

$n_{i0}$	characteristic constant for each family of substances
$\alpha_i$	molecular polarizability of the component $i$ , $\text{cm}^3 \text{mol}^{-1}$
$a_j$	polynomial coefficients in eq 4
$n_A, n_D$	refractive indexes of A and D in eq 6
$\varphi_A$	volume fraction of the component A in eq 6
$n$	polynomial degree
$\rho$	density of the solution, $\text{g cm}^{-3}$

**Registry No.** Methyl isobutyl ketone, 108-10-1; *sec*-butyl alcohol, 78-92-2; isobutyl alcohol, 78-83-1; *n*-butyl alcohol, 71-36-3.

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## Thermodynamic Properties of Isobutane in the Critical Region

J. M. H. Levelt Sengers,<sup>\*†</sup> B. Kamgar-Parsi,<sup>‡</sup> and J. V. Sengers<sup>††</sup>

*Thermophysics Division, National Bureau of Standards, Washington, D.C. 20234, and Institute for Physical Science and Technology, University of Maryland, College Park, Maryland 20742*

**For geothermal applications, a scaled fundamental equation has been formulated in order to represent and tabulate the thermodynamic properties of isobutane in the critical region. In the supercritical range, the surface joins smoothly with that of Waxman and Gallagher, to which it is a complement. The range of the surface is 405–438 K in temperature, 150–290 kg/m<sup>3</sup> in density. The critical constants are  $T_c = 407.84 \pm 0.02$  K,  $\rho_c = 225.5 \pm 2$  kg/m<sup>3</sup>,  $P_c = 3.629 \pm 0.002$  MPa. Comparisons are made with the PVT data of Beattie et al., and of Waxman, and also with the formulations of Waxman and Gallagher, and of Goodwin and Haynes.**

#### Introduction

Isobutane has been proposed as the working fluid in binary geothermal power cycles. In this application, the fluid would pass through the heat exchanger at a pressure exceeding the critical pressure ( $P_c = 3.63$  MPa), while it is heated from ambient to supercritical temperatures ( $T_c = 408$  K). The initial state of the fluid entering the turbine would be a supercritical pressure and temperature, while the density would be somewhat below the critical. The gas would then expand isentropically along a path that, preferably, should remain within the one-phase vapor region. Kestin and Khalifa (1, 2) pointed out that the then-existing formulations of the thermodynamic properties of isobutane were of insufficient reliability for design of an efficient cycle. The lack of reliability was due, to a considerable extent, to sparsity and inconsistency of the thermodynamic data. Since then, the situation has been remedied, at least to a good extent, by the acquisition of new data on the vapor pressure and on PVT of the vapor and supercritical phase by Waxman et al. (3–6), and on PVT of the liquid by Haynes (7). These new accurate data permitted Waxman et al. to select the bodies of reliable data.

It was decided to approach the formulation of the thermodynamic surface in two steps. Waxman and Gallagher (5, 6)

adapted the free energy model developed by Haar and co-workers (8) to represent the thermodynamic properties of isobutane up to 40 MPa and from 250 to 700 K with the exclusion of a region around the critical point the size of which is

$$0.985 \leq T_c/T \leq 1.015 \quad \text{i.e., } 401.8 \leq T \leq 414 \text{ K}$$

$$0.7 \leq \rho_c/\rho \leq 1.3 \quad \text{i.e., } 173.4 \leq \rho \leq 322 \text{ kg/m}^3 \quad (1)$$

The thermodynamic surface that we present here is valid in the range

$$405 \leq T \leq 438 \text{ K}$$

$$150 \leq \rho \leq 290 \text{ kg/m}^3 \quad (2)$$

and thus supplements the surface of Waxman et al. in most of the excluded range. The model that we use is that of revised and extended scaling, as developed according to the modern theory of critical phenomena (9). We have applied this model successfully to the thermodynamic properties of light and heavy water (10, 11) in the critical region. Here, however, we use a somewhat different approach toward determining the model parameters. We obtained most of our parameter values by a fit to the experimental PVT data of Beattie et al. (12, 13), which were recently validated by Waxman (6). There are a large number of PVT data in a very narrow temperature region, from 407.8 to 408.3 K, around the critical point; the only other data available in our range are on the 423.17 K isotherm. It is clear that temperature derivatives of the surface cannot be reliably taken if the surface is based on only two isotherms. We therefore supplemented the experimental data with PVT points generated from the surface of Waxman et al. in a range in which the surface is valid. This practice has yielded three benefits. It has helped pinpoint our surface, has ensured a smooth crossover to the analytic surface along most of the boundary, and has provided the entire analytic "background" for the caloric parameters, for which, in the case of isobutane, no experimental information is available.

The critical-point parameters incorporated in the scaled equation differ from those reported by Beattie et al. (12). If the critical parameters are freely adjusted in the fit to a scaled equation, the value of the critical temperature falls as much as

<sup>†</sup> National Bureau of Standards.

<sup>‡</sup> University of Maryland.

0.3 K below that deduced by Beattie et al. from the same data. An independent experimental determination of the critical temperature of isobutane by one of us (J.M.H.L.S.) gave results very close to the low value of  $T_c$  that we deduced from Beattie's data. This is the value that we then used in the fit.

We present here tabulated values derived from our fundamental equation for the saturation properties and for pressure, energy, enthalpy, entropy, specific heats at constant pressure and volume, and speed of sound, along isotherms in the range given by eq 2.

Comparisons are presented with the experimental *PVT* data, with the analytic surface of Waxman et al., and with the coexistence curve of Goodwin and Haynes (7).

### Scaled Fundamental Equation

Our fundamental equation involves a relationship between the intensive thermodynamic variables pressure  $P$ , chemical potential  $\mu$ , and temperature  $T$ . Specifically we consider the reduced variables

$$\tilde{P} = \frac{P}{P_c} \frac{T_c}{T} \quad \tilde{\mu} = \frac{\mu}{T_c} \frac{\rho_c T_c}{P_c} \quad \tilde{T} = -T_c/T \quad (3)$$

where  $P_c$  is the critical pressure,  $T_c$  the critical temperature, and  $\rho_c$  the critical density. The fundamental equation yields the thermodynamic potential  $\tilde{P}$  as a function of  $\tilde{\mu}$  and  $\tilde{T}$  and has the form

$$\tilde{P} = \tilde{P}_0(\tilde{T}) + \Delta\tilde{\mu} + \tilde{P}_{11}\Delta\tilde{\mu}\Delta\tilde{T} + \Delta\tilde{P} \quad (4)$$

with

$$\Delta\tilde{T} = \tilde{T} + 1 \quad (5)$$

$$\Delta\tilde{\mu} = \tilde{\mu} - \tilde{\mu}_0(\tilde{T}) \quad (6)$$

Here  $\tilde{P}_0(\tilde{T})$  and  $\tilde{\mu}_0(\tilde{T})$  are analytic functions of  $\Delta\tilde{T}$ , while  $\Delta\tilde{P}$  contains the singular, i.e., nonanalytic, contributions to the potential  $\tilde{P}$ . The equations for these functions are fully specified in Appendix A. The analytic functions are represented by truncated power series in terms of  $\Delta\tilde{T}$  while the singular part  $\Delta\tilde{P}$  is related to  $\Delta\tilde{\mu}$  and  $\Delta\tilde{T}$  with the aid of two auxiliary (parametric) variables  $r$  and  $\theta$ . The computer program that generates values of the thermodynamic functions from our fundamental equation has been published elsewhere (10).

