

**Figure 1.** Solubility isotherms for  $\text{Cu}(\text{O}_2\text{CR})_2 + \text{pyridine} + \text{water}$  systems, at 298.2 K:  $\text{R} = \text{CH}_3$  (X);  $\text{R} = \text{C}_2\text{H}_5$  (O). Solid phase in equilibrium with the saturated solutions indicated;  $s$  calculated per Cu atom.

$= \text{C}_2\text{H}_5$  and  $\text{R} = \text{CH}_3$ , respectively). At further dilution of the pyridine solutions with water, a gradual electrolytic dissociation and replacement of the pyridine molecules by water ligands occur. As could be expected, both processes are accompanied by an increase in solubility. For  $\text{R} = \text{C}_2\text{H}_5$  the concentration of the saturated solutions increases up to  $X_{\text{H}_2\text{O}} \approx 0.9$ , while for  $\text{R} = \text{CH}_3$  there is a region of nearly constant solubility between  $X_{\text{H}_2\text{O}} \approx 0.7$  and  $0.9$ . Above  $X_{\text{H}_2\text{O}} \approx 0.9$  the saturation curves of both systems drop very rapidly to the common value of  $\approx 0.45 \text{ mol dm}^{-3}$  at  $X_{\text{H}_2\text{O}} \approx 1$ . Now the solid phase becomes binuclear complex  $\text{Cu}_2(\text{O}_2\text{CR})_4\text{Py}_2$ , retaining the pyridine molecules even at as low a pyridine content as  $X_{\text{H}_2\text{O}} =$

0.99. The electronic spectra of the solutions saturated with the binuclear  $\text{Cu}_2(\text{O}_2\text{CR})_4\text{Py}_2$  correspond to mononuclear complexes only. The electronic spectra, solubilities, and conductivities of the two systems ( $\text{R} = \text{CH}_3$  and  $\text{C}_2\text{H}_5$ ) at pyridine concentrations approaching  $X_{\text{H}_2\text{O}} = 1$  are very similar to each other, which suggests that the additional  $\text{CH}_2$  group in the carboxylic ligand does not appreciably influence the solute-water interactions; at  $X_{\text{H}_2\text{O}} = 0.98$  the mean molar absorptivity coefficients are  $65 \pm 3$  at  $\lambda_{\text{max}} = 610 \text{ nm}$ , and the conductivities at  $X_{\text{H}_2\text{O}} = 0.8$  are 24 and  $21 \text{ cm}^2 \Omega^{-1} \text{ equiv}^{-1}$ , respectively. However this is not the case with the solute-nonpolar solvent interactions because the solubilities of two binuclear  $\text{Cu}_2(\text{O}_2\text{CR})_4\text{Py}_2$  in *n*-hexane and cyclohexane differ noticeably: they are  $10^{-3}$  and  $2 \times 10^{-3} \text{ mol dm}^{-3}$  for  $\text{R} = \text{C}_2\text{H}_5$  and of the order of  $10^{-4} \text{ mol dm}^{-3}$  for  $\text{R} = \text{CH}_3$ . This difference is particularly great for aromatic solvents: 0.95 and  $0.90 \text{ mol dm}^{-3}$  for  $\text{R} = \text{C}_2\text{H}_5$  in benzene and chlorobenzene and about  $2 \times 10^{-3} \text{ mol dm}^{-3}$  in the two solvents for  $\text{R} = \text{CH}_3$ . Our attempts to obtain reliable (errors below 5%) solubility isotherms for analogous  $\text{Cu}(\text{O}_2\text{CR})_2$  complexes with longer hydrophobic chains ( $\text{R} > \text{C}_2\text{H}_5$ ) were unsuccessful because of supersaturation effects. These effects increase rapidly with the length of  $\text{R}$  and make it difficult to obtain a real thermodynamic equilibrium between solid  $\text{Cu}(\text{O}_2\text{CR})_2\text{Py}_3\text{H}_2\text{O}$  and its saturated solutions. The results of the measurements for  $\text{R} > \text{C}_2\text{H}_5$  are too poor to be a basis for any reliable interpretation.

**Registry No.**  $\text{Cu}(\text{O}_2\text{CCH}_3)_2$ , 142-71-2;  $\text{Cu}(\text{O}_2\text{CC}_2\text{H}_5)_2$ , 3112-74-1; pyridine, 110-86-1;  $\text{Cu}(\text{O}_2\text{CCH}_3)_2\text{Py}_2$ , 82872-28-4;  $\text{Cu}(\text{O}_2\text{CC}_2\text{H}_5)_2\text{Py}_2$ , 105033-58-7.

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Received for review July 2, 1990. Accepted May 29, 1991. Financial support for this study was provided by Polish Academy of Sciences Grant No. CPBP 01.12-9.17.

## The *N,N*-Dimethylformamide/Ethane-1,2-diol Solvent System. Density, Viscosity, and Excess Molar Volume at Various Temperatures

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Density ( $\rho$ ), kinematic viscosity ( $\nu$ ), and absolute viscosity ( $\eta$ ) are presented for mixtures of ethane-1,2-diol and *N,N*-dimethylformamide from  $-10$  to  $+80$  °C. The above properties were fitted by empirical equations stating their dependence on temperature and mole fraction of the mixture. Furthermore, some considerations regarding the meaning of the obtained adjustment parameters are made. The excess functions, such as molar volumes  $V^E$ , have been derived. The trends of  $V^E$  data vs mole fraction of the mixtures have exhibited markedly negative deviations from ideality, indicating extensive molecular interactions between the components of the binary solvent system.

