

# Smoothed Experimental Enthalpy Data for Four Mixtures: Three Methane–Ethane Binary Mixtures and a Ternary Mixture with Propane

John E. Powers,\* Andre W. Furtado, Ravi Kant, and Adriana Kwan

Department of Chemical Engineering, University of Michigan, Ann Arbor, Michigan 48109

Experimental enthalpy determinations made on three methane–ethane binaries and one methane–ethane–propane ternary have been interpreted and smoothed. The resulting enthalpy values are thermodynamically self-consistent over the experimental range roughly  $-240$  to  $+300$  °F at pressures up to 2000 psia. Smoothed enthalpy values are presented in tabular form at the temperatures and pressures of measurement. Values of smoothed derivative functions are also given in the tables:  $C_p$  values corresponding to isobaric determinations and  $\phi \equiv (\partial H/\partial P)_T$  values derived from both isothermal and isenthalpic experiments. The smoothed values are probably accurate to  $\pm 1\%$  which makes them adequate to test most engineering correlations. The derivative properties are somewhat less accurate,  $\pm 2\%$ , with larger deviations near the critical point of the mixtures. The most firmly established enthalpy values are included in Table I. These extend over the greater portion of the range of temperatures and pressures investigated and should be particularly suited to testing methods of predicting enthalpy both because of their accuracy and because of their scope. The original experimental data have been placed on file in the microfilm edition.

## Introduction

The prediction of enthalpy differences for mixtures plays a vital role in the design of processing equipment. For identical conditions, various methods of prediction may yield values that differ markedly and it is valuable to have accurate experimental values against which to test the various methods of prediction. The calorimetric facilities in the Thermal Properties of Fluids Laboratory at the University of Michigan were developed to meet this need under the combined sponsorship of the National Science Foundation, the Petroleum Research Fund, and the Gas Processors Association. The methods that were developed to process the data combined with the fact that the basic data were taken with considerable care served to yield values of enthalpy and associated derivative properties that are thermodynamically self-consistent and appear to be quite accurate. These data for pure compounds (8, 11, 13, 16, 33, 36) as well as binary (3, 8, 14, 15, 17, 34, 35, 37) and ternary (8, 9) mixtures have been used to test prediction methods (1, 2, 4, 5, 8, 10, 18, 19, 22, 24–29, 31–34, 37, 38) and it was thought desirable to obtain additional results of this type. Mixtures of particular interest to the natural gas processing industry were selected for study to ensure immediate applicability of the results.

## Experimental Section

**Equipment and Procedure.** The basic principles and detailed description of equipment and procedures have been presented in detail elsewhere (8, 15, 33). The basic measurements center

Table I. Enthalpy Values at the Points of Thermodynamic Consistency<sup>a</sup>

Ia. Mixture 1 (52.3% C <sub>2</sub> )						
<i>P</i> , psia	−228.4 °F	−99.0 °F	1.75 °F	101.5 °F	252.5 °F	
0		301.4	351.4	395.8	472.3	
250		155.2	336.4			
500		122.2	307.9			
750		122.2	242.2			
978		122.4	214.6	348.0		
1250			206.3	331.2		
1500	38.1	123.2	203.3	316.4	433.9	
2500			200.1	295.4		
Ib. Mixture 2 (22.3% C <sub>2</sub> )						
<i>P</i> , psia	−253.2 °F	−150.6 °F	−58.4 °F	79.0 °F	255.0 °F	
0		291.7	332.4	397.1	490.8	
250		129.9		388.5		
500		99.6				
1000	23.2	100.2	193.8	358.9	471.2	
1500			182.8	337.8		
2000			179.1	319.4	403.3	
Ic. Mixture 3 (5.55% C <sub>2</sub> )						
<i>P</i> , psia	−242 °F	−150 °F	−97 °F	−47 °F	79 °F	200 °F
0			319.4	343.7	407.2	
250			302.8	331.4	400.4	
500	(36.8)	115.5	279.1	316.8		
700		115.0		302.8		
800		115.0	194.9	294.7		
1000	36.1	114.5	175.6	276.3	376.8	(455.3)
1200		114.3	170.7	256.1		
1500		114.2	166.5	233.6		
2000	(36.4)	114.5	163.4	217.3	346.3	
Id. Mixture 4 (Ternary)						
<i>P</i> , psia	−243 °F	−150 °F	−47 °F	1.5 °F	158.5 °F	300 °F
0			335.8	358.4	436.9	
250			320.0			
500	(29.8)	102.3	291.8	333.3	423.6	(508.4)
750		102.6	262.3	317.8		
1000		102.9	233.3	299.5		
1200			211.9	284.2		
1500	(34.0)	103.8	198.6	263.0	395.0	(490.8)
2000			191.7	242.5		

<sup>a</sup>Note: Values in parentheses are "best" values but *not* the result of duplicate determinations.

around flow calorimeters through which the fluid under investigation is passed. One calorimeter operates with very low pressure drops (the isobaric mode) whereas the other is designed to produce significant pressure drops (isothermal or isenthalpic operation). Electrical energy is supplied to the calorimeter and inlet and outlet temperatures and pressures are measured together with the mass flow rate. Such data are sufficient to permit determination not only of enthalpy differences but also of derivative properties as well.

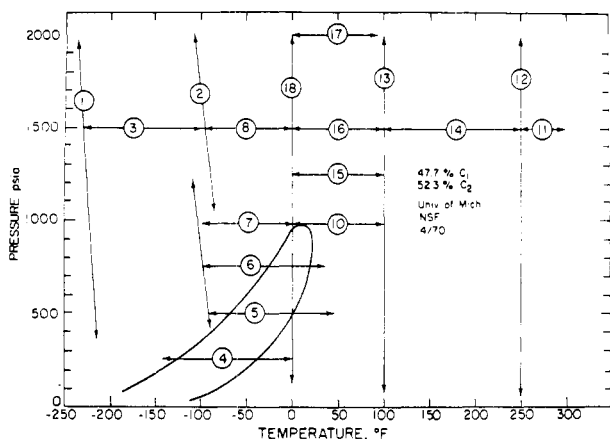
**Table II**  
Compositions of Standard Mixtures Used to Calibrate the Chromatograph

component	composition, mol %			
	1 (52.3%)	2 (22.3%)	3 (5.55%)	4 (ternary)
nitrogen, N <sub>2</sub>	0.05	0.08	a	a
carbon dioxide, CO <sub>2</sub>	0.03	0.03		
methane, CH <sub>4</sub>	47.90	77.71		
ethane, C <sub>2</sub> H <sub>6</sub>	51.70	22.10		
propane, C <sub>3</sub> H <sub>8</sub>	0.03	0.03		
propylene, C <sub>3</sub> H <sub>6</sub>	0.29	0.05		
	100.00	100.00		

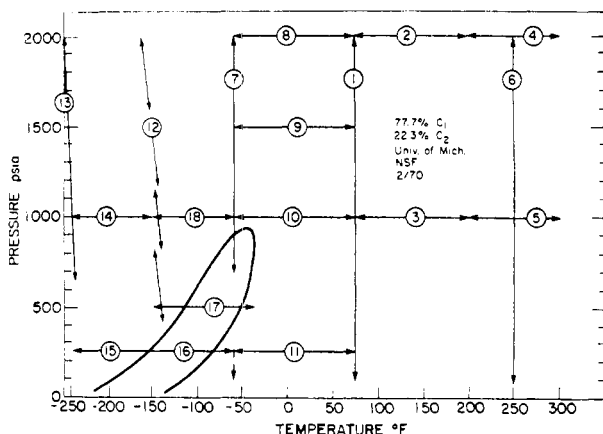
Nominal Compositions of the Mixtures Investigated

component	composition, mol %			
	1	2	3	4
methane	47.7	77.7	94.45	85.3
ethane	52.3	22.3	5.55	9.00
propane				5.70
	100.0	100.0	100.00	100.00

<sup>a</sup> Not available.

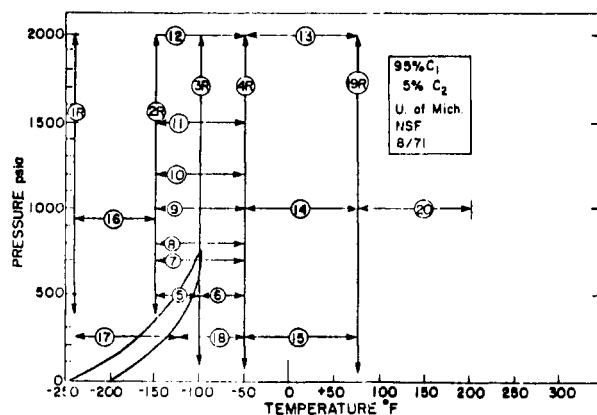


**Figure 1.** Pressures and temperatures of measurements for a 52.3 mol % ethane in methane mixture.

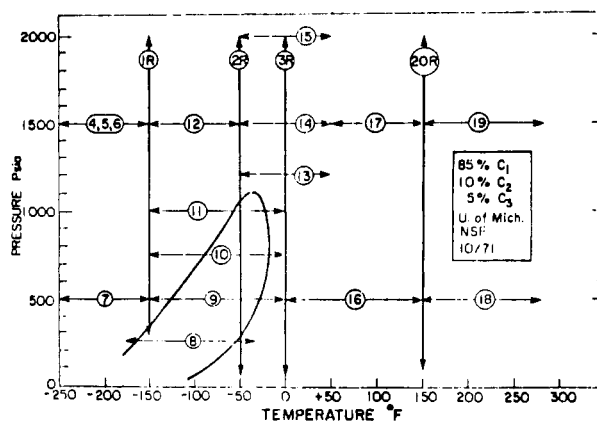


**Figure 2.** Pressures and temperatures of measurements for a 22.3 mol % ethane in methane mixture.

**Composition.** In addition to the basic data mentioned in the previous paragraph, it is essential that the composition of the mixture be known for each experiment and that the composition remains reasonably constant over the period of investigation for



**Figure 3.** Pressures and temperatures of measurements for a 5 mol % ethane in methane mixture.



**Figure 4.** Pressures and temperatures of measurements for a methane-ethane-propane mixture.

**Table III.** Zero Pressure Enthalpy Values Based on Published Data

	mixture no.			
	1 (51.2% C <sub>2</sub> )	2 (22.3% C <sub>2</sub> )	3 (5.55% C <sub>2</sub> )	4 (ternary)
Temp, °F	252.5	255.0	79.0	158.5
H <sup>o</sup> <sub>M</sub> , <sup>a</sup> Btu/lb	472.3	490.8	407.2	437.6

<sup>a</sup> These values are based on H = 0 for pure methane, ethane, and propane as saturated liquids at -280 °F.

**Table IV.** Estimated Values of Enthalpies of Liquid Mixtures to be Used as Checks on Calorimetric Determinations

mixture no.	T, °F	P, psia	enthalpies of pure components, <sup>a</sup> Btu/lb			H, <sup>E</sup> Btu/lb	H <sub>M</sub> , <sup>a</sup> Btu/lb
			CH <sub>4</sub>	C <sub>2</sub> -H <sub>6</sub>	C <sub>3</sub> -H <sub>8</sub>		
1 (52.3% C <sub>2</sub> )	-220	1500	54.0	37.7		0.6	43.5
2 (22.3% C <sub>2</sub> )	-240	1000	34.7	26.4		1.0	32.8
3 (5.55% C <sub>2</sub> )	-240	1000	34.7	26.4		0.3	34.2
4 (ternary)	-243	1500	35.0	25.0	21.2	0.3	32.0

<sup>a</sup> Based on H = 0 for pure components as saturated liquids at -280 °F.

each mixture. Samples taken from the recycle flow system at frequent intervals were analyzed by chromatograph utilizing direct comparison against samples from four tanks each containing a standard mixture. The composition of each standard tank was analyzed for trace components in addition to methane, ethane, and propane. The results of the analyses of the standard mixtures are given in Table II. Analyses for individual runs are



260.0	0.6913	0.6842	439.09
270.0	0.6883	0.6813	445.89
280.0	0.6862	0.6792	452.69
290.0	0.6850	0.6780	459.49
300.0	0.6855	0.6785	466.29
310.0	0.6860	0.6790	472.99

<sup>a</sup>  $C_p$  values at 250, 500 and 750 psia are not reported as most of the data lie in the two-phase region.

