# Table IV.Smoothed Values of Enthalpy for Mixture of 49.1 Wt % cis-2-Penteneand 50.9 Wt % n-Pentane

Units: Btu/lb. Base level: Pure saturated liquid components at -200°F

Tomn	Psia										
°F	0	300	400	450	500	515	600	700	800	1000	1400
350	416.6	392.1	306.9				305.0		303.1	301.9	300.7
360	421.9	398.6	315.1				313.2		311.5	310.0	308.0
360.4			315.6°								
365			387.2ª								
370	427.1	405.1	391.5	324.1			321.7		319.9	318.1	315.
375.8				$329.9^{a}$							
377.8				$385.1^{a}$							
380	432.4	411.6	399.6	388.5	334.4		330.7		328.2	326.0	322.
386.6					343.2ª						
389					378.2ª						
390	438.0	418.1	407.2	400.1	382.1	350.6	340.4		336.5	334.0	330.
391.6						361.3 <sup>b</sup>					
391.9						374.3°					
395	440.7	421.2	411.1	405.0	392.2	386.0	345.8	342.2	340.7	338.0	333.
400	443.3	424.6	415.0	409.2	399.0	394.5	352.0	347.7	345.0	341.8	337.
410	449.1	431.1	422.0	417.4	409.1	405 , $9$	375.8	359.3	354 , $1$	350.2	345.
420	454.8	437.9	429.1	424.3	417.9	415.0	398.0	371.9	364 , $2$	359.3	353.
430	460.7	444.4	436.0		425.5	423.5	410.7	388.0	375.3	367.9	361.
440	466.6	451.1	443.0		433.2	431.2	420.8	403.0	387.1	376.5	370.

#### LITERATURE CITED

- Ambrose, D., Cox, J. D., Townsend, R., Trans. Faraday Soc., 56, 1452 (1960).
- (2) American Petroleum Institute, Division of Refining, "Technical Data Book—Petroleum Refining," New York, 1966.
- (3) American Petroleum Institute Research Project 44, 'Selected Values of Properties of Hydrocarbons and Related Compounds,' Thermodynamic Research Center, Texas A & M University, College Station, Tex., April 30, 1969.
- (4) Kilpatrick, J. E., Prosen, F. J., Pitzer, K. S., Rossini, F. D., J. Res. Nat. Bur. Stand., 36, 559 (1946).
- (5) Kobe, K. A., Lynn, R. E., Chem. Rev., 52, 117 (1953).
- (6) Lenoir, J. M., Robinson, D. R., Hipkin, H. G., J. Chem. Eng. Data, 15 (23) 26 (1970).
- (7) Meyer, C. A., McClintock, R. B., Silvestri, G. J., Spencer, R. C., "Thermodynamic and Transport Properties of Steam," American Society of Mechanical Engineers, New York, 1967.
- (8) Parks, G. S., Huffman, H. M., J. Amer. Chem. Soc., 52, 4381 (1930).
- (9) Rebert, C. J., Kay, W. B., AIChE J., 5, 258 (1959).
- (10) Todd, S. S., Oliver, G. D., Huffman, H. M., J. Amer. Chem. Soc., 69, 1519 (1947).

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### Thermodynamic Properties of Gases in Propellants

Solubilities of Gaseous NH<sub>3</sub>, CO, CO<sub>2</sub>, and SF<sub>6</sub>

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Ordinary gases are generally used for blanketing and pressurizing liquid propellants. Absorption and desorption of these gases cause undesirable mechanical and hydrodynamic effects in space vehicles. A series of investigations was therefore carried out to measure the solubilities of He, N<sub>2</sub>, O<sub>2</sub>, Ar, and N<sub>2</sub>O<sub>3</sub> in liquid N<sub>2</sub>O<sub>4</sub>; and He, N<sub>2</sub>, and Ar in liquid hydrazine, methylhydrazines, and their mixtures (1-3). The present investigation is on the solubilities of NH<sub>3</sub>(g) in liquid hydrazine (N<sub>2</sub>H<sub>4</sub>), in methylhydrazine (MH; N<sub>2</sub>H<sub>3</sub>CH<sub>3</sub>), and in unsymmetrical dimethylhydrazine [UDMH; 1,1-N<sub>2</sub>H<sub>2</sub>(CH<sub>3</sub>)<sub>2</sub>]; CO(g) in UDMH; SF<sub>6</sub>(g) in MH and in N<sub>2</sub>O<sub>4</sub>; and CO<sub>2</sub>(g) in N<sub>2</sub>O<sub>4</sub>.