#### Introduction

Among the most characterizing intensive chemical-physical properties of the solvent systems, density ( $\rho$ ) and viscosity, either kinematic ( $\nu$ ) or dynamic ( $\eta$ ), represent some of the common thermomechanical parameters that are in general useful in order to study and interpret the medium effects on the transport phenomena, on the electrolyte behavior, and on any other reaction mechanism that takes place in solution. In particular, in the field of conductometric studies, it's impossible to approach any problem without the preliminary knowledge of the above-mentioned solvent properties. In fact, if one thinks about the phenomena of electrolyte diffusion and electropho-

Table I. Experimental Density Values (g cm<sup>-3</sup>) for the *N,N*-Dimethylformamide/Ethane-1,2-diol Solvent System

<i>t</i> , °C	<i>x</i> <sub>1</sub>							
	1.0000	0.8848	0.7734	0.5609	0.3623	0.1758	0.0864	0.0000
-10	0.981 48 <sub>5</sub>	0.998 20 <sub>2</sub>	1.013 12 <sub>1</sub>	1.045 86 <sub>1</sub>	1.080 51 <sub>4</sub>	1.110 46 <sub>6</sub>	1.123 32 <sub>5</sub>	1.133 63 <sub>4</sub>
-5	0.976 03 <sub>8</sub>	0.992 91 <sub>0</sub>	1.008 09 <sub>3</sub>	1.041 25 <sub>4</sub>	1.075 30 <sub>2</sub>	1.105 90 <sub>3</sub>	1.119 61 <sub>1</sub>	1.130 45 <sub>2</sub>
0	0.970 70 <sub>4</sub>	0.987 71 <sub>4</sub>	1.003 19 <sub>1</sub>	1.036 77 <sub>8</sub>	1.070 58 <sub>4</sub>	1.101 64 <sub>2</sub>	1.115 87 <sub>4</sub>	1.127 06 <sub>9</sub>
5	0.965 52 <sub>5</sub>	0.982 67 <sub>6</sub>	0.998 67 <sub>6</sub>	1.032 24 <sub>2</sub>	1.065 81 <sub>7</sub>	1.097 47 <sub>0</sub>	1.112 28 <sub>3</sub>	1.123 66 <sub>4</sub>
10	0.960 45 <sub>6</sub>	0.977 73 <sub>5</sub>	0.993 72 <sub>5</sub>	1.027 95 <sub>5</sub>	1.061 42 <sub>4</sub>	1.093 44 <sub>9</sub>	1.108 68 <sub>0</sub>	1.120 29 <sub>6</sub>
15	0.955 30 <sub>2</sub>	0.927 87 <sub>2</sub>	0.989 10 <sub>4</sub>	1.023 66 <sub>9</sub>	1.057 03 <sub>3</sub>	1.089 50 <sub>4</sub>	1.105 00 <sub>5</sub>	1.116 90 <sub>6</sub>
20	0.950 45 <sub>3</sub>	0.968 11 <sub>1</sub>	0.984 55 <sub>7</sub>	1.019 48 <sub>6</sub>	1.052 96 <sub>5</sub>	1.085 64 <sub>0</sub>	1.101 42 <sub>2</sub>	1.113 44 <sub>0</sub>
25	0.945 59 <sub>7</sub>	0.963 37 <sub>2</sub>	0.980 00 <sub>9</sub>	1.015 33 <sub>7</sub>	1.048 82 <sub>6</sub>	1.081 89 <sub>5</sub>	1.097 86 <sub>7</sub>	1.109 91 <sub>3</sub>
30	0.940 69 <sub>1</sub>	0.958 71 <sub>0</sub>	0.975 60 <sub>2</sub>	1.011 24 <sub>1</sub>	1.044 94 <sub>8</sub>	1.078 15 <sub>3</sub>	1.094 21 <sub>6</sub>	1.106 51 <sub>2</sub>
35	0.935 81 <sub>4</sub>	0.954 03 <sub>5</sub>	0.971 15 <sub>6</sub>	1.007 10 <sub>7</sub>	1.041 00 <sub>6</sub>	1.074 54 <sub>6</sub>	1.090 67 <sub>3</sub>	1.103 08 <sub>9</sub>
40	0.931 03 <sub>0</sub>	0.949 37 <sub>5</sub>	0.966 75 <sub>5</sub>	1.003 17 <sub>4</sub>	1.037 27 <sub>5</sub>	1.070 97 <sub>6</sub>	1.087 10 <sub>8</sub>	1.099 74 <sub>7</sub>
45	0.926 28 <sub>2</sub>	0.944 61 <sub>5</sub>	0.962 33 <sub>0</sub>	0.999 08 <sub>3</sub>	1.033 46 <sub>0</sub>	1.067 35 <sub>1</sub>	1.083 55 <sub>9</sub>	1.096 31 <sub>2</sub>
50	0.921 54 <sub>8</sub>	0.940 03 <sub>0</sub>	0.957 91 <sub>1</sub>	0.995 00 <sub>9</sub>	1.029 68 <sub>1</sub>	1.063 78 <sub>0</sub>	1.079 82 <sub>2</sub>	1.092 94 <sub>6</sub>
55	0.916 71 <sub>6</sub>	0.935 30 <sub>5</sub>	0.953 40 <sub>4</sub>	0.990 94 <sub>5</sub>	1.025 85 <sub>6</sub>	1.060 13 <sub>3</sub>	1.076 24 <sub>5</sub>	1.089 47 <sub>1</sub>
60	0.911 97 <sub>1</sub>	0.930 52 <sub>0</sub>	0.949 09 <sub>7</sub>	0.986 72 <sub>2</sub>	1.022 07 <sub>8</sub>	1.056 57 <sub>4</sub>	1.072 65 <sub>4</sub>	1.086 01 <sub>1</sub>
65	0.907 02 <sub>5</sub>	0.925 65 <sub>9</sub>	0.944 47 <sub>1</sub>	0.982 65 <sub>1</sub>	1.018 14 <sub>5</sub>	1.052 95 <sub>2</sub>	1.068 90 <sub>6</sub>	1.082 63 <sub>4</sub>
70	0.902 25 <sub>8</sub>	0.920 70 <sub>6</sub>	0.939 82 <sub>6</sub>	0.978 33 <sub>9</sub>	1.014 15 <sub>3</sub>	1.049 24 <sub>4</sub>	1.065 33 <sub>3</sub>	1.079 00 <sub>3</sub>
75	0.897 21 <sub>9</sub>	0.915 64 <sub>5</sub>	0.935 12 <sub>8</sub>	0.974 01 <sub>3</sub>	1.010 06 <sub>0</sub>	1.045 44 <sub>1</sub>	1.061 78 <sub>5</sub>	1.075 36 <sub>9</sub>
80	0.892 24 <sub>7</sub>	0.910 46 <sub>3</sub>	0.930 38 <sub>1</sub>	0.969 68 <sub>6</sub>	1.005 89 <sub>3</sub>	1.041 62 <sub>5</sub>	1.058 14 <sub>6</sub>	1.071 69 <sub>9</sub>

