remains the stable hydrate. Of the systems studied, only  $K_5P_3O_{10}$  increased the solubility of sodium tripolyphosphate in water.

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# Vapor-Liquid Equilibria of the Benzene-Cyclohexane-Acetic Acid System at Atmospheric Pressure

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Vapor-liquid equilibrium data of benzene-cyclohexane-acetic acid system are determined experimentally at atmospheric pressure. The ternary system is azeotropic. The activity coefficients are correlated by Van Laar equations involving the three relevant binary constants.

 $\Gamma_{
m HE}$  separation of the azeotropic mixture of benzene and cyclohexane has been studied by previous workers using various third components including n-propanol (5), methyl ethyl ketone (7), diethyl ether (9), and ethyl acetate (1). In the present work, acetic acid is chosen as the third component. A comparative study can be made regarding the suitability of the chosen third component.

#### APPARATUS

The vapor-liquid equilibrium data were determined in a Fowler-Norris still (2) with a special heating system for better agitation. To have a decreased total capacity for each run, an equilibrium still with reduced dimensions was used. The still was standardized with the benzeneacetic acid system for which equilibrium data have been reported (3, 6). The temperature was measured by a set of short range thermometers (0.2°C. accuracy). Radiation correction for the exposed thread as well as the boiling point correction to 760 mm. of mercury were applied as described by Hala *et al.* (4). The pressure variation from 760 mm. of mercury was  $\pm$  5 mm. of mercury.

#### ANALYSIS

Refractive index and specific gravity at 30° C. were chosen for analysis. The measurements were made with the aid of an ultra thermostat maintained at  $30^\circ \pm 0.05^\circ$ C., a semimicro Mettler balance, and an Abbé refractometer provided with a source for monochromatic light. A 20-ml. pycnometer was used for specific gravity determination.

Nine binary mixtures of benzene and cyclohexane with various concentrations were prepared. Then each one was subdivided into a number of fractions when various quantities of acetic acid were added to each of these fractions. Specific gravity and refractive index were determined for each of the ternary mixtures thus prepared. The data were first plotted on linear coordinates. Then, from these graphs, constant property compositions were read, and constant specific gravity and refractive index lines were constructed (Figure 1). This was used as a standard graph for analysis.

#### EQUILIBRIUM DATA AND CORRELATION

The properties of the pure components are given in Table I. The equilibrium data are presented in Table II and in



JOURNAL OF CHEMICAL AND ENGINEERING DATA



Figure 2. Constant temperature lines are shown in Figure 3. The activity coefficients are calculated using the equation

$$\gamma = \frac{\pi Y}{p \, \bar{X}} \tag{1}$$

These activity coefficients are correlated by Van Laar equa-

# Table I. Properties of Pure Components

	a a	
В.Р., °С.	Sp. Gr. at 30° C.	$n_{\rm D}^{30}$
80.1	0.8686	1.4944
80.8	0.7647	1.4201
118.1	1.0440	1.3691
	B.F., °C. 80.1 80.8 118.1	b.r.,         Sp. Gr.           ° C.         at 30° C.           80.1         0.8686           80.8         0.7647           118.1         1.0440



# Figure 3. Temperature-liquid composition data

- Constant temperature lines
  - Binary azeotropic temperature
  - A Ternary azeotropic temperature

tions as presented by Robinson and Gilliland (8). For a binary system,

$$T \ln \gamma_1 = \frac{B_{12} X_2^2}{\left(1 + A_{12} \frac{X_1}{X_2}\right)^2}$$
(2)

$$T \ln \gamma_2 = \frac{A_{12}B_{12}X_1^2}{\left(A_{12} + \frac{X_2}{X_1}\right)^2}$$
(3)

The constants  $A_{12}$  and  $B_{12}$  are evaluated from the plots of;

$$\frac{1}{(T \ln \gamma_1)^{1/2}} \text{ vs. } \frac{X_1}{X_2} \text{ and } \frac{1}{(T \ln \gamma_2)^{1/2}} \text{ vs. } \frac{X_2}{X_1}$$
(4)

