# Three-Phase Solid–Liquid–Vapor Equilibria of the Binary Hydrocarbon Systems Propane–Benzene, Propane–Cyclohexane, *n*-Butane–Benzene, *n*-Butane–Cyclohexane, *n*-Butane–*n*-Decane, and *n*-Butane–*n*-Dodecane

#### Wel-LI Chen, Kraemer D. Luks,<sup>†</sup> and James P. Kohn\*

Department of Chemical Engineering, University of Notre Dame, Notre Dame, Indiana 46556

Pressure, temperature, liquid-phase compositions, and liquid-phase molar volumes are presented along the solid-liquid-vapor loci of six binary systems: the solvent propane with solutes benzene and cyclohexane, and the solvent *n*-butane with solutes benzene, cyclohexane, n-decane, and n-dodecane. The data were taken by using cryoscopic techniques over a liquid compositional range extended from the solute triple point to dilute solute solutions. When represented as a plot of the logarithm of solute composition vs. reduced reciprocal temperature  $T_{\rm T}/T$ , the data are smooth curves which become linear at the low-temperature (low solute composition) end of the loci. The standard deviations of the liquid-phase solute composition data are 0.19% for the propane-benzene system, 0.47 % for the propane-cyclohexane system, 0.32% for the n-butane-benzene system, 0.45% for the n-butane-cyclohexane system, 0.08% for the n-butane-n-decane system, and 2.05% for the n-butane-n-dodecane system.

#### Introduction

Solid solubility data of hydrocarbon components in low molecular weight solvents are important for use in the design of liquefaction, vaporization, and transport systems for liquefied natural gas (LNG) and liquefied petroleum gas (LPG). We have been engaged in an extended program of obtaining and classifying such data, primarily in the low solute concentration range.

In previous papers, we reported the solubility of two different hydrocarbon solutes in methane (1), eight different hydrocarbon solutes in ethane (2-4), and two different hydrocarbon solutes in propane (4). In this present paper, we report the solubility of six different hydrocarbon solutes in the solvent species propane and *n*-butane. All of these binary data form a basis from which the solubility of paraffinic, aromatic, and naphthenic hydrocarbons in LNG and LPG systems can be correlated and predicted.

#### **Experimental Section**

The apparatus was identical with that described by Lee and Kohn (5), which was used in other cryoscopic studies (1-3). The experimental procedure is described in our earlier paper (6).

The propane and *n*-butane used in this study were Linde "instrument grade" stated to be 99.5 mol% pure. A 253.48 K isotherm determined on the propane indicated a difference between dew-point and bubble-point pressures of less than 0.1

temp, K	press., atm	compn <sup>a</sup>	molar vol, <sup>b</sup> mL/(g-mol)
265	1.79	0.764 8	85.0
260	1.75	0.6580	83.7
255	1.70	0.5525	82.3
250	1.61	0.445 2	81.1
245	1.48	0.3508	79.8
240	1.32	0.2741	78.6
235	1.14	0.215 2	77.5
230	0.94	0.168 9	76.5
225	0.84	0.1335	75.6
220	0.75	0.1067	74.8
215	0.66	0.084 87	74.1
210	0.58	0.067 96	73.4
205	0.51	0.054 34	72.7
200	0.46	0.04326	72.1
195		0.03455	71.4
190		0.027 35	70.7
185		0.021 57	70.0
180		0.016 76	69.4
175		0.01283	68.6
170		0.009 81	67.9
165		0.007 36	67.4
160		0.005 48	67.2

Table I. Solid-Liquid-Vapor Three-Phase Smoothed Data for the Propane-Benzene Binary System

<sup>a</sup> Liquid phase (mole fraction benzene). <sup>b</sup> Liquid phase.

atm. The vapor pressure and the liquid-phase molar volume at 50 vol% liquid were within 0.1 atm and 0.2 mL/(g-mol), respectively, of the literature values (7). The propane and n-butane were used without further purification.

The *n*-decane and *n*-dodecane were Humphrey-Wilkinson "Pure Grade" petroleum-derived products with a stated purity of 99%. The benzene was a Mallinckrodt "Spectrar" spectrophotometric-grade chemical. The cyclohexane used was an Eastman Reagent "ACS Grade" chemical. The air-saturated freezing points of these hydrocarbon solutes were within  $\pm 0.1$ K of the literature values, with the exception of benzene, which was within  $\pm 0.3$  K. The refractive indexes differed by no more than  $\pm 0.0003$  from the literature values for all of the hydrocarbon solutes. All four solutes were used without further purification.

#### Results

Tables I and II present the smoothed experimental data for the two propane solvent systems, and Tables III–VI present the smoothed experimental data for the four*n*-butane solvent systems. The pressures are precise to  $\pm 0.1$  atm, the temperatures to  $\pm 0.2$  K, and the liquid-phase molar volume to  $\pm 1.0$ mL/(g-mol). The liquid-phase composition data were smoothed

<sup>&</sup>lt;sup>†</sup>Present address: Department of Chemical Engineering, University of Tulsa, Tulsa, OK 74104.