The fundamental equation contains the following constants: three critical parameters,  $P_c$ ,  $T_c$  and  $\rho_c$ ; three critical exponents,  $\beta$ ,  $\delta$ , and  $\Delta$ ; five parameters,  $a$ ,  $k_0$ ,  $k_1$ ,  $c$ , and  $b^2$ , in the singular contribution  $\Delta\tilde{P}$ ; four "background" parameters,  $\tilde{P}_1$ ,  $\tilde{P}_2$ ,  $\tilde{P}_3$ , and  $\tilde{P}_{11}$ , that specify the analytic contributions to  $\tilde{P}$ ; and four "background" parameters,  $\tilde{\mu}_c$ ,  $\tilde{\mu}_1$ ,  $\tilde{\mu}_2$ , and  $\tilde{\mu}_3$ , that specify the analytic contribution to the thermal properties as a function of temperature. The three critical exponents are universal, i.e., the same for all fluids, and their "best" theoretical values are imposed on the evaluation of the other constants.

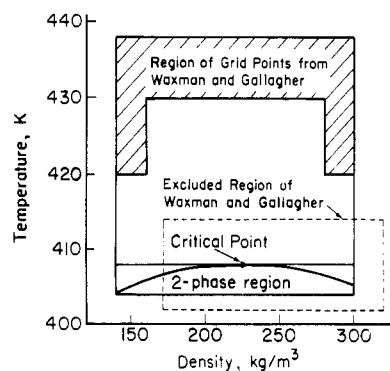
The values that we have assigned to the parameters in the fundamental equation for isobutane are listed in Appendix B. The way in which the parameters were determined is the topic of the following section. The equation is valid in the range of temperatures and densities given in eq 2.

### Data Sources

The *PVT* data of Beattie et al. consist of 13 isotherms (12) containing 174 points in the range

$$407.764 \leq T \leq 408.314 \text{ K} \quad 180.5 \leq \rho \leq 270.3 \text{ kg/m}^3$$

and data on a number of isotherms at higher temperatures (13). Of these, the 423.170 K isotherm contains six points in the density range 145.2–290.4 kg/m<sup>3</sup>. The next higher isotherm,



**Figure 1.** Range of validity of the present formulation is given by the heavy-drawn rectangle in the temperature–density plane. The dotted rectangle indicates the range excluded by Waxman and Gallagher. The hatched region is that in which data points were generated from the Waxman–Gallagher formulation in order to define our surface.

at 448.182 K, is outside the range of validity of our equation.

The following estimates were made of the experimental errors of the data of Beattie et al.:

$$\begin{aligned} \sigma_P &= 10^{-4} \text{ MPa} & \sigma_T &= 0.005 \text{ K} \\ \sigma_\rho &= 0.058 \text{ kg/m}^3 \text{ (0.001 mol/dm}^3\text{)} \end{aligned} \quad (7)$$

The mass of the sample was determined by weight, but the data were reported in molar units. Beattie et al. used  $M = 58.077 \text{ g/mol}$  for isobutane and, in order to conserve consistency, we used this same value of  $M$  to reconvert their density data to units of kg/m<sup>3</sup>.

For reasons given in the Introduction, we supplemented the experimental data with calculated points generated from the surface of Waxman and Gallagher (6). We generated 215 *PVT* data points on a grid in a region in the  $\rho$ – $T$  space bounded, on the sides, by

$$420 \leq T \leq 438 \text{ K} \quad 140 \leq \rho \leq 160 \text{ kg/m}^3$$

$$420 \leq T \leq 438 \text{ K} \quad 280 \leq \rho \leq 300 \text{ kg/m}^3$$

and at the top by

$$430 \leq T \leq 438 \text{ K} \quad 140 \leq \rho \leq 300 \text{ kg/m}^3$$

This range is indicated in Figure 1. The grid points were spaced by 2 K and 5 kg/m<sup>3</sup>. The range around the critical point excluded by Waxman and Gallagher, eq 1, is also indicated in Figure 1.

In the fitting procedure, we have assigned the same uncertainties to the generated points as to the experimental *PVT* data. Beattie's temperatures were reported on the International Practical Temperature Scale (IPTS) of 1948. We have converted the experimental temperatures to IPTS of 1968 for the present analysis. The surface of Waxman and Gallagher was assumed to be on IPTS-68. All temperatures reported in what follows will be on IPTS-68 unless a statement to the contrary is made.

### Critical-Point Parameters

Beattie et al. obtained the critical parameters of isobutane from their *PVT* data in a range of 0.6 K around  $T_c$  by a graphical construction of the coexistence dome (12). They obtained

$$\begin{aligned} T_c &= 408.14_4 \text{ K} & \rho_c &= 221 \text{ kg/m}^3 \\ P_c &= 3.648 \text{ MPa} \end{aligned} \quad (8)$$

It is our contention that this dome was not drawn sufficiently flat. A preliminary analysis of Beattie's data by a simple scaled equation yielded (3)

$$T_c = 407.865 \text{ K} \quad \rho_c = 226.85 \text{ kg/m}^3 \quad (9)$$

$$P_c = 3.6306 \text{ MPa}$$

Since scaled analyses of *PVT* data do not determine the critical temperature very precisely, one of us (J.M.H.L.S.) determined the critical temperature of 99.98% pure isobutane by observation of the meniscus disappearance, and the critical density by weight (Appendix E). The results are

$$T_c = 407.84 \pm 0.02 \text{ K} \quad \rho_c = 225.5 \pm 2 \text{ kg/m}^3 \quad (10)$$

These values are clearly consistent with those obtained by the simple scaled analysis of Beattie's data. We have therefore, in our present analysis, imposed the observed value of  $T_c = 407.84 \text{ K}$ .

If the experimental value of  $\rho_c$ , eq 10, is imposed on the fit to the present scaled equation, the reduced  $\chi^2$  equals 1.72, compared with a minimum value of 1.26 reached for  $\rho_c = 226.42 \text{ kg/m}^3$ . We felt that the increase in  $\chi^2$  could be tolerated and therefore we have imposed the critical parameter values

$$T_c = 407.84 \text{ K} \quad \rho_c = 225.5 \text{ kg/m}^3 \quad (11)$$

The critical pressure was treated as an adjustable parameter in the fit to the *PVT* data.

### Equation of State Parameters

The values that we have accepted for the universal parameters  $\beta$ ,  $\delta$ ,  $\Delta_1$ , and  $b^2$  (Appendix B) reflect the current theoretical knowledge (9) and are the same as the values that we used to represent the thermodynamic properties of light and heavy water (10, 11).

