

Excess Thermodynamic Functions for Ternary Systems. 4. Total-Pressure Data and G^E for Acetonitrile–Ethanol–Water at 50 °C

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Isothermal P - X data for the ternary system acetonitrile–ethanol–water at 50 °C are reported. Data are also presented for the constituent binaries at 50 °C. Reduction of the data by Barker's method allows calculation of G^E .

The data set reported here comprises VLE measurements for the system acetonitrile (1)–ethanol (2)–water (3) at 50 °C. Experimental results are presented for the three constituent binaries and for six runs on ternary mixtures formed by additions of each pure constituent to mixtures of the other two in molar proportions of 2 to 1.

Data were taken with the total-pressure apparatus of Gibbs and Van Ness (7), modified as described briefly in part 3 (5) of this series of papers.

The acetonitrile was chromatography reagent from Matheson Coleman and Bell; the reagent-grade ethanol was supplied by U.S. Industrial Chemicals, and the water was doubly deionized. Except for degassing, all reagents were used as received, with indicated purities of at least 99.8 mol %. Vapor pressures of the pure constituents as measured during the course of these experiments and their comparison with literature values are reported in Table I. Because of the excellent reproducibility of these measurements, P_i^{sat} values in all calculations are fixed at average values.

Results and Correlations

Tables II through IV give experimental values of total pressures for the three constituent binaries, and Table V contains all data for the six runs made with ternary mixtures. Data

Table I. Vapor Pressures of Pure Constituents at 50 °C in kPa

| | acetonitrile (1) | ethanol (2) | water (3) |
|--------------|------------------|-------------|----------------|
| present work | 33.859 | 29.490 | 12.363 |
| | 33.860 | 29.491 | 12.342 |
| | 33.864 | 29.494 | 12.348 |
| | 33.864 | 29.496 | 12.349 |
| av value | 33.862 | 29.493 | 12.350 |
| lit. values | 33.845 (8) | 29.481 (11) | 12.345 (3, 11) |
| | 33.872 (6) | 29.494 (4) | 12.349 (9) |
| | | 29.507 (10) | |

Table II. Total-Pressure Data for Acetonitrile (1)–Ethanol (2) at 50 °C

| x_1 | x_2 | P/kPa |
|--------|--------|----------------|
| 0.0 | 1.0000 | 29.496 |
| 0.0518 | 0.9482 | 33.343 |
| 0.1418 | 0.8582 | 38.000 |
| 0.2169 | 0.7831 | 39.878 |
| 0.3163 | 0.6837 | 41.203 |
| 0.4065 | 0.5935 | 41.952 |
| 0.4864 | 0.5136 | 42.313 |
| 0.5642 | 0.4358 | 42.395 |
| 0.6391 | 0.3609 | 42.239 |
| 0.7063 | 0.2937 | 41.851 |
| 0.7923 | 0.2077 | 40.854 |
| 0.8724 | 0.1276 | 39.204 |
| 0.9500 | 0.0500 | 36.499 |
| 1.0000 | 0.0 | 33.864 |

Table III. Total-Pressure Data for Acetonitrile (1)–Water (3) at 50 °C

| x_1 | x_3 | P/kPa |
|--------|--------|----------------|
| 0.0 | 1.0000 | 12.348 |
| 0.0328 | 0.9672 | 22.829 |
| 0.0974 | 0.9026 | 32.279 |
| 0.1699 | 0.8301 | 35.358 |
| 0.2261 | 0.7739 | 36.180 |
| 0.2846 | 0.7154 | 36.672 |
| 0.3556 | 0.6444 | 37.009 |
| 0.4215 | 0.5785 | 37.262 |
| 0.5041 | 0.4959 | 37.527 |
| 0.5748 | 0.4252 | 37.777 |
| 0.6687 | 0.3313 | 38.020 |
| 0.7418 | 0.2582 | 38.146 |
| 0.8330 | 0.1670 | 37.971 |
| 0.9026 | 0.0974 | 37.149 |
| 0.9472 | 0.0528 | 36.146 |
| 1.0000 | 0.0 | 33.860 |

