### Isothermal Vapor–Liquid Equilibrium of Binary Mixtures Containing Pyrrolidine

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We report measurements of the vapor-liquid equilibrium of pyrrolidine, and of binary mixtures of pyrrolidine separately with cyclohexane at 313.15 and 333.15 K, with water at 333.15 and 353.15 K, with ethanol at 313.15 and 333.35 K, and with tetrahydrofuran at 313.35 and 333.35 K. These data are correlated with five liquid activity coefficient models by the maximum likelihood parameter estimation method, including a correction for nonideal vapor-phase behavior. A comparison of our data with the predictions of the UNIFAC model is also included. The prediction of the UNIFAC model is so poor that a new functional group for the cyclic secondary amine group should be defined. In contrast, the prediction of the DISQUAC model is in excellent agreement with our data.

#### Introduction

Cyclic amines are solvents of interest in the chemical industry and in theoretical modeling because of their unique physicochemical nature. We have previously reported vapor-liquid equilibrium (VLE) data for mixtures containing tetrahydrofuran (1), which has a single cyclic ether group, and 1,3-dioxolane (2), which has two cyclic ether groups. We measured the VLE of these mixtures containing cyclic ethers in order to obtain liquid activity coefficients, which are of inherent interest and also of use in determining the importance of proximity effects, that is, the interference between close neighbor, nonalkyl functional groups in current group contribution activity coefficient models (3). In this paper, we report the VLE data for mixtures containing pyrrolidine. Pyrrolidine has a five-member ring structure similar to that of tetrahydrofuran; pyrrolidine and tetrahydrofuran differ only in that the latter has one cyclic ether group while the former has one cyclic secondary amine group. Another goal of our measurements is to examine whether the cyclic secondary amine group in pyrrolidine differs in the group-contribution context from a noncyclic secondary amine group, which could be tested by comparing our measurements with the prediction of the UNIFAC model (4). Since in the UNIFAC model the cyclic ether group in tetrahydrofuran is defined to be a different group than the noncyclic ether group, it may also be that the cyclic secondary amine group in pyrrolidine should be considered to be different from a noncyclic secondary amine group. In addition to determining the vapor pressure of pure pyrrolidine, four binary mixtures were measured, each at two isotherms: pyrrolidine with cyclohexane at 313.15 and 333.15 K, with water at 333.15 and 353.15 K, with ethanol at 313.15 and 333.35 K, and with tetrahydrofuran at 313.35 and 333.35 Κ.

#### Experiments

The experimental equipment and operating procedures have been described in detail previously (5). The VLE measurements were done with a Stage–Muller dynamic still. The temperature was measured with a platinum resistance thermometer (Rosemount Model 162N) accurate to 0.02 K with a resolution of 0.001 K. Pressures were measured with an accuracy of 0.02

## Table I. Vapor Pressure of Pyrrolidine as a Function of Temperature

T/K	P/kPa	T/K	P/kPa	T/K	$P/\mathbf{kPa}$
313.170	17.300	335.265	43.290	348.162	69.080
315.570	19.250	335.330	43.360	348.455	69.740
322.980	26.520	340.028	51.700	351.940	78.580
327.015	31.340	340.620	52.840	354.735	86.190
330.143	35.470	344.475	60.720	357.785	95.170
331.450	37.390	344.575	60.950		

Table II. Antoine Constants for Pure Components and the Temperature Range (T) of Determination (This Work):  $\log (P/kPa) = A - (B/[(T/K) + C])$ 

component	A	B	С	T range/K
pyrrolidine	5.93436	1118.946	-74.922	313-359
cyclohexane	6.15159	1301.67	-39.705	293-353
water	7.07510	1657.46	-46.130	333-363
eth <b>a</b> nol	7.16879	1552.60	-50.731	303 - 351
tetrahydrofuran	6.44102	1384.21	-26.997	303-333

kPa with use of a Wallace-Tiernan Model FA-187 precision mercury manometer. Vapor and liquid equilibrium samples were analyzed by a Hewlett-Packard Model 5730 gas chromatograph with a Model 3390 integrator, after calibration with gravimetrically prepared samples. The compositions determined in this way are accurate to better than 0.0005 in mole fraction.

In this study, pyrrolidine, cyclohexane, and tetrahydrofuran were purchased from the Aldrich Chemical Co. Water was found the main impurity in pyrrolidine (catalog no. P7380-3). Thus, the pyrrolidine was first purified to 99.9% by dehydration with molecular sieves. Cyclohexane (HPLC grade) and tetrahydrofuran (HPLC grade) were also dehydrated with molecular sieves so that the purity was higher than 99.9%. The water used was filtered, distilled, and deionized. The ethanol used was 200-proof (99.9%) dehydrated alcohol from U. S. Industrial Chemicals Corp. The vapor pressures we measured for cyclohexane, tetrahydrofuran, water, and ethanol agree with literature values (6-8). The vapor pressures of pyrrolidine that we measured, listed in Table I, also agree with literature values (6). The Antoine constants that we determined from our vapor pressure measurements are listed in Table II. The binary isothermal VLE data we measured are listed in Table III.