Table VI. Thermodynamic Properties at the Pressures of Isoobaric Determinations. Binary Mixture Containing Approximately 22.3 mol % Ethane in Methane<sup>a</sup>

temp., °F	P = 250 psia			P = 500 psia			P = 1000 psia			P = 1500 psia			P = 2000 psia			
	$C_p^b$ , Btu/(lb °F)	H, Btu/lb	$C_p$ (S), Btu/(lb °F)	H, Btu/lb	$C_p$ (S), Btu/(lb °F)	H, Btu/lb	$C_p$ (A), Btu/(lb °F)	H, Btu/lb	$C_p$ (S), Btu/(lb °F)	H, Btu/lb	$C_p$ (A), Btu/(lb °F)	H, Btu/lb	$C_p$ (S), Btu/(lb °F)	H, Btu/lb	$C_p$ (A), Btu/(lb °F)	H, Btu/lb
-260.0			0.7247	0.7207	18.26											
-250.0	0.7209	22.54	0.7304	0.7264	25.49											
-240.0	0.7305	29.80	0.7343	0.7303	32.78											
-230.0	0.7400	37.15	0.7377	0.7336	40.09											
-220.0	0.7495	44.60	0.7412	0.7371	47.44											
-210.0	0.7590	52.14	0.7465	0.7424	54.84											
-200.0	0.7685	59.78	0.7526	0.7485	62.29											
-190.0	0.7780	67.51	0.7588	0.7546	69.80											
-180.0	0.7872	75.34	0.7665	0.7623	77.38											
-170.0	0.7967	83.26	0.7767	0.7724	85.03											
-160.0	0.8058	91.27	0.7903	0.7860	92.91											
-150.0		131.37	0.8070	0.8031	100.65											
-140.0		170.67	0.8248	0.8208	109.08											
-130.0		196.37	0.8471	0.8430	117.37											
-120.0		215.87	0.8798	0.8756	125.96											
-110.0		233.87	0.9240	0.9196	134.86											
-100.0		252.77	0.9865	0.9818	144.36											
-90.0		274.27	1.0582	1.0531	154.56											
-80.0		296.57	1.1458	1.1403	165.46											
-70.0		308.87	1.2836	1.2774	177.46											
-60.0	0.5730	315.10	1.5582	1.5507	191.36											
-50.0	0.5410	320.66	2.1819	2.1695	209.97											
-40.0	0.5532	326.12	2.3519	2.3385	233.08											
-30.0	0.5445	331.61	1.9485	1.9374	254.79											
-20.0	0.5317	337.02	1.4988	1.4903	271.79											
-10.0	0.5272	342.34	1.1940	1.1872	285.10											
0.0	0.5224	347.59	1.0170	1.0112	296.00											
10.0	0.5199	352.80	0.9188	0.9136	305.61											
20.0	0.5186	357.99	0.8639	0.8590	314.51											
30.0	0.5174	363.17	0.8203	0.8156	322.81											
40.0	0.5169	368.34	0.7839	0.7794	330.82											
50.0	0.5169	373.51	0.7522	0.7479	338.42											
60.0	0.5169	378.68	0.7225	0.7184	345.72											
70.0	0.5169	383.85	0.6950	0.6910	352.83											
80.0	0.5169	389.02	0.6785	0.6741	359.60											
90.0			0.6680	0.6637	366.28											
100.0			0.6597	0.6554	373.00											
110.0			0.6531	0.6489	379.59											
120.0			0.6477	0.6435	386.09											
130.0			0.6427	0.6385	392.54											
140.0			0.6385	0.6345	398.97											
150.0			0.6356	0.6315	405.25											
160.0			0.6335	0.6294	411.53											
								1.1234	192.07	0.9154	178.11			0.9110	178.11	
								1.1902	203.60	0.9526	186.96			0.9480	186.96	
								1.2769	215.88	1.0246	196.62			0.9837	196.62	
								1.3945	229.29	1.0596	206.63			1.0197	206.63	
								1.4115	243.37	1.0897	217.01			1.0545	217.01	
								1.3487	257.20	1.1008	227.71			1.0844	227.71	
								1.2510	270.20	1.1028	238.62			1.0955	238.62	
								1.1423	282.18	1.0917	249.59			1.0975	249.59	
								1.0496	293.13	1.0677	260.51			1.0864	260.51	
								0.9755	303.19	1.0376	271.27			1.0626	271.27	
								0.9252	312.65	1.0055	281.70			1.0326	281.70	
								0.8865	321.71	0.9700	291.88			1.0007	291.88	
								0.8480	330.38	0.9330	301.75			0.9653	301.75	
								0.8160	338.64	0.9000	311.23			0.9285	311.23	
										0.8729	320.32			0.9009	320.32	
										0.8464	329.17			0.8738	329.17	
										0.8205	337.82			0.8472	337.82	
										0.8005	346.17			0.8213	346.17	
										0.7826	354.32			0.8013	354.32	
										0.7678	362.17			0.7834	362.17	
										0.7518	370.01			0.7686	370.01	
										0.7410	377.56			0.7526	377.56	
										0.7303	385.10			0.7410	385.10	

Table VI (Continued)

temp, °F	P = 250 psia			P = 500 psia			P = 1000 psia			P = 1500 psia			P = 2000 psia		
	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$H$ , Btu/lb
170.0	0.6319	0.6278	417.79	0.6319	0.6278	417.79	0.6319	0.6278	417.79	0.6319	0.6278	417.79	0.6319	0.6278	417.79
180.0	0.6310	0.6269	424.04	0.6310	0.6269	424.04	0.6310	0.6269	424.04	0.6310	0.6269	424.04	0.6310	0.6269	424.04
190.0	0.6305	0.6264	430.29	0.6305	0.6264	430.29	0.6305	0.6264	430.29	0.6305	0.6264	430.29	0.6305	0.6264	430.29
200.0	0.6307	0.6266	436.53	0.6307	0.6266	436.53	0.6307	0.6266	436.53	0.6307	0.6266	436.53	0.6307	0.6266	436.53
210.0	0.6320	0.6279	442.78	0.6320	0.6279	442.78	0.6320	0.6279	442.78	0.6320	0.6279	442.78	0.6320	0.6279	442.78
220.0	0.6345	0.6304	449.05	0.6345	0.6304	449.05	0.6345	0.6304	449.05	0.6345	0.6304	449.05	0.6345	0.6304	449.05
230.0	0.6373	0.6332	455.34	0.6373	0.6332	455.34	0.6373	0.6332	455.34	0.6373	0.6332	455.34	0.6373	0.6332	455.34
240.0	0.6400	0.6358	461.67	0.6400	0.6358	461.67	0.6400	0.6358	461.67	0.6400	0.6358	461.67	0.6400	0.6358	461.67
250.0	0.6426	0.6384	468.02	0.6426	0.6384	468.02	0.6426	0.6384	468.02	0.6426	0.6384	468.02	0.6426	0.6384	468.02
260.0	0.6450	0.6408	474.39	0.6450	0.6408	474.39	0.6450	0.6408	474.39	0.6450	0.6408	474.39	0.6450	0.6408	474.39
270.0	0.6476	0.6434	480.79	0.6476	0.6434	480.79	0.6476	0.6434	480.79	0.6476	0.6434	480.79	0.6476	0.6434	480.79
280.0	0.6510	0.6468	487.22	0.6510	0.6468	487.22	0.6510	0.6468	487.22	0.6510	0.6468	487.22	0.6510	0.6468	487.22
290.0	0.6542	0.6499	493.66	0.6542	0.6499	493.66	0.6542	0.6499	493.66	0.6542	0.6499	493.66	0.6542	0.6499	493.66
300.0	0.6575	0.6532	500.17	0.6575	0.6532	500.17	0.6575	0.6532	500.17	0.6575	0.6532	500.17	0.6575	0.6532	500.17
310.0	0.6598	0.6555	506.70	0.6598	0.6555	506.70	0.6598	0.6555	506.70	0.6598	0.6555	506.70	0.6598	0.6555	506.70
320.0	0.6610	0.6567	513.24	0.6610	0.6567	513.24	0.6610	0.6567	513.24	0.6610	0.6567	513.24	0.6610	0.6567	513.24

<sup>a</sup>  $C_p$  values at 500 psia are not reported as most of the data lies in the two-phase region. <sup>b</sup>  $C_p$  values at 250 psia are not reported in the two-phase region.

Table VII. Thermodynamic Properties at the Pressures of Isobaric Determinations. Binary Mixture Containing Approximately 5.5 mol % Ethane in Methane

temp, °F	P = 250 psia			P = 500 psia			P = 700 psia			P = 800 psia		
	$C_p^b$ , Btu/(lb °F)	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb	$C_p^b$ , Btu/(lb °F)	$C_p^b$ , Btu/(lb °F)	$H$ , Btu/lb
-240.0	0.8227	0.8029	39.0	0.8227	0.8029	39.0	0.8227	0.8029	39.0	0.8227	0.8029	39.0
-230.0	0.8252	0.8053	47.1	0.8252	0.8053	47.1	0.8252	0.8053	47.1	0.8252	0.8053	47.1
-220.0	0.8315	0.8115	55.2	0.8315	0.8115	55.2	0.8315	0.8115	55.2	0.8315	0.8115	55.2
-210.0	0.8418	0.8215	63.3	0.8418	0.8215	63.3	0.8418	0.8215	63.3	0.8418	0.8215	63.3
-200.0	0.8579	0.8372	71.6	0.8579	0.8372	71.6	0.8579	0.8372	71.6	0.8579	0.8372	71.6
-190.0	0.8872	0.8658	80.1	0.8872	0.8658	80.1	0.8872	0.8658	80.1	0.8872	0.8658	80.1
-180.0	0.9420	0.9193	89.0	0.9420	0.9193	89.0	0.9420	0.9193	89.0	0.9420	0.9193	89.0
-170.0	1.1580	1.1301	98.9	1.1580	1.1301	98.9	1.1580	1.1301	98.9	1.1580	1.1301	98.9
-160.0			154.1			154.1			154.1			154.1
-150.0			216.2			216.2			216.2			216.2
-140.0			262.2			262.2			262.2			262.2
-130.0			276.8			276.8			276.8			276.8
-120.0			288.6			288.6			288.6			288.6
-110.0			295.0			295.0			295.0			295.0
-100.0			301.1			301.1			301.1			301.1
-90.0	0.5904	0.5881	307.0	0.5904	0.5881	307.0	0.5904	0.5881	307.0	0.5904	0.5881	307.0
-80.0	0.5771	0.5749	312.8	0.5771	0.5749	312.8	0.5771	0.5749	312.8	0.5771	0.5749	312.8
-70.0	0.5688	0.5666	318.5	0.5688	0.5666	318.5	0.5688	0.5666	318.5	0.5688	0.5666	318.5
-60.0	0.5635	0.5613	324.5	0.5635	0.5613	324.5	0.5635	0.5613	324.5	0.5635	0.5613	324.5
-50.0	0.5591	0.5570	329.8	0.5591	0.5570	329.8	0.5591	0.5570	329.8	0.5591	0.5570	329.8
-40.0	0.5554	0.5553	335.3	0.5554	0.5553	335.3	0.5554	0.5553	335.3	0.5554	0.5553	335.3
-30.0	0.5524	0.5523	340.9	0.5524	0.5523	340.9	0.5524	0.5523	340.9	0.5524	0.5523	340.9
-20.0	0.5502	0.5501	346.37	0.5502	0.5501	346.37	0.5502	0.5501	346.37	0.5502	0.5501	346.37
-10.0	0.5485	0.5484	351.9	0.5485	0.5484	351.9	0.5485	0.5484	351.9	0.5485	0.5484	351.9
0.0	0.5472	0.5471	357.3	0.5472	0.5471	357.3	0.5472	0.5471	357.3	0.5472	0.5471	357.3
10.0	0.5458	0.5457	362.8	0.5458	0.5457	362.8	0.5458	0.5457	362.8	0.5458	0.5457	362.8

temp, °F	P = 1000 psia				P = 1200 psia				P = 1500 psia				P = 2000 psia			
	$C_p(S)$ , Btu/(lb °F)	$C_p(A)$ , Btu/(lb °F)	H(A), Btu/lb	$C_p(S)$ , Btu/(lb °F)	$C_p(A)$ , Btu/(lb °F)	H(A), Btu/lb	$C_p(S)$ , Btu/(lb °F)	$C_p(A)$ , Btu/(lb °F)	H(A), Btu/lb	$C_p(S)$ , Btu/(lb °F)	$C_p(A)$ , Btu/(lb °F)	H(A), Btu/lb	$C_p(S)$ , Btu/(lb °F)	$C_p(A)$ , Btu/(lb °F)	H(A), Btu/lb	
	20.0	0.5446	.5445	368.3	0.8072	0.8137	37.7	0.9180	0.9180	105.6	0.8930	0.8930	105.2	0.8239	0.8239	106.2
30.0	0.5431	.5430	373.7	0.8137	0.8137	45.8	0.9322	0.9322	114.3	0.9072	0.9072	114.2	0.8460	0.8460	114.5	
40.0	0.5416	.5415	379.1	0.8268	0.8268	54.0	0.9657	0.9657	123.8	0.9281	0.9281	123.4	0.8697	0.8697	123.2	
50.0	0.5408	.5407	384.5	0.8352	0.8352	62.23	1.0065	1.0065	133.6	0.9550	0.9550	132.8	0.8950	0.8950	132.1	
60.0	0.5398	.5397	389.9	0.8471	0.8471	70.5	1.0750	1.0750	144.0	0.9879	0.9879	142.5	0.9226	0.9226	141.2	
70.0	0.5385	.5384	395.34	0.8632	0.8632	78.9	1.1540	1.1540	155.0	1.0314	1.0314	152.6	0.9504	0.9504	150.7	
80.0	0.5374	.5374	400.7	0.8820	0.8820	87.5	1.2680	1.2680	166.7	1.0850	1.0850	163.2	0.9783	0.9783	160.4	
-240.0	0.8072	0.8072		1.1540	1.1540	157.9	1.4310	1.4310	180.4	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-230.0	0.8137	0.8137		1.1540	1.1540	170.9	1.4497	1.4497	186.7	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-220.0	0.8202	0.8202		1.1540	1.1540	188.5	1.4851	1.4851	196.0	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-210.0	0.8268	0.8268		1.1540	1.1540	214.2	1.5225	1.5225	215.0	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-200.0	0.8352	0.8352		1.1540	1.1540	240.1	1.5953	1.5953	235.0	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-190.0	0.8471	0.8471		1.1540	1.1540	258.5	1.6650	1.6650	251.9	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-180.0	0.8632	0.8632		1.1540	1.1540	284.4	1.7910	1.7910	284.4	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-170.0	0.8820	0.8820		1.1540	1.1540	294.8	1.4080	1.4080	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-160.0	0.9122	0.9122		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-150.0	0.9512	0.9512		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-140.0	1.0043	1.0043		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-130.0	1.0681	1.0681		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-120.0	1.1540	1.1540		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-110.0	1.2802	1.2802		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-100.0	1.4851	1.4851		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-90.0	2.1021	2.1044		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-80.0	2.8528	2.8559		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-70.0	2.1772	2.1796		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-60.0	1.5936	1.5953		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-50.0	1.2633	1.2647		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-40.0	1.0920	1.1019		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-30.0	0.9700	0.9788		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-20.0	0.8900	0.8980		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
-10.0	0.8360	0.8436		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
0.0	0.7960	0.8032		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
10.0	0.7580	0.7648		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
20.0	0.7260	0.7326		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
30.0	1.7060	0.7124		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
40.0	0.6920	0.6983		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
50.0	0.6780	0.6841		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
60.0	0.6660	0.6720		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
70.0	0.6540	0.6600		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
80.0	0.6441	0.6441		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
90.0	0.6370	0.6370		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
100.0	0.6320	0.6320		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
110.0	0.6280	0.6280		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
120.0	0.6270	0.6270		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
130.0	0.6320	0.6320		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
140.0	0.6310	0.6310		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
150.0	0.6420	0.6420		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
160.0	0.6567	0.6567		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
170.0	0.6650	0.6650		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
180.0	0.6752	0.6752		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
190.0	0.6870	0.6870		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	
200.0	0.7020	0.7020		1.1540	1.1540	294.8	1.4264	1.4264	294.8	1.1357	1.1357	174.0	1.0043	1.0043	170.4	



0.6710	0.6710	448.78
0.6791	0.6791	455.58
0.6884	0.6884	462.38
0.6980	0.6980	469.38
0.7096	0.7096	476.38
0.7224	0.7224	483.48
0.7360	0.7360	490.78

0.6003	0.6003	473.75
0.6027	0.6027	479.75
0.6051	0.6051	485.75
0.6076	0.6076	491.85
0.6101	0.6101	497.95
0.6127	0.6127	504.05
0.6155	0.6155	510.15

240.0
250.0
260.0
270.0
280.0
290.0
300.0

presented as part of the basic data available elsewhere. The individual analyses were averaged to give the nominal compositions listed in Table II. In obtaining the average values reported in Table II, added weight was given to the composition of runs made across the two-phase region and near the critical point.

