

Table III. Enthalpy of Solution of H<sub>2</sub>O in 9.93 m HCl at 40 °C

Sample wt, g	Cor temp rise, °C	-Enthalpy of soln, cal/sample	-ΔH <sub>4</sub> <sup>a</sup> , cal/mol
10.020 05	0.3551	254.4	457
11.010 88	0.3873	277.8	455
12.054 48	0.4242	305.7	456
13.021 93	0.4572	329.0	455
15.028 65	0.5268	380.1	456

<sup>a</sup> ΔH<sub>4</sub> = -458 + 0.20w, w = 13.144 93, std dev = 1, ΔH<sub>4</sub> = -455.

Table IV. Enthalpy of Solution of NH<sub>4</sub>H<sub>2</sub>PO<sub>4</sub> in 9.93 m HCl + Stoichiometric H<sub>2</sub>O at 40 °C

Sample wt, g	Cor temp rise, °C	Enthalpy of soln, cal/sample	ΔH <sub>5</sub> <sup>a</sup> , cal/mol
12.915 02	-0.8600	624.8	5565
13.310 58	-0.8879	646.3	5585
13.695 95	-0.9125	663.5	5572
14.119 04	-0.9392	684.3	5575
14.514 73	-0.9650	703.6	5576

<sup>a</sup> ΔH<sub>5</sub> = 5534 + 2.95w, w = 13.316 08, std dev = 7, ΔH<sub>5</sub> = 5573.

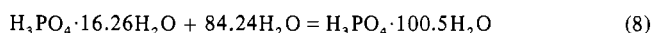
equations of the enthalpies of solution as a function of sample weight, *w*, were fitted to the observed values by the "least-squares" method. These equations were solved where *w* was the average weight of (NH<sub>4</sub>)<sub>5</sub>P<sub>3</sub>O<sub>10</sub>·H<sub>2</sub>O or the stoichiometric amount of H<sub>3</sub>PO<sub>4</sub>·16.26H<sub>2</sub>O, NH<sub>4</sub>H<sub>2</sub>PO<sub>4</sub>, or H<sub>2</sub>O corresponding to that weight. The equations along with the standard deviations and the values of ΔH<sub>2</sub>, ΔH<sub>3</sub>, ΔH<sub>4</sub>, and ΔH<sub>5</sub> for the specified values of *w* also are listed in Tables I-IV. Substitution of these calculated values of the enthalpies of solution in eq 6 gives -31 592 ± 66 cal (standard deviation) for the enthalpy of reaction 1 at 40 °C. This value was adjusted by 242 cal to give -31 350 ± 66 cal for the enthalpy of reaction 1 at 25 °C according to the equation

$$\Delta H_1(25^\circ\text{C}) = \Delta H_1(40^\circ\text{C}) + \int_{40}^{25} \Delta C_p dT \quad (7)$$

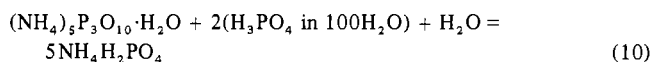
through use of polynomial equations for determining differences

between the heat capacities of the products and the reactants. The heat capacity equations were derived from the data of Osborne et al. for water (8), of Stephenson and Zettlemyer for NH<sub>4</sub>H<sub>2</sub>PO<sub>4</sub> (9), of Egan et al. for phosphoric acid solutions (2), and of Luff and Williard for (NH<sub>4</sub>)<sub>5</sub>P<sub>3</sub>O<sub>10</sub>·H<sub>2</sub>O (6).

The data of Egan and Luff (1) were used to determine ΔH<sub>8</sub> and ΔH<sub>9</sub>, the enthalpies of reactions 8 and 9 at 25 °C, as -436



and -1 cal, respectively. Subtracting twice the difference between ΔH<sub>8</sub> and ΔH<sub>9</sub> from ΔH<sub>1</sub> at 25 °C gives ΔH<sub>10</sub>, the enthalpy of reaction 10 at 25 °C, as -30 480 cal.



