| $a$ | helght of the observation cell, m |
| :--- | :--- |
| $A$ | constant in the Arrhenius law, $\mathrm{m}^{2} \mathrm{~s}^{-1}$ |
| $D$ | diffusion coefficient, $\mathrm{m}^{2} \mathrm{~s}^{-1}$ |
| $e$ | optical path length, m |
| $E$ | activation energy (Arrhenius law), $\mathrm{J} \mathrm{mol}{ }^{-1}$ |
| $k$ | constant in eq 2 |
| $n$ | refractlve index |
| $N$ | number of fringes |
| $R$ | Ideal gas constant, $\mathrm{J} \mathrm{K}^{-1} \mathrm{~mol}^{-1}$ |
| $t$ | time, s |
| $T$ | temperature, K |
| $x$ | mass ratlo of the solution, kg of solute/kg of water |
| $x^{\prime}$ | mass fraction of solute, $\mathrm{kg} \mathrm{of} \mathrm{solute/kg} \mathrm{of} \mathrm{solution}$ |
| $\lambda$ | wavelength of laser light, m |
| $\theta$ | temperature, ${ }^{\circ} \mathrm{C}$ |

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# Vapor Pressure Measurement of Tetralin at Reduced Pressures 

Hirotake Katayama* and Yasuhiro Harada<br>Chemical Laboratory, College of Engineering, Hosel Universty, Koganei, Tokyo, Japan


#### Abstract

The vapor pressure of Tetralin was measured over the pressure range of $0.40-32.5 \mathrm{kPa}, \mathrm{l.e}$. , the temperature range of $330.80-437.13 \mathrm{~K}$. The results were fitted to Chebyshev polynomials and the Miller and Antolne equations, the percent root mean square deviations of which were estimated as $0.22,0.29$, and 0.33 , respectively.


## Introduction

To measure vapor-liquid equilibrium and vapor pressure at reduced pressure, we constructed a new equilibrium still. In this work the vapor pressure of Tetralin (1,2,3,4-tetrahydronaphthalene) has been measured at $0.40-32.5 \mathrm{kPa}$, because there have been only a few data on the vapor pressure at reduced pressures: the six values by Herz and Schuftan (1) in 1922, the three by Linder (2) in 1931, the three by Lagrange et al. (3) in 1971, the four by Nasir et al. (4) in 1980, and the four by Katayama and Watanabe (5) in 1980. Some of these are not precise.

Recently Tetralin has been employed as a reagent for the liquefaction of coal.

## Experimental Section

Material. Commerclal-grade Tetralln was distllled in a wetted wall column with $1-\mathrm{m}$ length and $10-\mathrm{mm}$ i.d. at 1.3 kPa . The intermedlate distillate used for this work was monitored by measuring the change in the refractive indexes of each $10-\mathrm{mL}$ distillate.

The purity of the Tetralin was estimated to be $99.8 \%$ by gas chromatography with Porapak-s as described in the previous paper (5). The refractive index and the density of the Tetralln at $25.0^{\circ} \mathrm{C}$ have already been determined previously (5) as 1.5383, compared with the literature value 1.53919 (6), and $963.6 \mathrm{~kg} / \mathrm{m}^{3}$, compared with the literature value $963.24 \mathrm{~kg} / \mathrm{m}^{3}$ (7).