**Experimental Data.** Isobaric, isothermal, and isenthalpic measurements were made on each mixture from about  $-240$  to  $+250$  °F ( $300$  °F for two systems) at pressures between  $100$  and  $2000$  psia. The actual conditions of measurements for each mixture are presented on pressure-temperature diagrams as Figures 1-4. Each associated group of experiments is identified by a number within a circle. A group of isobaric measurements in the single-phase region included from 3 to 9 experiments with the same inlet temperature. Power input was adjusted to yield outlet temperatures increasing in increments of about  $20$  °F. In regions where  $C_p$  varied significantly (such as near the critical point) smaller temperature rises were used (as small as  $5$  °F). Isobaric determinations were made across the two-phase region to establish bubble- and dew-point temperatures in addition to yielding isobaric heats of vaporization and enthalpy values within the two-phase region. Isothermal determinations were made mainly in the single-phase region. Pressure drops were usually between  $100$  and  $500$  psi. A limited number of isenthalpic determinations were made at low temperatures in the liquid phase.

The basic experimental results obtained under sponsorship of the National Science Foundation are filed in the microfilm edition.

**Experimental Difficulties.** During the course of time required to make extensive calorimetric determinations on four different systems, a number of operational difficulties are usually encountered. Nothing unusual occurred during these investigations but in the process of checking out the equipment after completion of the determinations involving mixtures 1 and 2, several small leaks were noted in the all-important section between the calorimeter and flowmeter and later it was found that a short in the battery used to power the potentiometer probably caused somewhat erroneous readings.

It is impossible to determine whether any of these operational problems (which were only detected after completion of the investigation of mixtures 1 and 2) influenced the results to any appreciable degree but, at a minimum, the possibility of systematic error must be taken into account. It should be noted that leaks between the calorimeter and flowmeter will tend to yield property values that are too high.

#### Selection of Bases and Use of Other Published Data

In presenting enthalpy data for mixtures it is sufficient to select one reference state for each of the components in the mixture. The bases  $H = 0$  for pure methane, pure ethane, and pure propane as saturated liquids at  $-280$  °F were chosen so as to be consistent with prior analysis of calorimetric data for these pure components (8, 11, 13, 16, 33, 36) and a number of mixtures (3, 8, 9, 15, 17, 34, 35, 37).

Published data for pure methane, pure ethane, and pure propane served two purposes in the process of obtaining reliable enthalpy values for mixtures under investigation. Whereas operation of the equipment was limited in lower value to about  $100$  psia, excellent published data for the pure compounds are available at pressures of  $1$  atm and below (7, 12, 30) so that the experimental results were readily extended to the lower pressures. In addition, when used in connection with estimates based on published values of excess enthalpy of mixing for liquid hydrocarbon mixtures, a valuable check on the validity of the mixture data was obtained (6).

The procedures employed to utilize published data on the pure components to obtain enthalpy values for the individual mixtures



Table IX. Thermodynamic Properties at the Pressures of Isobaric Determinations in the Regions of Rapid Change (High  $(\partial C_p/\partial T)_p$ ) for Mixture 1 (52.3%  $C_2$ )

temp, °F	$P = 978$ psia			temp, °F	$P = 1250$ psia			temp, °F	$P = 1500$ psia		
	$C_p(S)$ , Btu/ (lb °F)	$C_p(A)$ , Btu/ (lb °F)	$H$ , Btu/lb		$C_p(S)$ , Btu/ (lb °F)	$C_p(A)$ , Btu/ (lb °F)	$H$ , Btu/lb		$C_p(S)$ , Btu/ (lb °F)	$C_p(A)$ , Btu/ (lb °F)	$H$ , Btu/lb
5.00	1.6682	1.6520	219.73	15.00	1.2581	1.2414	221.79	30.00	1.1497	1.1366	232.59
10.00	1.8773	1.8591	228.52	17.50	1.2914	1.2742	224.93	40.00	1.2295	1.2155	244.09
15.00	2.0835	2.0633	238.41	20.00	1.3258	1.3082	228.16	41.00	1.2407	1.2266	245.29
15.50	2.0996	2.0792	239.51	22.50	1.3622	1.3441	231.48	42.00	1.2497	1.2355	246.59
16.00	2.1178	2.0973	240.51	25.00	1.3965	1.3779	234.89	43.00	1.2588	1.2444	247.79
16.50	2.1340	2.1133	241.61	27.50	1.4268	1.4078	238.37	44.00	1.2659	1.2515	249.09
17.00	2.1451	2.1243	242.61	30.00	1.4572	1.4378	241.93	45.00	1.2720	1.2575	250.29
17.50	2.1501	2.1292	243.71	30.62	1.4642	1.4447	242.83	46.00	1.2760	1.2615	251.59
18.00	2.1532	2.1323	244.81	31.25	1.4703	1.4507	243.74	47.00	1.2790	1.2644	252.89
18.50	2.1552	2.1343	245.81	31.88	1.4774	1.4577	244.66	48.00	1.2801	1.2655	254.09
19.00	2.1542	2.1333	246.91	32.50	1.4844	1.4647	245.56	49.00	1.2811	1.2665	255.39
19.50	2.1522	2.1313	248.01	33.13	1.4905	1.4707	246.48	50.00	1.2821	1.2675	256.69
20.00	2.1461	2.1253	249.01	33.75	1.4956	1.4757	247.40	51.00	1.2831	1.2685	257.89
20.50	2.1380	2.1173	250.11	34.38	1.5006	1.4806	248.33	52.00	1.2841	1.2695	259.19
21.00	2.1279	2.1073	251.10	35.00	1.5067	1.4867	249.26	53.00	1.2841	1.2695	260.49
21.50	2.1148	2.0943	252.20	35.62	1.5117	1.4916	250.17	54.00	1.2841	1.2695	261.69
22.00	2.0996	2.0792	253.20	36.25	1.5168	1.4966	251.12	55.00	1.2831	1.2685	262.99
22.50	2.0824	2.0622	254.30	36.87	1.5218	1.5016	252.05	56.00	1.2821	1.2675	264.29
23.00	2.0663	2.0463	255.30	37.50	1.5259	1.5056	253.00	57.00	1.2811	1.2665	265.49
23.50	2.0491	2.0292	256.30	38.13	1.5279	1.5076	253.95	58.00	1.2801	1.2655	266.79
24.00	2.0329	2.0132	257.30	38.75	1.5299	1.5096	254.88	59.00	1.2790	1.2644	268.09
24.50	2.0188	1.9992	258.30	39.38	1.5319	1.5115	255.83	60.00	1.2760	1.2615	269.29
25.00	2.0077	1.9882	259.30	40.00	1.5340	1.5136	256.77	61.00	1.2720	1.2575	270.59
30.00	1.8349	1.8171	268.99	40.63	1.5340	1.5136	257.73	62.00	1.2659	1.2515	271.89
35.00	1.6763	1.6600	277.58	41.25	1.5340	1.5136	258.67	63.00	1.2598	1.2454	273.09
40.00	1.5338	1.5189	285.58	41.87	1.5340	1.5136	259.60	64.00	1.2528	1.2385	274.39
45.00	1.4166	1.4029	292.87	42.50	1.5329	1.5125	260.56	65.00	1.2467	1.2325	275.59
				43.13	1.5299	1.5096	261.51	66.00	1.2407	1.2266	276.79
				43.75	1.5279	1.5076	262.45	67.00	1.2346	1.2205	277.99
				44.38	1.5249	1.5046	263.39	68.00	1.2285	1.2145	279.29
				45.00	1.5208	1.5006	264.33	69.00	1.2225	1.2086	280.49
				45.63	1.5158	1.4956	265.27	70.00	1.2164	1.2025	281.69
				46.25	1.5117	1.4916	266.20	80.00	1.1548	1.1416	293.39
				46.88	1.5067	1.4867	267.14				
				47.50	1.5016	1.4816	268.06				
				48.12	1.4956	1.4757	268.98				
				48.75	1.4895	1.4697	269.91				
				49.38	1.4834	1.4637	270.83				
				50.00	1.4774	1.4577	271.74				
				50.63	1.4703	1.4507	272.65				
				51.25	1.4632	1.4437	273.55				
				51.88	1.4561	1.4367	274.46				
				52.50	1.4501	1.4308	275.35				
				53.13	1.4440	1.4248	276.25				
				53.75	1.4369	1.4178	277.13				
				54.38	1.4289	1.4099	278.02				
				55.00	1.4198	1.4009	278.90				
				57.50	1.3844	1.3660	282.35				
				60.00	1.3511	1.3331	285.74				
				62.50	1.3187	1.3012	289.03				
				65.00	1.2874	1.2703	292.24				

at zero pressure are described in detail elsewhere (21). In brief, for each pure component, one utilizes accurate published data on the heat capacity of saturated liquid,  $C_{p,l}$ , and the enthalpy change on vaporization,  $\Delta H_{vap}$ , together with an estimate of the enthalpy change from the pressure at which  $\Delta H_{vap}$  is known to zero pressure to estimate the enthalpy of the pure compound as an ideal gas at the temperature of vaporization relative to the reference state of saturated liquid at  $-280$  °F. Further, by using the properties of the ideal gas as calculated from theoretically based analyses of spectroscopic and calorimetric data (23), one can calculate the enthalpy of all of the pure components at zero pressure at any temperature of interest. At low pressure the gases form ideal mixtures and therefore the enthalpy of any of the investigated mixtures can be calculated using the relation

$$H^{\circ}_M = \sum y_i H^{\circ}_i \quad (1)$$

where the subscripts M and i refer to the mixture and the individual components respectively and  $y_i$  refers to the mole or mass fractions of the individual components in the mixture. Details of the calculations are presented elsewhere (21). The applicable results are summarized in Table III.

In addition to the uses made of published data mentioned above, enthalpy data for the pure components (utilizing the same bases) can be used together with estimates of the enthalpy change on mixing to calculate the mixture enthalpy where such data are available. The procedure provides valuable check points in the liquid region for the mixture data. The results of calculations described in detail elsewhere (21) are presented in Table IV.

#### Analysis of Experimental Data

In an attempt to obtain the most accurate and thermody-

Table X. Thermodynamic Properties at the Pressures of Isobaric Determinations in the Regions of Rapid Change (High  $(\partial C_p/\partial T)_p$ ) for Mixture 2 (22.3% C<sub>2</sub>)

P = 1000 psia			P = 1500 psia			P = 2000 psia					
temp, °F	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	temp, °F	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	temp, °F	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb
-60.00	1.5582	1.5507	191.36	-30.00	1.2769	1.2753	215.88	-30.00	1.0246	1.0197	206.63
-59.00	1.6185	1.6107	192.96	-27.50	1.3108	1.3091	219.12	-25.00	1.0426	1.0376	211.78
-58.45	1.6528	1.6449	193.76	-25.00	1.3437	1.3420	222.44	-20.00	1.0596	1.0545	217.01
-58.00	1.6809	1.6713	194.56	-22.50	1.3736	1.3718	225.83	-15.00	1.0767	1.0715	222.33
-57.00	1.7443	1.7344	196.26	-20.00	1.3945	1.3927	229.29	-10.00	1.0897	1.0844	227.71
-56.00	1.8067	1.7964	198.06	-18.75	1.4015	1.3997	231.03	-5.00	1.0957	1.0904	233.15
-55.00	1.8680	1.8574	199.86	-17.50	1.4055	1.4037	232.78	0.0	1.1008	1.0955	238.62
-54.00	1.9304	1.9194	201.76	-16.25	1.4095	1.4077	234.55	5.00	1.1028	1.0975	244.10
-53.00	1.9938	1.9824	203.66	-15.00	1.4125	1.4107	236.31	10.00	1.1028	1.0975	249.59
-52.00	2.0581	2.0464	205.66	-13.75	1.4135	1.4117	238.07	15.00	1.0987	1.0934	255.07
-51.00	2.1205	2.1084	207.77	-12.50	1.4145	1.4127	239.83	20.00	1.0917	1.0864	260.51
-50.00	2.1819	2.1695	209.97	-11.25	1.4135	1.4117	241.61	25.00	1.0807	1.0755	265.92
-49.00	2.2422	2.2294	212.17	-10.00	1.4115	1.4097	243.37	30.00	1.0677	1.0626	271.27
-48.00	2.2855	2.2725	214.37	-7.50	1.4015	1.3997	246.88				
-47.00	2.3116	2.2984	216.67	-5.00	1.3876	1.3858	250.36				
-46.00	2.3378	2.3245	218.97	-2.50	1.3706	1.3688	253.81				
-45.00	3.3519	2.3385	221.27	0.0	1.3487	1.3470	257.20				
-44.50	2.3589	2.3455	222.47	2.50	1.3228	1.3211	260.54				
-44.00	2.3650	2.3515	223.67	5.00	1.3028	1.3011	263.82				
-43.50	2.3690	2.3555	224.87	7.50	1.2769	1.2753	267.04				
-43.00	2.3710	2.3575	225.97	10.00	1.2510	1.2494	270.20				
-42.50	2.3720	2.3585	227.17								
-42.00	2.3710	2.3575	228.37								
-41.50	2.3690	2.3555	229.57								
-41.00	2.3650	2.3515	230.68								
-40.50	2.3589	2.3455	231.88								
-40.00	2.3519	2.3385	233.08								
-39.00	3.3378	2.3245	235.38								
-38.00	2.3116	2.2984	237.68								
-37.00	2.2855	2.2725	239.98								
-36.00	2.2503	2.2375	242.28								
-35.00	2.2080	2.1954	244.48								
-34.00	2.1607	2.1484	246.68								
-33.00	2.1105	2.0985	248.78								
-32.00	2.0561	2.0444	250.88								
-31.00	2.0018	1.9904	252.88								
-30.00	1.9485	1.9374	254.79								
-27.50	1.8157	1.8053	259.49								
-25.00	1.6920	1.6824	263.89								
-22.50	1.5894	1.5803	267.89								
-20.00	1.4988	1.4903	271.79								

namically consistent property values from the experimental data, a sequence of processing steps was employed. (1) A generalized correlation (20) was used to adjust experimental values to normalized values of composition, pressure level, and temperatures. (2) The normalized values were then smoothed to obtain consistency between data from different runs and to determine numerical values for the derivative properties and integral values of enthalpy differences. (3) The values so obtained were carefully checked for thermodynamic self-consistency and adjusted as necessary. (4) The adjusted values were checked for consistency with published data of superior quality and again adjusted as required. The resulting values should be reasonably accurate over the entire region of investigation. Further information with regard to each step outlined above is presented in the following paragraphs.