The standard enthalpies of formation of NH<sub>4</sub>H<sub>2</sub>PO<sub>4</sub>(c), H<sub>2</sub>O(l), and H<sub>3</sub>PO<sub>4</sub> in 100H<sub>2</sub>O are -345.38, -68.315, and -308.176 kcal/mol, respectively (7). Substituting these enthalpies of formation and the enthalpy of reaction 10 in the equation

$$\Delta H_f^\circ((\text{NH}_4)_5\text{P}_3\text{O}_{10} \cdot \text{H}_2\text{O}) = 5(\Delta H_f^\circ(\text{NH}_4\text{H}_2\text{PO}_4)) - 2(\Delta H_f^\circ(\text{H}_3\text{PO}_4 \text{ in } 100\text{H}_2\text{O})) - \Delta H_f^\circ(\text{H}_2\text{O}) - \Delta H_{10} \quad (11)$$

gives -1011.8 kcal/mol as the standard enthalpy of formation of (NH<sub>4</sub>)<sub>5</sub>P<sub>3</sub>O<sub>10</sub>·H<sub>2</sub>O.

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## Pressure-Volume-Temperature Relationships of Several Polar Liquids

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The specific volumes of liquid CCl<sub>2</sub>F<sub>2</sub>, CHClF<sub>2</sub>, CH<sub>3</sub>Cl, CH<sub>3</sub>I, CH<sub>3</sub>Br, C<sub>2</sub>H<sub>5</sub>Br, and CH<sub>3</sub>COOCH<sub>3</sub> have been measured at several temperatures from -20 to +40 °C and at pressures from the saturated vapor pressures to near 1600 atm with an accuracy better than 0.13%. The data were fitted to the Tait equation of state at each temperature with a maximum deviation of 0.2%.

An accurate knowledge of the specific volumes of polar liquids under high pressures is important in the interpretation of the polarity effect on the compressibility in connection with the elucidation of the internal structure problems of polar liquids.

Most studies of *P-V-T* relationships have been made on nonpolar liquids, and very few measurements are available on polar liquids. The purpose of the present work is, therefore, to obtain the specific volumes of polar liquids. The measurements were made at temperatures from -20 to +40 °C, and at pressures up to near 1600 atm.

#### Experimental Section

**Materials.** The origin and purity of samples are recorded as follows: CCl<sub>2</sub>F<sub>2</sub> and CHClF<sub>2</sub>, Daikin Kogyo Co., Ltd., Japan, 99.9%; CH<sub>3</sub>Cl, Matheson Gas Products, a Division of Will Ross, Inc., 99.5%; CH<sub>3</sub>I, Kokusan Kagaku Co., Ltd., Japan, 98.2%;

