

Isobaric Vapor-Liquid Equilibrium for Ethanol + Water + Cobalt(II) Chloride

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Isobaric vapor-liquid equilibrium for ethanol (1) + water (2) + cobalt(II) chloride (3) at different mole fractions of cobalt(II) chloride has been measured at 100.0 kPa. The results in the range where the mole fraction of salt in the liquid phase was less than 0.23 times the mole fraction of water were correlated by assuming that the salt was in ionic form and was associated only with the water. Thermodynamic consistency was checked by Herington's method with satisfactory results.

Introduction

Although the salt effect on the vapor-liquid equilibria (VLE) of volatile substances has been noted, well-established equations are not available for the correlation and prediction of VLE data of salt-containing systems. The reviews by Ciparis (1, 2) are the only compilations on the salt effect on the vapor-liquid equilibria in organic mixtures.

Some proposed methods for the correlation of experimental results [Natarajan (3), Schmitt and Vogelwohl (4), and Vercher et al. (5, 6)] consider that solvent mixtures containing a salt can be treated as pseudobinary systems. Recently, some researchers [Chen et al. (7, 8), Sander et al. (9), Tan (10), and Kikic et al. (11)] have used modifications of VLE local composition model to take account of the electrolyte contribution.

The vapor-liquid equilibrium of the ethanol + water system saturated with cobalt(II) chloride has been studied by several researchers, such as Alvarez et al. (12), Martinez de la Ossa and Galán (13, 14) and Jacques and Galán (15), but we have not found any reported vapor-liquid equilibrium for ethanol + water with varying concentrations of cobalt(II) chloride below saturation.

Experimental Section

The chemicals were absolute ethanol (Baker-analyzed reagent, >99.5 mass %), distilled water, and cobalt(II) chloride (Probus, >99.5 mass %). They were used without further purification.

The equilibrium apparatus was a recirculating still of the Labodest model, manufactured by Fischer. The vapor-liquid equilibrium data were obtained at 100.00 ± 0.04 kPa. The vapor pressure of water with a varying concentration of salt was also measured with the same apparatus.

Every experimental point was obtained from an initial sample prepared gravimetrically by using a Sartorius analytical balance with a precision of ± 0.0001 g and, afterward, by adding different quantities of ethanol, water, ethanol-salt solution or water-salt solution. Each experiment was kept at the boiling point for 15 min or more to ensure the stationary state. The accuracy of the temperature measurement was ± 0.1 K.

Compositions of the condensed vapor phase were analyzed by using a Hewlett-Packard 5700 A gas chromatograph with a thermal conductivity detector, connected to

a Hewlett-Packard 3394 A integrator. The chromatographic column (2 m \times 1/8 in.) was packed with Porapak P. The gas carrier was helium flowing at 50 cm³/min, and the column temperature was 383 K. The calibration was carried out with gravimetrically prepared standard solutions. The accuracy of the measured vapor-phase mole fraction was ± 0.002 .

The liquid phase was composed of ethanol, water, and cobalt(II) chloride. The salt composition in the liquid phase was gravimetrically determined after separating the volatile components by evaporation to dryness. Water and ethanol compositions in the liquid phase containing dissolved salt were obtained by density measurements with an Anton Paar DMA 55 densimeter matched to a Julabo circulator with proportional temperature control and an automatic drift correction system that kept the samples at 298.15 ± 0.01 K. The densimeter was calibrated by measuring a set of standard solutions with known mole fractions of ethanol, water, and salt in the ternary mixtures, and the correlation obtained was used to calculate the ethanol mole fraction with the known salt mole fraction. The accuracy in the measurement of the ethanol, water, and cobalt(II) chloride mole fractions in the liquid phase was ± 0.003 . This method of analyzing the composition of salt-containing mixtures was found to be reproducible and of consistent accuracy, as described in a previous work (6).

Results and Discussion

In Tables 1 and 2, the vapor-liquid equilibrium for the ethanol (1) + water (2) + cobalt(II) chloride (3) system at a pressure of 100.0 kPa is reported. Included are the equilibrium temperature (T/K), the mole fractions of ethanol (x_1), water (x_2), and salt (x_3) in the ternary liquid phase, and the mole fraction of ethanol in the vapor phase (y_1). In Table 1, we give the results in the range of $x_3 < 0.23x_2$, and in Table 2, we show the results in the range of $x_3 > 0.23x_2$.