**Normalization and Correction of Experimental Data.** The basic data (included in the microfilm edition) are in terms of experimentally determined differences in enthalpy for a particular experimental mixture,  $x_i$ , corresponding to values of temperature and pressure measured at the inlet,  $j$ , and the outlet,  $k$ , of the calorimeter:

$$\Delta H_M = [H_{T_k, P_k} - H_{T_j, P_j}]x_i \quad (2)$$

As mentioned previously, periodic checks were made of the composition of the experimental mixture and variations as

extreme as 1.2% ethane from the nominal values were noted. (Actually, variations were generally much less than that.) Similarly, during any series of isobaric runs, the system pressure ranged as much as  $\pm 3$  psi and the inlet temperature varied as much as  $\pm 1.5$  °F in extreme cases. Final interpretation of the data is both simplified and made more meaningful by adjusting the basic calorimetric data to the composition listed in Table II, normalizing all isobaric determinations obtained at one pressure level to a convenient value (such as 1000 psia), and adjusting to an average value all inlet temperatures for one set of isobaric determinations. The sum total of all such corrections was usually less than 0.1% with a maximum adjustment of 3%. Such large corrections occurred only for the run made through the critical point for mixture 1 (run 10). For all other runs the corrections did not exceed 1.5%. Details of this normalization procedure are presented elsewhere (8).

In addition to the minor corrections to normalized values mentioned above, small corrections were made to account for the small measured pressure drop in the isobaric calorimeter and the fact that small differences in temperature normally existed between the inlet and outlet of the calorimeter during isothermal runs. These corrections were made in a rigorous manner as described elsewhere (35) and in extreme cases such corrections amounted to 0.3% of the experimentally determined enthalpy difference.

Table XI. Thermodynamic Properties at the Pressures of Isobaric Determinations in the Regions of Rapid Change (High  $(\partial C_p / \partial T)_p$ ) for Mixture 3 (5.55% C<sub>2</sub>)

temp, °F	P = 800 psia				P = 1000 psia				P = 1200 psia				P = 1500 psia				P = 2000 psia			
	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	H, Btu/lb	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	H, Btu/lb	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	H, Btu/lb	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	H, Btu/lb	C <sub>p</sub> (S), Btu/(lb °F)	C <sub>p</sub> (A), Btu/(lb °F)	H, Btu/lb	H, Btu/lb
-120.0	1.2901	1.2901	147.8	147.8	1.4851	1.4851	170.9	170.9	1.5360	1.5360	187.9	187.9	1.4965	1.4965	145.87	145.87	1.1597	1.1597	-50.0	213.8
-119.0	1.3101	1.3101	149.2	149.2	1.5214	1.5214	172.4	172.4	1.5570	1.5570	189.5	189.5	1.5034	1.5034	146.54	146.54	1.1617	1.1617	-49.5	214.4
-118.0	1.3340	1.3340	150.5	150.5	1.5588	1.5588	174.1	174.1	1.5780	1.5780	191.0	191.0	1.5132	1.5132	147.49	147.49	1.1647	1.1647	-49.0	215.0
-117.0	1.3579	1.3579	151.8	151.8	1.6153	1.6153	175.6	175.6	1.6050	1.6050	192.7	192.7	1.5241	1.5241	148.56	148.56	1.1677	1.1677	-48.5	215.5
-116.0	1.3839	1.3839	153.2	153.2	1.6675	1.6675	177.3	177.3	1.6340	1.6340	194.3	194.3	1.5379	1.5379	149.90	149.90	1.1697	1.1697	-48.0	216.1
-115.0	1.4128	1.4128	154.6	154.6	1.7337	1.7337	179.0	179.0	1.6650	1.6650	196.0	196.0	1.5517	1.5517	151.25	151.25	1.1716	1.1716	-47.5	216.7
-114.0	1.4447	1.4447	156.0	156.0	1.7988	1.7988	180.7	180.7	1.6950	1.6950	197.7	197.7	1.5675	1.5675	152.79	152.79	1.1736	1.1736	-47.0	217.3
-113.0	1.4915	1.4915	157.5	157.5	1.8669	1.8669	182.6	182.6	1.7270	1.7270	199.4	199.4	1.5842	1.5842	154.41	154.41	1.1791	1.1791	-46.5	217.9
-112.0	1.5284	1.5284	159.0	159.0	1.9409	1.9409	184.5	184.5	1.7640	1.7640	201.2	201.2	1.6010	1.6010	156.05	156.05	1.1811	1.1811	-46.0	218.5
-111.0	1.5683	1.5683	160.5	160.5	2.0220	2.0220	186.4	186.4	1.8070	1.8070	203.0	203.0	1.6187	1.6187	157.78	157.78	1.1831	1.1831	-45.5	219.1
-110.0	1.6132	1.6132	162.1	162.1	2.1021	2.1021	188.5	188.5	1.8540	1.8540	204.8	204.8	1.6355	1.6355	159.41	159.41	1.1851	1.1851	-45.0	219.7
-109.0	1.6650	1.6650	163.8	163.8	2.1712	2.1712	190.6	190.6	1.9000	1.9000	206.8	206.8	1.6522	1.6522	161.04	161.04	1.1881	1.1881	-44.5	220.3
-108.0	1.7308	1.7308	165.5	165.5	2.2673	2.2673	192.8	192.8	1.9510	1.9510	208.7	208.7	1.6710	1.6710	162.88	162.88	1.1911	1.1911	-44.0	220.9
-107.0	1.8096	1.8096	167.2	167.2	2.3283	2.3283	194.0	194.0	2.0240	2.0240	210.7	210.7	1.6857	1.6857	164.31	164.31	1.1941	1.1941	-43.5	221.3
-106.0	1.9003	1.9003	169.1	169.1	2.3924	2.3924	195.2	195.2	2.1090	2.1090	212.8	212.8	1.6996	1.6996	165.66	165.66	1.1971	1.1971	-43.0	222.0
-105.0	2.0040	2.0040	171.0	171.0	2.4564	2.4564	196.4	196.4	2.2160	2.2160	215.0	215.0	1.7104	1.7104	166.72	166.72	1.1991	1.1991	-42.5	222.6
-104.0	2.1196	2.1196	173.1	173.1	2.5172	2.5172	197.6	197.6	2.2260	2.2260	217.2	217.2	1.7203	1.7203	167.68	167.68	1.2011	1.2011	-42.0	223.2
-103.0	2.2871	2.2871	175.3	175.3	2.5726	2.5726	198.9	198.9	2.2260	2.2260	219.5	219.5	1.7350	1.7350	169.11	169.11	1.2031	1.2031	-41.5	223.8
-102.0	2.4576	2.4576	177.7	177.7	2.6276	2.6276	199.2	199.2	2.2280	2.2280	221.8	221.8	1.7419	1.7419	170.67	170.67	1.2041	1.2041	-41.0	224.5
-101.0	2.7926	2.7926	180.3	180.3	2.6737	2.6737	201.5	201.5	2.2260	2.2260	223.9	223.9	1.7390	1.7390	172.66	172.66	1.2051	1.2051	-40.5	225.1
-100.0	3.2542	3.2542	183.3	183.3	2.7067	2.7067	202.9	202.9	2.2210	2.2210	226.1	226.1	1.7419	1.7419	174.19	174.19	1.2061	1.2061	-40.0	225.7
-99.5	3.4716	3.4716	185.0	185.0	2.7067	2.7067	204.2	204.2	2.2140	2.2140	228.2	228.2	1.7419	1.7419	175.78	175.78	1.2071	1.2071	-39.5	226.2
-99.0	3.6481	3.6481	186.8	186.8	2.7848	2.7848	205.6	205.6	2.2000	2.2000	229.9	229.9	1.7419	1.7419	177.29	177.29	1.2071	1.2071	-39.0	226.9
-98.5	3.3405	3.3405	188.6	188.6	2.8148	2.8148	207.0	207.0	2.1780	2.1780	230.1	230.1	1.7419	1.7419	178.82	178.82	1.2071	1.2071	-38.5	227.5
-98.0	4.0588	4.0588	190.6	190.6	2.8348	2.8348	208.4	208.4	2.1450	2.1450	231.8	231.8	1.7419	1.7419	180.36	180.36	1.2061	1.2061	-38.0	228.1
-97.5	4.2562	4.2562	192.7	192.7	2.8428	2.8428	209.8	209.8	2.1010	2.1010	233.1	233.1	1.7419	1.7419	181.91	181.91	1.2051	1.2051	-37.5	228.7
-97.0	4.5005	4.4991	194.9	194.9	2.8458	2.8489	211.4	211.4	2.0630	2.0899	234.1	234.1	1.7380	1.7380	183.46	183.46	1.2031	1.2031	-37.0	229.3
-96.5	4.7531	4.7517	197.2	197.2	2.8525	2.8559	212.8	212.8	2.0250	2.0514	235.5	235.5	1.7321	1.7321	185.01	185.01	1.2011	1.2011	-36.5	229.9
-96.0	4.9970	4.9955	199.6	199.6	2.8528	2.8559	214.2	214.2	1.9940	2.0200	236.9	236.9	1.7321	1.7321	186.56	186.56	1.1981	1.1981	-36.0	230.5
-95.5	5.2170	5.2154	202.2	202.2	2.8558	2.8589	215.6	215.6	1.9580	1.9835	238.2	238.2	1.7321	1.7321	188.11	188.11	1.1951	1.1951	-35.5	231.1
-95.0	5.3868	5.3852	204.8	204.8	2.8638	2.8670	217.1	217.1	1.9230	1.9481	239.5	239.5	1.7321	1.7321	189.66	189.66	1.1931	1.1931	-35.0	231.7
-94.5	5.4337	5.4321	207.5	207.5	2.8428	2.8459	218.5	218.5	1.8940	1.9187	240.8	240.8	1.7321	1.7321	191.21	191.21	1.1911	1.1911	-34.5	232.3
-94.0	5.4247	5.4231	210.2	210.2	2.8168	2.8199	219.9	219.9	1.8670	1.8914	242.1	242.1	1.7321	1.7321	192.76	192.76	1.1911	1.1911	-34.0	232.9
-93.5	5.4267	5.4251	213.0	213.0	2.7948	2.7979	221.3	221.3	1.8400	1.8640	243.4	243.4	1.7321	1.7321	194.31	194.31	1.1911	1.1911	-33.5	233.5
-93.0	5.4247	5.4231	215.7	215.7	2.7868	2.7898	222.7	222.7	1.8150	1.8387	244.7	244.7	1.7321	1.7321	195.86	195.86	1.1901	1.1901	-33.0	234.1
-92.5	5.4127	5.4111	218.4	218.4	2.7708	2.7738	224.1	224.1	1.7910	1.8144	246.0	246.0	1.7321	1.7321	197.41	197.41	1.1891	1.1891	-32.5	234.6
-92.0	5.3868	5.3852	221.1	221.1	2.7607	2.7637	225.4	225.4	1.7410	1.7637	247.3	247.3	1.7321	1.7321	198.96	198.96	1.1881	1.1881	-32.0	235.2
-91.5	5.1359	5.1344	223.7	223.7	2.6887	2.6916	226.8	226.8	1.6940	1.7161	248.6	248.6	1.7321	1.7321	200.51	200.51	1.1871	1.1871	-31.5	235.8
-91.0	4.8221	4.8207	226.2	226.2	2.6046	2.6074	228.1	228.1	1.6510	1.6725	249.9	249.9	1.7321	1.7321	202.06	202.06	1.1851	1.1851	-31.0	236.3
-90.5	4.5603	4.5589	228.6	228.6	2.4895	2.4922	230.7	230.7	1.6130	1.6340	251.2	251.2	1.7321	1.7321	203.61	203.61	1.1851	1.1851	-30.5	236.9
-90.0	4.2824	4.2811	230.8	230.8	2.4284	2.4311	233.1	233.1	1.5770	1.5976	252.5	252.5	1.7321	1.7321	205.16	205.16	1.1811	1.1811	-30.0	237.5
-89.0	3.5878	3.5867	234.7	234.7	2.3423	2.3449	234.5	234.5	1.5430	1.5631	253.8	253.8	1.7321	1.7321	206.71	206.71	1.1791	1.1791	-30.0	237.5
-88.0	3.1081	3.1072	238.1	238.1	2.2602	2.2627	237.8	237.8	1.5050	1.5246	255.1	255.1	1.7321	1.7321	208.26	208.26	1.1791	1.1791	-30.0	237.5
-87.0	2.7583	2.7575	241.0	241.0	2.1772	2.1796	240.0	240.0	1.4710	1.4902	256.4	256.4	1.7321	1.7321	209.81	209.81	1.1791	1.1791	-30.0	237.5
-86.0	2.5385	2.5377	243.6	243.6	2.0871	2.0894	242.2	242.2	1.4380	1.4568	257.7	257.7	1.7321	1.7321	211.36	211.36	1.1791	1.1791	-30.0	237.5
-85.0	2.3636	2.3629	246.1	246.1	2.0080	2.0102	244.2	244.2	1.4080	1.4264	259.0	259.0	1.7321	1.7321	212.91	212.91	1.1791	1.1791	-30.0	237.5
-84.0	2.1487	2.1481	248.3	248.3	1.9449	1.9470	246.2	246.2	1.4080	1.4264	260.3	260.3	1.7321	1.7321	214.46	214.46	1.1791	1.1791	-30.0	237.5
-83.0	2.0638	2.0632	250.4	250.4	1.8849	1.8870	248.1	248.1	1.4080	1.4264	261.6	261.6	1.7321	1.7321	216.01	216.01	1.1791	1.1791	-30.0	237.5
-82.0	2.0048	2.0042	252.5	252.5	1.8218	1.8238	249.9	249.9	1.4080	1.4264	262.9	262.9	1.7321	1.7321	217.56	217.56	1.1791	1.1791	-30.0	237.5

