.226	615.7	1.509	1.060	0.222	0.073	483.0	1.109	1.011
0.348	0.311	617.2	1.306	1.134	0.379	0.138	419.8	1.074	1.029
0.465	0.399	605.0	1.229	1.183	0.528	0.216	359.1	1.036	1.058
0.642	0.520	572.7	1.100	1.340	0.702	0.353	284.1	1.016	1.100
0.806	0.664	524.0	1.027	1.586	0.847	0.552	215.8	1.007	1.133
0.896	0.784	483.5	1.008	1.770	0.918	0.710	160.4	1.003	1,141
	n-Butylon	nine (1) and 1-1	Hevene (3)			Di-n-propyla $A_{13} =$	mine (1) and 1 1.1834, $A_{31} = 0$	- <b>Hexene</b> (3) 0.7780	
	$A_{13} =$	$0.7593, A_{31} = 0$	.7572		$x_1$	$y_1$	<i>P</i> , Mm.	$\gamma_1$	<b>γ</b> 3
					0.112	0.027	620.4	1.040	1.004
$x_1$	$y_1$	P, Mm.	$\gamma_1$	$\gamma_3$	0.218	0.058	564.1	1.045	1.007
0.129	0.119	680.6	1.479	1.013	0.376	0.116	478.0	1.034	1.009
0.251	0.206	676.4	1.306	1.056	0.379	0.116	477.9	1.018	1.015
0.354	0.277	661.8	1.221	1.091	0.534	0.196	394.7	1.021	1.020
0.483	0.368	634.8	1.142	1.146	0.694	0.322	308.1	1.016	1.028
0.634	0.478	592.5	1.057	1.253	0.834	0.506	231.6	1.004	1.044
0.791	0.635	532.8	1.017	1.383	0.921	0.703	182.5	0.999	1.050
0.897	0.784	481.9	1.003	1.517		Diisonropula	mine (1) and a	Uovana (2)	
						$A_{12} =$	1.0247, $A_{21} = 0$	).8821	
	Diethylan	ine $(1)$ and $n$ -l	Hexane (2)		$x_1$	$\mathbf{y}_1$	<i>P</i> , Mm.	$\gamma_1$	$\gamma_2$
	$A_{12} =$	$0.8703, A_{21} = 0$	0.8805		0.118	0.083	550.6	1.077	1.001
$\boldsymbol{x}_1$	$\mathbf{y}_1$	P, Mm.	$\gamma_1$	$\gamma_2$	0.208	0.148	533.3	1.057	1.001
0.114	0 102	622.0	1 919	1 009	0.351	0.256	506.6	1.033	1.019
0.218	0.152	678.5	1.210	1.002	0.491	0.379	478.1	1.034	1.025
0.351	0.467	732.2	1 110	1.000	0.647	0.526	442.4	1.010	1.048
0.499	0.600	781.7	1.066	1.007	0.801	0.705	405.0	1.005	1.062
0.657	0.727	823.2	1.032	1.123	0.908	0.850	378.4	1.001	1.088
0.807	0.845	857.4	1.014	1.178					
0.898	0.915	873.0	1.004	1.243		Diisopropyla	mine (1) and i	n-Hexane (2)	
	Disthulan	(1) and $1$	Uovono (2)			$A_{13} =$	$1.0879, A_{31} =$	0.8875	
	$A_{13} =$	$0.8129, A_{31} =$	1.0614		$x_1$	${\mathcal Y}_1$	<i>P</i> , <b>M</b> m.	$\gamma_1$	<b>γ</b> 3