There are no available data on these gas-liquid systems except on the  $\rm NH_3-N_2H_4$  system at very high concentrations

of ammonia (6). A small amount of ammonia in  $N_2H_4$  improves the performance of  $N_1H_4$  in special engines, and CO and CO<sub>2</sub> are potential pressurization gases for UDMH and  $N_2O_4$ . Compounds of sulfur and fluorine, in particular SF<sub>6</sub>, have electrophyllic properties in engines using MH and  $N_2O_4$ . An accurate investigation of these gas-liquid systems is therefore warranted.

#### EXPERIMENTAL

The apparatus and the method for measuring the solubilities of gases are described elsewhere in detail (1, 4). Briefly, the apparatus for solubility measurements consists of three calibrated volumes for measuring the amounts of gases, a container

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Solubilities of gases at various temperatures and pressures in the following gasliquid systems have been investigated:  $NH_3-N_2H_4$ ,  $NH_3-N_2H_3CH_3$ ,  $NH_3-1$ ,  $1-N_2H_2(CH_3)_2$ , CO-1,  $1-N_2H_2(CH_3)_2$ ,  $SF_6-N_2H_3CH_3$ ,  $SF_0-N_2O_4$ , and  $CO_2-N_2O_4$ . The first component is the dissolved gas or solute, and the second component is the propellant or solvent in each binary system. The solubilities of  $NH_3$  were found to obey Henry's law in the range of about 0.0-0.15 mol fraction of  $NH_3$ . All other gases are much less soluble than  $NH_3$  and obey Henry's law at all concentrations. The standard Gibbs energy of solution of each gas in each liquid has been expressed as a function of absolute temperature. The activities of  $NH_3$  and  $N_2H_4$  in the system  $NH_3-N_2H_4$  for the entire composition range have been calculated, and molecular interpretations for deviations from ideality are presented.

for the propellant stirred with a glass-enclosed magnet-bar, and a precision mercury manometer for measuring the pressure with a microslide cathetometer. The apparatus was all-Pyrex glass construction with short capillary connecting tubes joined by fusion. There are two capillary stopcocks sparingly lubricated with silicone grease and two Teflon O-ring joints.

The three volumes calibrated to  $\pm 0.0003$  ml, were interconnected with short capillary necks, each with a calibration mark. These volumes were immersed in a thermostat whose temperature was nearly the same as the thermostated room controlled to  $\pm 0.1^{\circ}$  where the apparatus was located. The volumes of all connecting tubes were also calibrated to the same precision. The pressure measurements were made with a barometer accurate to  $\pm 0.02$  mm, and the manometer readings were read to  $\pm 0.01$  mm with a micrometer slide-type cathetometer. The propellant bulb, with a capacity of about 100 ml, was calibrated with an accuracy of  $\pm 0.0002$  ml by using water or mercury and was immersed in a thermostat controlled to  $\pm 0.01^{\circ}$ C during the measurements.

The propellants had the following purity:  $N_2H_4$ , MH, and UDMH of 99% purity were further purified by double vacuum distillation; research grade  $N_2O_4$  of 99.5% minimum purity was oxidized to remove a trace of  $N_2O_3$  by bubbling oxygen, degassed under vacuum, and then distilled. The research grade gases, NH<sub>3</sub>, CO, and CO<sub>2</sub> were of 99.99, 99.8, and 99.995% minimum purity, respectively. Sulfur hexafluoride, SF<sub>6</sub>, initially 98.7% pure was purified by freezing in liquid nitrogen and evacuating to remove 1.1% air.

The volume occupied by the liquid was obtained by highly precise density measurements (1, 3). The gas and the liquid were brought to equilibrium at a constant temperature by vigorously stirring the liquid. The amount of dissolved gas was found by subtracting the remaining gas from the initially admitted gas. The experimental procedure was checked for the solubility of nitrogen in water, and the result agreed within 2% of published data. The maximum error in all measurements was 2% of all solubilities reported in this paper.