P = 800 psia (continued)

P = 1000 psia (continued)

Table XII. Thermodynamic Properties at the Pressures of Isobaric Determinations in the Regions of Rapid Changes (High  $(\partial C_p/\partial T)_p$ ) in Mixture 4 (Ternary)

$P = 1200$ psia				$P = 1500$ psia				$P = 2000$ psia			
temp, °F	$C_p(S)$ , Btu/ (lb °F)	$C_p(A)$ , Btu/ (lb °F)	$H(A)$ , Btu/lb	temp, °F	$C_p(S)$ , Btu/ (lb °F)	$C_p(A)$ , Btu/ (lb °F)	$H(A)$ , Btu/lb	temp, °F	$C_p(S)$ , Btu/ (lb °F)	$C_p(A)$ , Btu/ (lb °F)	$H(A)$ , Btu/lb
-45.0	1.595	1.578	214.99	-40.0	1.206	1.1971	206.79	-5.0	1.082	1.072	235.51
-44.5	1.608	1.591	215.78	-39.0	1.217	1.208	207.98	-4.5	1.083	1.073	236.04
-44.0	1.621	1.604	216.58	-38.0	1.227	1.218	209.17	-4.0	1.083	1.073	236.58
-43.5	1.635	1.618	217.38	-37.0	1.238	1.229	210.46	-3.5	1.084	1.074	237.12
-43.0	1.650	1.633	218.20	-36.0	1.249	1.240	211.65	-3.0	1.085	1.075	237.66
-42.5	1.665	1.647	219.02	-35.0	1.261	1.252	212.94	-2.5	1.086	1.076	239.19
-42.0	1.681	1.663	219.85	-34.0	1.271	1.262	214.14	-2.0	1.087	1.077	238.73
-41.5	1.698	1.680	220.68	-33.0	1.283	1.273	215.43	-1.5	1.088	1.078	238.27
-41.0	1.715	1.697	221.53	-32.0	1.295	1.285	216.72	-1.0	1.089	1.079	239.81
-40.5	1.732	1.714	222.38	-31.0	1.307	1.297	218.01	-0.5	1.089	1.079	240.35
-40.0	1.751	1.733	223.24	-30.0	1.319	1.309	219.30	0.0	1.090	1.080	240.89
-39.5	1.771	1.752	224.11	-29.0	1.331	1.321	220.69	0.5	1.091	1.081	241.43
-39.0	1.775	1.756	224.99	-28.0	1.344	1.334	221.98	1.0	1.092	1.082	241.97
-38.5	1.796	1.777	225.87	-27.0	1.357	1.347	223.27	1.5	1.092	1.082	242.51
-38.0	1.819	1.800	226.76	-26.0	1.358	1.348	224.66	2.0	1.093	1.083	243.05
-37.5	1.843	1.824	227.67	-25.0	1.359	1.349	225.95	2.5	1.094	1.084	243.59
-37.0	1.861	1.841	228.59	-24.0	1.375	1.365	227.34	3.0	1.095	1.085	244.14
-36.5	1.875	1.855	229.52	-23.0	1.393	1.383	228.73	3.5	1.096	1.086	244.68
-36.0	1.881	1.861	230.45	-22.0	1.412	1.402	230.12	4.0	1.096	1.086	245.23
-35.5	1.875	1.855	231.38	-21.0	1.429	1.418	231.51	4.5	1.097	1.087	245.77
-35.0	1.861	1.841	232.30	-20.0	1.450	1.439	233.00	5.0	1.098	1.088	246.31
-34.5	1.843	1.824	233.22	-19.5	1.459	1.448	233.69	5.5	1.099	1.089	246.85
-34.0	1.821	1.802	234.12	-19.0	1.468	1.457	234.38	6.0	1.100	1.090	247.40
-33.5	1.802	1.783	235.02	-18.5	1.476	1.465	235.08	6.5	1.101	1.091	247.95
-33.0	1.788	1.769	235.91	-18.0	1.484	1.473	235.87	7.0	1.101	1.091	248.50
-32.5	1.781	1.762	236.79	-17.5	1.491	1.480	236.57	7.5	1.100	1.090	249.04
-32.0	1.764	1.745	237.67	-17.0	1.497	1.486	237.36	8.0	1.099	1.089	249.58
-31.5	1.750	1.732	238.53	-16.5	1.502	1.491	238.06	8.5	1.097	1.087	250.13
-31.0	1.735	1.717	239.40	-16.0	1.506	1.495	238.85	9.0	1.095	1.085	250.67
-30.5	1.720	1.702	240.25	-15.5	1.510	1.499	239.55	9.5	1.094	1.084	251.22
-30.0	1.705	1.687	241.09	-15.0	1.513	1.502	240.34	10.0	1.093	1.083	251.75
-29.5	1.690	1.672	241.93	-14.5	1.514	1.503	241.03	10.5	1.091	1.081	252.29
-29.0	1.676	1.658	242.77	-14.0	1.514	1.503	241.83	11.0	1.090	1.080	252.83
-28.5	1.662	1.644	243.60	-13.5	1.513	1.502	242.62	11.5	1.089	1.079	253.37
-28.0	1.648	1.631	244.42	-13.0	1.512	1.501	243.32	12.0	1.088	1.078	253.91
-27.5	1.635	1.618	245.23	-12.5	1.511	1.500	244.11	12.5	1.088	1.078	254.45
-27.0	1.623	1.606	246.03	-12.0	1.510	1.499	244.81	13.0	1.087	1.077	245.99
-26.5	1.612	1.595	246.83	-11.5	1.504	1.493	245.60	13.5	1.086	1.076	255.53
-26.0	1.602	1.585	247.62	-11.0	1.493	1.482	246.30	14.0	1.085	1.075	256.07
-25.5	1.591	1.574	248.41	-10.5	1.474	1.463	247.09	14.5	1.084	1.074	256.60
-25.0	1.580	1.563	249.21	-10.0	1.445	1.434	247.79	15.0	1.083	1.073	257.14
				-9.5	1.405	1.395	248.48				
				-9.0	1.400	1.390	249.17				
				-8.5	1.377	1.367	249.87				
				-8.0	1.357	1.347	250.56				
				-7.5	1.340	1.330	251.26				
				-7.0	1.327	1.317	251.85				
				-6.5	1.318	1.308	252.55				
				-6.0	1.353	1.343	253.24				
				-5.5	1.344	1.334	253.84				
				-5.0	1.336	1.326	254.53				
				-4.5	1.328	1.318	255.23				
				-4.0	1.320	1.310	255.82				
				-3.5	1.312	1.302	256.52				
				-3.0	1.305	1.295	257.11				
				-2.5	1.298	1.288	257.81				
				-2.0	1.291	1.281	258.40				
				-1.5	1.285	1.275	259.10				
				-1.0	1.279	1.270	259.70				
				-0.5	1.273	1.264	260.39				
				0.0	1.268	1.259	260.99				
				1.0	1.258	1.249	262.28				
				2.0	1.248	1.255	263.49				
				3.0	1.238	1.245	264.79				
				4.0	1.230	1.237	266.00				
				5.0	1.222	1.229	267.21				
				6.0	1.212	1.218	268.41				
				7.0	1.203	1.209	269.62				
				8.0	1.189	1.195	270.83				
				9.0	1.179	1.185	272.03				
				10.0	1.170	1.176	273.23				

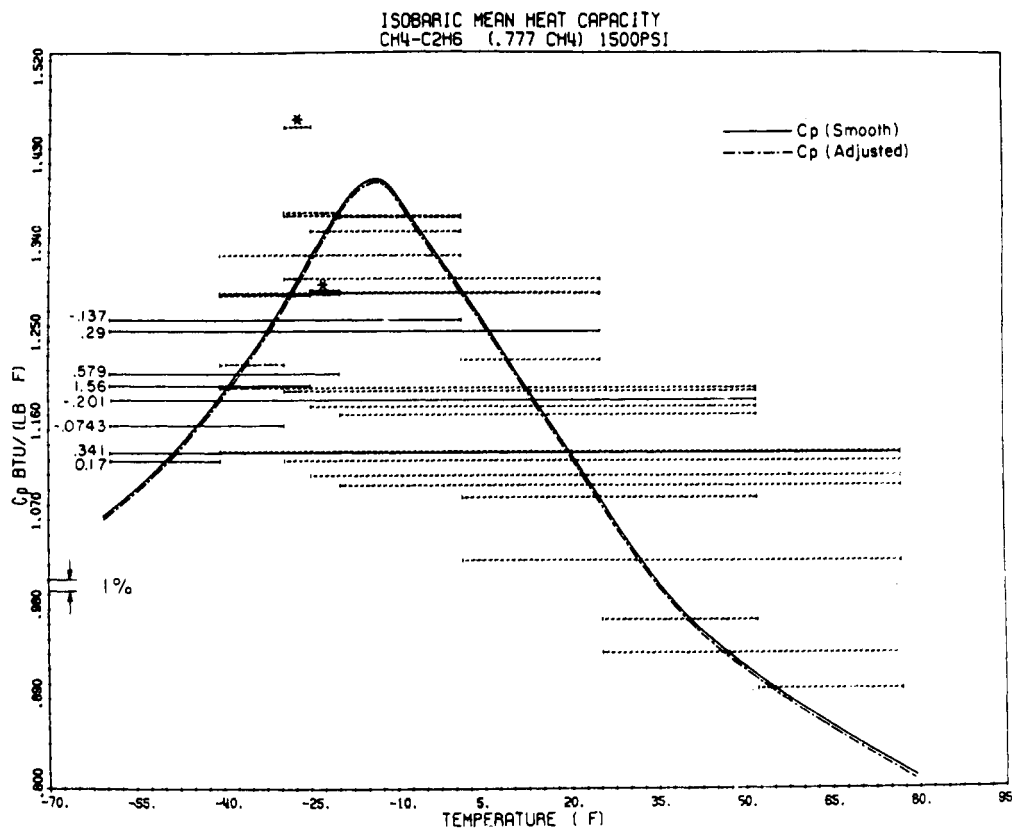


Figure 5. Isobaric heat capacity curve for a 22.3 mol % ethane in methane mixture at 1500 psia.

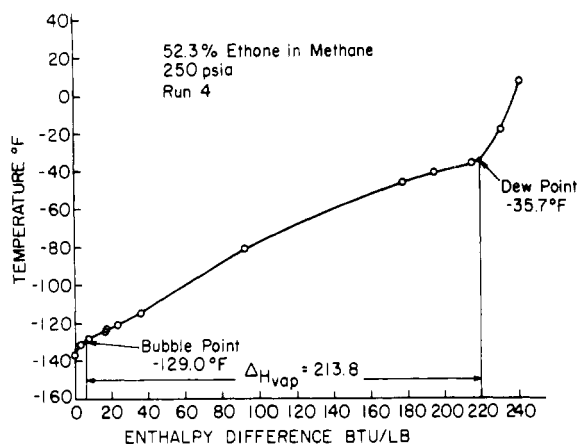


Figure 6. Isobaric enthalpy traverse through the two-phase region at 250 psia for a 52.3 mol % ethane in methane mixture.

**Smoothing of Normalized Calorimetric Data.** The isobaric, isothermal, and isenthalpic data obtained in the single-phase region were analyzed to yield values of the derivative functions  $C_p \equiv (\partial H/\partial T)_p$ ,  $\phi \equiv (\partial H/\partial P)_T$ , and  $\mu \equiv (\partial T/\partial P)_H$ , respectively. In this process it is a relatively easy matter to identify individual points with considerably greater than average experimental error and therefore the smoothed values are probably of improved accuracy compared to the individual data points. Integration of the smoothed derivative functions yield provisional values of enthalpy differences which must then be checked for thermodynamic consistency.

Data taken within and near the two-phase region are generally not interpreted in terms of derivative functions but are merely smoothed graphically to yield values of enthalpy differences in this important region.

Details of the analyses have been presented elsewhere (38). Brief summaries of the procedures employed are given below.