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Table II. Solid-Liquid-Vapor Three-Phase Smoothed Data for the Propane-Cyclohexane Binary System

temp, K	press., atm	compn <sup>a</sup>	molar vol, <sup>b</sup> mL/(g-mol)
245	0.65	0.8546	98.9
240	0.64	0.8316	97.6
235	0.63	0.8086	96.4
230	0.61	0.7852	95.1
225	0.60	0.7616	94.0
220	0.58	0.7379	92.8
215	0.55	0.7144	91.6
210	0.53	0.6915	90.5
205	0.51	0.6718	89.5
200	0.48	0.6538	88.3
195	0.45	0.6304	87.2
190		0.6056	86.1
185		0.5801	83.5
180		0.5114	81.4
175		0.4114	79.2
170		0.3302	77.1
165		0.2641	75.0
160		0.2083	72.8
156		0.1658	71.0
<sup>a</sup> Liquid phas	e (mole fraction	cvclohexane).	<sup>b</sup> Liquid phase.

Table III. Solid-Liquid-Vapor Three-Phase Smoothed Data for the *n*-Butane-Benzene Binary System

temp, K	press., atm	compn <sup>a</sup>	molar vol, <sup>ø</sup> mL/(g-mol)
 270	0.60	0.8637	88.4
265	0.59	0.7802	89.2
260	0.58	0.664 0	89.7
255	0.56	0.550 3	90.0
250	0.55	0.448 4	90.2
245	0.53	0.3600	90.2
240	0.51	0.2900	90.2
235	0.49	0.2306	90.1
230	0.47	0.1809	89.8
225	0.45	0.1464	89.3
220		0.118 4	88.7
215		0.097 36	87.9
210		0.079 81	87.1
205		0.065 48	86.1
200		0.05331	85.3
195		0.043 12	84.5
190		0.034 54	83.8
185		0.027 28	83.2
180		0.021 20	82.7
175		0.016 49	82.4
170		0.012 74	82.0
165		0.009 81	81.7
160		0.007 66	81.3

<sup>a</sup> Liquid phase (mole fraction benzene). <sup>b</sup> Liquid phase.

Table IV. Solid-Liquid-Vapor Three-Phase Smoothed Data for the *n*-Butane-Cyclohexane Binary System<sup>a</sup>

temp, K	compn <sup>b</sup>	molar vol, <sup>c</sup> mL/(g-mol)	temp, K	compn <sup>b</sup>	molar vol, <sup>c</sup> mL/(g-mol)
260	0.9630	108.5	205	0.6745	96.6
255	0.9329	107.2	200	0.6504	95.5
250	0.9059	106.1	195	0.6269	94.2
245	0.8787	105.1	190	0.6046	93.2
240	0.8522	104.2	185	0.5848	91.2
235	0.8260	103.0	180	0.4983	89.5
230	0.8004	102.5	175	0.3983	87.7
225	0.7749	101.5	170	0.3291	86.4
220	0.7497	100.1	165	0.2679	85.2
215	0.7246	99.0	160	0.2172	84.2
210	0.6995	97.7	157	0.1864	83.7

<sup>a</sup> Pressure is less than 0.45 atm at all data points. <sup>b</sup> Liquid phase (mole fraction cyclohexane). <sup>c</sup> Liquid phase.

Table V. Solid-Liquid-Vapor Three-Phase Smoothed Data for the *n*-Butane-*n*-Decane Binary System<sup>a</sup>

temp, K	compn <sup>b</sup>	molar vol, <sup>c</sup> mL/(g-mol)	temp, K	compn <sup>b</sup>	molar vol, <sup>c</sup> mL/(g-mol)
240	0.8156	166.5	200	0.048 13	90.0
235	0.6008	143.5	195	0.03161	88.0
230	0.4371	128.6	190	0.02043	86.6
225	0.3140	117.5	185	0.012 99	85.6
220	0.2224	109.0	180	0.008 15	84.6
215	0.1551	102.4	175	0.005 08	83.9
210	0.1066	97.2	170	0.003 17	83.0
205	0.07220	93.2	165	0.001 99	82.5

<sup>a</sup> Pressure is less than 0.45 atm at all data points. <sup>b</sup> Liquid phase (mole fraction *n*-decane). <sup>c</sup> Liquid phase.