r,	ν,	P Mm	~.	~	0.099	0.056	648.2	1.021	1.001
0.400		-,	11	1.000	0.195	0.117	617.9	1.024	1.002
0.108	0.148	713.5	1.120	1.000	0.344	0.219	571.2	1.010	1.009
0.217	0.276	744.2	1.078	1.008	0.000	0.351	018.0 470.1	1.009	1.010
0.347	0.412	111.1	1.049	1.024	0.004	0.455	470.1	1.000	1.010
0.510	0.509	012.0 929.0	1.028	1.042	0.800	0.000	387.7	1.001	1.020
0.000	0.701	861.6	1.013	1.001	0.000	0.021	507.1	1.001	1.020
0.901	0.913	877.0	1.003	1.118		Triethylan	nine (1) and $n$	Herane (2)	
						$A_{12} =$	$1.2166, A_{21} =$	0.7742	
	n-Hexylar $A_{12}$ =	nine (1) and $n$ - = 0.588, $A_{22} = 0$	Hexane (2) ).9378		$\boldsymbol{x}_1$	$\mathcal{Y}_1$	P, Mm.	$\gamma_1$	$\gamma_2$
		D M			0.052	0.028	559.6	1.032	1.002
$\boldsymbol{x}_1$	$\mathcal{Y}_1$	P, Mm.	$\gamma_1$	<b>Y</b> 2	0.104	0.058	544.8	1.019	1.002
0.123	0.022	518.8	1.546	1.013	0.192	0.111	520.7	1.024	1.003
0.232	0.041	473.8	1.378	1.040	0.348	0.220	477.1	1.025	1.004
0.375	0.069	414.7	1.258	1.091	0.512	0.351	433.6	1.014	1.017
0.563	0.115	335.2	1.130	1.207	0.623	0.457	400.5	1.004	1.021
0.656	0.147	287.6	1.073	1.271	0.799	0.668	349.0	1.003	1.022
0.808	0.246	201.7	1.032	1.420	0.913	0.840	315.2	0.999	1.031
0.906	0.412	132.3	1.018	1.486	0.956	0.916	302.4	0.999	1.030
	n-Hexylar $A_{13} =$	mine (1) and 1- = 0.8383, $A_{31} =$	Hexene (3) 0.8581			$\begin{array}{l} \text{Triethylar} \\ A_{13} = \end{array}$	mine (1) and 1 $1.2077, A_{31} =$	-Hexene (3) 0.8052	
$x_1$	$y_1$	<i>P</i> , Mm.	$\gamma_1$	<b>γ</b> 3	$x_1$	$\mathcal{Y}_1$	<i>P</i> , Mm.	$\gamma_1$	<b>γ</b> 3
0.112	0.014	612.8	1.270	1.005	0.103	0.048	639.4	1.007	1.001
0.216	0.029	557.0	1.210	1.024	0.200	0.099	600.9	1.003	1.001
0.360	0.054	480.5	1.175	1.060	0.348	0.189	543.8	0.999	1.005
0.553	0.099	371.7	1.096	1.127	0.505	0.309	481.6	1.005	1.001
0.648	0.132	317.1	1.073	1.178	0.652	0.450	425.1	1.002	1.006
0.841	0.281	183.4	1.033	1.260	0.820	0.666	359.8	1.003	1.005
0.890	0.369	145.6	1.021	1.270	0.912	0.818	324.6	1.003	1.009