Table IV. Total-Pressure Data for Ethanol (2)–Water (3) at 50 °C

| x_2 | x_3 | P/kPa |
|--------|--------|----------------|
| 0.0 | 1.0000 | 12.363 |
| 0.0325 | 0.9675 | 16.247 |
| 0.0575 | 0.9425 | 18.518 |
| 0.0920 | 0.9080 | 20.686 |
| 0.1244 | 0.8756 | 22.344 |
| 0.1587 | 0.8413 | 23.393 |
| 0.2007 | 0.7993 | 24.303 |
| 0.2388 | 0.7612 | 25.005 |
| 0.2813 | 0.7187 | 25.514 |
| 0.3598 | 0.6402 | 26.258 |
| 0.4403 | 0.5597 | 27.030 |
| 0.5214 | 0.4786 | 27.658 |
| 0.6405 | 0.3595 | 28.495 |
| 0.7701 | 0.2299 | 29.121 |
| 0.8726 | 0.1274 | 29.474 |
| 0.9589 | 0.0411 | 29.518 |
| 1.0000 | 0.0 | 29.490 |

reduction is by Barker's method, with analytical expressions for G^E provided by Margules or modified Margules expressions for the binary systems and by the Wohl equation for the ternary data. The procedures are fully described elsewhere (1, 2).

In particular, the data for the acetonitrile (1)–ethanol (2) and the ethanol (2)–water (3) binaries are correlated by the Margules equation:

$$g_{ij} \equiv \frac{G_{ij}^E}{RT} = [(A_{ij}x_i + A_{ji}x_j) - (\lambda_{ji}x_i + \lambda_{ij}x_j)x_i x_j] x_i x_j \quad (1)$$

Four parameters are required for acetonitrile–ethanol but only three for ethanol–water. In the latter case

$$\lambda_{ij} = \lambda_{ji}$$

For acetonitrile (1)–water (3) the five-parameter modified Margules equation is required for correlation of the data:

$$g_{13} \equiv \frac{G_{13}^E}{RT} = \left[(A_{31}x_1 + A_{13}x_3) - \frac{\alpha_{13}\alpha_{31}x_1x_3}{\alpha_{13}x_1 + \alpha_{31}x_3 + \eta x_1x_3} \right] x_1x_3 \quad (2)$$

