

Figure 3. Representative plots of the curve-straightening technique that was used to locate solidus points

curves lack  $0.15^{\circ}\,\mathrm{K}$  of merging at the freezing point minimum. This is about the difference that would be expected from the 0.1 mol % impurity in the samples.

The occurrence of the minimum (within experimental error) at a 1-1 stoichiometric composition suggests the possible formation of a 1-1 intermetallic compound. The thermal data alone, however, are not sufficient to confirm the existence of a compound.

Our results are in much better agreement with the earlier work of Rinck (2) than with that of Goria (1). Although Rinck's data show considerable scatter, the smoothed curve through his experimental points agrees with our results to within  $\pm 1^{\circ}$  K. Agreement with the data of Goria (1) is much poorer, the differences being as large as  $\pm 8^{\circ}$  K.

## LITERATURE CITED

- (1) Goates, J. R., Ott, J. B., Hsu, C. C., Trans. Faraday Soc., 66, 25 (1970).
- (2) Goria, C., Gazz. Chim. Ital., 65, 1226 (1935).
- (3) Ott. J. B., Goates, J. R., Anderson, D. R., Hall, H. T., Jr., Trans. Faraday Soc., 65, 2870 (1969).
- (4) Rinck, E., Compt. Rend., 203, 255 (1936).

RECEIVED for review June 15, 1970. Accepted October 3, 1970. The authors gratefully acknowledge the support given this project by the United States Atomic Energy Commission under contract No. AT(11-1)-1707.

# Density and Viscosity of Deuterium Oxide Solutions from 5–70°C

FRANK J. MILLERO<sup>1</sup>, ROGER DEXTER, and EDWARD HOFF Rosenstiel School of Marine and Atmospheric Sciences, University of Miami, Miami, Fla. 33149

The density and viscosity of deuterium oxide solutions have been measured from  $5-70^{\circ}$  C. The density measurements were made by a magnetic float technique, and the viscosity measurements were made using a modified Cannon-Ubbelohde viscometer with a semiautomatic optical viscometer reader. The results are briefly discussed and compared to the results obtained by other scientists.

In recent years various workers (13, 14, 16, 18) have studied the differences between the thermodynamic and transport properties of deuterium oxide, D<sub>2</sub>O, and normal water, H<sub>2</sub>O. Many studies (1, 5) have also been made on the differences between electrolyte and nonelectrolyte solutions of D<sub>2</sub>O and H<sub>2</sub>O. The results of most studies (1, 13, 16, 18) indicate that D<sub>2</sub>O solutions are more structured than H<sub>2</sub>O solutions at the same temperature.

This study of the density and viscosity of  $D_2O$  solutions was made to provide precise thermodynamic and transport data that may prove useful in elucidating the causes of the structural differences between  $D_2O$  and  $H_2O$  as a function of temperature.

### EXPERIMENTAL

The two samples of  $D_2O$  used in this study were obtained from Bio-Rad Chemical Co. and were used without further purification. Although both samples were supplied as 99.88 mole  $C_C$   $D_2O$ , the density determinations indicated that sample No. 1 (used in previous studies, 12) was 98.35  $\pm$  0.01 mole % D<sub>2</sub>O. The decrease in D<sub>2</sub>O in sample No. 1 was apparently caused by the exchange with atmospheric water before use. Ion-exchanged ( ${\sim}8~M\Omega)~H_2O$  was used in all the calibration runs.

The magnetic float densitometer used to make the density measurements has been described in detail elsewhere (11). The densitometer was calibrated using the densities for  $H_2O$  tabulated by Kell (8). The  $H_2O$  and  $D_2O$  solutions were degassed before use to prevent the formation of bubbles on the magnetic float during an experiment. The precision obtained in duplicate runs was  $\pm 2$  ppm. The mole %of the  $D_2O$  used in this study was checked from our density measurements using the linear equation,  $d_{D_2O} = d_{H_2O}$  +  $AX_{\rm D.0}$  (where d is the density, A is a constant, and X is the mole % D<sub>2</sub>O). The constant,  $A = (d_{D,O} - d_{H,O})/$ 100, was determined from the density data for 100%  $D_2O$ and normal H<sub>2</sub>O using the density data tabulated by Kell (8). This linear interpolation yielded 98.35  $\pm$  0.01 mole % for sample No. 1 and 99.88  $\pm$  0.01 mole % for sample No. 2 over the entire temperature range. Although the purity of the  $D_2O$  determined by this method is dependent

<sup>&</sup>lt;sup>1</sup>To whom correspondence should be addressed.

on the densities selected for 100 mole % D<sub>2</sub>O and H<sub>2</sub>O (8), the fact that we obtain the same value for the mole % over a wide temperature range indicates the consistency of both our densities and those tabulated by Kell (8).