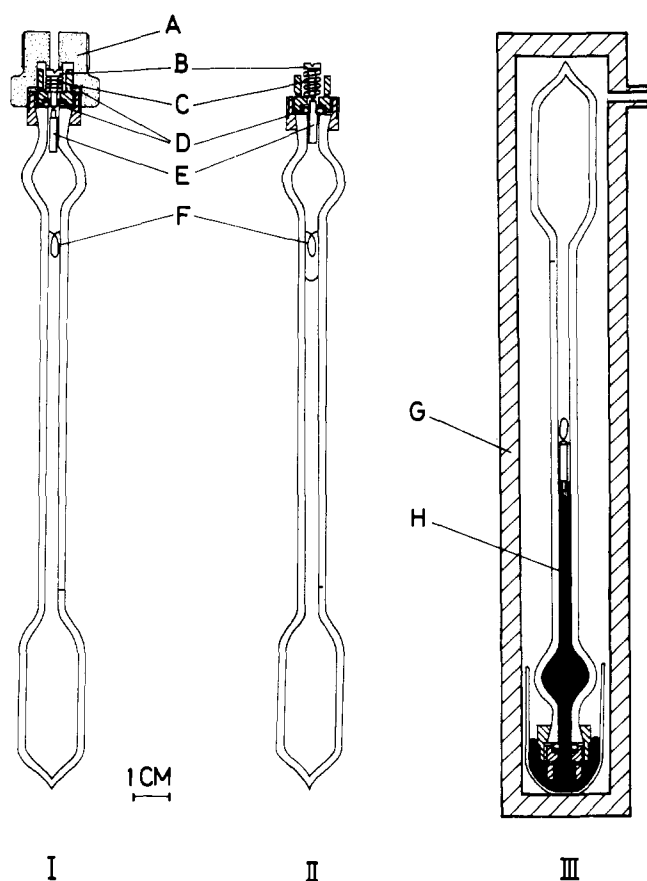
Table I. Experimental Specific Volumes

Compound	Pressure, atm	Specific volume, cm <sup>3</sup> /g				Ref of vol data	
		-20.00 °C	0.00 °C	20.00 °C	40.00 °C		
CCl <sub>2</sub> F <sub>2</sub>	(P <sub>0</sub> )	0.685 46 (1.5) <sup>a</sup>	0.715 92 (3.0) <sup>a</sup>	0.752 44 (5.6) <sup>a</sup>	0.798 02 (9.5) <sup>a</sup>	3	
	95.3			0.728 37	0.761 82		
	283.1	0.652 73	0.671 72	0.694 67	0.718 19		
	469.5	0.639 15	0.654 94	0.673 12	0.692 97		
	654.9	0.625 81	0.640 73	0.656 61	0.674 10		
	841.4	0.616 40	0.629 08	0.643 10	0.658 06		
	1027.9	0.607 75	0.619 66	0.632 67	0.645 40		
	1214.1	0.600 08	0.610 26	0.622 60	0.634 66		
	1400.5	0.592 90	0.603 50	0.614 27	0.626 08		
	1587.2	0.586 81	0.597 87	0.607 83	0.617 87		
	(P <sub>0</sub> )	0.742 74 (2.4) <sup>a</sup>	0.780 35 (4.9) <sup>a</sup>	0.826 46 (8.0) <sup>a</sup>	0.886 06 (15.1) <sup>a</sup>		8
	95.4			0.800 36	0.847 02		
	283.1	0.709 79	0.735 19	0.762 02	0.794 50		
468.6	0.693 73	0.712 86	0.736 69	0.763 25			
651.2	0.679 16	0.698 09	0.716 83	0.740 39			
836.9	0.669 00	0.686 79	0.702 69	0.722 34			
1022.4	0.658 75	0.675 96	0.690 51	0.706 68			
1206.5	0.652 13	0.664 38	0.679 53	0.695 00			
1390.7	0.643 33	0.656 13	0.669 55	0.684 24			
1574.7	0.636 38	0.649 07	0.659 98	0.673 90			
(P <sub>0</sub> )	0.99 72 (1.2) <sup>a</sup>	1.03 43 (2.5) <sup>a</sup>	1.07 75 (4.8) <sup>a</sup>	1.12 62 (8.3) <sup>a</sup>	8		
283.1	0.966 55	0.995 96	1.029 6	1.064 4			
468.6	0.950 16	0.976 24	1.004 3	1.035 2			
651.2	0.936 60	0.959 74	0.985 01	1.011 9			
836.9	0.924 42	0.945 16	0.968 27	0.992 89			
1022.4	0.913 16	0.932 97	0.954 21	0.976 60			
1206.5	0.904 79	0.922 12	0.942 26	0.962 66			
1390.7	0.894 28	0.912 06	0.931 25	0.950 14			
1574.2	0.886 42	0.903 01	0.920 64	0.939 62			
(P <sub>0</sub> )	0.417 73 (0.1) <sup>a</sup>	0.427 92 (0.2) <sup>a</sup>	0.438 44 (0.4) <sup>a</sup>	0.449 90 (0.9) <sup>a</sup>		8	
283.1	0.409 55	0.418 31	0.427 60	0.436 64			
468.6	0.405 26	0.413 30	0.421 36	0.429 96			
651.2	0.401 36	0.408 84	0.416 19	0.424 25			
836.9	0.397 78	0.404 50	0.411 92	0.418 97			
1022.4	0.394 33	0.400 91	0.407 72	0.414 17			
1206.5	0.391 27	0.397 59	0.403 77	0.410 07			
1390.7	0.388 33	0.394 22	0.400 44	0.406 40			
1574.2	0.385 69	0.391 28	0.397 24	0.402 86			
(P <sub>0</sub> )	0.560 60 (0.4) <sup>a</sup>	0.577 47 (0.9) <sup>a</sup>	0.595 92 (1.8) <sup>a</sup>	0.616 28 (3.3) <sup>a</sup>	8		
283.1	0.547 66	0.560 73	0.575 40	0.590 70			
468.6	0.540 28	0.552 70	0.565 61	0.579 49			
651.2	0.534 07	0.545 53	0.557 63	0.570 35			
836.9	0.528 48	0.538 89	0.550 01	0.561 48			
1022.4	0.523 25	0.533 01	0.543 66	0.554 01			
1206.5	0.519 00	0.527 71	0.537 77	0.547 34			
1390.7	0.514 51	0.522 74	0.532 16	0.541 33			
1574.2	0.510 57	0.518 28	0.526 49	0.535 36			
(P <sub>0</sub> )	0.648 45 (0.1) <sup>a</sup>	0.666 43 (0.2) <sup>a</sup>	0.685 23 (0.5) <sup>a</sup>	0.705 41 (1.1) <sup>a</sup>		8	
194	0.638 14	0.653 73	0.669 71	0.685 95			
388	0.629 67	0.643 82	0.657 38	0.672 95			
581	0.622 34	0.634 79	0.647 26	0.661 83			
774	0.615 88	0.627 13	0.638 50	0.651 28			
968	0.609 25	0.620 10	0.630 46	0.642 49			
1161	0.604 19	0.613 79	0.623 53	0.634 47			
1354	0.598 74	0.608 29	0.616 80	0.627 49			
1547	0.594 42	0.603 00	0.611 34	0.621 69			
(P <sub>0</sub> )	1.017 5 (0.0 <sub>3</sub> ) <sup>a</sup>	1.043 0 (0.1) <sup>a</sup>	1.072 7 (0.2) <sup>a</sup>	1.105 6 (0.5) <sup>a</sup>	8		
194	1.002 8	1.025 9	1.052 1	1.079 5			
388	0.990 1	1.011 5	1.035 0	1.060 0			
581	0.978 5	0.998 5	1.020 4	1.043 2			
774	0.968 5	0.988 0	1.008 1	1.028 2			
968	0.959 7	0.979 1	0.997 1	1.015 1			
1161	0.952 0	0.969 6	0.987 0	1.004 6			
1354	0.944 6	0.961 2	0.978 1	0.994 9			
1547	0.937 7	0.954 4	0.970 3	0.986 1			