Table V. Total-Pressure Data for Acetonitrile (1)-Ethanol (2)-Water (3) at 50 °C

| x_1 | x_2 | x_3 | P/kPa |
|--------|--------|--------|----------------|
| 1.0000 | 0.0 | 0.0 | 33.864 |
| 0.3326 | 0.6674 | 0.0 | 41.361 |
| 0.3273 | 0.6570 | 0.0157 | 41.326 |
| 0.3153 | 0.6327 | 0.0520 | 41.033 |
| 0.3002 | 0.6025 | 0.0973 | 40.639 |
| 0.2838 | 0.5695 | 0.1467 | 40.194 |
| 0.2639 | 0.5297 | 0.2064 | 39.521 |
| 0.2507 | 0.5031 | 0.2462 | 39.072 |
| 0.2341 | 0.4699 | 0.2960 | 38.477 |
| 0.2172 | 0.4358 | 0.3470 | 37.828 |
| 0.0 | 1.0000 | 0.0 | 29.491 |
| 0.6694 | 0.3306 | 0.0 | 42.089 |
| 0.6546 | 0.3233 | 0.0221 | 42.060 |
| 0.6310 | 0.3116 | 0.0574 | 41.948 |
| 0.6010 | 0.2969 | 0.1021 | 41.749 |
| 0.5687 | 0.2809 | 0.1504 | 41.434 |
| 0.5291 | 0.2613 | 0.2096 | 40.999 |
| 0.5023 | 0.2481 | 0.2496 | 40.641 |
| 0.4696 | 0.2319 | 0.2985 | 40.177 |
| 0.4295 | 0.2121 | 0.3584 | 39.580 |
| 1.0000 | 0.0 | 0.0 | 33.859 |
| 0.6700 | 0.0 | 0.3300 | 38.007 |
| 0.6543 | 0.3234 | 0.3223 | 38.460 |
| 0.6314 | 0.3576 | 0.3110 | 38.988 |
| 0.6036 | 0.3991 | 0.2973 | 39.526 |
| 0.5704 | 0.1487 | 0.2809 | 40.025 |
| 0.5305 | 0.2082 | 0.2613 | 40.451 |
| 0.5040 | 0.2478 | 0.2482 | 40.635 |
| 0.4705 | 0.2977 | 0.2318 | 40.785 |
| 0.4378 | 0.3465 | 0.2157 | 40.833 |
| 0.0 | 0.0 | 1.0000 | 12.342 |
| 0.3366 | 0.0 | 0.6634 | 36.996 |
| 0.3296 | 0.0208 | 0.6496 | 37.116 |
| 0.3177 | 0.0561 | 0.6262 | 37.286 |
| 0.3022 | 0.1022 | 0.5956 | 37.416 |
| 0.2842 | 0.1559 | 0.5599 | 37.493 |
| 0.2646 | 0.2140 | 0.5214 | 37.483 |
| 0.2511 | 0.2544 | 0.4945 | 37.447 |
| 0.2341 | 0.3048 | 0.4611 | 37.269 |
| 0.2174 | 0.3544 | 0.4282 | 37.250 |
| 0.0 | 1.0000 | 0.0 | 29.494 |
| 0.0 | 0.3433 | 0.6567 | 26.187 |
| 0.0211 | 0.3360 | 0.6429 | 28.164 |
| 0.0575 | 0.3235 | 0.6190 | 30.845 |
| 0.1056 | 0.3070 | 0.5874 | 33.390 |
| 0.1560 | 0.2897 | 0.5543 | 35.219 |
| 0.2186 | 0.2683 | 0.5131 | 36.894 |
| 0.2596 | 0.2542 | 0.4862 | 37.637 |
| 0.3103 | 0.2368 | 0.4529 | 38.370 |
| 0.3614 | 0.2193 | 0.4193 | 38.930 |
| 0.0 | 0.0 | 1.0000 | 12.349 |
| 0.0 | 0.6697 | 0.3303 | 28.608 |
| 0.0203 | 0.6561 | 0.3236 | 30.229 |
| 0.0565 | 0.6318 | 0.3117 | 32.436 |
| 0.1028 | 0.6008 | 0.2964 | 34.684 |
| 0.1537 | 0.5667 | 0.2796 | 36.676 |
| 0.2137 | 0.5266 | 0.2597 | 38.160 |
| 0.2541 | 0.4995 | 0.2464 | 39.008 |
| 0.3161 | 0.4580 | 0.2259 | 39.995 |
| 0.3514 | 0.4344 | 0.2142 | 40.359 |

The ternary data are well fit by the simple equation

$$g_{123} = g_{12} + g_{13} + g_{23} + Cx_1x_2x_3 \quad (3)$$

Correlations for the g_{ij} are provided by the binary data alone; the parameter C is found by regression of just the ternary data.

Second virial coefficients B_{ij} required to account for vapor-phase nonidealities are estimated by the method of Tsouopoulos (12).

Results of the correlations of data for the binary systems, together with all ancillary information, are summarized in Table VI. Correlation of the data for the ternary system, with binary