retic migration (which are affected by the thermokinetic delay effects related to the viscoelastic properties of the solutions) (1), it is possible to understand the importance of the availability of the solvent extrathermodynamic parameters, such as  $\rho$ ,  $\nu$ , and  $\eta$ . As it is well-known, these properties are functionally dependent on temperature and, at least for binary mixtures, on composition of the solvent systems. The changes vs mole fraction of the above-cited parameters often provide more and more detailed evidence about the structural character of the systems themselves. The magnitude of the cited thermomechanical parameters of a liquid system is determined by the molecular packing degree and by the nature of the mutual orientation of the individual units that may constrain the medium to assume a significant liquid structure (SLS) (2); on the basis of these considerations, measurements of those properties should be a powerful tool to investigate the intermolecular forces and the local order of which these forces are responsible in a fluid mixture.

Although many tabulated values of the above thermomechanical properties are generally available for the pure solvents, literature data relative to various binary solvent mixtures are often either incomplete, or reported as graphs only, or quite lacking.

Very few studies are reported about amido-alcoholic solvent systems, and this fact has encouraged us to realize a series of systematic investigations on the solvent properties of these mixtures. For these aims, we have chosen, in the present case, *N,N*-dimethylformamide (DMF) and dihydroxyethane (DHE) as pure solvents and as components of binary mixtures, investigated in the -10 to +80 °C temperature range and in the whole composition range, expressed by  $x_{\text{DMF}}$  ( $0 \leq x_{\text{DMF}} \leq 1$ ).

Even if DMF has been already investigated (3-8), nowadays it's one of the most important solvent in analytical chemistry and for practical purposes, being a very good aprotic protophilic medium for a lot of organic and inorganic substances. These characteristics are probably due to its molecular properties, such as the high tendency to provide hydrogen bonds via acceptor sites of the amido group  $-\text{C}(\text{O})\text{N}=\text{O}$ .

On the other hand, DHE is certainly one of the most interesting polyalcohols, being also the simplest homologue of the diol series, widely utilized in industrial applications (9) as a thermoregulating fluid and in chemical laboratories for its unusual viscosity and solvating properties (10-12), these last related to its character of protophilic solvent. Thus, further significant studies should be feasible on nonthermodynamic properties of binary (or higher) containing DHE solvent mixtures; the above properties are, in fact, tunable upon adding a more or less viscous dipolar cosolvent.

## Experimental Section

**Materials.** *N,N*-Dimethylformamide and ethane-1,2-diol (both containing <0.10% g of water/g of solution found by Karl-Fischer titration) were Carlo Erba high purity grade. The *N,N*-dimethylformamide was purified by passage on a neutral alumina column before use. The mixtures were gravimetrically prepared on a Mettler analytical balance just before their use, operating in a dry nitrogen atmosphere at 26 °C. The probable error in the DMF mole fraction ( $x_1$ ) is estimated to be less than  $1.5 \times 10^{-4}$ .

**Apparatus.** The densities were determined with a digital density meter Anton Paar Model DMA 60 equipped with a density measuring cell Model DMA 602, with a sensitivity up to 0.000 001 g cm<sup>-3</sup>. For the measurements, we have selected the period of 10 000 oscillation cycles, keeping 30 readouts for every sample at each temperature.

Viscosity measurements were performed by using a Schott-Geräte AVS 400 viscosity measuring system, equipped with a series of Ubbelohde viscometers, covering the  $0.6 \leq \nu \leq 3 \times 10^{-4} \text{ m}^2 \text{ s}^{-1}$  range. In all the determinations the kinetic energy correction has been taken into account according to Hagenbach in order to evaluate the absolute viscosity  $\eta$ . The temperature control was provided by a Lauda K2R thermostatic bath maintained to  $\pm 0.02$  °C.

In all the cases the experiments were generally performed at least in five replicates for each composition and at each temperature, and the results were averaged. The overall experimental standard deviation was approximately equal to  $1.6 \times 10^{-6}$  for  $\rho$  and  $1.4 \times 10^{-3}$  for  $\nu$ , respectively. The estimated accuracy (95% confidence interval) was  $\pm 3 \times 10^{-6}$  for  $\rho$  and  $\pm 4 \times 10^{-3}$  for  $\nu$ .

Karl Fischer titrations were performed with an automatic titration system (Crison Model KF431) equipped with a digital buret (Crison Model 738).