Table II. Equilibrium Data										
		Experimental						Calculated		
No.	<i>T</i> , °C.	$X_1$	$X_2$	$Y_1$	$Y_2$	$\gamma_1$	$\gamma_2$	$\gamma_3$	$Y_{1c}$	Y 2c
1	89.5	0.0250	0.0900	0.2200	0.4200	3.290	3.784	1.405	0.080	0.445
2	80.6	0.0750	0.2800	0.1750	0.4700	2.290	1.936	1.990	0.124	0.600
3	78.6	0.1500	0.4400	0.1950	0.5850	1.319	1.410	2.090	0.179	0.659
4	78.6	0.1900	0.5400	0.2150	0.5800	1.113	1.160	3.040	0.203	0.632
5	77.8	0.3250	0.4100	0.3550	0.4700	1.170	1.240	2.67	0.346	0.540
6	78.8	0.5500	0.1920	0.5950	0.2500	1.081	1.368	2.335	0.605	0.283
7	79.1	0.2900	0.3120	0.3600	0.4675	1.074	1.565	1.665	0.351	0.490
8	77.2	0.2950	0.6100	0.3000	0.6200	1.055	1.156	3.243	0.303	0.642
9	80.0	0.4200	0.1850	0.5150	0.2800	1.661	1.479	1.928	0.526	0.315
10	80.8	0.2100	0.2030	0.2900	0.4200	1.326	2.016	1.788	0.332	0.431
11	91.0	0.0930	0.0520	0.2200	0.2300	1.577	3.283	1.620	0.270	0.195
12	81.6	0.3400	0.1570	0.4800	0.2600	1.333	1.603	1.853	0.489	0.308
13	80.2	0.6600	0.0700	0.7900	0.1000	1.188	1.440	1.500	0.766	0.110
14	81.2	0.5000	0.0730	0.6150	0.1350	1.182	1.068	2.088	0.685	0.140
15	83.2	0.3140	0.1060	0.4800	0.2000	1.371	1.651	1.880	0.519	0.237
16	91.8	0.1550	0.0200	0.3500	0.1100	1.579	3.962	1.594	0.435	0.072
17	93.8	0.1300	0.0200	0.3300	0.1400	1.625	4.750	1.442	0.380	0.093
18	77.8	0.1900	0.7400	0.2050	0.7100	1.153	1.051	4.900	0.210	0.740
19	77.2	0.3500	0.5500	0.3500	0.5500	2.857	1.102	4.108	0.352	0.591
20	77.4	0.4500	0.4150	0.4600	0.3950	1.182	1.045	4.352	0.448	0.401
21	78.4	0.6100	0.1800	0.6250	0.2200	1.073	1.377	2.560	0.707	0.208

Table III. Binary Van Laar Constants					
System	A	В			
Benzene-cyclohexane Cyclohexane-acetic acid Benzene-acetic acid	$1.15 \\ 1.7631 \\ 2.1992$	$\begin{array}{c} 135.5 \\ 419.881 \\ 330.5488 \end{array}$			

 $A_{23}$ ,  $A_{13}$ , and  $B_{13}$  are also evaluated by the same method. The constants are given in Table III.

The following equations involving the binary constants are used for correlating the experimental equilibrium data for the ternary system.

$$T \ln \gamma_1 = (X_2 [B_{12}]^{1/2} + X_3 A_{32} [B_{13}]^{1/2})^2 / (X_1 A_{12} + X_2 + X_3 A_{32})^2$$
(5)

$$T \ln \gamma_2 = (X_1 A_{12} [B_{21}]^{1/2} + X_3 A_{32} [B_{23}]^{1/2})^2 / (X_1 A_{12} + X_2 + X_3 A_{32})^2$$
(6)

$$T \ln \gamma_3 = (X_1 A_{12} [B_{31}]^{1/2} + X_2 [B_{32}]^{1/2})^2 / (X_1 A_{12} + X_2 + X_3 A_{32})^2$$
(7)

# CONCLUSION

The experimental and calculated values of vapor compositions corresponding to the same liquid compositions varied to within 3 to 4%. The ternary system exhibited an azeotrope at 77.2°C. at atmospheric pressure. The composition of the azeotrope in mole fractions is: acetic acid = 0.10; benzene = 0.35; and cyclohexane = 0.55. Hence, acetic acid is unsuitable as a third component for the separation of the benzene-cyclohexane azeotrope, since a ternary azeotrope occurs.

# NOMENCLATURE

- A =binary Van Laar constant
- B= binary Van Laar constant

vapor pressure =

- $_T^p$ temperature (absolute) =
- X = mole fraction in liquid phase
- Y mole fraction in vapor phase = = activity coefficient γ
- $\pi$  = total pressure of the system

#### Subscripts

- 1 = acetic acid
- 2 benzene
- 3 = cyclohexane

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# Vapor-Liquid and Liquid-Liquid Equilibria of the System Acrylonitrile-Acetonitrile-Water

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Vapor-liquid equilibria of the ternary system acrylonitrile-acetonitrile-water have been measured under 760 mm. of Hg total pressure. Acrylonitrile and water are only partially miscible, and the ternary system presents an immiscibility field. Liquidliquid equilibria for the ternary at  $25^\circ$ ,  $40^\circ$ , and  $60^\circ$  C. and at normal boiling points have also been determined. Experimental vapor-liquid equilibrium data are well correlated by Redlich-Kister equations for three-component systems.

 $\mathbf{R}_{\mathrm{ECENTLY}}$  vapor-liquid and liquid-liquid equilibrium data for binary and ternary systems with acrylonitrile, acetonitrile, and water were published by Blackford and York (2). Independently, similar research was carried out by the author at the University of Naples. The results of the two investigations show some discrepancies. Whereas Blackford and York have not attempted an analytical correlation of their results, the author was able to correlate the activity coefficients for the binaries with both the Van Laar and Redlich-Kister equations for two component sys-

A detailed description of the apparatus and operating pro-

cedure is given by Volpicelli (5). Equipment and techniques used are mentioned here only in so far as discrepancies between Blackford and York's results and the author's may be attributable to differences in experimental conditions.

tems and the activity coefficients for the ternary with the

This paper gives equilibrium data for the ternary system and briefly summarizes the results for the binary systems.

appropriate forms of the Redlich-Kister equations.