Equilibrium temperatures were measured with copperconstantan thermocouples and a Leeds and Northrup Type K-2 potentiometer. The maximum error due to temperature measurement was estimated to be  $\pm 0.1^{\circ}$  C. A mercury manometer was used to measure system pressure. The mercury heights were measured with a cathetometer and a local gravity and temperature correction were applied. The maximum error due to pressure measurement was no more than  $\pm 0.5$  mm. of Hg. A Beckman GC-2 gas chromatograph was used in conjunction with a Brown 1-mv. recorder to determine composition. The maximum error encountered using this combination is no more than  $\pm 0.2$  mole %.

The quantities directly measured using this apparatus and procedure were the total pressure (P), the liquid composition (x), vapor composition (y), and the temperature  $(60^{\circ} C.)$ .

Calculation of the Activity Coefficient. Activity coefficients were calculated at each experimental composition point by Equation 1. This equation is valid only for vapor-liquid equilibria at low pressures. The interested reader may refer to Van Ness (10) for the detailed development.

$$\ln \gamma_{i} = \ln(y_{i}P/x_{i}P_{i}) + (B_{ii} - V_{i}^{L}) (P - P_{i})/RT + P\delta_{ij}y_{j}^{2}/RT$$
(1)

where

$$\delta_{ij} = 2B_{ij} - B_{ii} - B_{jj} \tag{2}$$

and

$$B_{ij} = (\overline{B} - y_i^2 B_{ii} - y_j^2 B_{jj}) / 2y_i y_j$$
(3)

where B is the mixture virial coefficient. Each of the quantities appearing in the first term on the right side of Equation 1 were measured experimentally.



Top. Diethylamine and n-hexane Bottom. Diethylamine and 1-hexene Correlated by the Wilson equation Evaluation of the second term requires second virial coefficients for the pure components at the temperature of interest ( $60^{\circ}$  C. in this case). Second virial coefficients for *n*-hexane and 1-hexene were determined using the correlation of McGlashan and Potter (6) and McGlashan and Wormold (7). Second virial coefficients for the amines were obtained from the data of Lambert (5) and by use of the Berthelot equation.

The largest contribution of the second term was about 6% (*n*-hexylamine-1-hexene system), and this term was included for all systems investigated.

The contribution of the third term on the right side of Equation 1 is most accurately determined if second virial coefficients for the mixture have been experimentally determined for the system at the temperature of interest. Unfortunately, such data are rarely available. To estimate the contribution of this term for the systems investigated. mixture second virial coefficient data for the cyclohexanediethylamine system at 76° C. (4) were used to approximate the behavior of the *n*-hexane-diethylamine system at  $60^{\circ}$  C. The resulting calculation indicated a maximum contribution of about 0.8% to the activity coefficient. Other variables remaining equal, the contribution of the third term increases with total pressure. Fortunately, the diethylaminehydrocarbon systems exhibited higher total pressures than the other systems studied and as a consequence of the small contribution in this higher pressure system, the third term was neglected for all systems investigated.

**Correlation of Data.** The Wilson equations have been tested for a number of systems by Orye and Prausnitz (8), and they were used in this investigation as a means to correlate





the activity coefficient data with composition. The Wilson equations for a binary system are:

$$\ln \gamma_{i} = -\ln(x_{i} + A_{ij}x_{j}) + x_{j} \left[ \frac{A_{ij}}{x_{i} + A_{ij}x_{j}} - \frac{A_{ii}}{A_{ii}x_{i} + x_{j}} \right]$$
(4)

$$\ln \gamma_j = -\ln(x_i + A_{ji}x_i) - x_i \left[\frac{A_{ij}}{x_i + A_{ij}x_i} - \frac{A_{ji}}{A_{ji}x_i + x_j}\right]$$
(5)

at  $x_i = 0$ , Equation 4 becomes

$$\ln \gamma_i^{\alpha} = -\ln A_{ij} + 1 - A_{ji} \tag{6}$$

while at  $x_i = 0$ , Equation 5 becomes

$$\ln \gamma_j^{z} = -\ln A_{ji} - A_{ij} + 1$$
(7)

The parameters  $(A_{ij} \text{ and } A_{ji})$  were determined for each binary by inserting the corresponding activity coefficients at infinite dilution into Equations 6 and 7. The solution of the resulting equations necessitates a trial and error computation which is easily accomplished with a computer. The activity coefficients at infinite dilution, necessary for use in Equations 6 and 7, were obtained by extrapolating the function ln  $(\gamma_i/\gamma_j)$  to each respective composition end point. The ability of the Wilson equations to correlate the activity coefficient data is illustrated by the solid curves in Figures 1 through 6.