#### **RESULTS AND DISCUSSION**

Ammonia in Propellants. The results for the solubility of ammonia in liquid N<sub>2</sub>H<sub>4</sub>, MH, and UDMH are listed in Table I and show that in the range of about 0–0.15 mole fraction of NH<sub>3</sub>, Henry's law is obeyed—i.e., the solubility of gas in mole fraction X is proportional to the fugacity, f, of the gas. The fugacity of ammonia, f, in the pressure range of interest, the compressibility factor, Z, and the pressure, P, are related by

$$f = ZP \tag{1}$$

where Z is calculated from the pressure-volume-temperature data summarized by Din (5). The proportionality between X and f is shown in the lower left corner of Figure 1 where f is plotted vs. X for NH<sub>3</sub> in N<sub>2</sub>H<sub>4</sub>; similar plots may be drawn



Figure 1. Fugacity of NH<sub>3</sub> over NH<sub>3</sub>-N<sub>2</sub>H<sub>4</sub> system

Extrapolation range is 88.5–124.9°C. Short dashed lines join sets of data

for  $NH_3$  in MH and UDMH by using Table I. The slope in each such plot is the equilibrium constant K for the following reaction

Gas at 
$$f$$
 atm = dissolved gas at  $X$  (2)

The constant K is given by

$$K = \frac{X}{f} \tag{3}$$

where f is in atmospheres, and K is in mole fraction per atmosphere. At sufficiently low pressures—i.e., less than 0.5 atm of NH<sub>3</sub>—f approaches P, and K approaches K' of the following equation:

$$K' = \frac{X}{P} \tag{4}$$

The deviation from Henry's law is noticeably large above f = 1 in NH<sub>3</sub>-N<sub>2</sub>H<sub>4</sub> and NH<sub>3</sub>-UDMH systems. The range of ammonia concentration in MH for the pressure range of interest is not large enough to show a measurable deviation from Henry's law. The thermodynamic equation representing K as a function of temperature T, in °K, is given by

$$\Delta G^{\circ} = -4.5756 \ T \ \log K = \Delta H^{\circ} - T \ \Delta S^{\circ} \tag{5}$$

where  $\Delta G^{\circ}$ ,  $\Delta H^{\circ}$ , and  $\Delta S^{\circ}$  are the standard Gibbs energy, enthalpy, and entropy of solution, respectively, for Reaction 2. The linear relationships represented by Equation 5 for the three gas-liquid systems are shown in Figure 2 where each point represents the average of all values of K at each temperature

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$2.1154$ $2.0802$ $0.1125$ $0.0532$ $0.0541^{b}$
Av 0.0514
MH 253.17 0.1561 0.1556 0.0786 0.5035 0.5051
0.2693 $0.2677$ $0.1310$ $0.4864$ $0.4894$
Av 0.4973
273.15 $0.1825$ $0.1820$ $0.0424$ $0.2323$ $0.2330$
0.5266  0.5224  0.1157  0.2197  0.2215
Av 0.2273
293.14  0.3425  0.3413  0.0423  0.1235  0.1239
0.6206  0.6165  0.0752  0.1212  0.1220
1.0055 $0.9948$ $0.1190$ $0.1183$ $0.1196$
Av 0.1218
UDMH 253.17 0.0752 0.0751 0.0320 0.4255 0.4261
0.2328 $0.2317$ $0.0973$ $0.4180$ $0.4199$
$0.9413  0.9225  0.3315  0.3522  0.3593^{b}$
$1.5035$ $1.4556$ $0.6222$ $0.4138$ $0.4275^{b}$
Av 0.4230
273.15  0.3133  0.3119  0.0650  0.2075  0.2084
0.4827  0.4792  0.0982  0.2034  0.2049
$1.1635$ $1.1432$ $0.2456$ $0.2111$ $0.2148^{b}$
$1.8406 \ 1.7898 \ 0.3963 \ 0.2153 \ 0.2214^{\circ}$
Av 0.2067
293.14  0.3336  0.3324  0.0363  0.1088  0.1092
0.7237 $0.7181$ $0.0786$ $0.1086$ $0.1095$
0.9594 $0.9496$ $0.1042$ $0.1086$ $0.1097$
$1.4333$ $1.4700$ $0.1002$ $0.1108$ $0.1226^{\circ}$ 2.1450 $2.0071$ $0.2377$ $0.1108$ $0.11235$
2.1709 2.0911 0.2011 0.1100 0.1133" Av 0 1095
af = fuggity = ZP; Y = mole fraction; K' = V/D; K =
X/f; $P = P$ (total) – P (solvent). <sup>b</sup> Not included in averaging