Apparatus and Procedure. The experimental apparatus was set up as in Figure 1. The equillbrium still is made of Pyrex
glass, and its cylinder is 400 mm high with a $70-\mathrm{mm}$ i.d. The funnel of the Cottrell pump does not entirely cover the liquid surface so that discharged vapor can ascend not only through the Cottrell tube but also from the outside of the funnel. The still is designed to decrease the pressure drop between the surface and the condenser sections.
The measurement and the control of pressure were carried out with a Mult-Range Model 157/100 pressure standard from Texas Instruments Inc. Its accuracy is $\pm 0.002 \mathrm{kPa}$ for the $35-10-\mathrm{kPa}$ range and $\pm 0.001 \mathrm{kPa}$ for the $10-0.40-\mathrm{kPa}$ range. The accuracy of pressure control on operation was found to be within $\pm 0.00003 \mathrm{kPa}$ for the $35-1-\mathrm{kPa}$ range, and within $\pm 0.0004 \mathrm{kPa}$ for the $1-0.40-\mathrm{kPa}$ range. Since the pressure below 0.40 kPa could not be controlled well, the vapor pressures below this pressure were not measured.
Mercury thermometers with immersion lines marked 18 cm from the bulb end, which consisted of three sets of graduation from 40 to 100,100 to 150 , and 150 to $200^{\circ} \mathrm{C}$, were used. They have been callibrated in $10^{\circ} \mathrm{C}$ intervals by Watanabe Kelki Seisakusho Co., Ltd., Tokyo. Their accuracies are within $\pm 0.04$ K.

The McLeod gage in Figure 1 was employed only when the zero counter (calibration) of the Bourdon capsule was to be determined.

About 120 mL of a sample was poured into the bottom of the still through the stopper 11. The circulation of vapor was carried out at the rate of 40 drops $/ \mathrm{min}$ for 2 h . The outside wall of the still was held at 3 K below the boiling point. Since the Tetralin is polymerized by heating as described previously (5), a fresh sample was used after every three measurements.

## Results and Discussion

The vapor pressure data of Tetralin are presented in Table I. The data are also plotted in Flgure 2 including a comparison with values from the literature. The data are in good agreement wth the literature in the pressure range between 32 and 5 kPa , but are somewhat smaller than quoted values below 5 kPa . The values of Nasir et al. (4) are larger than the others.


Floure 1. Experimental apparatus: (1) thermometer; (2) thermocouple; (3) nichrome heater; (4) asbestos; (5) Cottrell pump; (6) rotor; (7) greaseless stopper; (8) hot plate with magnettc stirrer; (9) condenser; (10) greaseless joint; (11) greaseless stopper; (12) buffer tank; (13-15) stopcocks; (16) cold trap; (17) molecular sleves; (18) pressure standard; (19) quartz Bourdon capsule.

Table I. Vapor Pressures of Tetralin

| obsd |  | $\epsilon,{ }^{a} \%$ |  |
| :---: | ---: | ---: | ---: |
| $T, \mathrm{~K}$ | $p, \mathrm{kPa}$ | Miller eq | Antoine eq |
| 437.13 | 32.500 | 0.40 | 0.12 |
| 434.41 | 30.000 | 0.16 | 0.02 |
| 431.51 | 27.500 | -0.10 | -0.12 |
| 428.48 | 25.000 | -0.62 | -0.55 |
| 425.00 | 22.500 | -0.58 | -0.43 |
| 420.94 | 20.000 | 0.31 | 0.49 |
| 416.73 | 17.500 | 0.46 | 0.65 |
| 412.28 | 15.000 | -0.26 | -0.12 |
| 406.81 | 12.500 | 0.15 | 0.22 |
| 400.56 | 10.000 | -0.04 | -0.10 |
| 392.72 | 7.500 | 0.22 | -0.01 |
| 382.42 | 5.000 | 0.06 | -0.34 |
| 366.21 | 2.500 | -0.06 | -0.40 |
| 355.27 | 1.500 | 0.00 | -0.06 |
| 347.22 | 1.000 | -0.20 | -0.04 |
| 345.20 | 0.900 | -0.19 | 0.00 |
| 342.96 | 0.800 | -0.07 | 0.14 |
| 340.53 | 0.700 | -0.25 | -0.04 |
| 339.15 | 0.650 | -0.05 | 0.13 |
| 337.63 | 0.600 | 0.44 | 0.58 |
| 336.17 | 0.550 | 0.03 | 0.10 |
| 334.45 | 0.500 | 0.41 | 0.37 |
| 332.72 | 0.450 | 0.03 | -0.17 |
| 330.80 | 0.400 | -0.25 | -0.69 |
|  |  | Miller eq | Antoine eq |
| mean dev |  | 0.22 | 0.25 |
| max dev |  | -0.62 | -0.69 |

${ }^{a} \epsilon=$ pressure deviation $=100\left(P_{\text {exptl }}-P_{\text {calca }}\right) / P_{\text {exptl }} \cdot{ }^{b} 100 \sum_{i}\left(\mid P_{\text {exptl }}\right.$ - $\left.P_{\text {calcd }} / / P_{\text {expt1 }}\right)_{i} / n$.