Table VI. Summary of Results for Binary Systems at 50 °C^a

| | acetonitrile (1)- ethanol (2) | acetonitrile (1)- water (3) | ethanol (2)- water (3) |
|---|----------------------------------|--------------------------------|---------------------------|
| P_i^{sat} , kPa | 33.862 | 33.862 | 29.493 |
| P_j^{sat} , kPa | 29.493 | 12.350 | 12.350 |
| V_i^{L} , cm ³ /mol | 54.71 | 54.71 | 60.36 |
| V_j^{L} , cm ³ /mol | 60.36 | 18.23 | 18.23 |
| B_{ii} , cm ³ /mol | -4036 | -4036 | -1706 |
| B_{jj} , cm ³ /mol | -1706 | -1674 | -1674 |
| B_{ij} , cm ³ /mol | -1142 | -287 | -948 |
| A_{ij} | 1.292 ± 0.029 | 2.587 ± 0.007 | 1.697 ± 0.007 |
| A_{ji} | 1.235 ± 0.030 | 2.000 ± 0.009 | 0.929 ± 0.012 |
| λ_{ij} | 0.047 ± 0.143 | | 0.313 ± 0.034 |
| λ_{ji} | 0.615 ± 0.150 | | 0.313 ± 0.034 |
| α_{ij} | | 1.202 ± 0.071 | |
| α_{ji} | | 0.578 ± 0.044 | |
| η | | -0.679 ± 0.079 | |
| RMS ΔP , kPa | 0.079 | 0.032 | 0.054 |
| max $ \Delta P $, kPa | 0.176 | 0.063 | 0.134 |
| x_i^{az} | 0.5454 | 0.7560 | 0.9439 |
| P_i^{az} , kPa | 42.419 | 38.140 | 29.537 |

^a Pairs of components are listed in the order i, j .

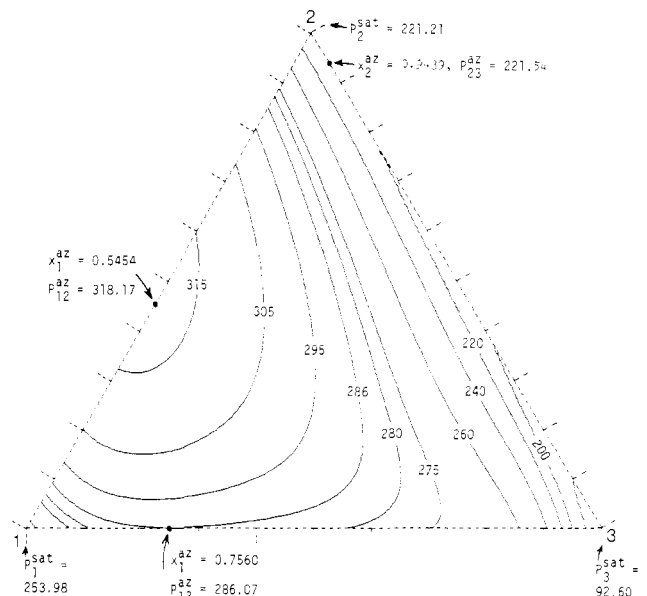


Figure 1. Computer-generated contour diagram showing lines of constant P (in mmHg) on a liquid-mole-fraction grid for acetonitrile (1)-ethanol (2)-water (3) at 50 °C.

parameters fixed at values as given in Table VI, yields for the ternary parameter the value

$$C = 3.686 \pm 0.007$$

The root-mean-square ΔP for the ternary data is 0.056 kPa; the maximum $|\Delta P|$ is 0.120 kPa. Inclusion of higher order ternary terms in eq 3 results in no significant improvement in the quality of correlation.

Discussion

The ethanol-water binary is the only system for which literature values are available for comparison with our results. Pemberton and co-workers (10, 11) report total-pressure values at 50 °C as part of an extensive data set for both VLE and H^E taken over a wide temperature range. Comparison of total pressures calculated from our correlation with their smoothed values shows only fair agreement:

$$\text{RMS } \Delta P = 0.10 \text{ kPa}$$

$$\text{max } |\Delta P| = 0.26 \text{ kPa}$$

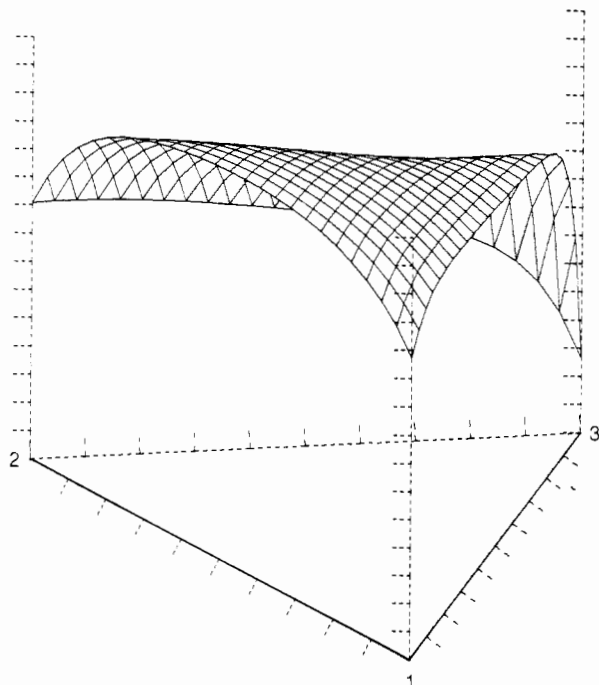


Figure 2. Computer-generated pictorial view of the P - x surface for acetonitrile (1)-ethanol (2)-water (3) at 50 °C.



Figure 3. Computer-generated contour diagram showing lines of constant G^E_{123} (in J/mol) on a liquid-mole-fraction grid for acetonitrile (1)-ethanol (2)-water (3) at 50 °C.

The results of this study are displayed pictorially by Figures 1 through 4. It is evident from Figure 1 that each binary system contains a maximum-pressure azeotrope. There is, however, no ternary azeotrope or other singular point on the pressure-composition surface.

Glossary

| | |
|------------------|---------------------------|
| A_{ij}, A_{ji} | parameters in eq 1 and 2 |
| B_{ij} | second virial coefficient |
| C | parameter in eq 3 |

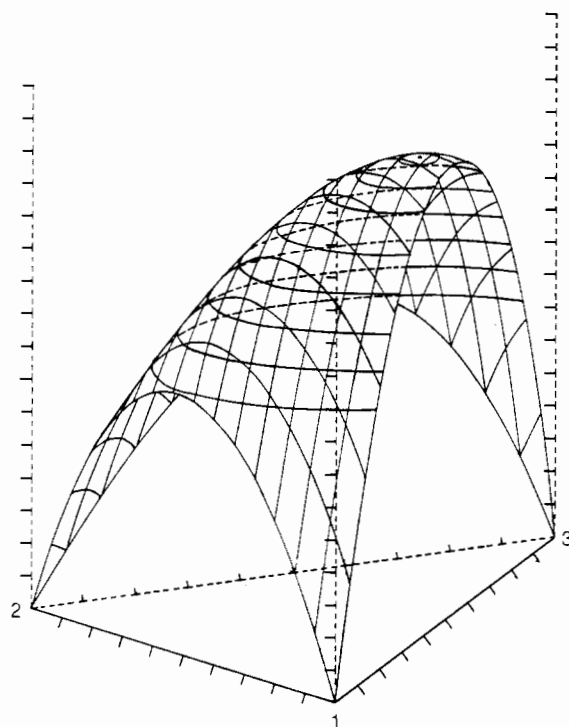


Figure 4. Computer-generated pictorial view of the G^E_{123} - x surface for acetonitrile (1)-ethanol (2)-water (3) at 50 °C.

| | |
|-------------|-------------------------------------|
| G^E | excess Gibbs function, liquid phase |
| g | G^E/RT |
| P | total pressure |
| p^{az} | azeotropic pressure |
| P_i^{sat} | vapor pressure of pure i |
| R | universal gas constant |
| T | absolute temperature |
| V_i^L | molar volume of pure liquid i |
| x | mole fraction, liquid phase |
| x^{az} | azeotropic composition |

Greek Letters

| | |
|------------------------------|------------------------|
| α_{ij}, α_{ji} | parameters in eq 2 |
| η | parameter in eq 2 |
| $\lambda_{ij}, \lambda_{ji}$ | parameters in eq 1 |
| Δ | signifies a difference |

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