<sup>a</sup> Saturated vapor pressure.

CH<sub>3</sub>Br and C<sub>2</sub>H<sub>5</sub>Br, Tokyo Kasei Kogyo Co., Ltd., Japan, 99.8 and 99%, respectively; CH<sub>3</sub>COOCH<sub>3</sub>, Nakarai Chemicals, Ltd., Japan, 97.0%. These samples were subjected to further purification by distillation before use, and the reagent grade mercury was purified by a modified automatic mercury washer (7).

**Apparatus and Method.** The method used in this study was similar to one presented earlier (10), but the volume changes of liquids at high pressures were measured by a modified glass piezometer as shown in Figure 1. The glass piezometer used previously had the fault that air may be introduced into the piezometer during the removal of it from a vacuum line. The



**Figure 1.** Glass piezometers: A, joint in vacuum line; B, screw; C, spring; D, O-ring; E, float; F, glass indicator; G, pressure vessel; H, mercury.

joint of this piezometer was modified for sampling in vacuo. I in Figure 1 indicates the piezometer under its connection with the vacuum line. As the piezometer filled with the liquid is removed from the line, the float (E) and the screw (B) are raised by the action of spring (C), and at last the float is tightly contacted with the O-ring (D) as shown in Figure 1, II. The specific volumes of liquids at high pressures are determined in a similar manner reported earlier after removing the screw and the spring from the float (see III in Figure 1). The saturated liquid volumes except for  $\text{CCl}_2\text{F}_2$  and  $\text{CHClF}_2$  were determined directly using the same piezometer placed in the thermostat by the usual method.