Chebyshev polynomials (8) and Miller (9) and Antoine equations of the following forms were used to fit the results: Chebyshev polynomials

$$
t \ln (p)=a_{0} / 2+\sum_{i=1}^{0} a F_{l}(x)
$$



Figure 2. Vapor pressures of Tetralin vs. 1/T.
where $t=T-273.15, E_{1}(x)=x, E_{2}(x)=2 x^{2}-1, E_{l}(x)=$ $2 x E_{i-1}(x)-E_{i-2}(x)$, and $x$ is a function of temperature defined as

$$
x=\frac{2 T-\left(T_{\max }+T_{\min }\right)}{T_{\max }-T_{\min }}
$$

where $T_{\max }$ and $T_{\text {min }}$ are 437.13 and 330.80 K , respectively Miller equation

$$
\ln (p)=A_{m}+B_{m} / t+C_{m} t+D_{m} t^{2}
$$

or

$$
t \ln (p)=A_{m} t+B_{m}+C_{m} t^{2}+D_{m} t^{3}
$$

Antoine equation

$$
\ln (p)=A_{\mathrm{a}}-B_{\mathrm{a}} /\left(t+C_{\mathrm{a}}\right)
$$

or

$$
t \ln (p)=A_{\mathrm{a}} t+D_{\mathrm{a}}-C_{\mathrm{a}} \ln (p)
$$

where

$$
D_{\mathrm{a}}=A_{\mathrm{a}} C_{\mathrm{a}}-B_{\mathrm{a}}
$$

All the coefficients of the expressions were decided by the fits of $t \ln (\rho)$ as written in Table II.

Table II. Constants of Chebyshev Polynomials and Miller and Antoine Equations from Least-Squares Fit of $\boldsymbol{t} \ln$ ( $\boldsymbol{p}$ )

| Chebyshev constants |  |  |  | Miller constants |  | Antoine constants |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $a_{0}$ | 443.986 | $a_{4}$ | 0.17822 | $A_{\text {m }}$ | -3.00640 | $A_{\text {a }}$ | 13.64979 |
| $a_{1}$ | 314.899 | $a_{5}$ | 0.18306 | $B_{\text {m }}$ | -48.9855 | $B_{\text {a }}$ | 3586.62 |
| $a_{2}$ | 36.795 | $a_{6}$ | 0.1374 | $C_{\text {m }}$ | $0.562848 \times 10^{-4}$ | $C_{\text {a }}$ | 188.697 |
| $a_{3}$ | -3.3684 | $a_{7}$ | 0.1920 | $D_{\text {m }}$ | $-0.910118 \times 10^{-4}$ |  |  |
| Chebyshev polynomial |  |  |  |  | Miller eq | Antoine eq |  |
| prms ${ }^{\text {a }}$ |  | 0.22 |  |  | 0.29 | 0.33 |  |

${ }^{a}$ Percent root mean square deviation defined by $100\left[\sum_{i}\left(\left(P_{\text {expt1 }}-P_{\text {calcad }}\right) / P_{\text {expt }}\right)_{i}^{2 / n}\right]^{1 / 2}$.