To make possible the thermodynamic treatment of vapor-liquid equilibrium, we postulate that, in the range of liquid-phase salt compositions studied, the salt is in ionic form and is associated only with the water (5). Therefore, the ternary system can be treated as a pseudobinary system composed of pure ethanol (I) and water + salt (II) components. This assumption is only acceptable when there is enough water to dissolve all the salt present in

Table 1. Vapor-Liquid Equilibrium for Ethanol + Water + Cobalt(II) Chloride at 100.0 kPa in the Range of $x_3 < 0.23x_2$

T/K	x_1	x_2	x_3	y_1	γ_I	γ_{II}	T/K	x_1	x_2	x_3	y_1	γ_I	γ_{II}
364.2	0.035	0.936	0.029	0.374	6.341	0.954	353.7	0.365	0.593	0.042	0.702	1.690	1.239
364.3	0.038	0.919	0.043	0.424	6.635	0.933	353.2	0.390	0.572	0.038	0.705	1.615	1.279
363.9	0.040	0.908	0.052	0.459	6.925	0.934	353.7	0.397	0.554	0.049	0.721	1.595	1.329
362.3	0.051	0.934	0.015	0.397	5.022	0.956	353.9	0.398	0.549	0.053	0.723	1.580	1.360
360.2	0.061	0.889	0.050	0.539	6.130	0.936	353.4	0.405	0.556	0.039	0.711	1.558	1.292
361.4	0.061	0.930	0.009	0.415	4.485	0.952	353.3	0.406	0.586	0.009	0.653	1.436	1.249
360.1	0.067	0.919	0.014	0.455	4.692	0.954	353.2	0.413	0.569	0.019	0.681	1.477	1.239
358.7	0.076	0.896	0.028	0.527	5.021	0.930	353.2	0.416	0.554	0.030	0.703	1.512	1.272
358.0	0.086	0.874	0.040	0.565	4.910	0.944	353.5	0.428	0.525	0.048	0.730	1.508	1.384
358.3	0.089	0.854	0.057	0.601	4.987	0.942	353.1	0.435	0.533	0.031	0.711	1.465	1.313
358.0	0.096	0.891	0.013	0.516	3.999	0.949	353.6	0.474	0.468	0.058	0.758	1.405	1.538
357.3	0.107	0.846	0.047	0.601	4.286	0.951	352.8	0.475	0.509	0.016	0.698	1.336	1.332
357.5	0.117	0.876	0.007	0.515	3.364	0.974	353.1	0.478	0.477	0.045	0.744	1.396	1.474
356.8	0.121	0.863	0.016	0.551	3.558	0.959	353.8	0.488	0.447	0.065	0.765	1.369	1.601
356.9	0.124	0.821	0.055	0.630	3.946	0.966	353.4	0.492	0.454	0.055	0.759	1.369	1.575
356.3	0.127	0.838	0.035	0.605	3.790	0.943	352.7	0.498	0.471	0.031	0.732	1.339	1.441
355.8	0.148	0.827	0.025	0.591	3.242	0.979	352.7	0.505	0.469	0.026	0.728	1.315	1.403
355.9	0.153	0.828	0.019	0.586	3.104	0.966	352.8	0.506	0.457	0.036	0.744	1.333	1.482
355.8	0.154	0.801	0.045	0.632	3.321	0.985	353.5	0.539	0.396	0.066	0.790	1.294	1.644
355.2	0.181	0.786	0.033	0.628	2.883	0.992	352.4	0.547	0.439	0.014	0.721	1.216	1.450
355.2	0.186	0.791	0.023	0.608	2.712	1.000	353.3	0.548	0.392	0.061	0.787	1.279	1.700
355.5	0.187	0.762	0.051	0.652	2.865	1.033	352.9	0.548	0.401	0.051	0.779	1.284	1.689
355.4	0.189	0.800	0.012	0.579	2.530	1.019	353.7	0.548	0.380	0.072	0.797	1.274	1.564
354.7	0.221	0.752	0.027	0.629	2.404	1.033	352.5	0.556	0.414	0.030	0.754	1.245	1.550
354.6	0.233	0.745	0.022	0.624	2.274	1.045	352.6	0.576	0.383	0.041	0.779	1.236	1.704
354.7	0.239	0.722	0.040	0.656	2.323	1.065	352.2	0.593	0.382	0.025	0.761	1.192	1.608
354.7	0.250	0.741	0.009	0.601	2.033	1.067	352.0	0.597	0.382	0.021	0.759	1.190	1.569
354.2	0.251	0.718	0.031	0.652	2.234	1.059	352.8	0.613	0.331	0.056	0.814	1.204	1.785
354.4	0.257	0.713	0.030	0.650	2.161	1.062	353.2	0.617	0.316	0.067	0.826	1.197	1.494
354.4	0.262	0.702	0.036	0.659	2.149	1.084	352.2	0.621	0.345	0.033	0.788	1.177	1.774
354.3	0.271	0.711	0.018	0.631	1.998	1.075	352.0	0.625	0.363	0.012	0.753	1.127	1.586
354.5	0.272	0.722	0.007	0.602	1.890	1.095	352.1	0.634	0.342	0.024	0.782	1.149	1.686
354.2	0.283	0.682	0.036	0.666	2.031	1.104	351.7	0.654	0.339	0.007	0.780	1.129	1.485
354.0	0.298	0.659	0.044	0.685	1.996	1.148	351.8	0.688	0.293	0.019	0.795	1.090	1.819
354.0	0.301	0.684	0.015	0.632	1.822	1.116	351.8	0.690	0.295	0.016	0.796	1.088	1.738
354.2	0.302	0.657	0.041	0.679	1.938	1.145	352.3	0.708	0.242	0.050	0.856	1.117	1.731
353.9	0.315	0.657	0.028	0.666	1.841	1.123	351.8	0.717	0.255	0.027	0.831	1.092	2.014
354.0	0.320	0.644	0.036	0.677	1.832	1.156	352.0	0.724	0.237	0.039	0.849	1.097	2.103
353.9	0.336	0.622	0.041	0.692	1.791	1.192	351.4	0.777	0.210	0.013	0.837	1.030	2.042
353.7	0.346	0.643	0.011	0.641	1.627	1.165	351.4	0.778	0.211	0.011	0.838	1.031	1.967
354.0	0.348	0.605	0.047	0.701	1.748	1.234	351.8	0.788	0.182	0.030	0.878	1.050	2.230
353.5	0.361	0.615	0.024	0.674	1.649	1.178	351.5	0.795	0.188	0.017	0.872	1.046	1.983