**Isobaric Data. Single Phase.** The normalized and corrected

Table XIII. Empirical Data Obtained from Interpretation of Isobaric Enthalpy Traverses

mixture no.	pressure, psia	bubble point, °F	dew point, °F	$\Delta H_{vap}$ , Btu/lb
1. (52.3% C <sub>2</sub> )	250	-129.0	-35.7	213.80
	500	-76.5	2.7	173.40
	750	-33.25	14.2	102.30
2. (22.3% C <sub>2</sub> )	250	-154.2	-77.2	204.2
	500	-112.5	-46.8	166.5
3. (5.55% C <sub>2</sub> )	250	-168 <sup>a</sup>		
	500	-127.5 <sup>a</sup>	-112 <sup>a</sup>	113 <sup>a</sup>
	700	-102 <sup>a</sup>	-98 <sup>a</sup>	59 <sup>a</sup>
4. (ternary)	250	-159.5	-48 <sup>a</sup>	227 <sup>a</sup>
	500	-119	-40 <sup>a</sup>	168 <sup>a</sup>
	750	-89		
	1000	-67 <sup>a</sup>		

<sup>a</sup> Not well defined by the data.

values of isobaric differences in enthalpy and temperature were used to calculate mean values of  $\hat{C}_p$ .

$$\hat{C}_p \equiv \frac{[H_{T_k} - H_{T_j}]_p}{T_k - T_j} \quad (3)$$

Values thus calculated apply over the temperature interval  $T_j \rightarrow T_k$  and are plotted as solid horizontal lines as illustrated on Figure 5. Prior adjustment of  $T_j$  to an average value for any isobaric set of runs permits calculation of additional isobaric enthalpy differences and therefore additional values of  $\hat{C}_p$ . Typical values obtained by difference are plotted as dashed horizontal lines in Figure 5.

Point values of the derivative function,  $C_p$ , are determined to satisfy the constraint

$$[H_{T_k} - H_{T_j}]_p = \int_{T_j}^{T_k} C_p dT_p \quad (4)$$

i.e., "equal area" requirements were met. Computer-aided graphical procedures were used as described in detail elsewhere

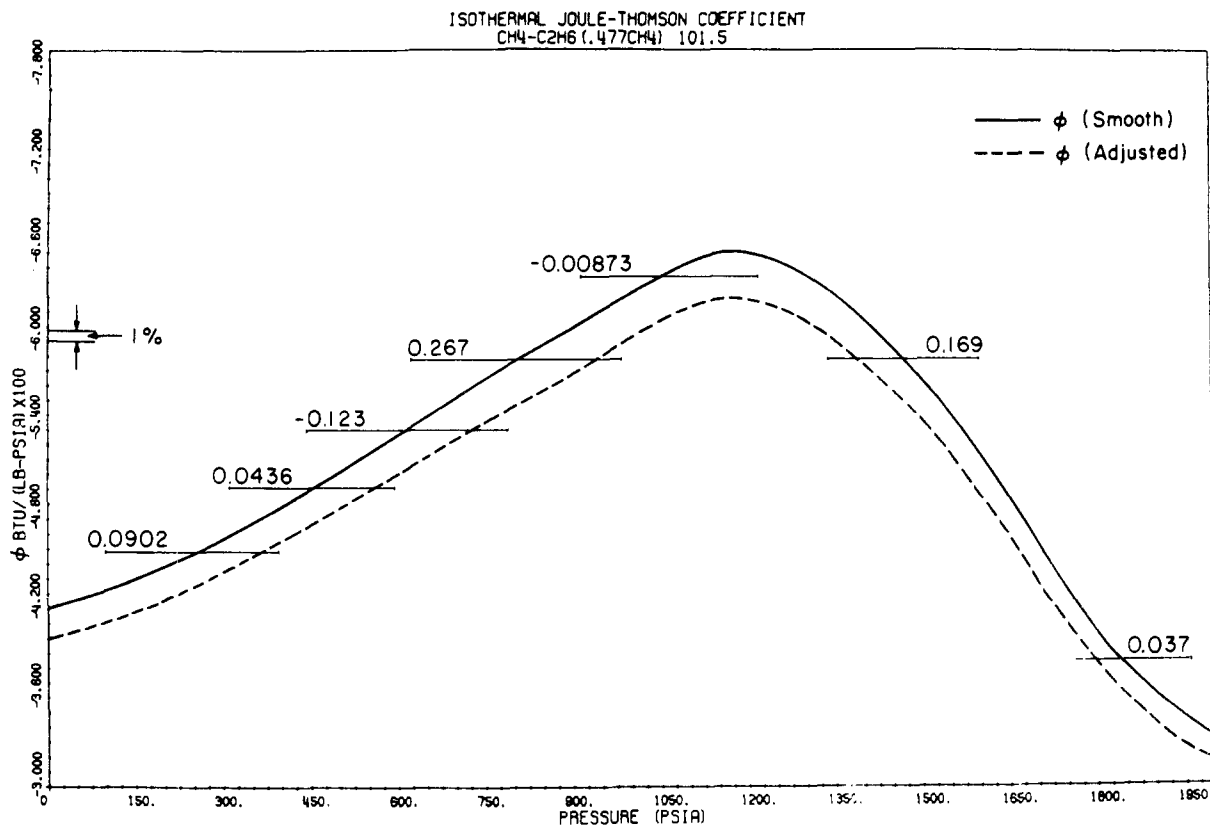


Figure 7. Isothermal throttling coefficient for a 52.3 mol % ethane in methane mixture at 101.5 °F.

(8). After each trial curve for  $C_p = f(T)$  was established, integration of eq 4 was carried out over the temperature interval of each individual data point and difference point. The integration was carried out by computer using the Gauss-Legendre technique. Values of percentage error are listed on Figure 5 for each of the original data points used to generate the curve. One point has an indicated error of 1.56%. Note also that several values of  $\hat{C}_p$  obtained by differences involving this point (indicated by asterisks) deviate markedly from the curve. It was thus concluded that this point was in error and it was given little weight in determining the final curve.

All isobaric data obtained in the single phase were interpreted in this way. The values of  $C_p$  so obtained are reported as  $C_p(S)$  (for smoothed) in Tables V-XII. In general, the differences between the experimental data and values calculated by numerical integration of the smoothed values of  $C_p$  showed random variation in sign and agreement was on the order of  $\pm 0.2\%$  or better.

The smoothed values of  $C_p(T)$  were also integrated to obtain isobaric enthalpy differences between temperatures of the experimental isothermal determinations. These differences were used in checking the thermodynamic consistency of the data as described subsequently.

**Two Phase (Enthalpy Traverse).** The calorimetric determinations within and through the two-phase region were obtained with a constant inlet temperature. Plots of temperature vs. enthalpy difference were made as illustrated in Figure 6.

Interpretation of such plots yielded not only smoothed values of enthalpy within and near the two-phase region but also the isobaric heat of vaporization and values of the bubble and dew points (Table XIII).

**Isothermal Data.** Interpretation of the isothermal data to yield smooth values of  $\hat{\phi}$  is very similar to the interpretation of the isobaric data. Figure 7 is a plot of

$$\hat{\phi} = \frac{[H_{P_k} - H_{P_j}]_T}{P_k - P_j} \quad (5)$$

as represented by horizontal lines extending over the experimentally measured pressure interval. The solid curve results from use of an iterative, computer-aided, graphical-numerical procedure described elsewhere (8). Percentage deviations between the experimental data and values calculated by Gauss-Legendre integration of  $\phi$

$$[H_{P_k} - H_{P_j}]_T = \int_{P_j}^{P_k} \phi \, dP_T \quad (6)$$

are presented as applicable for the individual points on the figure.

The lower limit of pressure which could be attained in the course of isothermal experiments was about 100 psia. At lower pressures, values of  $\phi(P)$  in the gas phase were estimated by several prediction methods (8) and used together with the experimental values to produce a smoothed curve extending the calorimetric data down to zero pressure. Thus the curve drawn on Figure 7 between 0 and 350 psia is in good agreement with the experimental data between 100 and 350 psia (0.09% deviation) and is of a shape in agreement with predictions made at low pressures. Several isothermal runs were made completely in the liquid region, i.e., at low temperatures above the two-phase region as indicated in Figures 1-4.

All isothermal data were interpreted in the manner described above and illustrated in Figure 7. The values of  $\phi$  so obtained are reported as  $\phi(S)$  in Tables XIV-XIX.

The numerical integration procedure was applied to yield values of isothermal enthalpy differences between the pressures of isobaric determinations for use together with similar isobaric integrations to check the thermodynamic consistency of the data.

**Ienthalpic Data.** Ienthalpic determinations were made with no energy added to the calorimeter when a drop in pressure through the calorimeter resulted in an increase in temperature of the flowing fluid. Experimental constraints did not permit isenthalpic determinations to be made from the highest to the lowest pressure. Instead, one run consisted of a series of relatively small pressure drops made with the same inlet







Table XVI. Thermodynamic Properties at the Temperatures of Isothermal and Isenthalpic Determinations. Binary Mixture Containing Approximately 5.5 mole % Ethane in Methane

pressure, psia	$T = -242.0^{\circ}\text{F}$		$T = -150.0^{\circ}\text{F}$		$T = -97.0^{\circ}\text{F}$		
	$\phi \times 10^4$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb	$\phi \times 10^4$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb	$-\phi(\text{S}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb
0.0					6.067	5.704	319.4
50.0					6.438	6.053	316.4
100.0	43.75	38.2			6.810	6.403	313.3
150.0					7.200	6.770	310.0
200.0	38.40	37.8			7.625	7.169	306.6
250.0					8.100	7.616	302.8
300.0	33.30	37.4			8.640	8.123	298.9
350.0					9.437	8.872	294.7
400.0	28.70	37.1			10.400	9.778	290.0
450.0					11.530	10.840	284.9
500.0	24.25	36.8	-35.50	115.5	12.970	12.194	279.1
550.0					15.370		272.1
600.0	19.90	36.6	-28.00	115.2	20.420		263.4
650.0					34.400		249.7
700.0	16.00	34.4	-20.00	115.0	42.230		230.0
750.0					41.840		208.8
800.0	12.20	36.3	-17.20	114.8	30.320	30.32	194.9
850.0					15.130	13.57	184.8
900.0	9.00	36.2	-14.2	114.6	7.360	6.60	180.0
950.0					4.780	4.29	177.5
1000.0	5.80	36.0	-11.8	114.5	3.440	3.09	175.6
1050.0					2.800	2.7440	174.1
1100.0	3.20	36.1	-8.8	114.4	2.420	2.3716	172.8
1150.0					2.1600	2.1168	171.7
1200.0	1.00	36.0	-6.6	114.3	1.8800	1.8424	170.7
1250.0					1.6610	1.7015	169.8
1300.0	-1.00	36.0	-4.0	114.2	1.4800	1.5161	169.0
1350.0					1.3480	1.3809	168.3
1400.0	-2.80	36.1	-1.4	114.2	1.2400	1.2702	167.6
1450.0					1.1330	1.1606	167.0
1500.0	-4.00	36.0	1.0	114.2	1.0300	1.055	166.5
1550.0					0.9210	0.8652	166.0
1600.0	-4.50	36.0	2.8	114.2	0.8220	0.7722	165.6
1650.0					0.7486	0.7032	165.3
1700.0	-5.00	36.1	5.0	114.3	0.6900	0.6482	164.9
1750.0					0.6430	0.6040	164.6
1800.0	-5.50	36.2	7.7	114.3	0.6000	0.5636	164.3
1850.0					0.5498	0.5165	164.0
1900.0	-5.80	36.3	9.0	114.4	0.5000	0.4697	163.8
1950.0					0.4534	0.4259	163.5
2000.0	-5.90	36.4	11.0	114.5	0.4130	0.3880	163.4

pressure, psia	$T = -47.0^{\circ}\text{F}$			$T = 79.0^{\circ}\text{F}$		
	$-\phi(\text{S}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H(\text{A})$ , Btu/lb	$-\phi(\text{S}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H(\text{A})$ , Btu/lb
0.0	4.828	4.568	343.7	2.944	2.768	407.2
50.0	4.953	4.686	341.4	2.968	2.791	405.8
100.0	5.100	4.825	339.0	2.995	2.816	404.4
150.0	5.266	4.982	336.6	3.024	2.843	403.0
200.0	5.451	5.157	334.0	3.055	2.872	401.6
250.0	5.650	5.346	331.4	3.088	2.903	400.1
300.0	5.853	5.503	328.7	3.124	2.937	398.7
350.0	6.075	5.712	325.9	3.161	2.971	397.2
400.0	6.320	5.942	323.0	3.199	3.007	395.7
450.0	6.606	6.211	320.0	3.239	3.045	394.2
500.0	6.900	6.488	316.8	3.277	3.080	392.7
550.0	7.169	6.737	313.49	3.307	3.109	391.1
600.0	7.450	7.002	310.1	3.333	3.133	389.6
650.0	7.772	7.304	306.5	3.354	3.153	388.0
700.0	8.130	7.641	302.8	3.371	3.169	386.4
750.0	8.541	8.021	298.9	3.387	3.184	384.8
800.0	8.970	8.424	294.7	3.401	3.197	383.2
850.0	9.378	8.814	290.4	3.413	3.208	381.6
900.0	9.800	9.211	285.9	3.422	3.217	380.0
950.0	10.250	9.634	281.2	3.430	3.224	378.4
1000.0	10.620	9.981	276.3	3.435	3.229	376.8
1050.0	10.810	10.161	271.2	3.438	3.231	375.2
1100.0	10.880	10.227	266.2	3.438	3.231	373.6
1150.0	10.750	10.104	261.0	3.436	3.230	372.0
1200.0	10.290	9.672	256.1	3.432	3.225	370.4
1250.0	9.610	8.896	251.5	3.424	3.217	368.8
1300.0	8.940	8.275	247.2	3.413	3.207	367.2