High concentration of dissolved gas is beyond validity of Henry's Law. However, these data are plotted in Figure 1.

in the range of validity of Equation 3. The thermodynamic relationships for the linear plots in terms of  $\Delta G^{\circ}$  are as follows:

 $\Delta G^{\circ}(\mathrm{NH}_{3} \text{ in } \mathrm{N}_{2}\mathrm{H}_{4}) = -5204 + 22.53 T$ (6)

$$\Delta G^{\circ}(\mathrm{NH}_{3} \text{ in MH}) = -5196 + 21.93 T \tag{7}$$

$$\Delta G^{\circ}(\mathrm{NH}_{3} \text{ in UDMH}) = -4986 + 21.40 T \tag{8}$$

The equations for  $\Delta G^{\circ}$  show that ammonia releases about the same amount of heat—i.e.,  $\Delta H^{\circ} \approx -5000$  cal/mol when 1 mole of NH<sub>3</sub> is dissolved in these propellants. This is also true for the entropy of solution,  $\Delta S^{\circ} \approx -22$  cal/mol °K. The decreasing trend in the absolute values of  $\Delta H^{\circ}$  and  $\Delta S^{\circ}$  follows the increasing number of CH<sub>3</sub> radicals in the propellants and shows that the interacting forces between H atoms in NH<sub>3</sub> and H in N<sub>2</sub>H<sub>4</sub> are stronger than those between H in NH<sub>3</sub> and H in CH<sub>3</sub> radicals in MH and UDMH.

The liquid-vapor equilibrium data for NH<sub>3</sub>-N<sub>2</sub>H<sub>4</sub> system



Figure 2. Variation of atmospheric solubility, K, with temperature for  $NH_3-N_2H_4$ ,  $NH_3-MH$ , and  $NH_3-UDMH$  systems

have been obtained by Drago and Sisler (6) in the range of 0.30-0.95 mole fraction of NH<sub>3</sub> and 88.5-124.9°C. Their results are extrapolated from 88.5°C to lower temperatures by plotting the logarithm of fugacity of ammonia at a series of fixed compositions of liquid vs. 1/T in °K<sup>-1</sup>. Such plots are the classical van't Hoff correlation in thermodynamics and extrapolate reliable data with confidence when scattering is extremely small. The resulting extrapolation correlates well with our data (Figure 1). The activity of  $NH_3$ ,  $a_{NH_3}$ , which is defined by the fugacity of NH<sub>3</sub> over a given solution divided by the fugacity of NH<sub>3</sub> over pure liquid NH<sub>3</sub>, obeys Henry's law and Raoult's law in their proper domains for large ranges of concentration. For example,  $a_{NH_3}$  at 25°C, is equal to its mole fraction in the range of about 0.6-1.00 mole fraction of  $NH_3$  (Raoult's law), and  $a_{NH_3}$  is proportional to its mole fraction in the range of 0.0-0.15 mole fraction (Henry's law).

Activities in  $NH_3-N_2H_4$  System. The activity of  $NH_3$ from this investigation and from Drago and Sisler (6) has been calculated and listed in Table II. The calculation requires plotting log  $f_{NH_3}$  over each solution vs. 1/T to obtain an equation of log f as a linear function of (1/T). When the linear function for log  $f_{NH_3}$ \* for pure liquid  $NH_3$  is subtracted from log  $f_{NH_3}$ , an equation for log  $(f/f^*) = \log a_{NH_3}$  is obtained

Table II. Thermodynamic Properties of NH<sub>3</sub> and N<sub>2</sub>H<sub>4</sub> in Liquid NH<sub>3</sub>-N<sub>2</sub>H<sub>4</sub> System at 298.15 and 373.15°K