The parameters  $a$ ,  $k_0$ ,  $k_1$ ,  $c$  in the scaled contribution, and the pressure background parameters  $\bar{P}_1$ ,  $\bar{P}_2$ ,  $\bar{P}_3$ ,  $\bar{P}_{11}$ , are system dependent. These parameters, together with the critical pressure  $P_c$ , are determined by fitting the equation of state to the *PVT* data, with the exception of  $\bar{P}_{11}$ , which is determined from the slope of the diameter of the coexistence curve; this slope was deduced from the equation of Waxman et al. to be equal to  $-0.4971 \text{ kg/m}^3$ , or  $-0.9011$  in reduced units. In our analysis we found that the coefficient  $\bar{P}_3$  was not statistically significant and did not improve the accuracy of the representation; it was therefore set equal to zero.

The constant  $\bar{P}_1$  is related to the slope of the vapor pressure curve at the critical point. Our first approach was to estimate this slope by fitting Waxman's new vapor pressure data (6) in the range of 298.15–398.15 K with a scaled equation, while imposing our choices of  $P_c$  and  $T_c$ . The equation and the results of the fit are summarized in Appendix C. From this fit, we obtained  $\bar{P}_1 = 5.8038$ . We realize, however, that the use of a scaled equation in such a large range is not justified. If  $\bar{P}_1$  is left a free parameter in the fit to Beattie's data, we obtain  $\bar{P}_1 = 5.8858 \pm 0.0015$ , a significantly higher value. The low value from the vapor pressure analysis cannot be reconciled with the *PVT* data. It is the high value from the *PVT* data that we have adopted for  $\bar{P}_1$ .

The values of the parameters of the equation of state, obtained by fitting the *PVT* data of Beattie et al. plus points generated from the surface of Waxman et al. to our equation, are listed in Appendix B. The reduced  $\chi^2$  of the fit is 1.72.

In Figures 2 and 3 we show the pressure deviations of the experimental data of Beattie et al. from our surface. In Figure 3 we also show the deviations of the surface of Waxman et al. from our surface along selected isotherms as indicated by the dashed curves. Most of the Beattie data are fitted to better than 0.002 MPa and the departures of the Waxman surface from our own for temperatures 423 K and higher are also within the 0.002 MPa range.

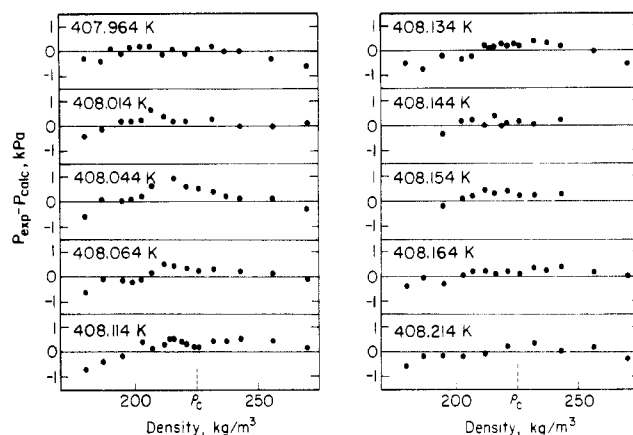


Figure 2. Departures of the isothermal *PVT* data of Beattie et al. (12) from our surface (1 kPa = 0.001 MPa = 0.01 bar).

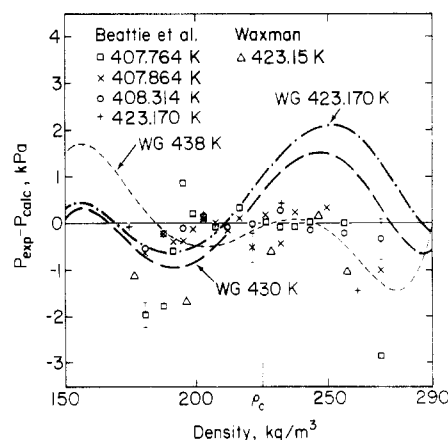
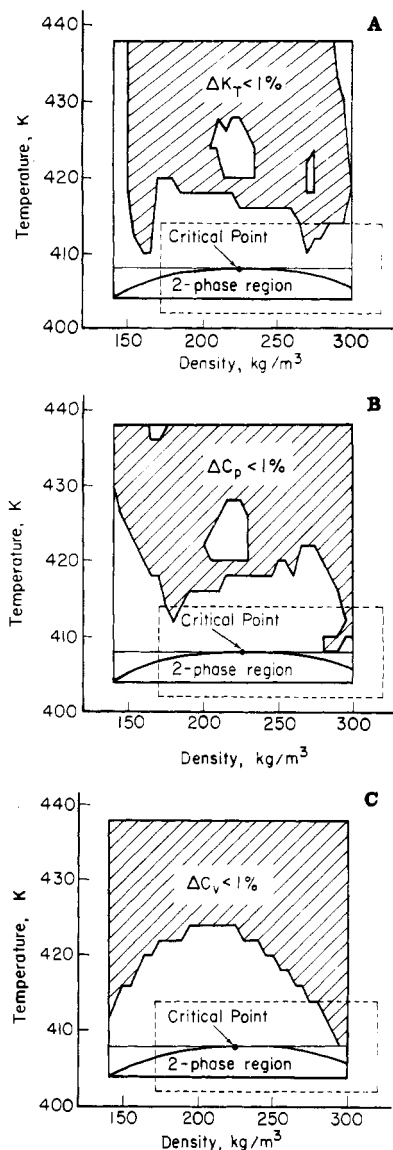


Figure 3. Departures of the *PVT* data of Beattie et al. (12, 13) and of Waxman (6) from our surface along selected isotherms. The curves denote the departures of the Waxman-Gallagher formulation (6) from our surface. All departures are well within the 0.002-MPa range (1 kPa = 0.001 MPa = 0.01 bar).

### Coexistence Curve

The location of the phase boundary turned out to be the most frustrating part of the correlation. Reliable experimental data for the saturation properties are not available for the vapor above 368 K and for the liquid above 396 K. The coexistence curve that we predict is based on Beattie's *PVT* data which extend over a range of no more than 0.1 K below the critical point. Our coexistence curve ceases to be valid below 405 K. The coexistence curve prediction of Waxman and Gallagher, however, is not valid for temperatures exceeding 401.8 K, eq 1. We have compared with the coexistence curve from the correlation of Goodwin and Haynes (7) which equation incorporates some of the critical anomalies and has its critical point at the physical critical temperature. The comparison is shown in Table I. It is seen that the liquid densities agree on the level of 0.2%, which is excellent. The vapor densities of our equation are up to 1.8% lower than those of Goodwin and Haynes. In the absence of data above 368 K, this is probably not a bad agreement. Even though a "blend" with the Waxman surface has been our goal, we have not tried to readjust our surface in order to match up with Waxman's coexistence curve: doing this would have brought our coexistence curve further from the dome predicted by Goodwin and Haynes and would have put undue strain on our surface in other regions.