Table XVI (Continued)

pressure, psia	$T = -47.0^\circ\text{F}$			$T = 79.0^\circ\text{F}$		
	$-\phi(\text{S}) \times 10^2,$ Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2,$ Btu/(lb in. <sup>-2</sup> )	$H(\text{A}),$ Btu/lb	$-\phi(\text{S}) \times 10^2,$ Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2,$ Btu/(lb in. <sup>-2</sup> )	$H(\text{A}),$ Btu/lb
1350.0	8.227	7.615	243.2	3.401	3.195	365.6
1400.0	7.420	6.868	239.6	3.381	3.176	364.1
1450.0	6.566	6.078	236.3	3.357	3.154	362.5
1500.0	5.740	5.313	233.6	3.331	3.129	360.9
1550.0	5.042	4.751	231.0	3.300	3.100	359.4
1600.0	4.450	4.193	228.8	3.266	3.067	357.9
1650.0	3.970	3.741	226.8	3.232	3.036	356.4
1700.0	3.567	3.361	225.0	3.198	3.004	354.9
1750.0	3.225	3.039	223.4	3.163	2.971	353.4
1800.0	2.930	2.761	222.0	3.128	2.938	351.9
1850.0	2.688	2.533	220.6	3.092	2.904	350.5
1900.0	2.480	2.337	219.4	3.055	2.870	349.1
1950.0	2.292	2.160	218.3	3.017	2.834	347.6
2000.0	2.110	1.988	217.3	2.977	2.796	346.3

Table XVII. Thermodynamic Properties at the Temperatures of Isothermal and Isenthalpic Determinations. Ternary Mixture Containing Methane, Ethane, and Propane

pressure, psia	$T = -150.0^\circ\text{F}$		$T = -47.0^\circ\text{F}$			$T = 1.5^\circ\text{F}$			$T = 158.5^\circ\text{F}$		
	$10^4 \phi,$ Btu/ in. <sup>-2</sup> )	$H,$ Btu/lb	$\phi(\text{S}),$ Btu/ (lb in. <sup>-2</sup> )	$\phi(\text{A}),$ Btu/ (lb in. <sup>-2</sup> )	$H,$ Btu/lb	$\phi(\text{S}),$ Btu/ (lb in. <sup>-2</sup> )	$\phi(\text{A}),$ Btu/ (lb in. <sup>-2</sup> )	$H,$ Btu/lb	$\phi(\text{S}),$ Btu/ (lb in. <sup>-2</sup> )	$\phi(\text{A}),$ Btu/ (lb in. <sup>-2</sup> )	$H,$ Btu/lb
0.0						-0.0442	-0.04256	358.4	-0.02630	-0.0254	436.90
50.0						-0.04593	-0.04422	356.23	-0.02665	-0.02571	435.62
100.0						-0.04754	-0.04577	353.98	-0.02696	-0.02600	434.33
150.0						-0.04907	-0.04724	351.65	-0.02724	-0.02627	433.02
200.0						-0.05054	-0.04866	349.26	-0.02749	-0.02652	431.70
250.0						-0.05200	-0.05006	346.79	-0.02773	-0.02675	430.37
300.0						-0.05347	-0.05148	344.25	-0.02796	-0.02697	429.03
350.0						-0.05496	-0.05291	341.64	-0.02819	-0.02719	427.67
400.0	3.68	102.29				-0.05660	-0.05449	338.95	-0.02835	-0.02734	426.31
450.0						-0.05835	-0.05618	336.19	-0.02848	-0.02747	424.94
500.0	6.32	102.34				-0.06020	-0.05796	333.34	-0.02859	-0.02758	423.56
550.0						-0.06216	-0.05915	330.28	-0.02870	-0.02922	422.10
600.0	8.85	102.42				-0.0642	-0.06109	327.42	-0.02874	-0.02926	420.65
650.0						-0.06629	-0.06308	324.32	-0.02873	-0.02925	419.18
700.0	10.94	102.51				-0.06840	-0.06509	321.11	-0.02869	-0.02921	417.72
750.0						-0.07050	-0.06867	317.81	-0.02866	-0.02918	416.26
800.0	12.68	102.63				-0.07256	-0.07067	314.32	-0.02860	-0.02912	414.80
850.0						-0.07454	-0.07260	310.74	-0.02853	-0.02905	413.35
900.0	14.20	102.77				-0.07640	-0.07441	307.07	-0.02845	-0.02897	411.89
950.0						-0.07810	-0.07607	303.31	-0.02835	-0.02886	410.46
1000.0	15.60	102.92				-0.07960	-0.07753	299.46	-0.02825	-0.02876	409.01
1050.0						-0.08000	-0.07723	295.61	-0.02814	-0.02865	407.57
1100.0	16.88	103.08				-0.07980	-0.07703	291.75	-0.02802	-0.02853	406.15
1150.0						-0.07887	-0.07613	287.91	-0.02789	-0.02840	404.72
1200.0	18.10	103.25				-0.07710	-0.07443	284.15	-0.02776	-0.02826	403.31
1250.0			-0.05100	-0.06179	208.85	-0.07504	-0.07626	280.28	-0.02762	-0.02812	401.89
1300.0	19.28	103.44	-0.04140	-0.05016	206.07	-0.07280	-0.07399	276.53	-0.02748	-0.02798	400.50
1350.0			-0.03460	-0.04192	206.96	-0.07008	-0.07122	272.89	-0.02732	-0.02782	399.10
1400.0	20.50	103.64	-0.03000	-0.03635	201.83	-0.06700	-0.06809	269.40	-0.02714	-0.02763	397.71
1450.0			-0.02620	-0.03174	200.13	-0.06343	-0.06446	266.09	-0.02695	-0.02744	396.33
1500.0	21.60	103.85	-0.02280	-0.02280	198.65	-0.05980	-0.06078	262.96	-0.02674	-0.02723	394.97
1550.0			-0.01990	-0.01990	197.59	-0.05609	-0.05568	260.08	-0.02653		393.64
1600.0	22.76	104.07	-0.01757	-0.01757	196.65	-0.05227	-0.05189	257.40	-0.02630		392.32
1650.0			-0.01590	-0.01590	195.81	-0.04840	-0.04805	254.92	-0.02607		391.01
1700.0	23.96	104.31	-0.01452	-0.01452	195.06	-0.04450	-0.04418	252.64	-0.02583		389.71
1750.0			-0.01335	-0.01335	194.36	-0.04059	-0.04029	250.45	-0.02558		388.42
1800.0	25.16	104.55	-0.01216	-0.01216	193.72	-0.03680	-0.03653	248.57	-0.02533		387.15
1850.0			-0.01105	-0.01105	193.14	-0.03342	-0.03318	246.78	-0.02508		385.89
1900.0	26.35	104.81	-0.01005	-0.01005	192.61	-0.03027	-0.03005	245.19	-0.02484		384.64
1950.0			-0.00915	-0.00915	192.13	-0.02732	-0.02712	243.80	-0.02460		383.41
2000.0	27.60	105.08	-0.00836	-0.00836	191.70	-0.02450	-0.02432	242.51	-0.02436		382.18

temperature. These data, when used in conjunction with results of isobaric experiments, permitted rigorous calculation of isothermal enthalpy changes over the same pressure interval as explained in detail elsewhere (34). These isothermal values were analyzed as described in the preceding section to yield smoothed values of  $\phi(\text{S})$ . These values together with  $C_p(\text{S})$  values yielded  $\mu(\text{S})$  according to the rigorous relation

$$\mu = -\phi / C_p \quad (7)$$

The values thus calculated are included in the skeleton tables where applicable.

**Adjustment to Ensure Thermodynamic Consistency.** The individual enthalpy differences calculated by numerical integration of smoothed values of  $C_p$  and  $\phi$  obtained as described in the

Table XVIII. Thermodynamic Properties at the Temperatures of Isothermal Determinations, in the Regions of Rapid Change (High  $(\partial\phi/\mu\rho)\tau$ ) for Mixture 3 (5.55% C<sub>2</sub>)

$T = -47.0^\circ\text{F}$				$T = 79^\circ\text{F}$			
pressure, psia	$-\phi(S) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(A) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb	pressure, psia	$-\phi(S) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(A) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb
900.0	9.800	9.211	285.9	1000.0	3.435	3.229	376.8
910.0	9.891	9.296	285.0	1010.0	3.436	3.229	376.5
920.0	9.983	9.383	284.0	1020.0	3.436	3.229	376.2
930.0	10.070	9.464	283.1	1030.0	3.437	3.230	375.8
940.0	10.160	9.549	282.2	1040.0	3.438	3.231	375.5
950.0	10.250	9.634	281.2	1050.0	3.438	3.231	375.2
960.0	10.330	9.709	280.2	1060.0	3.438	3.231	374.9
970.0	10.410	9.784	279.2	1070.0	3.438	3.231	374.6
980.0	10.500	9.869	278.3	1080.0	3.438	3.231	374.2
990.0	10.560	9.925	277.3	1090.0	3.438	3.231	373.9
1000.0	10.620	9.981	276.3	1100.0	3.438	3.231	373.6
1010.0	10.670	10.029	275.3	1110.0	3.438	3.231	373.2
1020.0	10.710	10.067	274.3	1120.0	3.437	3.230	373.0
1030.0	10.750	10.104	273.3	1130.0	3.437	3.230	372.6
1040.0	10.780	10.133	272.3	1140.0	3.437	3.230	372.3
1050.0	10.810	10.161	271.2	1150.0	3.436	3.229	372.0
1060.0	10.840	10.189	270.2	1160.0	3.435	3.228	371.6
1070.0	10.860	10.208	269.2	1170.0	3.435	3.228	371.3
1080.0	10.880	10.227	268.2	1180.0	3.434	3.227	371.0
1090.0	10.880	10.227	267.2	1190.0	3.433	3.226	370.7
1100.0	10.880	10.227	266.2	1200.0	3.432	3.225	370.4
1110.0	10.870	10.217	265.1				
1120.0	10.850	10.198	264.1				
1130.0	10.830	10.180	263.1				
1140.0	10.790	10.142	262.1				
1150.0	10.750	10.104	261.0				
1160.0	10.690	10.048	260.0				
1170.0	10.610	9.973	260.0				
1180.0	10.520	9.888	258.1				
1190.0	10.410	9.785	257.1				
1200.0	10.290	9.672	256.1				

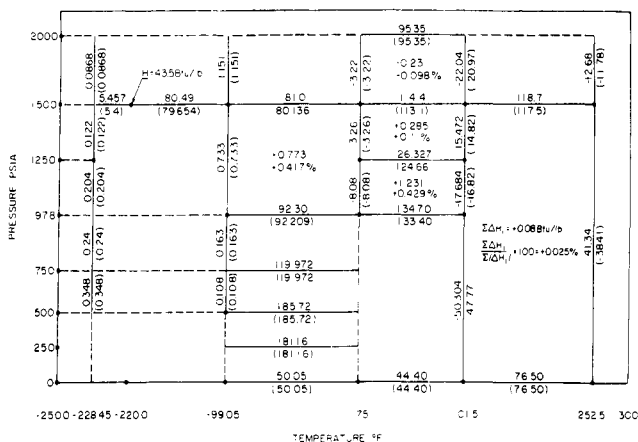


Figure 8. Summary of consistency checks, 52.3 mol % ethane in methane mixture.

preceding section are summarized on  $P-T$  diagrams as Figures 8–11. These values are represented by numbers that are not included in parentheses.

Enthalpy is a point function of state and therefore these independently determined values of differences in enthalpy can be tested against the rigorous thermodynamic requirement that the sum of all differences around a closed loop must equal zero, theoretically. Practically, the values of the actual sums (taken in the clockwise direction with proper attention to sign),  $\sum \Delta H_i$ , and the percentage deviations,

$$\text{percentage deviation} \equiv \frac{\sum \Delta H_i}{\sum |\Delta H_i|} \times 100 \quad (8)$$

provide a quantitative measure of the internal thermodynamic consistency of the smoothed data and are included within each

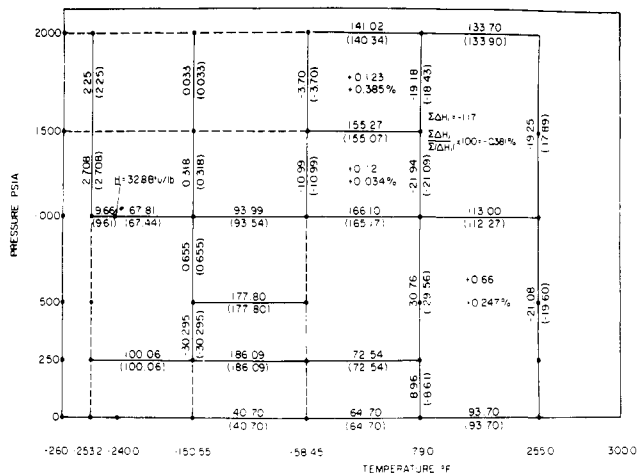


Figure 9. Summary of consistency checks, 22.3 mol % ethane in methane mixture.

closed loop. Consideration of the values presented in Figures 8–11 reveals that the data are indeed self-consistent to about 1.0% in most cases.