The volume data for  $\text{H}_2\text{O}$  at 25 °C and up to 1000 atm show agreement with the data of the literature (9) within the limits of accuracy of measurement (0.06%).

### Result and Discussion

The specific volumes at four temperatures, -20, 0, 20, and 40 °C, were determined from the saturated vapor pressures to near 1600 atm. The specific volumes for seven liquids are presented in Table I. The maximum deviation from the smooth curves is 0.13% over the whole range of measurements. There are sources of  $P$ - $V$ - $T$  data for  $\text{CHClF}_2$  (13),  $\text{CH}_3\text{Cl}$  (7),  $\text{CH}_3\text{I}$  (5), and  $\text{C}_2\text{H}_5\text{Br}$  (2, 4, 12), but the direct comparison of the present results with those is impossible because temperatures and pressures differ.

Many  $P$ - $V$ - $T$  data for liquids have been represented by the Tait equation (6), which may be written in the form

$$V_P = V_0(1 - C \ln [(B + P)/(B + P_0)])$$

The Tait parameters  $B$  and  $C$  were computed for each isotherm by a least-squares method fit to the  $P$ - $V$ - $T$  data and listed in

**Table II.** Tait Parameters,  $B$  and  $C$

Compound	$T$ , °C	$B$ , atm	$C$	Av dev, <sup>a</sup> %	Max dev, %
$\text{CCl}_2\text{F}_2$	-20.00	394	0.0888	0.07	0.19
	0.00	285		0.07	0.17
	20.00	197		0.04	0.10
	40.00	125		0.08	-0.20
$\text{CHClF}_2$	-20.00	460	0.0963	0.10	0.17
	0.00	325		0.12	-0.21
	20.00	214		0.08	-0.19
	40.00	126		0.06	0.13
$\text{CH}_3\text{Cl}$	-20.00	791	0.1014	0.03	-0.13
	0.00	626		0.02	0.05
	20.00	485		0.05	-0.12
	40.00	368		0.04	-0.09
$\text{CH}_3\text{I}$	-20.00	1275	0.0953	0.02	0.05
	0.00	1085		0.03	-0.05
	20.00	936		0.03	±0.05
	40.00	786		0.02	-0.04
$\text{CH}_3\text{Br}$	-20.00	1020	0.0956	0.02	0.04
	0.00	822		0.03	-0.08
	20.00	670		0.05	-0.13
	40.00	536		0.07	-0.16
$\text{C}_2\text{H}_5\text{Br}$	-20.00	1085	0.0942	0.03	0.05
	0.00	887		0.01	-0.05
	20.00	722		0.02	-0.05
	40.00	610		0.06	-0.18
$\text{CH}_3\text{COOCH}_3$	-20.00	1063	0.0874	0.02	-0.04
	0.00	938		0.03	0.07
	20.00	779		0.02	±0.02
	40.00	631		0.03	±0.07

<sup>a</sup> Average deviation =  $\sum_{n=1}^n (|V_{\text{calcd}} - V_{\text{exptl}}| / V_{\text{exptl}}) \times 100 / n$ .  $n$  = number of data.  $V_{\text{calcd}}$ ,  $V_{\text{exptl}}$  = specific volumes calculated by the Tait equation with parameters  $B$  and  $C$  in Table II and experimental values, respectively.

Table II. The specific volume at the saturated vapor pressure,  $P_0$ , was chosen as  $V_0$  in this evaluation. It has previously been reported (11) that the  $C$  value for  $\text{NH}_3$  became constant in the lower temperatures and decreased in the neighborhood of the critical temperature. The  $C$  values for other liquids, as well as  $\text{NH}_3$ , were regarded as constant at experimental temperatures far from the critical temperature. Also, the average and the maximum deviation of the calculated values by the equation against the experimental data are indicated in Table II.

### Glossary

$B, C$	Tait equation parameters
$P$	pressure, atm
$P_0$	saturated vapor pressure, atm
$V_0, V_P$	specific volumes at pressures, $P_0$ and $P$ atm, respectively, $\text{cm}^3/\text{g}$

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