The temperature of the bath containing the magnetic float densitometer was set to  $\pm 0.02^{\circ}$  C with Brooklyn calorimeter thermometers and regulated to better than  $\pm 0.001^{\circ}$  C with a Hallikainen thermoregulator.

The apparatus used to make the viscosity measurements has been described in detail elsewhere (9). A Cannon-Ubbelohde (suspended level) viscometer with a flow time for H<sub>2</sub>O at 25° of about 244 sec was used to measure the viscosity of D<sub>2</sub>O. The flow times were measured to  $\pm 0.002$  sec with a Rehovoth viscometer reader and a TSI universal counter. The viscometer was calibrated with H<sub>2</sub>O using the viscosities tabulated by Korson *et al.* (9). The temperature of the bath was set to  $\pm 0.01^{\circ}$  with a Hewlett-Packard quartz crystal thermometer and regulated to  $\pm 0.001^{\circ}$  with a Hallikainen thermoregulator.

#### RESULTS AND DISCUSSION

Flow times,  $\tau$ , for D<sub>2</sub>O were measured (to  $\pm 0.002$  sec) over the temperature range from 5–70° at 5° intervals. The absolute viscosity of D<sub>2</sub>O,  $\eta$ , was determined from these flow times using the equation (9)

$$\eta = \tau K (\mathrm{d}^{\circ} - \mathrm{d}^{\circ}) - L \mathrm{d}^{\circ} / \tau^{2}$$
(1)

where  $d^0$  is the density of  $D_2O$  (given in Table I),  $d^a$ is the density of 100% H<sub>2</sub>O saturated air, K is the instrument constant and L is the kinetic energy correction constant. The constants K and L were determined from the flow times of  $H_2O$  (assuming that they are independent of temperature) using the values for the viscosity of water (9) at eight temperatures from 5-60° together with the densities of water tabulated by Kell (8). Since the constants were found to change slightly when the viscosity system was reassembled, the H<sub>2</sub>O calibration runs were made after the  $D_2O$  run was completed (*i.e.*, without disassembling the system). These changes were caused by not placing the viscometer in exactly the same position in reference to the viscometer photocells. The constants, K = 3.9318 $\times$  10<sup>-3</sup> and L = 91.83 and K = 3.9358  $\times$  10<sup>-3</sup> and L = 90.76 were determined, respectively, for the first and second calibration runs. By use of these constants (the flow times for  $D_2O$  and the densities of  $D_2O$ ), the viscosities of  $D_2O$  have been determined from 5-70°. The results are given in Table I along with the densities.

In Table II the viscosities of 100 mole % (obtained

Table I. Density and Viscosity of Deuterium Oxide at Various Temperatures

Temp, °C	Density, g/ml		Viscosity, cP			
	Run $1^a$	Run $2^{\flat}$	Run 1	Run 2		
5	1.103909	1.105531	1.9745	1.9812		
10	1.104218	1.105849	1.6675	1.6725		
15	1.104113	1.105751	1.4306	1.4343		
20	1.103580	1.105215	1.2431	1.2468		
25	1.102714	1.104362	1.0928	1.0963		
30	1.101491	1.103142	0.9700	0.9730		
35	1.099978	1.101631	0.8683	0.8708		
40	1.098213	1.099867	0.7828	0.7852		
45	1.096210	1.097864	0.7106	0.7126		
50	1.093966	1.095618	0.6487	0.6503		
55	1.091500	1.093151	0.5953	0.5965		
60	1.088852	1.090500	0.5488	0.5502		
65	1.086042	1.087688	0.5080	0.5094		
70	1.083177	1.084822	0.4720	0.4731		
$^{\circ}$ 98.35 mole $\%$ D <sub>2</sub> O. $^{\circ}$ 99.88 mole $\%$ D <sub>2</sub> O						