## Results and Discussion

Experimental values for density ( $\rho$ ) and kinematic ( $\nu$ ) and absolute viscosities ( $\eta$ ) were collected for the two pure components and for six mixtures of them in the whole composition range  $0 \leq x_{\text{DMF}} \leq 1$ , working in the -10 to +80 °C temperature range.

**1. Density and Excess Molar Volumes.** The experimental density values, Table I, were fitted vs the variable quantity temperature by the polynomial equation

$$\frac{1}{\rho}(t) = \sum_{k=0}^m \frac{1}{k+1} t^k \quad t(^{\circ}\text{C}) \quad (1)$$

Table II.  $\rho_i^{-1}$  Coefficients of Equation 2 for the *N,N*-Dimethylformamide/Ethane-1,2-diol Solvent System

$t, ^\circ\text{C}$	$\rho_0^{-1}$	$\rho_1^{-1} \times 10$	$\rho_2^{-1} \times 10^2$	$\rho_3^{-1} \times 10^3$	$\rho_4^{-1} \times 10^3$	$\sigma(\rho) \times 10^4$
-10	1.018 659	-1.436 73	3.098 08	-10.249 8	78.8208	6.09
-5	1.024 393	-1.482 27	3.349 91	-9.615 63	71.1531	4.52
0	1.030 057	-1.520 48	3.287 94	-8.831 37	64.6729	3.93
5	1.035 657	-1.590 67	4.893 66	-10.585 1	70.1766	3.13
10	1.041 120	-1.605 92	4.088 96	-9.074 80	61.8040	5.92
15	1.046 755	-1.661 67	4.799 03	-9.530 92	61.8818	4.92
20	1.052 110	-1.687 39	4.449 89	-8.742 34	57.4572	5.41
25	1.057 534	-1.721 81	4.559 09	-8.744 29	57.2166	6.18
30	1.063 049	-1.763 46	4.567 72	-8.280 94	53.9288	5.99
35	1.068 599	-1.807 54	4.934 94	-8.620 88	55.3089	6.06
40	1.074 095	-1.831 84	4.130 66	-7.056 38	47.3996	6.04
45	1.079 625	-1.851 34	3.373 97	-5.784 32	41.5030	5.94
50	1.085 159	-1.875 74	2.776 44	-4.645 13	35.8505	5.28
55	1.090 884	-1.901 39	2.135 62	-3.484 20	30.3993	5.47
60	1.096 601	-1.932 30	1.924 19	-3.115 81	29.1429	4.66
65	1.102 586	-1.951 57	0.711 334	-0.925 526	18.2022	4.90
70	1.108 452	-1.956 34	-0.402 234	0.473 242	13.0348	5.50
75	1.114 721	-1.986 41	-0.852 482	1.198 40	10.1000	6.53
80	1.120 998	-1.995 72	-2.179 89	3.164 16	1.49401	8.12

Table III. Coefficients  $\rho_{kl}^{-1}$  of Equation 3 for the *N,N*-Dimethylformamide/Ethane-1,2-diol Solvent System

$\rho_{kl}^{-1}$	coefficient value	$\rho_{kl}^{-1}$	coefficient value
$\rho_{00}^{-1}$	1.060 973	$\rho_{12}^{-1}$	$1.702 73 \times 10^{-3}$
$\rho_{01}^{-1}$	-0.313 556	$\rho_{22}^{-1}$	$-1.532 96 \times 10^{-5}$
$\rho_{02}^{-1}$	$8.760 20 \times 10^{-2}$	$\rho_{32}^{-1}$	$-5.399 86 \times 10^{-7}$
$\rho_{03}^{-1}$	-0.167 449	$\rho_{42}^{-1}$	$3.336 09 \times 10^{-9}$
$\rho_{04}^{-1}$	0.119 632	$\rho_{13}^{-1}$	$1.230 48 \times 10^{-4}$
$\rho_{10}^{-1}$	$2.313 57 \times 10^{-3}$	$\rho_{23}^{-1}$	$-2.262 18 \times 10^{-5}$
$\rho_{20}^{-1}$	$1.158 76 \times 10^{-8}$	$\rho_{33}^{-1}$	$1.541 40 \times 10^{-5}$
$\rho_{30}^{-1}$	$2.415 59 \times 10^{-8}$	$\rho_{43}^{-1}$	$-9.768 77 \times 10^{-9}$
$\rho_{40}^{-1}$	$1.365 83 \times 10^{-10}$	$\rho_{14}^{-1}$	$-1.077 18 \times 10^{-3}$
$\rho_{11}^{-1}$	$-2.153 35 \times 10^{-3}$	$\rho_{24}^{-1}$	$3.667 67 \times 10^{-5}$
$\rho_{21}^{-1}$	$5.288 24 \times 10^{-8}$	$\rho_{34}^{-1}$	$-1.074 61 \times 10^{-6}$
$\rho_{31}^{-1}$	$1.201 27 \times 10^{-8}$	$\rho_{44}^{-1}$	$6.567 91 \times 10^{-9}$
$\rho_{41}^{-1}$	$7.550 59 \times 10^{-12}$		

$$\sigma(\rho) = 0.0007$$

for each binary solvent system by the least-squares method. On the basis of a careful examination of the results obtained by using equations of different degree  $m$ , it was noted that the best correlation was obtained when  $m = 4$ . The rational eq 1 reproduces the experimental values better than the nonrational one of the type  $\rho(t) = \sum_k \rho_k t^k$ . In order to take into account the dependence of  $\rho$  on the composition of the binary mixtures, the polynomial equation

$$\frac{1}{\rho}(x_1) = \sum_{i=0}^4 \frac{1}{\rho_i} x_1^i \quad (2)$$

was used to fit the experimental data at each temperature. Table II summarizes the  $\rho_i$  coefficients of eq 2 and the relative standard deviations ( $\sigma$ ) at each investigated temperature.