Table III. Temperature Difference between Experimental and Calculated Values against Vapor Pressure Using Miller and Antoine Equations

|  | $\Delta T,{ }^{a} \mathrm{~K}$ |  |
| :---: | :---: | :---: |
| $P, \mathrm{kPa}$ | Miller eq | Antoine eq |
| 32.500 | -0.14 | -0.04 |
| 30.000 | -0.06 | -0.01 |
| 27.500 | 0.03 | 0.04 |
| 25.000 | 0.21 | 0.18 |
| 22.500 | 0.19 | 0.14 |
| 20.000 | -0.10 | -0.16 |
| 17.500 | -0.14 | -0.20 |
| 15.000 | 0.08 | 0.03 |
| 12.500 | -0.04 | -0.06 |
| 10.000 | 0.01 | 0.03 |
| 7.500 | -0.06 | 0.00 |
| 5.000 | -0.01 | 0.08 |
| 2.500 | 0.01 | 0.09 |
| 1.500 | 0.00 | 0.01 |
| 1.000 | 0.04 | 0.01 |
| 0.900 | 0.04 | 0.00 |
| 0.800 | 0.01 | -0.03 |
| 0.700 | 0.05 | 0.01 |
| 0.650 | 0.01 | -0.02 |
| 0.600 | -0.08 | -0.10 |
| 0.550 | 0.00 | -0.02 |
| 0.500 | -0.07 | -0.06 |
| 0.450 | -0.01 | 0.03 |
| 0.400 | 0.04 | 0.12 |
|  | Miller eq | Antoine eq |
| mean dif ${ }^{b}$ | 0.06 | 0.06 |
| max dif, ${ }^{\text {a }} \mathrm{K}$ | 0.21 | -0.20 |

${ }^{a} T=T_{\text {expt1 }}-T_{\text {calad. }}$. ${ }^{b} \sum_{i} \mid T_{\text {oxpt1 }}-T_{\text {calcal }} / n . n:$ number of data (=24).

Since the percent root mean square deviations of pressures (prms) using Chebyshev polynomlals with the number of parameters from 3 to 10 were estimated as 2.70 at 3 parameters, 0.29 at 4 and $5,0.26$ at 6 and $7,0.22$ at $8-10$, respectlvely, here 8 parameters are selected as written in Table II. The prms of the Miller and Antoine equations are listed as 0.29 and 0.33, respectively, in Table II. Percent pressure deviations and
mean absolute deviations from the equations have also been presented in Table I.

Conversely, the temperatures were calculated by using the Milier and Antoine equations, and the differences between experimental and calculated values are shown in Table III. The mean differences of the temperatures obtained in both were equal to 0.06 K .

The Miller equation, having four constants, gave somewhat better correlations than the Antoine equation, having three constants, but the degrees of differences were very small.

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Glossary
$p$ pressure, kPa
$T$ temperature, K
$t \quad T-273.15 \mathrm{~K}$
Greek Letters
$\epsilon \quad$ percent pressure deviation ( $=100\left(P_{\text {expt }}-P_{\text {calcod }}\right)$ / $P_{\text {expt }}$ )
Reglatry No. Tetralin, 119-64-2.

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# Investigation of Vapor Pressures and Enthaipies and Entropies of Vaporization of Xanthene at Elevated Temperatures 

Alwarappa Sivaraman and RIki Kobayashl*<br>George R. Brown School of Engineering, Department of Chemical Engineering, Rice University, Houston, Texas 77251

Vapor pressures ( $6.35-817.29 \mathrm{mmHg}$ ) of xanthene, a polynuclear aromatic (three-ring) compound containing an oxygen group, over the temperature range 423-589 K, were measured. The measurements were performed in a high-temperature static apparatus. Chebyshev polynomlals have been used to tht experimental vapor pressure data. The results have been further processed to evaluate the enthalples of vaporization and compared with the predicted enthalpy values, by a recently developed generallzed correlation which incorporates the renormalization group theory with the corresponding states princlple. The entroples of vaporization were also evaluated at their respective temperatures for xanthene.

## Introduction

Vapor pressures and enthalpies and entropies of vaporization are a few of the important physical properties required in designing coal-liquid and shale oil processing and separation plants. The thermodynamic propertles are virtually unknown at high temperatures for the three-ring heavy polynuclear hydrocarbons. We reported previously $(1-3)$ the vapor pressures of various condensed aromatic compounds. In this work we continue the measurements of vapor pressures of a three-ring, oxygen-containing, coal-derived liquid, xanthene. The vapor pressures of xanthene are reported over a wide range of temperatures up to the onset of thermal decomposition. No experimental vapor pressures or enthalpies of vaporization are