Table 2. Vapor-Liquid Equilibrium for Ethanol + Water + Cobalt(II) Chloride at 100.0 kPa in the Range of $x_3 > 0.23x_2$

T/K	x_1	x_2	x_3	y_1
353.6	0.625	0.299	0.076	0.843
353.8	0.631	0.287	0.082	0.845
352.8	0.678	0.260	0.062	0.854
353.8	0.683	0.229	0.089	0.883
353.1	0.707	0.218	0.075	0.880
352.8	0.730	0.204	0.067	0.889
353.7	0.740	0.170	0.090	0.921
353.0	0.760	0.160	0.081	0.917
354.0	0.760	0.142	0.098	0.935
352.3	0.776	0.171	0.054	0.899
352.0	0.792	0.166	0.042	0.894
354.0	0.804	0.097	0.099	0.965
352.9	0.807	0.119	0.074	0.938
353.2	0.827	0.085	0.089	0.962
354.4	0.840	0.051	0.109	0.983
352.4	0.856	0.084	0.060	0.953
352.1	0.869	0.085	0.046	0.947
351.8	0.874	0.093	0.033	0.938
351.5	0.892	0.088	0.020	0.931

the liquid phase, which happens when $x_3 < 0.23x_2$. When equilibrium is established between vapor and liquid phases, the activity coefficients of both pseudocomponents will be given by these expressions:

$$\gamma_I = y_I \phi_I P / x_I P_I^\circ \quad \gamma_{II} = y_{II} \phi_{II} P / x_{II} P_{II}^\circ \quad (1)$$

where x_I is the mole fraction of pseudocomponent I in the

Table 3. Boiling Points of Water + Cobalt(II) Chloride Mixtures at 100.0 kPa

x_3^*	T/K	x_3^*	T/K
0.113	387.7	0.055	378.6
0.109	386.9	0.053	378.4
0.106	386.5	0.051	378.1
0.102	385.6	0.049	377.8
0.097	384.9	0.048	377.6
0.094	384.4	0.046	377.3
0.091	383.9	0.044	377.1
0.089	383.6	0.041	376.7
0.085	383.1	0.039	376.4
0.082	382.5	0.034	375.8
0.077	382.0	0.031	375.4
0.074	381.5	0.028	375.0
0.071	380.9	0.025	374.7
0.069	380.6	0.023	374.4
0.066	380.3	0.020	374.2
0.065	380.0	0.018	373.9
0.062	379.6	0.015	373.7
0.060	379.3	0.012	373.4
0.057	378.9		

liquid phase ($=x_1$), x_{II} is the mole fraction of pseudocomponent II in the liquid phase ($=x_2 + x_3$), y_I is the mole fraction of ethanol in the vapor phase ($=y_1$), y_{II} is the mole fraction of water in the vapor phase ($=1 - y_1$), ϕ_I is the fugacity coefficient of pseudocomponent I in the vapor phase, ϕ_{II} is the fugacity coefficient of pseudocomponent II in the vapor phase, P is the system pressure (kPa), P_I° is the vapor pressure of pure ethanol ($=P_1^\circ$), and P_{II}° is the vapor pressure of pseudocomponent II, both calculated at

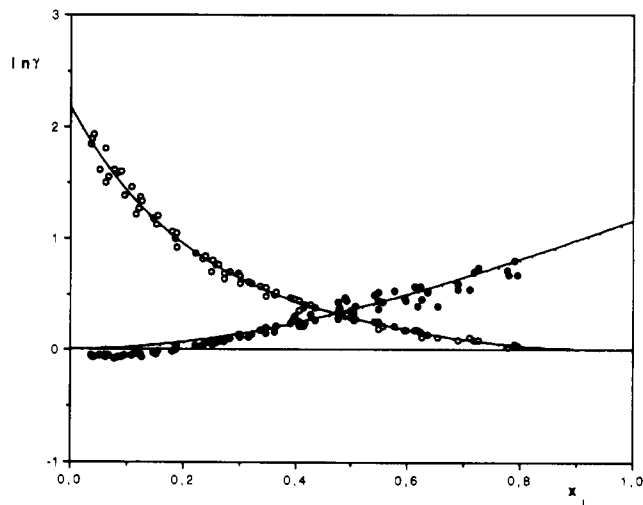


Figure 1. Experimental solvent activity coefficients for the system ethanol + water + cobalt(II) chloride at 100.0 kPa: (○) $\ln \gamma_1$, (●) $\ln \gamma_{II}$.

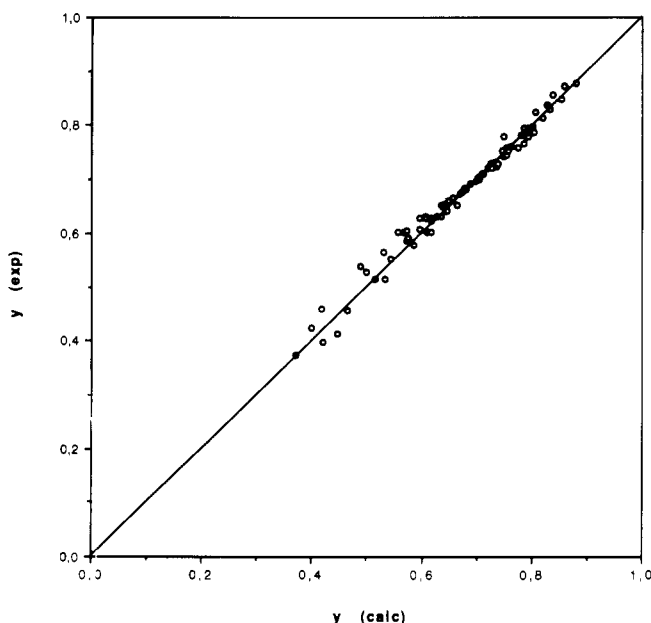


Figure 2. Comparison of calculated vapor composition, y_{calc} , with experimental values, y_{expt} .