These two equations (1 and 2) were simply combined in order to propose an empirical approach to solving the problem of a single function  $\rho = \rho(t, x_1)$ :

$$\frac{1}{\rho}(t, x_1) = \left[ \frac{1}{\rho}(t) \frac{1}{\rho}(x_1) \right]^{1/2} \quad (3)$$

where  $(1/\rho)(t)$  and  $(1/\rho)(x_1)$  are eqs 1 and 2, respectively. The above equation, written in its expanded form, is composed of 25 terms that have been evaluated by fitting the set of experimental density values of Table I with the multilinear regression package TSP (13). These coefficients are summarized in Table III, together with the standard deviations ( $\sigma$ ), and we may suppose that these differences should not be exceeded over all the points of the surface  $\rho = \rho(t, x_1)$ .

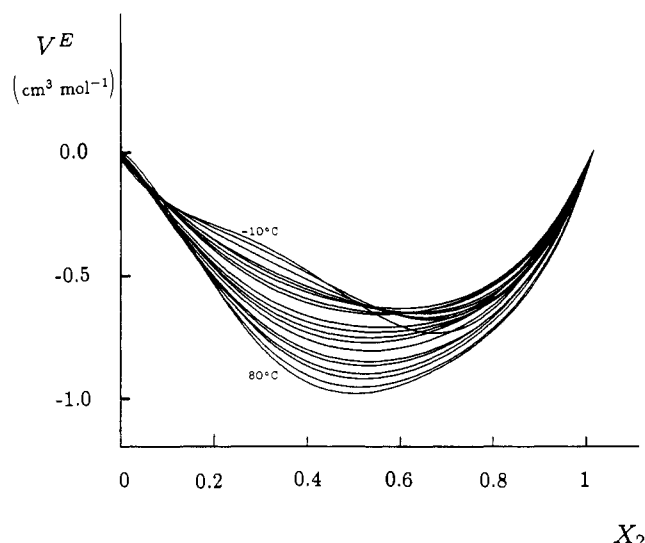


Figure 1. Excess molar volume  $V^E$  ( $\text{cm}^3 \text{mol}^{-1}$ ) curves for the *N,N*-dimethylformamide/ethane-1,2-diol solvent system at different temperatures.

The density values were converted into excess molar volumes  $V^E$ , assuming ideal mole fraction additivity of the molar volumes  $V_i$ . The equation

$$V^E = \frac{\sum_{i=1}^2 x_i M_i}{\rho} - \sum_{i=1}^2 x_i V_i \quad (4)$$

was used to evaluate the  $V^E$  quantity for each isothermal set of data, where  $M_i$  represents the molecular weight of the  $i$ th component. The values calculated by eq 4 have been fitted by a smoothing equation of the type

$$V^E = x_1 x_2 \sum_{k=0}^3 a_k (x_1 - x_2)^k \quad (5)$$

where  $a_k$  are the adjustment coefficients.

Figure 1 shows the trend of excess volumes of mixing DMF and DHE ( $V_1/V_2 = 1.38$  at  $25^\circ\text{C}$ ) at various temperatures; as it is particularly evident from the graph, the system exhibits negative deviations from ideality at all the investigated temperatures.

The trend of the curves is quite interesting, showing a continuous deformation with the temperature. At the lowest temperatures, the minimum of the  $V^E$  function is centered at  $x_2 \approx 0.7$  (molar ratio DMF:DHE  $\approx 1:2$ ). By increasing the temper-

**Table IV. Experimental Values of Kinematic Viscosity,  $\nu$  (cS), and Ratio of Molecular Radii for the *N,N*-Dimethylformamide/Ethane-1,2-diol Solvent System at Various Temperatures**

$t, ^\circ\text{C}$	$x_1$								$r_2/r_1^a$
	1.0000	0.8848	0.7734	0.5609	0.3623	0.1758	0.0864	0.0000	
-10	1.397	2.072	3.151	7.632	19.02	45.78	67.40	98.91	0.994
-5	1.289	1.876	2.791	6.428	15.10	34.41	49.97	71.08	0.995
0	1.192	1.705	2.494	5.465	12.13	26.35	37.53	52.42	0.996
5	1.108	1.561	2.238	4.696	9.995	20.69	28.96	39.54	0.997
10	1.034	1.435	2.024	4.051	8.333	16.51	22.66	30.44	0.998
15	0.9693	1.326	1.842	3.558	7.017	13.43	18.06	23.89	0.999
20	0.9121	1.230	1.686	3.168	5.962	10.98	14.63	19.04	1.000
25	0.8605	1.147	1.549	2.818	5.130	9.170	12.06	15.44	1.000
30	0.8130	1.071	1.427	2.523	4.440	7.652	9.974	12.67	1.001
35	0.7712	1.003	1.323	2.273	3.885	6.536	8.374	10.49	1.002
40	0.7337	0.9428	1.226	2.058	3.424	5.601	7.107	8.806	1.002
45	0.6975	0.8907	1.139	1.875	3.037	4.845	6.097	7.481	1.003
50	0.6650	0.8416	1.067	1.720	2.709	4.237	5.252	6.434	1.004
55	0.6374	0.7971	0.9992	1.576	2.432	3.724	4.592	5.532	1.004
60	0.6102	0.7570	0.9401	1.452	2.197	3.287	4.014	4.777	1.005
65	0.5867	0.7210	0.8880	1.343	0.993	2.936	3.529	4.192	1.005
70	0.5635	0.6863	0.8380	1.247	1.818	2.632	3.134	3.688	1.006
75	0.5401	0.6560	0.7939	1.162	1.666	2.367	2.804	3.279	1.006
80	0.5210	0.6274	0.7553	1.088	1.537	2.159	2.544	2.910	1.007