Calculation of Selectivity. An important parameter in the sizing of a distillation column is the relative volatility, which is defined as



Bottom. Diisopropylamine and 1-hexene Correlated by the Wilson equation

$$\alpha_{ij} = (y_i/x_i)/(y_j/x_j)$$
(8)

The liquid and vapor equilibrium compositions may, at moderate pressures, be related by combination of Raoult's and Dalton's laws. The result is:

$$y_i = P_i x_i \gamma_i / P \tag{9}$$

Direct use of Equations 8 and 9 yield

$$\alpha_{ij} = (P_i/P_j)(\gamma_i/\gamma_j) \tag{10}$$

The contribution of the change in the ratio  $P_i/P_j$  to the change in  $\alpha_{ij}$ , which is due to addition of a solvent, is normally negligible compared with the contribution of the ratio  $\gamma_i/\gamma_j$ . As a result, the ratio  $\gamma_i/\gamma_j$  takes on a special significance and is defined as the selectivity.

$$S_{ij} = \gamma_i / \gamma_j \tag{11}$$

Equation 11 is applicable to the ternary composed of the hydrocarbons plus the solvent.

To form a relative comparison of solvent effectiveness from binary data alone, hydrocarbon activity coefficients were determined at the composition end point, where the concentration of solvent in each hydrocarbon-solvent binary approaches unity. Values determined in this manner are given the following symbolism.

$$S_{23} = \gamma_2 / \gamma_3$$
 (12)

where  $\gamma_2^*$  = activity coefficient of *n*-hexane(2) in the *n*-hexane-solvent binaries at  $x_2 = 0$ ; and  $\gamma_3^{*} =$  activity coefficient of 1-hexene(3) in 1-hexene-solvent binaries at  $x_3 = 0.$ 

The limiting selectivities so obtained are tabulated, for each amine, in Table III.



t 60° C.
S <b>2</b> 3
1.23
1.18
1.14
1.10
1.07
1.03

## RESULTS AND CONCLUSIONS

Experimental data for each hydrocarbon and solvent binary indicate that the deviation from ideality increases in either isomeric solvent series as the number of nitrogenbonded hydrogen atoms increases, or with respect to solvent type, in the order of tertiary, secondary, to primary amine. In addition, the deviation increases with decreasing molecular weight for the same type of amine. The largest deviations occur in the *n*-butylamine and *n*-hexane binary while the smallest values occur in the essentially ideal system, triethylamine and 1-hexene.

The selectivity values, tabulated in Table III, show that n-butylamine, containing the most nitrogen-bonded hydrogen atoms and smallest molecular size, is the most selective. Furthermore, for the same molecular size, the selectivity increases in the same order as it does for the deviation from ideality, tertiary, secondary, to primary amine, and for a given type of amine, such as primary, the selectivity increases with decrease in size. In particular, n-butylamine is more selective than diethylamine, yet they have identical molecular weights and similar molecular structures, the principal difference being in the number of hydrogen atoms bonded to the nitrogen atom. The same is true for the n-hexylamine and di-n-propylamine pair. Triethylamine, containing no nitrogen-bonded hydrogen atoms produces the lowest selectivity.

The difference in selectivities, taking the nature of the solvents into account, points to the formation of a complex between the nitrogen-bonded hydrogen atoms and the double bond of 1-hexene as the principal contributor to the selectivity mechanism for the amines and two hydrocarbons investigated here.

## NOMENCLATURE

- $A_{ij}, A_{ji} =$ Wilson parameters
  - B mixture virial coefficient =
  - $B_{ii} =$ virial coefficient of pure component i
  - $B_{ij}$ = interaction virial coefficient
  - ₽ = total system pressure
  - $\boldsymbol{P}_{\boldsymbol{i}}$ vapor pressure of component i at the system temperature
  - R = universal gas constant
  - selectivity (ratio of  $\gamma_2^*$  to  $\gamma_3^*$ ) =
  - $S_{^{23}}_{T}$ = absolute temperature
  - $\tilde{V}_{i}^{L}$ = liquid molar volume of pure component i
  - mole fraction of component i in the liquid phase  $\boldsymbol{x}_i$ =
  - $\gamma_i$ = mole fraction of component i in the vapor phase
- Greek
  - volatility of hydrocarbon i relative to j=  $\alpha_{ii}$
  - liquid phase activity coefficient for pure component i =  $\gamma_i$ = liquid phase activity coefficient of component i at  $x_i$  $\gamma_i$ 
    - = 0
  - special virial function δa =

Subscripts

- solvent (amine) 1 =
- 2 n-hexane =
- 3 = 1-hexene

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