We note that classical equations lead to a coexistence dome which is not sufficiently flat (14). As a consequence such equations tend to imply a critical temperature which is too high (15). Indeed, when the analytic equation of Waxman and



**Figure 4.** In the  $T$ - $\rho$  plane, the range is indicated in which specific thermodynamic derivatives from the Waxman-Gallagher surface agree with the present surface to better than 1%: (A) compressibility  $K_T$ , (B) specific heat  $C_p$ , (C) specific heat  $C_v$ . The dotted rectangle indicates the range excluded by the Waxman-Gallagher formulation.

Gallagher, valid away from the critical point, is extrapolated into the critical region, it implies values for  $T_c$  and  $P_c$  about 1.8 K and 0.11 MPa too high.

#### Thermal Background Parameters

In our analyses of the thermodynamic properties of  $H_2O$  and  $D_2O$ , we used experimental data on the thermal properties such as specific heats or speed of sound to determine the thermal background parameters  $\tilde{\mu}_2$  and  $\tilde{\mu}_3$ . Since experimental data on the thermal properties of isobutane in the critical region are not available, we used the thermodynamic surface of Waxman et al. to determine the values of the parameters  $\tilde{\mu}_2$  and  $\tilde{\mu}_3$ .

We therefore generated isochoric specific heat,  $C_v$ , data from the equation of Waxman et al. in the range shown in Figure 1. After subtracting the scaled contributions to  $C_v$  from these generated data, we have fitted the remainder to a linear expression to determine the parameters  $\tilde{\mu}_2$  and  $\tilde{\mu}_3$ .

First, in order to determine whether the inclusion of the background parameter  $\tilde{\mu}_3$  significantly improves our surface, we set  $\tilde{\mu}_3 = 0$  and fitted the  $C_v$  remainder to  $\tilde{\mu}_2$ . We find  $\tilde{\mu}_2 = -37.705 \pm 0.023$ . With this value for  $\tilde{\mu}_2$ , the differences in  $C_v$  calculated from our equation and that of Waxman et al.

**Table I.** Comparison with the Coexistence Dome of Goodwin and Haynes

temp, K	saturated liquid densities, kg/m <sup>3</sup>			diff, %
	Goodwin	scaled	diff	
404.0	315.18	314.60	0.58	0.18
404.5	310.75	310.10	0.65	0.21
405.0	305.88	305.19	0.69	0.22
405.5	300.44	299.77	0.67	0.22
406.0	294.22	293.61	0.61	0.21
406.5	286.81	286.36	0.45	0.16
407.0	277.36	277.19	0.17	0.06
407.5	263.11	263.43	-0.32	-0.12
407.8	243.92	244.09	-0.17	-0.07

temp, K	saturated vapor densities, kg/m <sup>3</sup>			diff, %
	Goodwin	scaled	diff	
404.0	143.24	140.64	2.60	1.85
404.5	147.10	144.63	2.47	1.71
405.0	151.35	149.01	2.34	1.57
405.5	156.11	153.92	2.19	1.43
406.0	161.56	159.54	2.02	1.27
406.5	168.06	166.25	1.81	1.09
407.0	176.34	174.86	1.48	0.85
407.5	188.82	188.04	0.78	0.42
407.8	205.84	206.98	-1.14	-0.55

**Table II**

Critical Parameters	
$T_c = 407.84 \text{ K}^a$	$P_c = 3.6290 \text{ MPa}^b$
$\rho_c = 225.5 \text{ kg/m}^3 \text{ }^{a,b}$	
Critical Exponents	
$\beta = 0.325^c$	$\Delta_1 = 0.50^c$
$\delta = 4.82^c$	
Parameters in Scaling Functions	
$a = 22.0163^b$	$c = -0.0096833^b$
$k_0 = 1.19385^b$	$b^2 = 1.3757^d$
$k_1 = 0.50552^b$	
Pressure Background Parameters	
$\tilde{P}_1 = 5.8858^b$	$\tilde{P}_3 = 0^b$
$\tilde{P}_2 = -22.0805^b$	$\tilde{P}_{11} = -0.068209^e$
Thermal Background Parameters	
$\tilde{\mu}_c = -4.9535^f$	$\tilde{\mu}_2 = -32.2295^g$
$\tilde{\mu}_1 = -21.6912^f$	$\tilde{\mu}_3 = -33.5271^g$

<sup>a</sup> From direct determination. <sup>b</sup> From fit to PVT data. <sup>c</sup> Fixed from theory. <sup>d</sup> Same as for  $H_2O$  and  $D_2O$ . <sup>e</sup> From the slope of the coexistence curve diameter. <sup>f</sup> From identification of our surface with that of Waxman et al. at  $T = 438 \text{ K}$  and  $\rho = 205 \text{ kg/m}^3$ . <sup>g</sup> From matching our  $C_v$  with that of Waxman et al. in the range shown in Figure 1.

become as much as 8% in the range where both equations claim validity (Figure 1).

Next, with both  $\tilde{\mu}_2$  and  $\tilde{\mu}_3$  adjustable, we found

$$\begin{aligned}\tilde{\mu}_2 &= -32.230 \pm 0.111 \\ \tilde{\mu}_3 &= -33.527 \pm 0.665\end{aligned}\quad (12)$$

With these parameter values the differences in  $C_v$  are less than 1% throughout the above range. We therefore conclude that the presence of the parameter  $\tilde{\mu}_3$  in the thermal background improves our surface significantly, and we adopt the values for the parameters  $\tilde{\mu}_2$  and  $\tilde{\mu}_3$  as specified in eq 12. In Figure 4 we show the regions where compressibility  $K_T$  and specific heats  $C_v$  and  $C_p$  of our equation agree with those of Waxman et al. to better than 1%.

In order to complete our equation we need to adopt values for  $\tilde{\mu}_c$  and  $\tilde{\mu}_1$  which are related to the zero points of entropy and energy. We determine these zero-point constants by

Table III

	temp, K	$P_{\text{exptl}}$ , MPa	$P_{\text{calcd}}$ , MPa	$P_{\text{exptl}} - P_{\text{calcd}}$ , MPa
1	298.15	0.3500	0.3501	-0.0001
2	303.15	0.4043	0.4041	0.0002
3	308.15	0.4641	0.4640	0.0001
4	313.15	0.5304	0.5304	0.0000
5	318.15	0.6032	0.6036	-0.0004
6	323.15	0.6836	0.6840	-0.0004
7	328.15	0.7725	0.7720	0.0005
8	333.15	0.8683	0.8682	0.0001
9	333.15	0.8676	0.8682	-0.0006
10	343.15	1.0867	1.0866	0.0001
11	353.15	1.3432	1.3429	0.0003
12	363.15	1.6408	1.6411	-0.0003
13	373.15	1.9855	1.9859	-0.0004
14	383.15	2.3819	2.3821	-0.0002
15	393.15	2.8361	2.8362	-0.0001
16	398.15	3.0879	3.0875	0.0004

identifying the energy and entropy of our surface at  $T = 438$  K and  $\rho = 205 \text{ kg/m}^3$  with the energy and entropy of the global equation of Waxman and co-workers. At this point the difference in pressures calculated from our equation and from that of Waxman et al. is 0.009%, the difference in specific heat at constant volume is 0.07%, the difference in specific heat at constant pressure is 0.1%, and the difference in compressibility is 0.07%. The condition that the values of the energy and entropy coincide with those calculated from the global surface of Waxman et al. at this point yields

$$\bar{\mu}_c = -4.953$$

$$\bar{\mu}_1 = -21.691 \quad (13)$$

The reference points of enthalpy and entropy of that correlation are the liquid at the normal boiling point as defined by the surface ( $T = 261.395$  K for  $P = 0.101325$  MPa). This completes the determination of the parameters. A complete listing