$$^a r_2/r_1 = (M_2\rho_1/M_1\rho_2)^{1/3}$$

ature, starting from 15 °C up to the higher values, the minimum shifts to  $x_2 \approx 0.5$  (DMF:DHE = 1:1) and becomes more and more deep as the temperature increases. These observations could be very useful in order to try to verify the possibility of a solvent-cosolvent complex formation and to determine its hypothetical molar ratio composition. Indeed, the maximum degree of molecular packing is found in correspondence of a minimum value of  $V^E$  in the 1:1 and 1:2 DMF:DHE molar composition range.

By deriving eq 5 with respect to  $x_1$  and  $x_2$  (7), one obtains the relative partial molar volumes of the two components for each binary composition and temperature.

**2. Kinematic Viscosity.** Table IV reports the experimental values of the kinematic viscosities ( $\nu$ ) experimentally determined in the temperature range  $-10 \leq t \leq 80$  °C with thermal scanning of 5 °C. The results of these measurements have been used to test the common empirical approach of McAllister (14), in order to try to predict the viscosities of the binary liquid mixtures not directly detected. In this treatment the author took into account the specific interactions between contiguous fluid layers of molecules that move of stationary motion. In this representation the molecules which have an activation energy that overcomes the potential barrier due to the velocity gradient may jump between adjacent layers, changing their individual motion conditions. For a binary mixture, McAllister derived the following cubic semiempirical equation for the kinematic viscosity:

$$\ln \nu = x_1^3 \ln \nu_1 + 3x_1^2x_2 \ln \nu_{12} + 3x_1x_2^2 \ln \nu_{21} + x_2^3 \ln \nu_2 + R_0 \quad (6)$$

where

$$R_0 = -[\ln(x_1 + x_2M_2/M_1)] + 3x_1^2x_2 \ln(2/3 + M_2/3M_1) + 3x_1x_2^2 \ln(1/3 + 2M_2/3M_1) + x_2^3 \ln(M_2/M_1) \quad (7)$$

In eq 6,  $\nu_1$  and  $\nu_2$  refer to the kinematic viscosities of the pure components having mole fractions  $x_1$  and  $x_2$ , while in eq 7  $M_1$  and  $M_2$  refer to their molecular weights. Equation 6 contains also the crossing terms  $\nu_{12}$  and  $\nu_{21}$  that are two adjustable parameters of the fit, characteristic of each binary system 1/2 and determinable by a least-squares method. The term  $R_0$  can be calculated if one knows the binary composition of the solvent system and the molecular weight of the components. It is noteworthy that eq 6 may be used only if the ratio of the mo-

**Table V. Values of Adjustment Parameters and Standard Deviations  $\sigma(\nu)$  for the McAllister Equation at Various Temperatures**

$t, ^\circ\text{C}$	$\nu_{12}$	$\nu_{21}$	$\sigma(\nu) \times 10^3$
-10	3.954	23.59	2.6
-5	3.483	18.52	2.2
0	3.123	14.51	2.1
5	2.781	11.85	2.0
10	2.492	9.741	2.4
15	2.259	8.139	2.4
20	2.076	6.820	1.6
25	1.895	5.828	1.9
30	1.753	4.935	1.3
35	1.610	4.316	1.5
40	1.482	3.780	1.2
45	1.379	3.319	1.2
50	1.296	2.917	0.79
55	1.196	2.634	1.3
60	1.119	2.376	1.3
65	1.052	2.139	0.81
70	0.9843	1.954	0.85
75	0.9362	1.772	0.76
80	0.8741	1.670	2.0

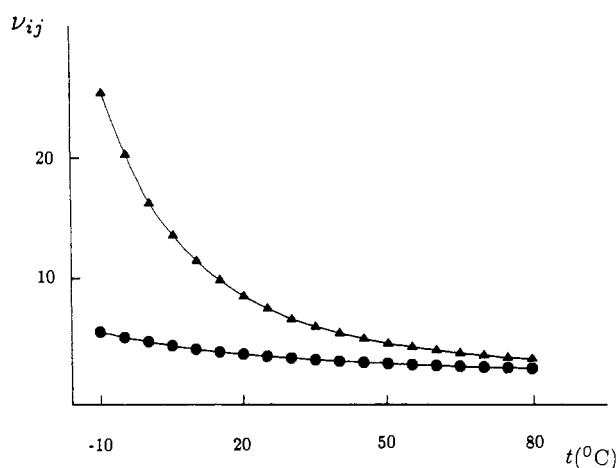
lecular radii of the two components in the mixture is smaller than 1.5. The choice and the use of this cubic equation is justified in all the investigated temperature range since, for each temperature value, the ratio of the radii is smaller than the imposed limit, as shown in Table IV. In Table V are summarized the adjustment parameters  $\nu_{12}$ ,  $\nu_{21}$ , and the  $\sigma(\nu)$  values for each isothermal experimental data fit. By analyzing a reasonably large set of these parameters, we can consider an assessment of their meaning. Figure 2 reports, in a graphic form, the obtained crossing terms  $\nu_{12}$  and  $\nu_{21}$  vs temperature and the curve represents a fit of the type

$$\nu_{ij} = C_0 e^{C_1/T} \quad \text{for } (i \neq j) = 1, 2 \quad (8)$$

having, in its linear logarithmic form, a correlation coefficient  $r = 0.999$  for  $\nu_{12}$  and  $r = 0.994$  for  $\nu_{21}$ . Now, interpreting these parameters in terms of quantities related to the specific interactions between unlike molecules, it is possible to represent them in an oversimplified picture of the type  $\{1-1-2\}$ ,  $\{2-1-2\}$  for  $\nu_{12}$ , and  $\{1-2-1\}$ ,  $\{1-2-2\}$  for  $\nu_{21}$ , where the central molecule is involved in a hypothetical ternary aggregate. Obviously, the relative intensities of these interactions between a central unit and the surrounding molecules, or other aggregates, in any space direction are different for different neighboring arrangements. It is however reasonable to think that the nature of