the equilibrium temperature (kPa). The value of P_{II}° depends on the temperature and on the salt concentration. Jaques and Furter (16) propose that this dependency can be expressed as

$$P_{II}^\circ = P_2^\circ(T) \epsilon(x_3^*) \quad (2)$$

where P_2° is the vapor pressure of pure water (kPa) and ϵ is the vapor pressure correction factor, which only depends on x_3^* , the mole fraction of the component salt in the pseudocomponent II ($=x_3/(x_2 + x_3)$).

The vapor pressure correction factor was computed by the method of Jaques and Furter (16) from results of the vapor pressure of water with different amounts of salt that we have obtained, given in Table 3, and the vapor pressure of pure water obtained from the Antoine equation with the parameters given in the literature (17), both at the same temperature.

The correlation equation obtained from experimental results for the vapor pressure correction factor (ϵ) with the

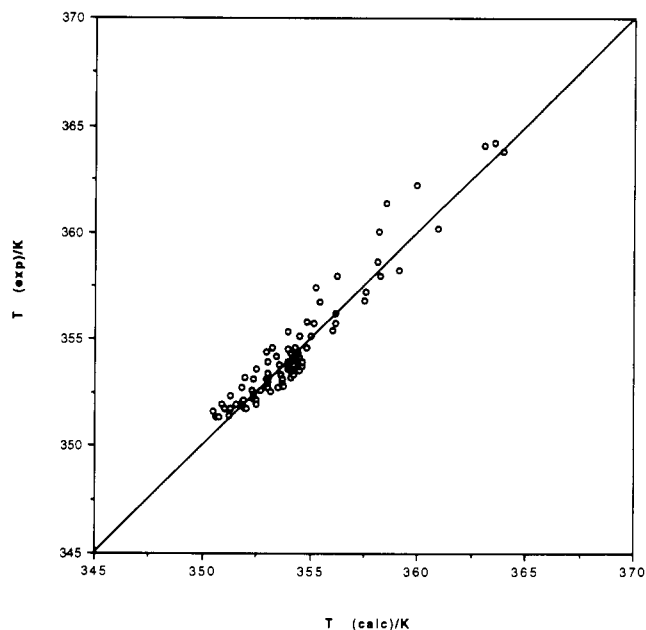


Figure 3. Comparison of calculated bubble points with experimental values.

salt mole fraction in pseudocomponent II (x_3^*), for the entire range of salt concentrations studied, is

$$\epsilon = 1 - 1.9393x_3^* - 36.6838(x_3^*)^2 + 204.6836(x_3^*)^3 \quad (3)$$

The fugacity coefficients ϕ_I and ϕ_{II} were calculated by means of the virial equation of state, and the second virial coefficients were calculated from the Pitzer and Curl equations (18) and the Tsonopoulos correlation correction (19) for polar compounds.

For each experimental value, the activity coefficients of pseudocomponents I and II in the liquid phase have been calculated following the above procedure. The obtained values of γ_I and γ_{II} are shown in columns 6 and 7 of Table 1.

In Figure 1, the logarithms of γ_I and γ_{II} are plotted against x_1 . In this figure, the logarithms of activity coefficients for both pseudocomponents can be adjusted to one curve whatever the salt concentration may be. This fact implies that the pseudobinary model proposed explains the behavior of the system in the range of compositions established.

The thermodynamic consistency of the results was tested by the integral method described by Herington (20, 21) and Redlich and Kister (22). The area test parameters, D and J , obtained were

$$D = 9.92\%, \quad J = 5.51\%, \quad \text{and} \quad D - J = 4.41\%$$

According to Herington's interpretation of the area test results, the results were probably consistent.