Table IV. Coexisting Phase Properties

temp, K	press., MPa	density, kg/m <sup>3</sup>	latent heat, kJ/kg	internal energy, kJ/kg	enthalpy, kJ/kg	entropy, kJ/(kg K)	$c_v$ , kJ/(kg K)	$c_p$ , kJ/(kg K)	velocity of sound, m/s
Liquid									
406.00	3.5186	293.61	68.50	413.9	425.9	1.2407	2.432	19.98	124.8
406.10	3.5245	292.27	67.11	414.7	426.7	1.2426	2.441	21.07	123.6
406.20	3.5304	290.87	65.67	415.4	427.5	1.2446	2.451	22.31	122.4
406.30	3.5363	289.43	64.17	416.2	428.4	1.2466	2.461	23.72	121.2
406.40	3.5423	287.92	62.62	416.9	429.2	1.2487	2.472	25.34	119.9
406.50	3.5482	286.36	61.01	417.7	430.1	1.2508	2.484	27.24	118.6
406.60	3.5542	284.72	59.32	418.6	431.1	1.2530	2.497	29.47	117.3
406.70	3.5601	283.00	57.55	419.4	432.0	1.2553	2.511	32.13	116.0
406.80	3.5661	281.18	55.69	420.3	433.0	1.2577	2.527	35.36	114.6
406.90	3.5721	279.25	53.72	421.3	434.0	1.2602	2.545	39.36	113.2
407.00	3.5781	277.19	51.61	422.2	435.1	1.2629	2.565	44.42	111.7
407.10	3.5841	274.97	49.35	423.3	436.3	1.2657	2.587	51.02	110.1
407.20	3.5901	272.56	46.90	424.4	437.6	1.2687	2.614	59.94	108.5
407.30	3.5962	269.89	44.19	425.6	438.9	1.2720	2.646	72.61	106.8
407.40	3.6022	266.90	41.16	426.9	440.4	1.2756	2.685	91.87	105.0
407.50	3.6083	263.43	37.65	428.4	442.1	1.2797	2.736	124.21	103.0
407.60	3.6144	259.22	33.42	430.2	444.2	1.2846	2.809	188.17	100.7
407.70	3.6205	253.65	27.84	432.5	446.8	1.2910	2.928	362.66	97.8
407.80	3.6266	244.09	18.33	436.3	451.2	1.3018	3.241	1726.56	92.6
407.84	3.6290	225.50	0.00	443.8	459.9	1.3231			0.0
Vapor									
405.00	3.4602	149.01	80.56	476.1	499.3	1.4224	2.507	20.62	120.1
405.10	3.4660	149.95	79.47	475.8	498.9	1.4213	2.513	21.35	119.9
405.20	3.4718	150.90	78.37	475.5	498.5	1.4201	2.520	22.14	119.6
405.30	3.4776	151.88	77.23	475.1	498.0	1.4189	2.527	22.99	119.4
405.40	3.4834	152.88	76.08	474.8	497.6	1.4177	2.534	23.92	119.1
405.50	3.4893	153.91	74.89	474.4	497.1	1.4164	2.542	24.94	118.8
405.60	3.4951	154.97	73.68	474.0	496.6	1.4151	2.550	26.05	118.6
405.70	3.5010	156.06	72.44	473.6	496.1	1.4138	2.558	27.28	118.3
405.80	3.5068	157.18	71.16	473.2	495.6	1.4124	2.567	28.63	118.0
405.90	3.5127	158.34	69.85	472.8	495.0	1.4109	2.576	30.13	117.7
406.00	3.5186	159.54	68.50	472.4	494.4	1.4094	2.585	31.80	117.4
406.10	3.5245	160.78	67.11	471.9	493.8	1.4079	2.595	33.69	117.1
406.20	3.5304	162.06	65.67	471.4	493.2	1.4062	2.606	35.82	116.8
406.30	3.5363	163.40	64.17	470.9	492.6	1.4045	2.617	38.24	116.4
406.40	3.5423	164.79	62.62	470.4	491.9	1.4028	2.630	41.03	116.1
406.50	3.5482	166.25	61.01	469.8	491.1	1.4009	2.643	44.27	115.7
406.60	3.5542	167.78	59.32	469.2	490.4	1.3989	2.657	48.06	115.3
406.70	3.5601	169.39	57.55	468.5	489.6	1.3968	2.672	52.58	114.9
406.80	3.5661	171.10	55.69	467.9	488.7	1.3946	2.689	58.03	114.4
406.90	3.5721	172.92	53.72	467.1	487.8	1.3922	2.708	64.74	114.0
407.00	3.5781	174.86	51.61	466.3	486.8	1.3897	2.729	73.18	113.4
407.10	3.5841	176.96	49.35	465.4	485.7	1.3869	2.753	84.09	112.8
407.20	3.5901	179.26	46.90	464.4	484.5	1.3839	2.780	98.72	112.1
407.30	3.5962	181.81	44.19	463.3	483.1	1.3805	2.813	119.26	111.3
407.40	3.6022	184.69	41.16	462.1	481.6	1.3766	2.853	150.03	110.4
407.50	3.6083	188.04	37.65	460.6	479.8	1.3721	2.905	200.80	109.2
407.60	3.6144	192.12	33.42	458.8	477.6	1.3666	2.977	298.76	107.5
407.70	3.6205	197.55	27.84	456.3	474.6	1.3593	3.094	556.28	105.0
407.80	3.6266	206.98	18.33	452.0	469.5	1.3467	3.396	2416.05	99.0
407.84	3.6290	225.50	0.00	443.8	459.9	1.3231			0.0



## Appendix A

**Revised and Extended Scaling Equations for the Thermodynamic Properties of Fluids.****Reduced Thermodynamic Quantities:**

$$\begin{aligned}\bar{T} &= -\frac{T_c}{T} & \bar{\mu} &= \frac{\mu}{T} \frac{\rho_c T_c}{P_c} & \bar{P} &= \frac{P}{T} \frac{T_c}{P_c} \\ \bar{\rho} &= \frac{\rho}{\rho_c} & \bar{U} &= \frac{U}{V} \frac{1}{P_c} & \bar{S} &= \frac{S}{V} \frac{T_c}{P_c} \\ \bar{A} &= \frac{A}{VT} \frac{T_c}{P_c} & \bar{H} &= \frac{H}{VT} \frac{T_c}{P_c} & \bar{\chi}_T &= \left( \frac{\partial \bar{p}}{\partial \bar{\mu}} \right) \\ \bar{C}_v &= \frac{C_v}{V} \frac{T_c}{P_c} & \bar{C}_p &= \frac{C_p}{V} \frac{T_c}{P_c}\end{aligned}\quad (\text{A.1})$$

( $T$  is temperature,  $\mu$  is chemical potential,  $P$  is pressure,  $\rho$  is density,  $U$  is energy,  $S$  is entropy,  $A$  is Helmholtz free energy,  $H$  is enthalpy,  $V$  is volume,  $C_v$  is heat capacity at constant  $V$ ,  $C_p$  is heat capacity at constant  $P$ ).