**Table VI. Experimental Viscosity Values (cP) for the *N,N*-Dimethylformamide/Ethane-1,2-diol Solvent System at Various Temperatures**

<i>t</i> , °C	<i>x</i> <sub>1</sub>							
	1.0000	0.8848	0.7734	0.5609	0.3623	0.1758	0.0864	0.0000
-10	1.371	2.069	3.192	7.983	20.55	50.84	75.70	112.2
-5	1.258	1.863	2.813	6.693	16.24	38.06	55.94	80.36
0	1.157	1.684	2.502	5.666	12.99	29.03	41.88	59.08
5	1.070	1.534	2.234	4.848	10.65	22.70	32.21	44.43
10	0.9933	1.403	2.011	4.164	8.844	18.05	25.12	34.11
15	0.9260	1.290	1.822	3.643	7.418	14.64	19.96	26.68
20	0.8669	1.191	1.660	3.230	6.277	11.93	16.12	21.20
25	0.8136	1.105	1.518	2.852	5.381	9.921	13.24	17.14
30	0.7647	1.027	1.392	2.551	4.639	8.250	10.91	14.01
35	0.7217	0.9570	1.285	2.289	4.044	7.023	9.133	11.58
40	0.6831	0.8951	1.185	2.064	3.551	5.998	7.725	9.684
45	0.6460	0.8415	1.096	1.873	3.139	5.171	6.606	8.203
50	0.6128	0.7911	1.022	1.711	2.789	4.507	5.671	7.032
55	0.5843	0.7455	0.9527	1.562	2.495	3.949	4.942	6.027
60	0.5565	0.7044	0.8921	1.433	2.245	3.473	4.305	5.188
65	0.5321	0.6674	0.8386	1.320	2.029	3.091	3.772	4.538
70	0.5084	0.6319	0.7876	1.220	1.843	2.761	3.339	3.978
75	0.4846	0.6007	0.7424	1.132	1.683	2.475	2.977	3.525
80	0.4602	0.5725	0.7044	1.055	1.546	2.249	2.692	3.117

**Figure 2.** McAllister's equation  $\nu_{12}$  (●) and  $\nu_{21}$  (▲) parameters vs temperature.

these specific interactions is about the same either for the 1 or 2 central species. On the basis of these considerations, the crossing terms in the fit equations should have nearly the same statistical weight and consequently, for any fixed temperature, very little different values. For this binary solvent system, McAllister's equation provides adjustment parameters very different in magnitude, especially at the lowest temperatures, while, with an increase in the temperature, the relative differences  $\delta_r$  evaluated as follows

$$\delta_r = \frac{|\nu_{12} - \nu_{21}|}{|\nu_{12} - \nu_{21}|_{\max}} \quad (9)$$

are largely reduced. Therefore, McAllister's treatment appears to be more effective to describe this system at the highest temperatures, while probably it is less efficacious at the lowest ones. Equation 6 provides a set of calculated  $\nu$  values with an average uncertainty of  $\pm 0.0031$  cS.

**3. Absolute Viscosity.** The absolute viscosity values, Table VI, were obtained from the kinematic ones by the equation

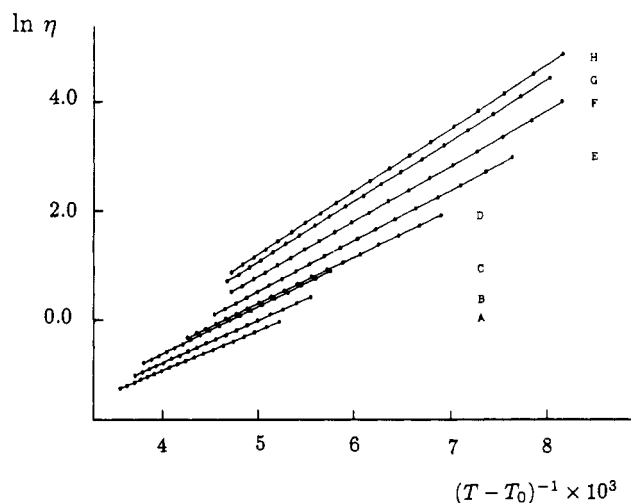
$$\eta = \nu\rho \quad (10)$$

An interesting empirical treatment for the viscosity data fit vs temperature was provided by Williams-Landel-Ferry-Doolittle (15), and the three adjustment parameters equation WLF

$$\ln \eta = \frac{A_0}{T - T_0} + A_1 \quad (11)$$

**Table VII. Adjustment Parameters and Average Percent Deviations ( $\Delta\%$ )<sub>av</sub> for the WLF Treatment, Equation 11**

<i>x</i> <sub>1</sub>	<i>A</i> <sub>0</sub>	<i>A</i> <sub>1</sub>	<i>T</i> <sub>0</sub>	( $\Delta\%$ ) <sub>av</sub>
1.0000	648.28	-3.0603	71.00	0.16
0.8848	696.90	-3.1310	82.40	0.13
0.7734	771.10	-3.2746	89.21	0.12
0.5609	765.99	-3.2003	117.92	0.27
0.3623	832.53	-3.3314	132.07	0.12
0.1758	905.98	-3.4520	140.38	0.18
0.0864	993.93	-3.6477	138.54	0.21
0.0000	1034.3	-3.7239	140.61	0.22

**Figure 3.**  $\ln \eta$  of the *N,N*-dimethylformamide/ethane-1,2-diol solvent system as a function of  $(T - T_0)^{-1}$ .

was used in order to check the validity of this theory for this binary solvent system. The results are reported in Table VII, and the reproducibility of the experimental  $\eta$  values is demonstrated by the average percent deviations ( $\Delta\%$ )<sub>av</sub>, very close to the experimental standard deviation.