#### **Results and Discussion**

We correlated our measured vapor-liquid equilibrium data with five liquid activity coefficient models and virial coefficients from the correlation of Hayden and O'Connell (9) [see Table IV] by using the maximum likelihood parameter estimation method (10). The experimental data, together with the fit of the activity coefficient models that led to the best correlation, are plotted for each binary mixture in Figures 1–4. It is worth noting that the isothermal VLE data for pyrrolidine + cyclohexane at 298.15 K have also been reported in the literature (11). Our measured VLE data for pyrrolidine + cyclohexane at 313.15 and 333.15 K compare well with the data in the literature at 298.15 K, and all three sets could be correlated with the three-parameter Redlich-Kister equation. The sets of data at the three temperatures were found to be consistent in the

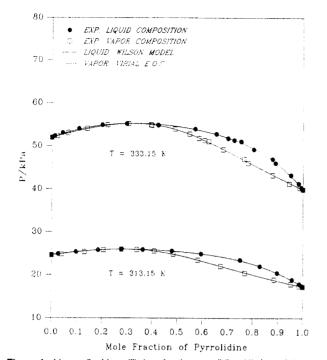
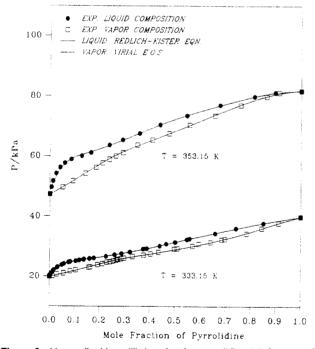


Figure 1. Vapor-liquid equilibrium for the pyrrolidine (1) + cyclohexane (2) system at 313.15 and 333.15 K. The points are our experimental data, and the lines resulted from the Wilson model.



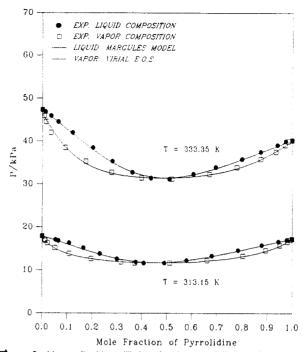
**Figure 2.** Vapor-liquid equilibrium for the pyrrolidine (1) + water (2) system at 333.15 and 353.15 K. The points are our experimental measurements, and the lines resulted from the Legendre polynomial expansion.

sense that the Gibbs-Helmholtz equation below can be used to interrelate the data. No VLE data have been reported for the other pyrrolidine-containing systems, except vapor pressure measurements in dilute aqueous solutions (12).

The molar heats of mixing,  $H^{E}$ , were estimated from the fitted Wilson  $G^{E}$  model at two temperatures with the Gibbs–Helmholtz relation:

$$H^{\mathsf{E}} = \partial (G^{\mathsf{E}}/T) / \partial (1/T) \tag{1}$$

where the partial derivative was approximated by the finite difference. The calculated values of  $H^{E}$  for mixtures of pyr-



**Figure 3.** Vapor-liquid equilibrium for the pyrrolidine (1) + ethanol (2) system at 313.15 and 333.35 K. The points are our experimental measurements, and the lines resulted from the Margules model.

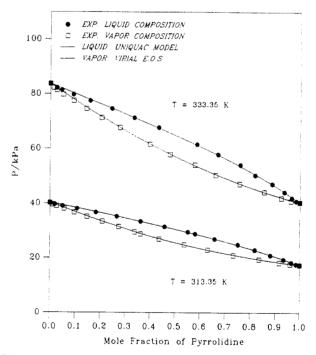


Figure 4. Vapor-liquid equilibrium for the pyrrolidine (1) + tetrahydrofuran (2) system at 313.35 and 333.35 K. The points are our experimental measurements, and the lines resulted from the UNIQUAC model.

rolidine with cyclohexane at temperatures ranging from 313.15 to 333.15 K are compared with directly measured data (*13*) at 298.15 K in Figure 5. There are no directly measured heats of mixing for the other mixtures we considered.