86 Journal of Chemical and Engineering Data, Vol. 16, No. 1, 1971

Table	11.	Viscosity	of	Deute	rium	Oxide
	at	Various	Ter	nperat	tures	

Temp, ° C	Run 1	Run 2	Literature Values
5.00	1.9822	1.9818	$1.9825,^{*}1.9883^{\circ}$
10.00	1.6737	1.6730	$1.6742.^{\circ} 1.6804^{\circ}$
15.00	1.4356	1.4347	$1.4357,^{\flat} 1.4420,^{\circ} 1.4319^{d}$
20.00	1.2470	1.2471	$1.2477,^{\circ} 1.2515,^{\circ} 1.2515^{\circ}$
25.00	1.0961	1.0966	1.0964,° 1.0969,° 1.0969,'
			1.0951
30.00	0.9730	0.9732	$0.9728,^{b}0.9690,^{c}0.9793^{d}$
35.00	0.8708	0.8710	$0.8706,^{\flat} 0.8619^{\circ}$
40.00	0.7849	0.7854	$0.7849^{i}$
45.00	0.7125	0.7127	$0.7123^{\circ}$
50.00	0.6504	0.6504	$0.6502,^{\flat} 0.6560^{d}$
55.00	0.5968	0.5966	$0.5966^{i}$
60.00	0.5501	0.5503	$0.5500,^{b}0.5543^{a}$
65.00	0.5093	0.5095	$0.5092^{\circ}$
70.00	0.4732	0.4732	$0.4733,^{b}0.4762^{d}$

<sup>*c*</sup> Linearly extrapolated to 100<sup>*c*</sup><sub>c</sub> from 98.35<sup>*c*</sup><sub>c</sub> (run 1) and 99.88<sup>*c*</sup><sub>c</sub> (run 2). The literature values have been calculated from  $\eta_{rel} = \eta_{D,O}/\eta_{H,O}$  using  $\eta_{H,O}$  from reference 9. <sup>*c*</sup> Reference 6. <sup>*c*</sup> Reference 10. <sup>*c*</sup> Reference 17. <sup>*c*</sup> Reference 15. <sup>*f*</sup> Reference 2. <sup>*s*</sup> Reference 7.

by linear extrapolation of the values given in Table I) are given along with the values obtained by other workers (2, 6, 7, 10, 15, 17). Our results for the viscosity of D<sub>2</sub>O are in excellent agreement with the very careful work of Hardy and Cottington (6).

The following equation can be used to obtain the viscosity of  $D_2O$  at temperatures between those listed in Table II.

$$\log \eta_t / \eta_{20} = A \left( 20 - t \right) - B \left( t - 20 \right)^2 / \left( t - C \right)$$
(2)

where  $\eta_i$  is the viscosity of D<sub>2</sub>O at any temperature  $(t, ^{\circ}C)$  between 5° and 70°,  $\eta_{20}$  is the viscosity of D<sub>2</sub>O at 20° (1.2471 cP), A = 1.3580, B = 0.00067, and C = 96.71 (with a standard deviation of  $\pm 0.0003$  cP).

In Figure 1 the viscosity of  $D_2O$  and  $H_2O(\theta)$  are given as a function of temperature. The viscosity of  $D_2O$  is larger



Figure 1. The viscosity of deuterium oxide,  $D_2O$  (closed circles) and normal water,  $H_2O$  (open circles), as a function of temperature

than  $H_2O$  over the entire temperature range; however, at the higher temperatures the viscosities of  $D_2O$  and  $H_2O$ appear to approach each other. For example, at 5° the difference between the viscosity of  $D_2O$  and  $H_2O$  is 0.4628 cP while at  $70^{\circ}$  the difference is only 0.0693 cP. One might attribute the decrease in the difference between the  $\eta$  of  $D_2O$  and  $H_2O$  to the formation of similar structure for  $D_2O$  and  $H_2O$  at high temperatures (*i.e.*, if the larger  $\eta$ of  $D_2O$  is due to greater structure). The effect of temperature on the differences between the compressibilities of  $D_2O$  and  $H_2O$  also agree with this suggestion (3, 4, 12).

In future work, we plan to investigate the temperature dependence of other pure solvents and hopefully use these results to obtain a better understanding of the structural properties of water by comparison.

### LITERATURE CITED

- Arnett, E., McKelvey, D., "Solute-Solvent Interactions," p (1)653. edited by Coetzee, J., and Ritchie, C., Marcel Dekker, New York, N. Y. (1969).
- Baker, W. N., LaMer, V. K., J. Chem. Phys., 3, 406 (1935). Davis. C. M., Jr., Bradley, D. L., Ibid., 45, 2461 (1966). (2)
- (3)
- Feates, F. S., Ives, D. J. G., J. Chem. Soc., (London) 1956, (4)p 2798.
- (5) Greyson, J., J. Phys. Chem., 71, 2210 (1967).