It is obvious from Figure 3 that the viscosity data are linear for this function over a wide temperature range, even if a sudden increase in this property at lower temperatures in the DHE-rich region is observed. In fact, the greatest values of  $\eta$  are due to the highly polymerized structure of the DHE solvent, in particular at the lower temperatures. This structure is easily depolymerized either by increasing the temperature of the system and/or by forming heteropolymers as a consequence of the increase in the cosolvent molar fraction. On the basis

of these considerations, for these binary mixtures we may suggest the onset of a pseudo-glassy state in the region of the low temperatures and high molar fraction of DHE component. Therefore, expression 11 is not only an excellent three-adjustment-parameters fit equation of the experimental data but also may provide a model for low-temperature behavior as well.

The empirical meaning of the  $T_0$  parameter is the temperature below which the system viscosity becomes infinite and, after WLF theory, defines the temperature field below which the free intermolecular volume is not available for viscous flow. However, we have doubts about it. The melting points of the two pure components are  $-60.5$  and  $-11.5$  °C for DMF and DHE, respectively (16). Already at these temperatures one might observe a dramatic increase of the viscosity that becomes infinite in the solid state. Hence, the condition  $\eta \simeq \infty$  may be achieved for temperature values higher than those reported in Table VII.

#### Acknowledgment

We thank Dr. Luca Rovatti for his experimental work and the "Centro Interdipartimentale di Calcolo Automatico ed Informatica Applicata" (CICAIA) of Modena University for the computing facilities.

#### Glossary

$A_0, A_1$	coefficients in eq 11
$C_0, C_1$	coefficients in eq 8
$M_i$	molecular weight of the $i$ th component
$T_0$	coefficient in eq 11
$T$	absolute temperature
$V_i$	molar volume ( $\text{cm}^3 \text{mol}^{-1}$ ) of the $i$ th component
$V^E$	excess molar volume ( $\text{cm}^3 \text{mol}^{-1}$ )
$a_k$	coefficients of eq 5
$t$	Celsius temperature
$x_i$	mole fraction of the $i$ th component

#### Greek Letters

$\delta_r$	relative differences in eq 9
$\eta$	absolute viscosity (cP)
$\nu$	kinematic viscosity (cS)
$\nu_1, \nu_2$	kinematic viscosities of pure components
$\nu_{ij}$	McAllister parameters in eq 6
$\rho$	density ( $\text{g cm}^{-3}$ )
$\rho_1, \rho_2$	densities of the pure components
$\rho_k^{-1}$	coefficients in eq 1
$\rho_l^{-1}$	coefficients in eq 2
$\rho_{kl}^{-1}$	coefficients in eq 3
$\sigma$	standard deviation

Registry No. DMF, 68-12-2; ethane-1,2-diol, 107-21-1.

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Received for review July 26, 1990. Accepted March 26, 1991. We thank the Consiglio Nazionale delle Ricerche (CNR) of Italy for the financial support.

## The *N,N*-Dimethylformamide + Ethane-1,2-diol Solvent System. Dielectric Constant, Refractive Index, and Related Properties at Various Temperatures

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Dielectric constant ( $\epsilon$ ) and refractive indexes ( $n$ ) were measured for pure *N,N*-dimethylformamide, ethane-1,2-diol, and their six mixtures over the entire composition range and, where possible, at nineteen selected temperatures ranging between  $-10$  and  $+80$  °C. The above properties were fitted by empirical equations stating their dependence on temperature ( $T$ ) and mole fraction ( $x_1$ ) of the mixture. The refractive indexes of the binary mixtures were used to test the validity of mixing rules at different temperatures.

#### Introduction

As a part of our studies on binary liquid mixtures and, in particular, on the influence of these solvents on the acid-base equilibria that take place (1-3), we report static dielectric constant ( $\epsilon$ ), refractive index ( $n$ ), and some derived properties

of *N,N*-dimethylformamide (DMF), ethane-1,2-diol (DHE), and six mixtures over, where possible, a temperature range from  $-10$  to  $+80$  °C.

The *N,N*-dimethylformamide is a very good aprotic protophilic solvent, with a high dipole moment ( $\mu = 3.28$  D at 25 °C) (4) and a medium dielectric constant ( $\epsilon = 37.52$  at 25 °C) in the general classification of Charlot (5).

The ethane-1,2-diol was chosen for its unusual solvent properties, such as the protic protophilic character, the high autoprotolysis constant ( $\text{p}K_{\text{autoprot}} = 15.8$  at 25 °C) (6), and the high dipole moment ( $\mu = 2.28$  D), and, in particular, because it is almost isodielectric ( $\epsilon = 37.7$  at 25 °C) with *N,N*-dimethylformamide over the temperature range studied.

#### Experimental Section

**Materials.** *N,N*-Dimethylformamide and ethane-1,2-diol (both containing  $<0.10\%$  g of water/g of solvent found by Karl-