The Wilson model is best for correlating the experimental data for the pyrrolidine + cyclohexane mixture. The UNIQUAC model provides the best correlation of the pyrrolidine + tetrahydrofuran mixture, while the Margules model best correlates the experimental data for the pyrrolidine and ethanol mixture. However, no one model is satisfactory for all the mixtures studied here, and none of the five models gives a satisfactory correlation for the mixtures of pyrrolidine with water. These

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Table III. Experimental Vapor Pressure P, Liquid Mole Fractions  $x_1$ , and Vapor Mole Fractions  $y_1$  of Binary Mixtures at Constant Temperature T

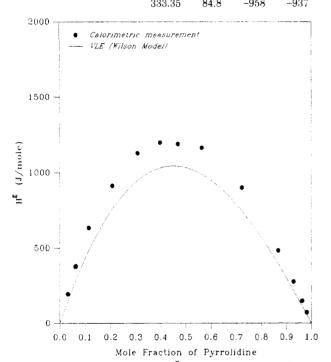
1	r = 313.15 H	X	Т	= 313.15 I	ζ	Т	= 333.15 H	K	Т	= 333.15 H	X
$\overline{P/kPa}$	<i>x</i> <sub>1</sub>	<i>y</i> <sub>1</sub>	P/kPa	<i>x</i> <sub>1</sub>	<i>y</i> <sub>1</sub>	P/kPa	<i>x</i> <sub>1</sub>	<i>y</i> <sub>1</sub>	$\overline{P/\mathrm{kPa}}$	<i>x</i> <sub>1</sub>	$\mathcal{Y}_1$
					lidine (1) +	Cyclohexa	ne (2)				
24.614	0.0000	0.0000	23.500	0.7498	0.5824	51.886	0.0000	0.0000	51.790	0.7013	0.5856
24.865	0.0264	0.0403	22.040	0.8287	0.6729	52.270	0.0109	0.0219	51.360	0.7255	0.6093
25.380	0.0981	0.1313	20.470	0.8977	0.7677	53.000	0.0425	0.0630	51.070	0.7527	0.6243
25.820	0.1854	0.2067	18.900	0.9574	0.8857	53.980	0.1077	0.1404	49.210	0.8030	0.6810
26.000	0.2787	0.2799	17.900	0.9863	0.9524	54.870	0.2004	0.2218	46.980	0.8777	0.7645
25.920	0.3639	0.3399	17.300	0.9963	0.9849	55.170	0.2981	0.3054	46.040	0.8897	0.7801
25.600	0.4791	0.4087	17.270	1.0000	1.0000	54.880	0.4224	0.3946	43.230	0.9516	0.8779
24.920	0.5959	0.4848	11.210	1.0000	1.0000	54.790	0.4233	0.3984	41.250	0.9824	0.9447
24.520	0.0909	0.4040				53.970	0.5709	0.4891	40.280	0.9936	0.9862
						52.800	0.6548	0.4891 0.5480	40.280 39.920	1.0000	1.0000
7	T = 333.15 ]	ĸ	7	' = 333.15 ]	κ		' = 353.15 I			' = 353.15 I	
$\frac{1}{P/kPa}$	x <sub>1</sub>	<i>y</i> <sub>1</sub>	$\frac{1}{P/kPa}$	x <sub>1</sub>	<i>y</i> <sub>1</sub>	$\frac{1}{P/kPa}$	x <sub>1</sub>	<i>y</i> <sub>1</sub>	$\frac{1}{P/kPa}$	x <sub>1</sub>	y <sub>1</sub>
<u></u>	~1					) + Water				1	
19.930	0.0000	0.0000	26.010	0.1775	0.2981	47.377	0.0000	0.0000	63.620	0.2383	0.3496
20.170	0.0020	0.0123	26.580	0.2270	0.3311	49.640	0.0061	0.0507	65.340	0.2920	0.4093
20.680	0.0041	0.0120	27.100	0.2614	0.3746	51.700	0.0121	0.0915	67.470	0.3581	0.4763
21.040	0.0079	0.0558	27.500		0.4021	54.190	0.0239	0.1415	70.340	0.4398	0.5572
21.040	0.0079	0.0338	28.040	0.3225	0.4021 0.4353	56.180	0.0405	0.1843	73.400	0.5469	0.6583
21.720								0.1343 0.2112	76.960	0.6785	0.7592
22.080	0.0179	0.1049	29.060	0.3740	0.4994	57.680	0.0591	0.2112	70.900		
22.920	0.0310	0.1577	29.210	0.3879	0.5099	58.880	0.0851	0.2377	79.850	0.8146	0.8634
23.090	0.0321	0.1633	30.080	0.4397	0.5701	60.000	0.1272	0.2645	81.230	0.8975	0.913
23.800	0.0496	0.1922	30.770	0.4671	0.5953	61.090	0.1644	0.2931	81.784	1.0000	1.0000
24.140	0.0579	0.2119	31.320	0.5026	0.6420						
24.680	0.0768	0.2305	32.230	0.5487	0.6860						
24.810	0.0832	0.2430	32.500	0.5597	0.6991						
25.050	0.1053	0.2553	34.310	0.6611	0.7847						
25.320	0.1200	0.2675	36.000	0.7435	0.8452						
25.540	0.1371	0.2750	37.750	0.8527	0.9130						
		0.0505	39.920	1.0000	1.0000						
25 650	0.1381	0.2737									
$25.650 \\ 25.840$	$0.1381 \\ 0.1602$	$0.2737 \\ 0.2869$	09.920								
25.840		0.2869		' = 313.15 l		<i>T</i>	' = 333.35 l	K	T	' = 333.35 ]	ĸ
25.840	0.1602 T = 313.15	0.2869 K			ĸ	$\frac{T}{P/kPa}$	$\frac{1}{x_1} = 333.35$		$\frac{T}{P/kPa}$	r = 333.35 ]	К у <sub>1</sub>
25.840	0.1602	0.2869 K y <sub>1</sub>	7	$\frac{r}{x_1} = 313.15$	$\frac{K}{y_1}$	P/kPa + Ethanol	(2)	<i>y</i> <sub>1</sub>	P/kPa	<i>x</i> <sub>1</sub>	<i>y</i> <sub>1</sub>
25.840	$   \begin{array}{r}     0.1602 \\     \overline{T = 313.15} \\     \hline     x_1 \\     \hline     0.0000   \end{array} $	$ \begin{array}{r} 0.2869 \\ \underline{\text{K}} \\ \underline{y_1} \\ 0.0000 \end{array} $	7 P/kPa 11.670	r = 313.15 $x_1$ $y_1$ 0.4904	K y <sub>1</sub> rolidine (1) 0.5122	P/kPa + Ethanol 47.334	(2) 0.0000	y <sub>1</sub> 0.0000	P/kPa 31.180	x <sub>1</sub> 0.5099	y <sub>1</sub> 0.519