**Thermodynamic Relations:**

$$\begin{aligned}d\bar{P} &= \bar{U} d\bar{T} + \bar{p} d\bar{\mu} \\ d\bar{A} &= -\bar{U} d\bar{T} + \bar{\mu} d\bar{p} \\ d\bar{H} &= -\bar{T} d\bar{U} + \bar{p} d\bar{\mu} \\ d\bar{S} &= -\bar{T} d\bar{U} - \bar{\mu} d\bar{p}\end{aligned}\quad (\text{A.2})$$

with

$$\begin{aligned}\bar{A} &= \bar{p}\bar{\mu} - \bar{P} \\ \bar{H} &= \bar{P} - \bar{T}\bar{U} \\ \bar{S} &= \bar{H} - \bar{p}\bar{\mu} = -\bar{T}\bar{U} - \bar{A}\end{aligned}\quad (\text{A.3})$$

**Fundamental Equations:**

$$\Delta\bar{T} = \bar{T} + 1 \quad (\text{A.4a})$$

$$\Delta\bar{\mu} = \bar{\mu} - \bar{\mu}_0(\bar{T}) \quad (\text{A.4b})$$

$$\bar{P} = \bar{P}_0(\bar{T}) + \Delta\bar{\mu} + \bar{P}_{11}\Delta\bar{\mu}\Delta\bar{T} + \Delta\bar{P} \quad (\text{A.5})$$

with

$$\bar{\mu}_0(\bar{T}) = \bar{\mu}_c + \sum_{j=1}^3 \bar{\mu}_j(\Delta\bar{T})^j \quad (\text{A.6a})$$

$$\bar{P}_0(\bar{T}) = 1 + \sum_{j=1}^3 \bar{P}_j(\Delta\bar{T})^j \quad (\text{A.6b})$$

**Derived Thermodynamic Quantities:**

$$\bar{p} = 1 + \bar{P}_{11}\Delta\bar{T} + (\partial\Delta\bar{P}/\partial\Delta\bar{\mu})_{\Delta\bar{T}} \quad (\text{A.7})$$

$$\bar{U} = \frac{d\bar{P}_0}{d\bar{T}} - \bar{p} \frac{d\bar{\mu}_0}{d\bar{T}} + \bar{P}_{11}\Delta\bar{\mu} + \left( \frac{\partial\Delta\bar{P}}{\partial\Delta\bar{T}} \right)_{\Delta\bar{\mu}} \quad (\text{A.8})$$

$$\bar{\chi}_T = (\partial^2\Delta\bar{P}/\partial\Delta\bar{\mu}^2)_{\Delta\bar{T}} \quad (\text{A.9})$$

$$\left( \frac{\partial\bar{P}}{\partial\bar{T}} \right)_{\bar{p}} =$$

$$\frac{d\bar{P}_0}{d\bar{T}} + \bar{P}_{11} \left[ \Delta\bar{\mu} - \frac{\bar{p}}{\bar{\chi}_T} \right] + \left( \frac{\partial\Delta\bar{P}}{\partial\Delta\bar{T}} \right)_{\Delta\bar{\mu}} - \frac{\bar{p}}{\bar{\chi}_T} \frac{\partial^2\Delta\bar{P}}{\partial\Delta\bar{\mu} \partial\Delta\bar{T}} \quad (\text{A.10})$$

$$\begin{aligned}\frac{\bar{C}_v}{\bar{T}^2} &= \frac{d^2\bar{P}_0}{d\bar{T}^2} - \bar{p} \frac{d^2\bar{\mu}_0}{d\bar{T}^2} - \frac{\bar{P}_{11}^2}{\bar{\chi}_T} + \left( \frac{\partial^2\Delta\bar{P}}{\partial\Delta\bar{T}^2} \right)_{\Delta\bar{\mu}} - \\ &\quad \frac{2\bar{P}_{11}}{\bar{\chi}_T} \frac{\partial^2\Delta\bar{P}}{\partial\Delta\bar{\mu} \partial\Delta\bar{T}} - \frac{1}{\bar{\chi}_T} \left( \frac{\partial^2\Delta\bar{P}}{\partial\Delta\bar{\mu} \partial\Delta\bar{T}} \right)^2\end{aligned}\quad (\text{A.11})$$

$$\bar{C}_p = \bar{C}_v + \frac{\bar{\chi}_T}{\bar{\rho}^2} \left[ \bar{P} - \bar{T} \left( \frac{\partial\bar{P}}{\partial\bar{T}} \right)_{\bar{p}} \right]^2 \quad (\text{A.12})$$

**Critical Exponents:**

$$\begin{aligned}\alpha_0 &= \alpha & \alpha_1 &= \alpha - \Delta_1 \\ \beta_0 &= \beta & \beta_1 &= \beta + \Delta_1 \\ \gamma_0 &= \gamma & \gamma_1 &= \gamma - \Delta_1\end{aligned}\quad (\text{A.13})$$

with

$$2 - \alpha = \beta(\delta + 1) \quad \gamma = \beta(\delta - 1) \quad (\text{A.14})$$