For the purpose of reproducing experimental data, the activity coefficients obtained for every pseudocomponent were adjusted against their composition in the liquid phase, and the equations found were

$$\ln \gamma_I^* = (2.1860 - 5.0650x_1 + 8.9881x_1^2 - 5.8914x_1^3)(1 - x_1)^2 \quad (4)$$

$$\ln \gamma_{II}^* = (1.1558 + 0.56619x_{II})(1 - x_{II})^2 \quad (5)$$

These equations were used to recalculate the vapor composition and temperature values in equilibrium from the

liquid phase composition. From comparison of experimental and calculated values, we found

$$y_{\text{exptl}} - y_{\text{calcd}}: \text{ mean, 0.012}$$

$$\text{standard deviation, 0.015}$$

$$T_{\text{exptl}} - T_{\text{calcd}}: \text{ mean, 0.67 K}$$

$$\text{standard deviation, 0.83 K}$$

The experimental values are plotted against the corresponding calculated ones in Figure 2 for the vapor composition and in Figure 3 for the temperature. In these figures, the agreement between both experimental and calculated values can be noted.

Literature Cited

- (1) Ciparis, J. N. *Data on Salt Effect In Vapour-Liquid Equilibrium*; Lithuanian Agricultural Academy: Kaunas, Lithuania, 1966.
- (2) Ciparis, J. N. *Liquid-Vapour Equilibrium. Ternary Systems with One Nonvolatile Component. Handbook*; Khimiya, Leningrad Otd.: Leningrad, 1973.
- (3) Natarajan, T. S.; Srinivasan, D. *J. Chem. Eng. Data* **1980**, *25*, 215.
- (4) Schmitt, D.; Vogelphol, A. *Fluid Phase Equilib.* **1983**, *9*, 167.
- (5) Vercher, E.; Muñoz, R.; Martínez-Andreu, A. *J. Chem. Eng. Data* **1991**, *36*, 274.
- (6) Vercher, E.; Peña, M. P.; Martínez-Andreu, A. *J. Chem. Eng. Data* **1994**, *39*, 316.
- (7) Chen, C. C.; Britt, H. I.; Boston, J. F.; Evans, L. B. *AIChE J.* **1982**, *28*, 588.
- (8) Chen, C. C.; Evans, L. B. *AIChE J.* **1986**, *32*, 444.
- (9) Sander, B. *Chem. Eng. Sci.* **1986**, *41*, 1179.
- (10) Tan, T. C. *Chem. Eng. Res. Des.* **1987**, *65*, 421.
- (11) Kikic, I.; Fermeglia, M.; Rasmusen, P. *Chem. Eng. Sci.* **1991**, *46*, 2775.
- (12) Alvarez, J. R.; Bueno, J.; Galán, M. A. *An. Quim.* **1974**, *70*, 262.
- (13) Martínez de la Ossa, E.; Galán, M. A. *Am. J. Enol. Vitic.* **1986**, *37*, (4), 253.
- (14) Martínez de la Ossa, E.; Galán, M. A. *Am. J. Enol. Vitic.* **1991**, *42*, (3), 252.
- (15) Jaques, D.; Galán, M. A. *Chem. Eng. Sci.* **1980**, *35*, 1803.
- (16) Jaques, D.; Furter, W. F. *AIChE J.* **1972**, *18*, 343.
- (17) Gmehling, J.; Onken, U.; Arlt, W. *Vapor-Liquid Equilibrium Data Collection*; Chemistry Data Series; DECHEMA: Frankfurt, 1981; Vol. I/1.
- (18) Pitzer, K. S.; Curl, Jr. R. F. *J. Am. Chem. Soc.* **1957**, *79*, 2369.
- (19) Tsouopoulos, C. *AIChE J.* **1974**, *20*, 263.
- (20) Herington, E. F. G. *Nature* **1947**, *160*, 610.
- (21) Herington, E. F. G. *J. Ind. Pet.* **1951**, *37*, 457.
- (22) Redlich, O. and Kister, A. T. *Ind. Eng. Chem.* **1948**, *40*, 345.

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