25.840 7 P/kPa	$   \begin{array}{r}     0.1602 \\     T = 313.15 \\     x_1   \end{array} $	0.2869 K y <sub>1</sub>	7 P/kPa 11.670 12.270	r = 313.15 $x_1$ $x_1$ 0.4904 0.5802	K y <sub>1</sub> crolidine (1) 0.5122 0.6616	P/kPa + Ethanol 47.334 46.830	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \end{array}$	<i>y</i> <sub>1</sub> 0.0000 0.0076	P/kPa 31.180 32.340	x <sub>1</sub> 0.5099 0.6067	y <sub>1</sub> 0.519 0.670
25.840 <u>P/kPa</u> 17.877 17.050 16.800	$   \begin{array}{r}     0.1602 \\     \overline{T = 313.15} \\     \hline     x_1 \\     \hline     0.0000   \end{array} $	$ \begin{array}{r} 0.2869 \\ \underline{\text{K}} \\ \underline{y_1} \\ 0.0000 \end{array} $	7 P/kPa 11.670 12.270 13.330	r = 313.15 $x_1$ $x_1$ 0.4904 0.5802 0.6805	K y <sub>1</sub> rolidine (1) 0.5122	P/kPa + Ethanol 47.334	$\begin{array}{r} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \end{array}$	<i>y</i> <sub>1</sub> 0.0000 0.0076 0.0073	P/kPa 31.180 32.340 33.930	x <sub>1</sub> 0.5099 0.6067 0.6955	y <sub>1</sub> 0.519 0.670 0.778
25.840 <u>P/kPa</u> 17.877 17.050 16.800	$     \begin{array}{r}       0.1602 \\       \overline{T = 313.15} \\       \overline{x_1} \\       0.0000 \\       0.0544     \end{array} $	0.2869 K y <sub>1</sub> 0.0000 0.0105	7 P/kPa 11.670 12.270 13.330 14.640	r = 313.15 $x_1$ 0.4904 0.5802 0.6805 0.7837	K y <sub>1</sub> crolidine (1) 0.5122 0.6616 0.8027 0.8942	P/kPa + Ethanol 47.334 46.830 45.900 44.500	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \end{array}$	<i>y</i> <sub>1</sub> 0.0000 0.0076 0.0073 0.0143	P/kPa 31.180 32.340	x <sub>1</sub> 0.5099 0.6067	y <sub>1</sub> 0.519 0.670 0.778
25.840 P/kPa 17.877 17.050 16.800 16.310	$0.1602$ $T = 313.15$ $x_1$ $0.0000$ $0.0544$ $0.0652$ $0.1085$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213	7 P/kPa 11.670 12.270 13.330 14.640	r = 313.15 $x_1$ 0.4904 0.5802 0.6805 0.7837	K y <sub>1</sub> crolidine (1) 0.5122 0.6616 0.8027 0.8942	P/kPa + Ethanol 47.334 46.830 45.900 44.500	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \end{array}$	<i>y</i> <sub>1</sub> 0.0000 0.0076 0.0073 0.0143	P/kPa 31.180 32.340 33.930	x <sub>1</sub> 0.5099 0.6067 0.6955	$y_1$ 0.519 0.670 0.778 0.873
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180	$ \begin{array}{r} 0.1602\\ \overline{T = 313.15}\\ \hline x_1\\ \hline 0.0000\\ 0.0544\\ 0.0652\\ 0.1085\\ 0.1653\\ \end{array} $	$ \begin{array}{c} 0.2869 \\ \underline{K} \\ \hline y_1 \\ 0.0000 \\ 0.0105 \\ 0.0128 \\ 0.0213 \\ 0.0511 \\ \end{array} $	7 P/kPa 11.670 12.270 13.330 14.640 15.810	r = 313.15 $x_1$ $r_1$ 0.4904 0.5802 0.6805 0.7837 0.8781	K y <sub>1</sub> crolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503	P/kPa + Ethanol 47.334 46.830 45.900 44.500 41.990	$\begin{array}{r} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \end{array}$	y <sub>1</sub> 0.0000 0.0076 0.0073 0.0143 0.0350	P/kPa 31.180 32.340 33.930 35.810 37.490	x <sub>1</sub> 0.5099 0.6067 0.6955 0.7988 0.8739	y <sub>1</sub> 0.519 0.670 0.778 0.873 0.933
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840	$\begin{array}{r} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640	r = 313.15 $x_1$ $p_{y1}$ 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453	K y <sub>1</sub> rrolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808	P/kPa + Ethanol 47.334 46.830 45.900 44.500 41.990 38.470	$\begin{array}{r} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \end{array}$	y <sub>1</sub> 0.0000 0.0076 0.0073 0.0143 0.0350 0.0922	P/kPa 31.180 32.340 33.930 35.810 37.490 39.100	x <sub>1</sub> 0.5099 0.6067 0.6955 0.7988 0.8739 0.9408	y <sub>1</sub> 0.519 0.670 0.778 0.873 0.933 0.931