Table VI. Solid-Liquid-Vapor Three-Phase Smoothed Data for the *n*-Butane-*n*-Dodecane Binary System<sup>a</sup>

temp, K	compn <sup>b</sup>	molar vol, <sup>c</sup> mL/(g-mol)	temp, K	compn <sup>b</sup>	molar vol, <sup>c</sup> mL/(g-mol)
255	0.5795	163.5	215	0.024 61	91.1
250	0.4125	141.5	210	0.015 41	88.9
245	0.2886	126.0	205	0.00954	87.5
240	0.1987	115.0	200	0.005 82	86.3
235	0.1345	107.2	195	0.00350	85.2
230	0.08985	101.2	190	0.00206	84.5
225	0.05914	96.6	185	0.001 24	83.9
220	0.03836	93.0			

<sup>a</sup> Pressure is less than 0.45 atm at all data points. <sup>b</sup> Liquid phase (mole fraction n-dodecane). <sup>c</sup> Liquid phase.

Table VII. Standard Deviation for Liquid-Phase Solute Compositions, Total Number of Data Points, and Number of Cell Loadings for the Six Binary Systems Studied

system	SD, %	no. of data points	no. of cell loadings
propane-benzene	0.19	39	6
propane-cyclohexane	0.47	19	2
n-butane-benzene	0.32	47	5
n-butane-cyclohexane	0.45	38	2
n-butane-n-decane	0.08	44	6
n-butane-n-dodecane	2.05	51	6



Figure 1. Experimental solute mole fraction vs. reduced reciprocal temperature as compared with ideal predictions for the systems propane-benzene and propane-cyclohexane. The heavy lines are the smoothed data presented in Tables I and II, while the light lines are the ideal solubility loci for both systems.

before tabulation by use of the same procedure reported earlier (2, 3). Table VII gives the standard deviation between



**Figure 2.** Experimental solute mole fraction vs. reduced reciprocal temperatures as compared with ideal predictions for the system *n*-butane-benzene and *n*-butane-cyclohexane. The heavy lines are the smoothed data presented in Tables III and IV, while the light lines are the ideal solubility loci for both systems.

smoothed and raw data, as well as the number of cell loadings and data points taken.

The raw data and the smoothed composition lines for the first four systems are presented in Figures 1 and 2. The straight lines on these semilogarithmic plots are "ideal" solubility lines. At high values of  $1/T^*$ , the data start to become linear in these coordinates, a characteristic observed in our earlier studies and interpreted as the region in which Henry's law for dilute solutions might be expected to be valid. It is feit that linear extrapolation of these data in these semilogarithmic plots would be reasonably accurate. All raw data are available as suplementary material.)

No plot is presented of the data for the systems n-butanen-decane and n-butane-n-dodecane, as the compositions of these two systems are quite close to those which would be predicted by "ideal" solubility.

All of the S–L–V loci presented herein are continuous from solute triple point to dilute solute region, as the molecular differences between the solute and the solvent are not severe. The nearly "ideal" behavior in the systems n-butane with n-

decane and *n*-dodecane is not surprising if one recalls the near "ideal" behavior of the systems propane and these same solutes (7). Looking at these solutes and the solubility behavior in ethane (2, 3), propane, and butane, one notes that the solute composition increases with solvent molecule size at a given temperature. The same effect is noted with the solute benzene; however, along a portion of the *n*-butane-cyclohexane locus, the solute composition values are less than their corresponding values on the propane-cyclohexane locus.

From examination of the data herein and earlier data on n-paraffin solutes, one can suggest that nonideality is significant with the solvent ethane for n-paraffin solutes above n-octane, and with the solvent propane for solutes above n-decane, while the solvent n-butane is ideal for solutes up to n-dodecane.

#### Glossary

- L liquid phase
- S solid phase
- T temperature in K
- *T*<sub>T</sub> triple-point temperature in K: 278.69 K for benzene, 279.83 K for cyclohexane, 243.51 K for *n*-decane, and 263.61 K for *n*-dodecane

 $T^* = T/T_T$ 

x solute mole fraction in phase L

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Supplementary Material Available: Complete tables of raw data for all six binary systems (8 pages). Ordering information is given on any current masthead page.

## Viscosities and Densities of Four Binary Liquid Systems at 25.00 °C

#### Abdul-Fattah A. Asfour<sup>†</sup> and Francis A. L. Dullien\*

Chemical Engineering Department, University of Waterloo, Waterloo, Ontario, Canada N2L 3G1

### Densities and viscosities of four binary systems, viz., benzene-toiuene, chloroform-toiuene,

chloroform-benzene, and benzene-*n*-hexane, have been determined at 25.00 °C, over the complete composition ranges. The results have been discussed in the light of ideal solution behavior. A few of the existing predictive equations of mixture viscosities have been tested.

<sup>†</sup>Present address: Imperial Oil Limited, Research Department, P.O. Box 3022, Sarnia, Ontario N7T 7M1, Canada.

#### Introduction

The ideal mixture concept, widely used in solution thermodynamics, corresponds to a limiting behavior that has a physical basis in the properties of highly dilute solutions, but may lack such basis in the case where the ideal mixture concept is extended to cover the entire mole fraction range of a liquid system. Presented in this paper are results of density and viscosity determinations on carefully selected binary liquid mixtures, such that could be expected to approximate ideal solution behavior as closely as any liquid system of chemically different components may.