	$\mathrm{NH}_{3}{}^{a}$		$N_2H_4$		$298.15^{\circ}\mathrm{K}$		$373.15^{\circ}\mathrm{K}$		
X <sub>NH8</sub>	$_{3}\Delta\overline{H}$	$\Delta \bar{S}$	$\Delta \vec{H}$	$\Delta \bar{S}$	$a_{\rm NH_3}$	$a_{ m N_2H_4}$	$a_{\rm NH_3}$	$a_{\rm N_2H_4}$	
0.0			0.0	0.0	0.000	1.000	0.000	1.000	
0.1	-1	4.01	-178	-0.39	0.133	0.902	0.163	0.958	
0.2	-1	2.63	-178	-0.16	0.266	0.802	0.326	0.852	
0.3	1	1.83	-183	+0.09	0.398	0.701	0.398	0.746	
0.4	$+25\bar{8}$	2.10	-298	+0.01	0.537	0.601	0.493	0.665	
0.5	+400	2.19	-441	-0.13	0.653	0.508	0.570	0.590	
0.6	+264	1.55	-267	+0.68	0.718	0.453	0.656	0.496	
0.7	+150	1.02	-59	+1.65	0.773	0.395	0.734	0.403	
0.8	+32	0.50	+295	+3.22	0.828	0.326	0.814	0.295	
0.9	+127	0.56	+375	+4.62	0.931	0.184	0.905	0.162	
1.0	0.0	0.0	, 5.0	,	1.000	0.000	1.000	0.000	
<sup>a</sup> $\overline{H}$ is in cal/mol, and $\Delta \overline{S}$ is in cal/mol °K.									

at the selected composition. The activity of ammonia is related to the Gibbs energy change by

$$\Delta \bar{G} = \Delta H - T \Delta S = RT \ln a_{\rm NH_2} \tag{9}$$

where  $\Delta \bar{G}$  is defined by  $\bar{G} - G^*$ ,  $\bar{G}$  being the partial molar Gibbs energy of NH<sub>3</sub>, and G\*, that of pure liquid ammonia. The changes in the partial molar enthalpy  $\Delta \overline{H}$  and the entropy  $\Delta \overline{S}$  are similarly defined. The values of  $\Delta \overline{H}$  and  $\Delta \overline{S}$  are listed in Table II. The activity coefficient of  $N_2H_4$ ,  $\gamma_{N_2H_4}$  has been calculated by graphical integration of the Gibbs-Duhem relationship d ln  $\gamma_{N_2H_4} = -(X_{NH_3}/X_{N_2H_4})$  d ln  $\gamma_{NH_3}$ . For this purpose,  $X_{\rm NH_5}/X_{\rm N_2H_4} = (\alpha_{\rm NH_5}/\alpha_{\rm N_2H_4})$  is in  $\gamma_{\rm NH_5}$ . For this purpose,  $X_{\rm NH_5}/X_{\rm N_2H_4}$  was plotted vs. ln  $\gamma_{\rm NH_5}$ , and the area under the curve was measured from  $X_{\rm N_2H_4} = 1.0-0.1$  at 0.1 intervals. The value of  $\gamma_{\rm N_2H_4}$  from  $X_{\rm N_2H_4} = 0.1-0.0$  is a constant in accordance with Henry's law. The results show that this quatum exhibits positive deside. this system exhibits positive deviations from Raoult's, and the effect of temperature on the activity coefficients is small. The reason for this behavior stems from the fact that the interaction between the component molecules is through their H atoms which shield the  $\hat{N}$  atoms. The two contacting H atoms, one from NH<sub>3</sub> and the other N<sub>2</sub>H<sub>4</sub>, are energetically in similar states and therefore repel each other slightly to cause small positive deviations from ideality.

The values of  $\Delta \vec{H}$  and  $\Delta \vec{S}$  for  $N_2H_4$  are also listed in Table II. The values of  $\Delta \vec{H}$  and  $\Delta \vec{S}$  are small as expected from a small deviation from ideality. A slight irregularity in the pattern of variation for  $\Delta \vec{H}$  is not serious because a small degree of scattering in the experimental data is ample to account for the scatter.