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070	r = 313.15 $x_1$ $p_{y1}$ 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9453 0.9792	K y <sub>1</sub> rolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930	P/kPa 47.334 46.830 45.900 44.500 41.990 38.470 35.320	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \end{array}$	$\begin{array}{c} y_1 \\ \hline 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \end{array}$	P/kPa 31.180 32.340 33.930 35.810 37.490 39.100 40.000	x <sub>1</sub> 0.5099 0.6067 0.6955 0.7988 0.8739 0.9408 0.9740	y <sub>1</sub> 0.519 0.670 0.778 0.873 0.933 0.933 0.971 0.984
25.840 <u>P/kPa</u> 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \end{array}$	0.2869 <u>X</u> <u>y</u> <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640	r = 313.15 $x_1$ $p_{y1}$ 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453	K y <sub>1</sub> rrolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \end{array}$	$\begin{array}{c} y_1 \\ \hline 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \end{array}$	P/kPa 31.180 32.340 33.930 35.810 37.490 39.100	x <sub>1</sub> 0.5099 0.6067 0.6955 0.7988 0.8739 0.9408	y <sub>1</sub> 0.519 0.670 0.778 0.873 0.933 0.933 0.971 0.984
25.840 27.877 17.877 17.050 16.800 15.180 13.840 12.650 11.900 11.670	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162 0.3722	P/kPa           11.670           12.270           13.330           14.640           15.810           16.640           17.070           17.270	r = 313.15 $x_1$ $p_{y1}$ 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000	K y <sub>1</sub> rrolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \end{array}$	$\begin{array}{c} y_1 \\ \hline 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230	x <sub>1</sub> 0.5099 0.6067 0.6955 0.7988 0.8739 0.9408 0.9740	<i>y</i> <sub>1</sub> 0.5196 0.670 0.7786 0.873' 0.9333 0.9711 0.9844 1.0006
25.840 27.877 17.877 17.050 16.800 15.180 13.840 12.650 11.900 11.670	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162 0.3722 K	P/kPa           11.670           12.270           13.330           14.640           15.810           16.640           17.070           17.270	$r = 313.15$ $x_1$ Pyr 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000 $r = 313.35$	K y <sub>1</sub> vrolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \end{array}$	$\begin{array}{c} y_1 \\ \hline 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230	x <sub>1</sub> 0.5099 0.6067 0.6955 0.7988 0.8739 0.9408 0.9740 1.0000	$\begin{array}{c} y_1 \\ 0.519 \\ 0.670 \\ 0.778 \\ 0.873 \\ 0.933 \\ 0.971 \\ 0.984 \\ 1.000 \end{array}$
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162 0.3722	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070 17.270 7	$r = 313.15$ $x_1$ Py1 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000 $r = 313.35$ $x_1$		P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \end{array}$	y1           0.0000           0.0076           0.0073           0.0143           0.0350           0.0922           0.1734           0.2771           0.3976           K	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           2           P/kPa	$\begin{array}{c} x_1 \\ 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline r = 333.35 \\ \hline x_1 \end{array}$	y <sub>1</sub> 0.5190 0.670 0.778 0.873 0.933 0.971 0.984 1.000 K K y <sub>1</sub>
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162 0.3722 K	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070 17.270 7 P/kPa	$r = 313.15$ $x_1$ Py1 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000 $r = 313.35$ $x_1$		P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \end{array}$	y1           0.0000           0.0076           0.0073           0.0143           0.0350           0.0922           0.1734           0.2771           0.3976           K	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230	$\begin{array}{c} x_1 \\ 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \end{array}$	y <sub>1</sub> 0.5190 0.670 0.7780 0.873 0.933 0.9711 0.984 1.0000 K <u>y<sub>1</sub></u>