- (6) Hardy, R. C., Cottington, R. L., J. Res. Natl. Bur. Stds., 42, 573 (1949).
- Jones, G., Fornwalt, H. J., J. Chem. Phys., 4, 30 (1936). (7)
- Kell, G. S., J. Chem. Eng. Data, 12, 66 (1967). (8)Korson, L., Drost-Hansen, W., Millero, F. J., J. Phys. Chem., (9)73, 34 (1969).
- Lewis, G. N., MacDonald, R. T., J. Amer. Chem. Soc., 55, (10)4730 (1933).
- Millero, F. J., Rev. Sci. Instrum., 38, 1441 (1967). (11)
- (12)Millero, F. J., Lepple, F. K., J. Chem. Phys., in press (1971).
- Nemethy, G., Scheraga, H. A., J. Chem. Phys., 41, 680 (1964). (13)
- Swain, C. G., Badar, R. F. W., Tetrahedron, 10, 182 (1960). (14)
- Taylor, H. S., Selwood, P. W., J. Amer. Chem. Soc., 56, 998 (15)(1934).
- (16)Thomas, M. R., Scheraga, H. A., Schrier, E. E., J. Phys. Chem., 69, 3722 (1965).
- Timrot, D. L., Shiuskaya, K. P., At. Energ., 7, 459 (1959). (17)
- Whalley, E., "Proceedings of 1957 IUPAC Joint Conference (18)on Thermodynamics and Transport Properties of Fluids,' pub. by Inst. Mech. Eng., London, 1959, p 15-25.

RECEIVED for review June 18, 1970. Accepted October 7, 1970. The authors wish to acknowledge the support of the Office of Naval Research (NONR 4008-02) and the National Science Foundation (GA-17386) for this study. Contribution number 1283 from the Rosenstiel School of Marine and Atmospheric Sciences, University of Miami, Fla. 33149

# Heats of Combustion, Heats of Formation and Vapor Pressures of Some Organic Carbonates

# Estimation of Carbonate Group Contribution to Heat of Formation

JONG KWON CHOI<sup>1</sup> and MICHAEL J. JONCICH<sup>2</sup> Department of Chemistry, Northern Illinois University, Dekalb, III. 60115

> Heats of combustion were measured, using oxygen bomb calorimetry, for some organic carbonates—i.e., ethylene carbonate, diethyl carbonate, propylene carbonate, vinylene carbonate, di-(p-phenylbenzyl)carbonate. Sublimation pressure of low vapor pressure compounds—i.e., ethylene carbonate—were measured by the Knudsen effusion method. High vapor pressure compounds—*i*.e., propylene carbonate, diethyl carbonate, and vinylene carbonate—were measured using a modified manometric apparatus. The gaseous phase heats of formation were used to estimate the carbonate group contribution to the heat of formation. A value of  $-133 \pm 1$  kcal/mole was obtained.

Dimple methods of calculating thermodynamic properties of organic compounds readily and with a minimum of data have been developed by a number of workers, and have been reviewed critically by Reid and Sherwood (11), Janz (6) and Benson (1). From the various possibilities, the additive-atomic group method was selected to calculate the organic carbonate group contribution to the heat of formation in the gaseous state. An additive-atomic group contribution method for heats of formation (gas) has been developed by Franklin (4) for hydrocarbons and other organic compounds such as simple free radicals. The method of Franklin is based on the extension of the relations and principles developed by Pitzer (10) for the long-chain paraffins.

EXPERIMENTAL

Vapor Pressure Measurements. The Knudsen effusion method (7, 12) was employed to measure the sublimation pressure of low vapor pressure compounds, whereas a modified manometric method was employed for high vapor pressure compounds.

Knudsen Effusion Method. The measurement of weight loss in a known period of time at a known constant temperature allows the calculation of the vapor pressure, using the effusion formula, and assuming that the pressure in the vacuum above the effusion hole is negligibly small compared to the vapor pressure of compounds to be measured. A high vacuum system is required when using this method; details of this system are available elsewhere (3).

The following Knudsen effusion formula was used to calculate the sublimation pressure after insertion of proper values for the constants:

<sup>&</sup>lt;sup>1</sup>To whom correspondence should be addressed.

<sup>&</sup>lt;sup>2</sup> Present address, Special Training Division, Oak Ridge Associated Universities, Oak Ridge, Tenn. 37830