**CO** in **UDMH** and **SF**<sub>6</sub> in **MH**. The solubilities of CO in UDMH and SF<sub>6</sub> in MH are listed in Table III. Both gases obey Henry's law at all pressures at each temperature because the concentrations of dissolved gases are small. The values of K at each temperature are therefore constant, and a small scattering is simply due to the experimental errors. The logarithm of K is plotted vs. 1/T in  $^{\circ}$ K<sup>-1</sup> in Figure 3 wherein the relationship is linear. The equations for log K have been obtained as functions of 1/T by the least-squares method, and  $\Delta G^{\circ} = -4.5756 T \log K$  has been used to derive the following equations:

$$\Delta G^{\circ}(\text{CO in UDMH}) = 448 + 13.37 T$$
  
 $\Delta G^{\circ}(\text{SF}_{6} \text{ in MH}) = -286 + 17.82 T$ 



Figure 3. Variation of atmospheric solubility, K, with temperature for CO<sub>2</sub>–N<sub>2</sub>O<sub>4</sub>, SF<sub>6</sub>–N<sub>2</sub>O<sub>4</sub>, CO–UDMH, and SF<sub>6</sub>–MH systems

	Table III.	Solubilitie	s of CO	in UDMH	l and S	$F_6$ in $N$	٨H
		<i>T</i> , °K	P, atm	f, atm°	$10^{4}X$	104K'	10 <b>4</b> K
co	in UDMH	253.24	$\begin{array}{c} 0.9302 \\ 1.0190 \\ 1.5276 \\ 1.7539 \end{array}$	$\begin{array}{c} 0.9293 \\ 1.0179 \\ 1.5252 \\ 1.7507 \end{array}$	4.62 4.99 7.60 8.60	4.97 4.90 4.98 4.90 Av	$\begin{array}{r} 4.97 \\ 4.90 \\ 4.98 \\ 4.91 \\ 4.94 \end{array}$
		278.13	0.8772 1.0861 1.6077 1.8643	$\begin{array}{c} 0.8767 \\ 1.0854 \\ 1.6061 \\ 1.8622 \end{array}$	$4.59 \\ 5.70 \\ 8.46 \\ 9.80$	5.23 5.25 5.26 5.26 5.26 Av	$5.24 \\ 5.25 \\ 5.27 \\ 5.26 \\ 5.26 \\ 5.26$
		298.16	$\begin{array}{c} 1.0391\\ 1.4056\\ 1.8454\\ 2.1012 \end{array}$	$\begin{array}{c} 1.0387\\ 1.4049\\ 1.8442\\ 2.0997 \end{array}$	5.86 7.95 10.46 11.89	5.64 5.66 5.67 5.66 Av	5.64 5.66 5.67 5.66 5.66
SF	, in MH	253.17	$\begin{array}{c} 0.2337 \\ 0.3233 \\ 0.9890 \\ 1.0524 \\ 1.9580 \\ 2.0329 \end{array}$	$\begin{array}{c} 0.2326 \\ 0.3212 \\ 0.9692 \\ 1.0299 \\ 1.8802 \\ 1.9490 \end{array}$	$\begin{array}{c} 0.52 \\ 0.72 \\ 2.18 \\ 2.32 \\ 4.28 \\ 4.44 \end{array}$	2.23 2.23 2.20 2.20 2.18 2.18 Av	2.242.242.252.252.272.28 $2.26$
		273.15	$\begin{array}{c} 0.5344 \\ 0.7783 \\ 0.8072 \\ 1.0920 \\ 1.9985 \\ 2.0802 \end{array}$	$\begin{array}{c} 0.5299 \\ 0.7687 \\ 0.7969 \\ 1.0731 \\ 1.9352 \\ 2.0117 \end{array}$	$1.11 \\ 1.61 \\ 1.69 \\ 2.28 \\ 4.13 \\ 4.29$	2.08 2.07 2.09 2.09 2.07 2.06 Av	$\begin{array}{c} 2.09 \\ 2.09 \\ 2.12 \\ 2.12 \\ 2.13 \\ 2.13 \\ 2.11 \end{array}$
		293.14	$\begin{array}{c} 0.7206 \\ 1.0085 \\ 1.0815 \\ 1.0955 \\ 1.9515 \\ 1.9557 \\ 2.1767 \end{array}$	$\begin{array}{c} 0.7141 \\ 0.9957 \\ 1.0668 \\ 1.0804 \\ 1.9037 \\ 1.9077 \\ 2.1173 \end{array}$	$\begin{array}{c} 1.50 \\ 2.11 \\ 2.24 \\ 2.27 \\ 4.16 \\ 4.06 \\ 4.48 \end{array}$	2.08 2.09 2.07 2.07 2.13 2.08 2.06 Av	$\begin{array}{c} 2.10\\ 2.12\\ 2.10\\ 2.10\\ 2.10\\ 2.19\\ 2.13\\ 2.12\\ 2.12\\ 2.12\end{array}$
		313.23	$\begin{array}{c} 0.9514 \\ 1.7330 \end{array}$	$\begin{array}{c} 0.9423 \\ 1.7028 \end{array}$	$\begin{array}{c}1.85\\3.47\end{array}$	1.94 2.00 Av	$1.96 \\ 2.04 \\ 2.00$
a	f = ZP =	fugacity	Y = mo	la fraction	K' =	= X/P	· K =

X = ZP = fugacity; X = mole fraction; K = X/P; K = X/f. Z for CO is from Hilsenrath *et al.* (8), and Z for SF<sub>5</sub> is calculated by using the Berthelot equation of state (9).