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \\ \hline x_1 \end{array}$	$\begin{array}{c c} 0.2869 \\ \hline \\ $	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070 17.270 7 P/kPa 28.790	$r = 313.15$ $x_1$ Pyr 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000 $r = 313.35$ $x_1$ Pyrrolic	$ \frac{y_1}{y_1} $ rrolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K y_1 dine (1) + 7	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           Tetrahydrof	$\begin{array}{c} x_1 \\ \hline (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \\ \hline uran (2) \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \\ \hline \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           2           P/kPa           57.800	$\begin{array}{c} x_1 \\ 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline r = 333.35 \\ \hline x_1 \end{array}$	$y_1$ 0.5190 0.670 0.7780 0.873' 0.9333 0.9714 0.9844 1.0000 K y_1 0.984 0.4783
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200 39.640	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0195 \end{array}$	$\begin{array}{c c} 0.2869 \\ \hline \\ $	7           P/kPa           11.670           12.270           13.330           14.640           15.810           16.640           17.070           17.270           P/kPa           28.790           26.920	$r = 313.15$ $r_{1}$ $r_{1}$ $r_{2}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{1}$ $r_{3}$ $r_{1}$ $r_{2}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{2}$ $r_{2}$ $r_{2}$ $r_{2}$ $r_{1}$ $r_{2}$ $r_{2}$ $r_{2}$ $r_{1}$ $r_{2}$		P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           Tetrahydrof           83.690           82.140	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline \\ r = 333.35 \\ \hline x_1 \\ \hline \\ uran (2) \\ 0.0000 \\ 0.0260 \\ \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           2           P/kPa           57.800           54.030	$\begin{array}{c} x_1 \\ \hline 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline r = 333.35 \\ \hline x_1 \\ \hline 0.6718 \\ 0.7614 \\ \end{array}$	y1           0.5190           0.670           0.7780           0.873'           0.933:           0.971:           0.984           1.000           K           y1           0.478'           0.579
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200 39.640 39.060	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0195 \\ 0.0501 \\ \end{array}$	$\begin{array}{c c} 0.2869 \\ \hline \\ $	7           P/kPa           11.670           12.270           13.330           14.640           15.810           16.640           17.070           17.270           P/kPa           28.790           26.920           24.900	$r = 313.15$ $r_{1}$ $r_{1}$ $r_{2}$ $r_{3}$ $r_{1}$ $r_{2}$ $r_{3}$	$\begin{array}{c} K \\ \hline y_1 \\ \hline 0.5122 \\ 0.6616 \\ 0.8027 \\ 0.8942 \\ 0.9503 \\ 0.9808 \\ 0.9930 \\ 1.0000 \\ \hline K \\ \hline y_1 \\ \hline \\ 1ine (1) + 7 \\ 0.3616 \\ 0.4364 \\ 0.5381 \\ \hline \end{array}$	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           Tetrahydrof           83.690           82.140           81.310	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \\ \hline uran (2) \\ 0.0000 \\ 0.0260 \\ 0.0452 \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \\ \hline \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ 0.0245 \\ \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           7           P/kPa           57.800           54.030           50.250	$\begin{array}{c} x_1 \\ 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline r = 333.35 \\ x_1 \\ \hline 0.6718 \\ 0.7614 \\ 0.8203 \\ \end{array}$	$\begin{array}{c} y_1 \\ 0.5190 \\ 0.670 \\ 0.778 \\ 0.873 \\ 0.933 \\ 0.971 \\ 0.984 \\ 1.000 \\ \hline \\ K \\ y_1 \\ 0.478 \\ 0.579 \\ 0.662 \end{array}$