**Parametric Equations for Singular Terms:**

$$\Delta\bar{\mu} = r^{\beta\delta} a \theta(1 - \theta^2) \quad (\text{A.15})$$

$$\Delta\bar{T} = r(1 - b^2\theta^2) - c \Delta\bar{\mu} \quad (\text{A.16})$$

$$\Delta\bar{P} = \sum_{i=0}^1 r^{2-\alpha_i} a_i k_i p_i(\theta) \quad (\text{A.17})$$

$$(\partial\Delta\bar{P}/\partial\Delta\bar{\mu})_{\Delta\bar{T}} = \sum_{i=0}^1 [r^{\beta_i} k_i \theta + cr^{1-\alpha_i} a_i k_i s_i(\theta)] \quad (\text{A.18})$$

$$(\partial\Delta\bar{P}/\partial\Delta\bar{T})_{\Delta\bar{\mu}} = \sum_{i=0}^1 r^{1-\alpha_i} a_i k_i s_i(\theta) \quad (\text{A.19})$$

$$(\partial^2\Delta\bar{P}/\partial\Delta\bar{\mu}^2)_{\Delta\bar{T}} =$$

$$\sum_{i=0}^1 \left[ r^{-\gamma_i} \frac{k_i}{a} u_i(\theta) + 2cr^{\beta_i-1} k_i v_i(\theta) + c^2 r^{-\alpha_i} a_i k_i w_i(\theta) \right] \quad (\text{A.20})$$

$$\frac{\partial^2\Delta\bar{P}}{\partial\Delta\bar{\mu} \partial\Delta\bar{T}} = \sum_{i=0}^1 [r^{\beta_i-1} k_i v_i(\theta) + cr^{-\alpha_i} a_i k_i w_i(\theta)] \quad (\text{A.21})$$

$$(\partial^2\Delta\bar{P}/\partial\Delta\bar{T}^2)_{\Delta\bar{\mu}} = \sum_{i=0}^1 r^{-\alpha_i} a_i k_i w_i(\theta) \quad (\text{A.22})$$

**Auxiliary Functions:**

$$p_i(\theta) = p_{0i} + p_{2i}\theta^2 + p_{4i}\theta^4 \quad (\text{A.23})$$

$$s_i(\theta) = s_{0i} + s_{2i}\theta^2 \quad s'_i(\theta) = 2s_{2i}\theta \quad (\text{A.24})$$

$$q(\theta) = 1 + \{b^2(2\beta\delta - 1) - 3\}\theta^2 - b^2(2\beta\delta - 3)\theta^4 \quad (\text{A.25})$$

$$u_i(\theta) = [1 - b^2(1 - 2\beta_i)\theta^2]/q(\theta) \quad (\text{A.26})$$

$$v_i(\theta) = [\beta_i(1 - 3\theta^2)\theta - \beta\delta(1 - \theta^2)\theta]/q(\theta) \quad (\text{A.27})$$

$$w_i(\theta) = [(1 - \alpha_i)(1 - 3\theta^2)s_i(\theta) - \beta\delta(1 - \theta^2)\theta s'_i(\theta)]/q(\theta) \quad (\text{A.28})$$

with

$$p_{0i} = + \frac{\beta\delta - 3\beta_i - b^2\alpha_i\gamma_i}{2b^4(2 - \alpha_i)(1 - \alpha_i)\alpha_i}$$

$$p_{2i} = - \frac{\beta\delta - 3\beta_i - b^2\alpha_i(2\beta\delta - 1)}{2b^2(1 - \alpha_i)\alpha_i}$$

$$p_{4i} = + \frac{2\beta\delta - 3}{2\alpha_i} \quad (\text{A.29})$$

$$s_{0i} = (2 - \alpha_i)p_{0i}$$

$$s_{2i} = - \frac{\beta\delta - 3\beta_i}{2b^2\alpha_i} \quad (\text{A.30})$$

**Two-Phase Properties:**

variables

$$\begin{aligned}\theta &= \pm 1 \\ \Delta\bar{\mu} &= 0 \\ \Delta\bar{T} &= r(1 - b^2)\end{aligned}\quad (\text{A.31})$$

vapor pressure

$$\bar{P}_{\text{vap}} = \bar{P}_0(\bar{T}) + \sum_{i=0}^1 r^{2-\alpha_i} a_i k_i p_i(1) \quad (\text{A.32})$$

coexisting densities

$$\begin{aligned}(\bar{\rho}_L + \bar{\rho}_V)/2 &= 1 + \bar{P}_{11}\Delta\bar{T} + \sum_{i=0}^1 cr^{1-\alpha_i} a_i k_i p_i(1) \\ (\bar{\rho}_L - \bar{\rho}_V)/2 &= \sum_{i=0}^1 r^{\beta} k_i\end{aligned}\quad (\text{A.33})$$

Helmholtz free energy

$$\bar{A} = \bar{\rho}\bar{\mu}_0(\bar{T}) - \bar{P}_0(\bar{T}) - \sum_{i=0}^1 r^{2-\alpha_i} a_i k_i p_i(1) \quad (\text{A.34})$$

energy

$$\bar{U} = \frac{d\bar{P}_0}{d\bar{T}} - \bar{\rho} \frac{d\bar{\mu}_0(\bar{T})}{d\bar{T}} + \frac{1}{1-b^2} \sum_{i=0}^1 (2-\alpha_i) r^{1-\alpha_i} a_i k_i p_i(1) \quad (\text{A.35})$$

entropy

$$\begin{aligned}\bar{S} &= -\bar{\rho}\bar{\mu}_0(\bar{T}) + \bar{P}_0(\bar{T}) - \bar{T} \left[ \frac{d\bar{P}_0}{d\bar{T}} - \bar{\rho} \frac{d\bar{\mu}_0}{d\bar{T}} \right] + \\ &\sum_{i=0}^1 r^{2-\alpha_i} a_i k_i p_i(1) - \frac{\bar{T}}{1-b^2} \sum_{i=0}^1 (2-\alpha_i) r^{1-\alpha_i} a_i k_i p_i(1)\end{aligned}\quad (\text{A.36})$$

specific heat  $C_v$ 

$$\begin{aligned}\frac{\bar{C}_v}{\bar{T}^2} &= \\ \frac{d^2\bar{P}_0}{d\bar{T}^2} - \bar{\rho} \frac{d^2\bar{\mu}_0}{d\bar{T}^2} &+ \left( \frac{1}{1-b^2} \right)^2 \sum_{i=0}^1 (2-\alpha_i)(1-\alpha_i) r^{-\alpha_i} a_i k_i p_i(1)\end{aligned}\quad (\text{A.37})$$

## Appendix B

Parameter values are listed in Table II.

## Appendix C

**Vapor Pressure of Isobutane.** The vapor pressure data of Waxman (5) in the range 298–398 K were fitted to the simple scaled equation

$$P^* = 1 + A_1 \Delta T^* + A_2 (\Delta T^*)^{2-\alpha} + A_3 (\Delta T^*)^2 + A_4 (\Delta T^*)^3 \quad (\text{C.1})$$

where  $P^* = P/P_c$ ,  $\Delta T^* = (T_c - T)/T_c$  and the critical exponent  $\alpha = 0.1085$ . Choosing  $T_c = 407.84$  K,  $P_c = 3.6290$  MPa, we obtain  $A_1 = -6.8038$ ,  $A_2 = 21.5688$ ,  $A_3 = -10.1751$ ,  $A_4 = -7.0260$  and the deviations listed in Table III.

This fit corresponds with a value of  $\bar{P}_1$  of 5.8038. Retaining the form of the vapor pressure equation, eq C.1 and the choice of  $T_c$ , we can obtain higher values of  $\bar{P}_1$  only by raising  $P_c$ . We would have to raise  $P_c$  by as much as 0.07 MPa to obtain a value  $\bar{P}_1 = 5.88$  consistent with Beattie's PVT data. This choice of  $P_c$ , however, would be quite inconsistent with Beat-

tie's and Waxman's supercritical PVT data.