 $\Delta G^{\circ}$  for CO in UDMH is similar to N<sub>2</sub> and Ar in UDMH, and in fact  $\Delta S^{\circ}$  is about -13 for all three gases in UDMH (3).

 $CO_2$  and  $SF_6$  in  $N_2O_4$ . The solubilities of  $CO_2$  and  $SF_6$  in  $N_2O_4$  are summarized in Table IV and represented in Figure 3. The corresponding equations for  $\Delta G^\circ$  are as follows:

$$\Delta G^{\circ}(\text{CO}_2 \text{ in } \text{N}_2\text{O}_4) = -2,828 + 17.33 T$$
  
$$\Delta G^{\circ}(\text{SF}_6 \text{ in } \text{N}_2\text{O}_4) = -1,748 + 15.44 T$$

The values of  $\Delta H^{\circ}$  are strongly negative in both systems because CO<sub>2</sub> and SF<sub>6</sub> do not break up the NO<sub>2</sub>—NO<sub>2</sub> bond in N<sub>2</sub>O<sub>4</sub> as He, Ar, N<sub>2</sub>, and O<sub>2</sub> in N<sub>2</sub>O<sub>4</sub> (1). The solubility of CO<sub>2</sub> in N<sub>2</sub>O<sub>4</sub> is close to the ideal solubility at 1 atm computed from  $X(CO_2) = 1/f^{\circ}$ , where  $f^{\circ}$  is the fugacity of pure liquid CO<sub>2</sub> at the temperature of interest, and X is the mole fraction. For example, the ideal solubility at 0°C is 0.0257 mole fraction (7), and the actual solubility is 0.0307 mole fraction as shown in Table IV. It is not surprising that CO<sub>2</sub>-N<sub>2</sub>O<sub>4</sub> are close to ideality since both CO<sub>2</sub> and N<sub>2</sub>O<sub>4</sub> are anhydrous acidic compounds.

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Tabl	e IV. S	olubilitie	s of CO	₂ and SF₅	in N₂O₄			
	<i>T</i> , °K	p, atm	f, atmª	$10^{8}X$	10 <sup>8</sup> K'	10 <b>3</b> K		
COs in N2O4	$262.15 \\ 273.15$	$0.5773 \\ 0.1700 \\ 0.3366$	$0.5746 \\ 0.1698 \\ 0.3358$	$21.03 \\ 5.276 \\ 10.18$	36.43 31.04 30.24 Av	36.60 31.07 30.32 30.70		
	283.20	0.3495 0.6690	$0.3488 \\ 0.6663$	$\begin{array}{c} 8.712 \\ 16.42 \end{array}$	24.93 24.54 Av	$24.98 \\ 24.65 \\ 24.82$		
	293.15	$\begin{array}{c} 0.1763 \\ 0.3175 \\ 0.6225 \end{array}$	$0.1761 \\ 0.3169 \\ 0.6203$	$3.742 \\ 6.524 \\ 12.65$	21.23 20.55 20.32 Av	$21.25 \\ 20.59 \\ 20.39 \\ 20.74$		
SF₅−N₂O₄	263.15	0.7095 1.3778	0.7005 1.3439	$\begin{array}{c} 8.179\\ 16.48\end{array}$	11.53 11.96 Av	$11.68 \\ 12.26 \\ 11.97$		
	278.13	0.6635 1.3957	0.6570 1.3667	6.427 13.96	9.687 10.00 A	9.782 10.214 v 9.998		
	293.14	0.4394 0.9478 1.1006	$0.4370 \\ 0.9365 \\ 1.0854$	3.643 8.013 9.346	8.291 8.454 8.492 A	8.336 8.556 8.611 v 8.501		
<sup>a</sup> $f = ZP$ = fugacity; $X$ = mole fraction; $K' = X/P$ ; $K = X/f$ . Z for CO <sub>2</sub> has been taken from Hilsenrath et al. (8).								