25.840 P/kPa 17.877 17.050 16.800 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200 39.640 39.060 38.070	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \\ \hline x_1 \\ \hline 0.0000 \\ 0.0195 \\ 0.0501 \\ 0.1082 \\ \end{array}$	$\begin{array}{c c} 0.2869 \\ \hline \\ $	7           P/kPa           11.670           12.270           13.330           14.640           15.810           16.640           17.070           17.270           7           P/kPa           28.790           26.920           24.900           22.950	$r = 313.15$ $r_{1}$ $r_{1}$ $r_{2}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{3}$ $r_{1}$ $r_{2}$ $r_{3}$ $r_{3}$ $r_{1}$ $r_{2}$ $r_{3}$ $r_{3}$ $r_{1}$ $r_{2}$ $r_{3}$	$K = \frac{y_1}{0.5122}$ orolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K = \frac{y_1}{0.3616} 0.4364 0.5381 0.6316	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           Tetrahydrof           83.690           82.140           81.310           79.700	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \\ \hline uran (2) \\ 0.0000 \\ 0.0260 \\ 0.0452 \\ 0.0914 \\ \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \\ \hline \\ K \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ 0.0245 \\ 0.0508 \\ \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           P/kPa           57.800           54.030           50.250           47.090	$\begin{array}{c} x_1 \\ \hline 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline r = 333.35 \\ \hline x_1 \\ \hline 0.6718 \\ 0.7614 \\ 0.8203 \\ 0.8874 \\ \end{array}$	$\begin{array}{c} y_1 \\ 0.5190 \\ 0.670 \\ 0.778 \\ 0.873 \\ 0.933 \\ 0.971 \\ 0.984 \\ 1.000 \\ \hline \\ K \\ y_1 \\ 0.478 \\ 0.579 \\ 0.662 \\ 0.759 \\ \end{array}$
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200 39.640 39.060 38.070 36.720	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline T = 313.35 \\ \hline x_1 \\ \hline 0.0000 \\ 0.0195 \\ 0.0501 \\ 0.1082 \\ 0.1827 \\ \end{array}$	$\begin{array}{c c} 0.2869 \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0105 \\ 0.0128 \\ 0.0213 \\ 0.0511 \\ 0.1082 \\ 0.1961 \\ 0.3162 \\ 0.3722 \\ \hline \\ \\ y_1 \\ \hline \\ \hline \\ \hline \\ \\ 0.0000 \\ 0.0100 \\ 0.0264 \\ 0.0559 \\ 0.0958 \\ \hline \end{array}$	7           P/kPa           11.670           12.270           13.330           14.640           15.810           16.640           17.070           17.270           28.790           26.920           24.900           22.950           21.010	r = 313.15 $x_1$ $p_{yr}$ 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9453 0.9792 1.0000 r = 313.35 $x_1$ $p_{yrrolic}$ 0.6594 0.7524 0.8194 0.8810	$K = \frac{y_1}{0.5122}$ orolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K = \frac{y_1}{0.3616} 0.4364 0.5381 0.6316 0.7335	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           Cetrahydrof           83.690           82.140           81.310           79.700           77.450	$\begin{array}{c} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \\ \hline uran (2) \\ 0.0000 \\ 0.0260 \\ 0.0452 \\ 0.0914 \\ 0.1588 \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \\ \hline \\ K \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ 0.0245 \\ 0.0508 \\ 0.0926 \\ \hline \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           P/kPa           57.800           54.030           50.250           47.090           44.160	$\begin{array}{c} x_1 \\ \hline 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline \end{array}$	$\begin{array}{c} y_1 \\ 0.5190 \\ 0.670 \\ 0.7780 \\ 0.933 \\ 0.933 \\ 0.9711 \\ 0.984 \\ 1.000 \\ \hline \\ K \\ y_1 \\ 0.478 \\ 0.579 \\ 0.662 \\ 0.759 \\ 0.856 \end{array}$
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200 39.640 39.060 38.070 36.720 35.180	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline \\ T = 313.35 \\ \hline \\ x_1 \\ \hline \\ 0.0000 \\ 0.0195 \\ 0.0501 \\ 0.1082 \\ 0.1827 \\ 0.2652 \\ \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162 0.3722 K y <sub>1</sub> 0.0000 0.0100 0.0264 0.0559 0.0958 0.1469	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070 17.270 7 P/kPa 28.790 26.920 24.900 22.950 21.010 19.490	$r = 313.15$ $x_1$ Pyr 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000 $r = 313.35$ $x_1$ Pyrrolic 0.5815 0.6594 0.7524 0.8194 0.8810 0.9344	$K = \frac{y_1}{0.5122}$ orolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K = \frac{y_1}{0.5361} orolidity of the second seco	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           P/kPa           Tetrahydroft           83.690           82.140           