Unfortunately, this important consistency check does not eliminate the possibility of experimental error. For example, if the flow determinations for all runs are in error by a constant percentage, all experimental results will incorporate this same percentage error and the results will be thermodynamically consistent but inaccurate. As mentioned previously, leaks were found in the system after completion of the investigation. Note that it is highly improbable to have leaks of the same percentage of flow for both isobaric and isothermal determinations because two different calorimeters were used. Nevertheless, it was decided to make additional adjustments to ensure not only internal thermodynamic consistency but also agreement with

Table XIX. Thermodynamic Properties at the Temperatures of Isothermal Determinations, in the Regions of Rapid Change (High  $(\partial\phi/\mu\rho)_T$ ) for Mixture 4 (Ternary)

$T = 158.5^\circ\text{F}$				$T = 1.5^\circ\text{F}$			
pressure, psia	$-\phi(\text{S}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb	pressure, psia	$-\phi(\text{S}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$-\phi(\text{A}) \times 10^2$ , Btu/(lb in. <sup>-2</sup> )	$H$ , Btu/lb
900.0	7.640	7.441	307.07	400.0	2.835	2.734	426.31
910.0	7.675	7.475	306.32	410.0	2.838	2.737	426.04
920.0	7.710	7.509	305.57	420.0	2.841	2.740	425.76
930.0	7.744	7.543	304.82	430.0	2.843	2.742	425.49
940.0	7.777	7.575	304.07	440.0	2.846	2.745	425.22
950.0	7.810	7.607	303.31	450.0	2.848	2.747	424.94
960.0	7.844	7.640	302.54	460.0	2.850	2.749	424.67
970.0	7.877	7.672	302.07	470.0	2.853	2.752	424.39
980.0	7.908	7.702	301.01	480.0	2.855	2.754	424.12
990.0	7.936	7.730	300.24	490.0	2.857	2.756	423.84
1000.0	7.960	7.753	299.46	500.0	2.859	2.758	423.56
1010.0	7.975	7.698	298.69	510.0	2.861	2.913	423.27
1020.0	7.986	7.709	297.93	520.0	2.864	2.916	422.99
1030.0	7.994	7.717	297.15	530.0	2.866	2.918	422.69
1040.0	7.998	7.721	296.38	540.0	2.868	2.920	422.40
1050.0	8.000	7.723	295.61	550.0	2.870	2.922	422.10
1060.0	8.001	7.724	294.84	560.0	2.871	2.923	421.81
1070.0	8.000	7.723	294.06	570.0	2.872	2.924	421.52
1080.0	7.996	7.719	293.29	580.0	2.873	2.925	421.28
1090.0	7.989	7.712	292.52	590.0	2.874	2.926	420.93
1100.0	7.980	7.703	291.75	600.0	2.874	2.926	420.65
1110.0	9.968	7.692	290.97	610.0	2.874	2.926	420.35
1120.0	7.952	7.676	290.21	620.0	2.874	2.926	420.06
1130.0	7.934	7.659	289.44	630.0	2.874	2.926	419.76
1140.0	7.912	7.638	288.68	640.0	2.874	2.926	419.48
1150.0	7.887	7.613	287.91	650.0	2.873	2.925	419.18
1160.0	7.857	7.585	287.15	660.0	2.872	2.924	418.89
1170.0	7.823	7.552	286.40	670.0	2.872	2.924	418.59
1180.0	7.787	7.517	285.65	680.0	2.871	2.923	418.31
1190.0	7.749	7.480	284.89	690.0	2.870	2.922	418.01
1200.0	7.710	7.443	284.15	700.0	2.869	2.921	417.72
1210.0	7.671	7.796	283.37	710.0	2.868	2.920	417.43
1220.0	7.630	7.754	282.58	720.0	2.868	2.920	417.14
1230.0	7.589	7.713	281.81	730.0	2.867	2.919	416.84
1240.0	7.547	7.670	281.05	740.0	2.867	2.919	416.56
1250.0	7.504	7.626	280.28	750.0	2.866	2.918	416.26
1260.0	7.462	7.584	279.53	760.0	2.865	2.917	415.96
1270.0	7.418	7.539	278.76	770.0	2.864	2.916	415.68
1280.0	7.374	7.494	278.01	780.0	2.863	2.915	415.38
1290.0	7.328	7.448	277.27	790.0	2.861	2.913	415.09
1300.0	7.280	7.399	276.53	800.0	2.860	2.912	414.80
				810.0	2.859	2.911	414.51
				820.0	2.857	2.909	414.22
				830.0	2.856	2.908	413.92
				840.0	2.854	2.905	413.63
				850.0	2.853	2.905	412.35
				860.0	2.852	2.904	413.05
				870.0	2.850	2.902	412.77
				880.0	2.848	2.900	412.47
				890.0	2.847	2.899	412.19
				900.0	2.845	2.897	411.89

other published data of acceptable accuracy.

**Utilization of Published Data.** As discussed under the section entitled, Selection of Bases and Use of Other Published Data, accurate data for pure methane (11, 33), ethane (8), and propane (33, 36) were used to establish enthalpy values for the mixture in the gaseous state at zero pressure as listed in Table III. Similarly, estimates of the excess enthalpy of mixing of liquid methane, ethane, and propane served to establish enthalpy values for one set of conditions in the liquid region for each binary and ternary mixture as summarized in Table IV. These "check points" serve to establish values of enthalpy differences for comparison with the experimentally obtained values. The comparisons are summarized in Table XX. The discrepancies [up to 6.7 Btu/lb (1.5%) in one case] are much larger than had been expected as similar comparisons made with other data (3, 8, 15, 33-37) had yielded remarkable agreement. Therefore, it was decided to adjust all values in accordance with several goals and limitations: (1) obtain

agreement with the values of enthalpy differences between pairs of check points based on other published data (Table XX); (2) utilize estimates of the isothermal effect of pressure on enthalpy based on volumetric data at high temperatures where such estimations have proven to be accurate (8); (3) make adjustments in the derivative functions  $C_p$  and  $\phi$  such that integration yields thermodynamic consistency. Further, these adjustments should not be excessive, i.e., in keeping with corrections made for similar determinations on the same equipment.

With the exception that it was necessary to make corrections to both the isobaric and isothermal data somewhat in excess of those applied in the analysis of data for similar systems, it was possible to satisfy all other conditions by a laborious trial-and-error procedure. The resulting thermodynamically consistent values of enthalpy differences are listed in parentheses on Figures 8-11. In some cases, it was necessary to make adjustments to isothermal determinations by as much

Table XX. Comparison of Enthalpy Differences as Estimated from Published Data (Tables III and IV) with Those Determined from Calorimetric Measurements

	mixture no.							
	1 (52.3% C <sub>2</sub> )		2 (22.3% C <sub>2</sub> )		3 (5.55% C <sub>2</sub> )		4 (ternary)	
	°F	psia	°F	psia	°F	psia	°F	psia
pairs of check points	252.5	0	255	0	79	0	158.5	0
	-220	1500	-240	1000	-242	1000	-243	1500
enthalpy diff	Btu/lb		Btu/lb		Btu/lb		Btu/lb	
published data	429.2		458.7		373.0		404.9	
exptl value	435.9		462.0		371.1		402.9	
diff %	-6.7 (1.5)		-3.3 (0.7)		+1.9 (0.5)		+2.0 (0.5)	

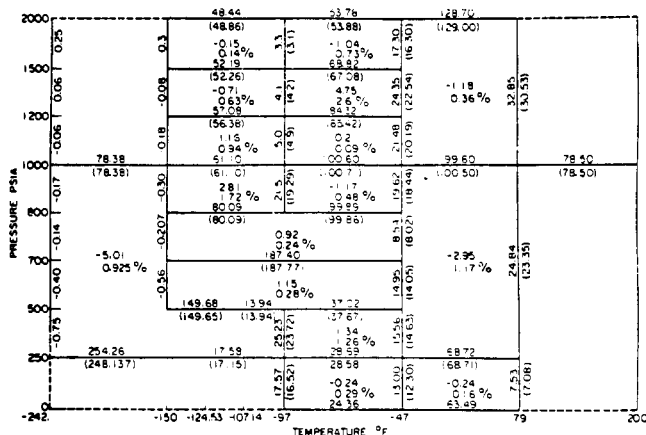


Figure 10. Summary of consistency checks, 5.55 mol % ethane in methane mixture.

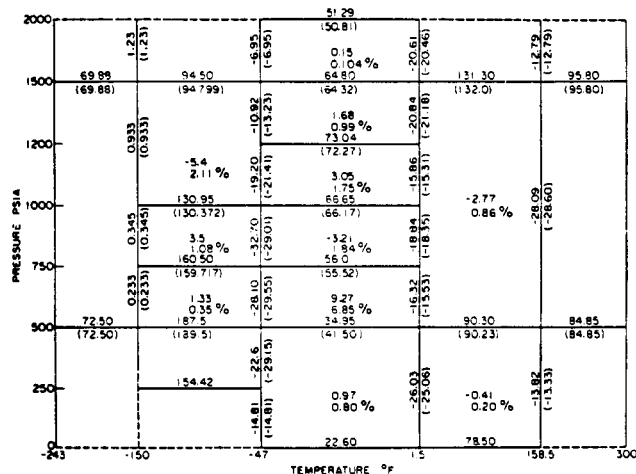


Figure 11. Summary of consistency checks, methane-ethane-propane as 7.1% as indicated by the dashed curve in Figure 7. Corrections as large as 1.3% were made on the isobaric values (center-line on Figure 5). Thus, these data, although thermodynamically consistent to about 1% were judged to be in error by somewhat larger amounts. Taking into account the possibility of systematic errors during the experiment, unusually large adjustments were made in preparing the skeleton tables of thermodynamic data. The values so adjusted are listed as  $C_p(A)$  and  $\phi(A)$  together with values of  $H$  which are consistent with the adjusted values of the derivative functions.

### Skeleton Tables of Thermodynamic Data

Table I contains selected values of thermodynamic properties for the three methane-ethane binaries and the ternary. These values were obtained as described in preceding sections. These tables include only those values of enthalpy at intersections of isobaric and isothermal determinations; i.e., the values are, in

effect, measured twice (except as otherwise indicated). These values are probably the better known of all enthalpy values included in this manuscript and, since they cover the entire range of experimental investigation, should serve well to test prediction methods.

Values of  $C_p$ ,  $\phi$ , and  $H$  reported in Tables VI and VIII comprise the major contribution of this investigation. Both smooth and adjusted values of  $C_p$  and  $\phi$  are listed as discussed previously. The enthalpy values are consistent with the adjusted values of the derivative functions  $C_p(A)$  and  $\phi(A)$ .

Table VI contains values of  $C_p$  and  $H$  at the pressures of measurement over a temperature range from -260 to +320 °F at temperature intervals of 10 °F. At pressures below the critical, values of  $C_p$  are not reported within or near the two-phase region except for the 250 psia isobar in Table VIa.

Similarly, Table VIII consists of values of  $\phi$  and  $H$  at the temperatures of isothermal determinations and  $\mu$ ,  $\phi$ , and  $H$  at temperatures of isenthalpic determinations. Results of isothermal determinations are reported at intervals of 50 psi and those corresponding to isenthalpic determinations at intervals of 100 psi.

Data obtained from enthalpy traverses across the two-phase region are reported in Table VIII.

Near the critical point of the mixture,  $C_p$  attains a maximum. In this region  $C_p$  is a strong function of temperature (as well as pressure), i.e.,  $(\partial C_p / \partial T)_P$  is large and consequently thermodynamic properties change very rapidly. Therefore, it was felt necessary to report  $C_p$  and  $H$  at closer intervals of temperature in this region. Table VI contains these values. The format of this table is the same as VI. Similarly, Table IX contains values of  $\phi$  and  $H$  at closer intervals of pressure at pressures near the critical point of the mixture.

### Acknowledgment

The data presented in this report were obtained by Joseph C. Golba and he is commended for his patience and attention to detail so necessary to obtain precise calorimetric data.

### Glossary

$C_p$	isobaric heat capacity $\equiv (\partial H / \partial T)_P$ , Btu/(lb °F)
$C_p(A)$	values of $C_p$ adjusted to ensure thermodynamic consistency
$C_p(S)$	smoothed $C_p$ values before thermodynamic consistency checks
$H$	specific enthalpy, Btu/lb
$H_i$	specific enthalpy of <i>i</i> th component, Btu/lb
$H_M$	specific enthalpy of mixture, Btu/lb
$H^E$	excess enthalpy, Btu/lb
$P$	pressure, psia
$T$	temperature, °F
$x_i$	mole fraction of component <i>i</i> in the liquid phase
$y_i$	mole fraction of component <i>i</i> in the vapor phase

## Greek Notation

$\Delta H_i$	change in $H$ of pure component $i$ between two states, Btu/lb
$\Delta H_p$	change in $H$ between two temperatures at constant pressure, Btu/lb
$\Delta H_T$	change in $H$ between two pressures at constant temperature, Btu/lb
$\Delta H_{\text{vap}}$	specific enthalpy of vaporization, Btu/lb
$\mu$	Joule-Thomson coefficient $\equiv (\partial T/\partial P)_H$ , °F/psia
$\phi$	isothermal throttling coefficient $\equiv (\partial H/\partial P)_T$ , Btu/lb-psia
$\phi(A)$	values of $\phi$ adjusted to ensure thermodynamic consistency
$\phi(S)$	smoothed $\phi$ values before thermodynamic consistency checks

## Subscripts

$i$	component in a mixture
$j, k$	identify specific experimental values of temperature or pressure
$l$	saturated liquid
$M$	mixture
$P$	property at pressure $P$ , psia
$T$	property at temperature $T$ , °F
$1, 2$	component number in a mixture

## Superscripts

$E$	excess property
$^\circ$	designates ideal gas property mean property

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**Supplementary Material Available:** Tables of isobaric, isothermal, and isenthalpic data (8 pages). Ordering information is given on any current masthead page.

## A Refractometric Study of Trialkyl Borates<sup>†</sup>

Phoebus M. Christopher,\* Pradeep B. Deshpande, and Stephen Frimpong

Department of Chemical & Environmental Engineering, University of Louisville, Louisville, Kentucky 40208

**Refractive indices at wavelengths of 5893, 5461, and 4358 Å have been observed for the following trialkyl borates: methyl, ethyl, propyl, isopropyl, butyl, and isobutyl. The measurements, which were made at temperatures between 5 and 60 °C for methyl borate and from 5 to 90 °C for the remaining homologues, were then correlated with temperature and wavelength. Thermal coefficients of the refractive indices and of the Lorentz-Lorenz molar refractions were calculated, and structural interpretations were offered whenever possible.**

Since the amount of physical data for the trialkyl borates is somewhat meager and scattered throughout the literature,

studies have been undertaken in this laboratory in order to obtain systematic and extensive measurements for the following series of homologues: methyl, ethyl, propyl, isopropyl, butyl, and isobutyl. These studies have thus far yielded data on the vapor pressures (1), densities and absolute viscosities (2), and surface tensions (3), as functions of temperature up to the normal boiling point. A further search of the literature has revealed a paucity of information with regard to the refractometric properties of this class of compounds. Individual refractive indices have been reported (for the D line), at a few different temperatures (4, 5), and one reference (6) offered a temperature correlation of the form,  $n_D^t = A - Bt$ , with constants  $A$  and  $B$  being given for the D line at temperature  $t$  °C; since the data which served as the

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