The solubilities of  $CO_2$  in  $N_2O_4$  and CO in UDMH are small enough to permit the use of these gases as pressurants in the low cost boosters. The solubility of  $SF_6$  is small in MH but large enough in  $N_2O_4$  to permit the use of this gas as an electrophyllic substance.

#### LITERATURE CITED

- (1) Chang, E. T., Gokcen, N. A., J. Phys. Chem., 70, 2394 (1966)
- Chang, E. T., Gokcen, N. A., ibid., 72, 2556 (1968). (2)
- Chang, E. T., Gokcen, N. A., Poston, T. M., ibid., p 638. (3)
- Chang, E. T., Gokcen, N. A., Poston, T. M., J. Spacecr. (4)Rockets, 7, 1177 (1969).
- Din, F., Ed., "Thermodynamic Functions of Gases," Vol 1, Butterworths, London, England, 1956, p 94. (5)
- (6) Drago, R. S., Sisler, H. H., J. Phys. Chem., 70, 2394 (1966).
- D'ago, R. S., Sister, H. H., J. Phys. Chem., 70, 2394 (1966).
   Hildebrand, J. H., Scott, R. L., "The Solubility of Non-electrolytes," Reinhold, New York, N.Y., 1950, p 248.
   Hilsenrath, J. H., Beckett, C. W., Benedict, W. S., Fano, L., Hoge, H. J., Masi, J. F., Nuttall, R. L., Toulaukian, Y. S., Woolley, H. W., "Tables of Thermal Properties of Gases," National Standards Circuit 564, U.S. Compared to Standards Circuit 18, 189 (1990). National Bureau of Standards Circular 564, U.S. Government Printing Office, Washington, D.C., 1955.
- (9) "Matheson Gas Data Book," 4th ed., Matheson Co., Inc., East Rutherford, N. J., 1966, p 455.

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## Vapor Pressures and Second Virial Coefficients of Some Five-Membered Heterocyclic Derivatives

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> Vapor pressures and second virial coefficients of furan, thiophene, pyrrole, and some of their substituted derivatives were measured by an isoteniscopic method in the temperature range 60-100°C.

Knowledge of vapor pressures and virial coefficients is necessary for the study of molecular interactions in systems involving a vapor phase-homogeneous gas phases or hetero-geneous liquid-vapor systems. Especially gas-liquid chromatography allows the determination of activity coefficients  $\gamma_i$  of volatile solutes in the liquid stationary phase, from the wellknown relationship:

$$V_{\sigma} = \frac{273 R}{f_i^0 \gamma_i^0 M} \tag{1}$$

where  $V_{g}$  is the specific retention volume of the compound *i*,  $f_i^{0}$  is its vapor fugacity at the column temperature, and M is the molecular weight of the stationary phase.

When helium is used as the carrier gas, the interactions between the vapor of the solute i and this carrier gas can be neglected, and the fugacity  $f_i^0$  is related to the vapor pressure  $P_{i}^{0}$  and to the second virial coefficient  $B_{ii}$  by the equation:

$$\ln f_{i}^{0} = \ln P_{i}^{0} + \frac{P_{i}^{0}}{RT} (B_{ii} - v_{i}^{0})$$
(2)

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where  $v_i^{0}$  is the molar volume of the pure liquid compound *i*. The derivation of these equations and the range of validity were discussed previously (1, 2).

The following measurements were performed with the aim of calculating the activity coefficients  $\gamma_i$  from chromatographic retention data using Equation 1. Since the values of  $P_i^{0}$  and  $B_{ii}$  thus obtained were of more general use, it seemed useful to publish these data independently of any application.

#### EXPERIMENTAL

Measurements were made by the isoteniscopic method with the apparatus shown in Figure 1. The flask (A) containing the investigated compound and the null manometer (B) were immersed in a thermostated oil bath. The pressure measurements were made with the external manometer (C). Metallic contacts (m) and an electrovalve (D) permitted regulation of the mercury levels in the null manometer when the pressure in A approached equilibrium.

The investigated compound was introduced in the flask (A) through the Torion valve (E) (Prolabo, Paris, France) with a