## Appendix D

**Tables of Thermodynamic Properties.** In Table IV we list the values of the thermodynamic properties of isobutane along the coexistence curve on the liquid and vapor sides as a function of temperature. In Table V we have tabulated the thermodynamic properties along isotherms at regular density increments.

## Appendix E

**Measurement of the Critical Density and Temperature of Isobutane.** The critical temperature and density of isobutane were determined by observation of the disappearance of the meniscus in the center of an optical cell. The cell was formed by clamping a 316 stainless-steel ring of i.d. 25.4 mm, o.d. 35 mm, and thickness 12.7 mm between two sapphire disks of o.d. 35 mm and thickness 6 mm, with tin foil of 0.025-mm thickness serving as a gasket. A steel capillary with an o.d. of 1.6 mm was welded into the steel ring and connected to a pressure valve. The volume of the cell was calculated from its dimensions to be 6.448 cm<sup>3</sup> at room temperature. The cell volume was corrected for the volume of the line and valve (+0.022 cm<sup>3</sup>) and that of a small magnetic bar (-0.123 cm<sup>3</sup>) which was used as a stirrer. The volume of the cell at higher temperatures was calculated by using the value  $16.5 \times 10^{-6}$ /K for the average coefficient of linear thermal expansion of the steel ring for temperatures between room temperature and 408 K.

The cell was filled with a sample of isobutane from the same research-grade supply used by Waxman for his PVT measurements (6) and certified by the supplier to be at least 99.9% pure. The amount of isobutane was determined by weighing the cell before and after filling it and was chosen such that the density exceeded the critical density by about 8%. The weighings were done on an analytical balance with a precision to within 0.5 mg.

The cell assembly was immersed in a commercial regulated bath which was provided with windows and filled with high-viscosity silicone oil. The temperature was controlled to  $\pm 0.01$  K and measured by a platinum resistance thermometer and a 7-decade Mueller bridge. The resistance thermometer had been calibrated at NBS and its indication at the water triple point was monitored during the experiments.

The bath was heated and the meniscus was observed to disappear at the top of the cell. Small amounts of isobutane were subsequently released and trapped above water inside an inverted graduated glass. An account was kept of the amounts of isobutane released (in 15 steps, from 8% above to 8% below the critical density). The critical temperature and density were taken as those corresponding to the case where the meniscus disappeared in the center of the cell. At the end of the experiments the cell was weighed again. The weight loss was found to be 230 mg—it differed from the loss calculated from the volumes released by 15 mg. Since the weight of the critical sample was 1.435 g, we estimate it to be known to better than 15 mg or 1%.

For the seven different fill densities at which the meniscus disappeared at some level inside the cell, the measured temperatures of meniscus disappearance varied from 407.83 to 407.85 K.

Thus, we conclude that  $T_c = 407.84 \pm 0.02$  K and  $\rho_c = 225.5 \pm 2$  kg/m<sup>3</sup>.

### Thermodynamic Properties

$P$	pressure
$P_c$	critical pressure
$T$	temperature
$T_c$	critical temperature



$V$	volume
$V_c$	critical volume
$\rho$	density
$\rho_c$	critical density
$\mu$	chemical potential
$A$	Helmholtz free energy
$H$	enthalpy
$U$	energy
$S$	entropy
$K_T$	isothermal compressibility
$C_p$	specific heat at constant pressure
$C_v$	specific heat at constant volume
$M$	molecular weight, $M = 0.0581243$ kg/mol
$R$	gas constant, $R = 143.045$ J/(kg K)
$\sigma_p$	experimental error in the pressure
$\sigma_T$	experimental error in the temperature
$\sigma_\rho$	experimental error in the density

**Reduced Thermodynamic Properties**

$\tilde{P}$	reduced pressure, $PT_c/(P_cT)$
$\Delta\tilde{P}$	singular part of $\tilde{P}$
$\tilde{T}$	reduced temperature, $-T_c/T$
$\Delta\tilde{T}$	$\tilde{T} + 1$
$\tilde{\rho}$	reduced density, $\rho/\rho_c$
$\tilde{\mu}$	reduced chemical potential, $\mu\rho_cT_c/(P_cT)$
$\tilde{\mu}_0(\tilde{T})$	chemical potential on the saturation curve and its analytic continuation
$\Delta\tilde{\mu}$	$\tilde{\mu} - \tilde{\mu}_0(\tilde{T})$
$\tilde{A}$	reduced Helmholtz free energy density, $AT_c/(VTP_c)$
$\tilde{H}$	reduced enthalpy density, $HT_c/(VTP_c)$
$\tilde{U}$	reduced energy density, $U/(VP_c)$
$\tilde{S}$	reduced entropy density, $ST_c/(VP_c)$
$\tilde{\chi}_T$	reduced susceptibility, $K_TV_c^2P_cT/(V^2T_c)$
$\tilde{C}_p$	reduced specific heat density, $C_pT_c/(VP_c)$
$\tilde{C}_v$	reduced specific heat density $C_vT_c/(VP_c)$

**Critical Exponents**

$\alpha \equiv \alpha_0$	critical exponent for the specific heat
$\beta \equiv \beta_0$	critical exponent for the coexistence curve
$\gamma \equiv \gamma_0$	critical exponent for the compressibility
$\delta$	critical exponent for the critical isotherm
$\Delta_1$	gap exponent for first Wegner correction
$\alpha_1$	$\alpha_0 - \Delta_1$
$\beta_1$	$\beta_0 + \Delta_1$
$\gamma_1$	$\gamma_0 - \Delta_1$

**Parametric Scaled Equation**

$r$	parametric distance variable
$\theta$	parametric contour variable
$a, k_0,$ $k_1, c,$ $b^2$	constants in scaled equation

$\tilde{P}_0(\tilde{T})$	analytic part of the vapor pressure equation
$\tilde{P}_1, \tilde{P}_2,$ $\tilde{P}_3$	coefficients of $\tilde{P}_0(\tilde{T})$ written as a polynomial in $\tilde{T}$
$\tilde{P}_{11}$	coefficient of the term $(\Delta\tilde{\mu})(\Delta\tilde{T})$ in the expression for $\tilde{P}$
$\mu_1, \mu_2,$ $\mu_3$	coefficients of $\tilde{\mu}_0(\tilde{T})$ as a polynomial in $\tilde{T}$
$p_i(\theta),$ $s_i(\theta),$ $q_i(\theta)$	polynomials in $\theta$ , $i = 0, 1$
$u_i(\theta),$ $v_i(\theta),$ $w_i(\theta)$	ratios of polynomials in $\theta$ , $i = 0, 1$
$p_{0i}, p_{2i},$ $p_{4i}$	coefficients of the polynomials $p_i(\theta)$
$s_{0i}, s_{2i}$	coefficients of the polynomials $s_i(\theta)$

Registry No. Isobutane, 75-28-5.

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