81.310           79.700           77.450           74.520	$\begin{array}{c} x_1 \\ \hline (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \\ \text{uran (2)} \\ 0.0000 \\ 0.0260 \\ 0.0452 \\ 0.0914 \\ 0.1588 \\ 0.2452 \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.2771 \\ 0.3976 \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ 0.0245 \\ 0.0508 \\ 0.0926 \\ 0.1439 \\ \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           7           P/kPa           57.800           54.030           50.250           47.090           44.160           42.000	$\begin{array}{c} x_1 \\ 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline \end{array}$	$\begin{array}{c} y_1 \\ 0.5196 \\ 0.670 \\ 0.7786 \\ 0.873' \\ 0.933 \\ 0.9711 \\ 0.984 \\ 1.0006 \\ \hline \\ K \\ y_1 \\ 0.478' \\ 0.579 \\ 0.662i \\ 0.759 \\ 0.856( \\ 0.924' \\ \end{array}$
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.670 11.670 P/kPa 40.200 39.640 39.060 38.070 36.720 35.180 33.360	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline \\ T = 313.35 \\ \hline \\ x_1 \\ \hline \\ 0.0000 \\ 0.0195 \\ 0.0501 \\ 0.1082 \\ 0.1827 \\ 0.2652 \\ 0.3624 \\ \end{array}$	$\begin{array}{c c} 0.2869 \\ \hline \\ $	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070 17.270 7 P/kPa 28.790 26.920 24.900 24.900 24.900 22.950 21.010 19.490 18.360	$\begin{array}{c} r = 313.15\\ \hline x_1\\ \hline Pyr\\ 0.4904\\ 0.5802\\ 0.6805\\ 0.7837\\ 0.8781\\ 0.9453\\ 0.9792\\ 1.0000\\ \hline r = 313.35\\ \hline x_1\\ \hline Pyrrolic\\ 0.5815\\ 0.6594\\ 0.7524\\ 0.8194\\ 0.8810\\ 0.9344\\ 0.9664\\ \end{array}$	$\frac{y_1}{y_1}$ rrolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K y_1 dine (1) + 7 0.3616 0.4364 0.5381 0.6316 0.7335 0.8361 0.9159	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           P/kPa           Cetrahydrof           83.690           82.140           81.310           77.700           74.520           71.180	$\begin{array}{r} x_1 \\ (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline x_1 \\ \hline $	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.3976 \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ 0.0245 \\ 0.0508 \\ 0.0926 \\ 0.1439 \\ 0.2046 \\ \hline \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           7           P/kPa           57.800           54.030           50.250           44.160           42.000           40.880	$\begin{array}{c} x_1 \\ \hline 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline \end{array}$	$\begin{array}{c} y_1 \\ 0.5196 \\ 0.670 \\ 0.778 \\ 0.933 \\ 0.933 \\ 0.9711 \\ 0.984 \\ 1.0006 \\ \hline \\ \textbf{K} \\ \hline \\ y_1 \\ \hline \\ 0.478 \\ 0.579 \\ 0.662 \\ 0.759 \\ 0.856 \\ 0.924 \\ 0.963 \\ \end{array}$
25.840 P/kPa 17.877 17.050 16.800 16.310 15.180 13.840 12.650 11.900 11.670 P/kPa 40.200 39.640 39.060 38.070 36.720 35.180	$\begin{array}{c} 0.1602 \\ \hline T = 313.15 \\ \hline x_1 \\ \hline \\ 0.0000 \\ 0.0544 \\ 0.0652 \\ 0.1085 \\ 0.1653 \\ 0.2311 \\ 0.3001 \\ 0.3762 \\ 0.4075 \\ \hline \\ T = 313.35 \\ \hline \\ x_1 \\ \hline \\ 0.0000 \\ 0.0195 \\ 0.0501 \\ 0.1082 \\ 0.1827 \\ 0.2652 \\ \end{array}$	0.2869 K y <sub>1</sub> 0.0000 0.0105 0.0128 0.0213 0.0511 0.1082 0.1961 0.3162 0.3722 K y <sub>1</sub> 0.0000 0.0100 0.0264 0.0559 0.0958 0.1469	7 P/kPa 11.670 12.270 13.330 14.640 15.810 16.640 17.070 17.270 7 P/kPa 28.790 26.920 24.900 22.950 21.010 19.490	$r = 313.15$ $x_1$ Pyr 0.4904 0.5802 0.6805 0.7837 0.8781 0.9453 0.9792 1.0000 $r = 313.35$ $x_1$ Pyrrolic 0.5815 0.6594 0.7524 0.8194 0.8810 0.9344	$K = \frac{y_1}{0.5122}$ orolidine (1) 0.5122 0.6616 0.8027 0.8942 0.9503 0.9808 0.9930 1.0000 K = \frac{y_1}{0.5361} orolidity of the second seco	P/kPa           P/kPa           47.334           46.830           45.900           44.500           41.990           38.470           35.320           32.760           31.430           P/kPa           P/kPa           Tetrahydroft           83.690           82.140           81.310           79.700           77.450           74.520	$\begin{array}{c} x_1 \\ \hline (2) \\ 0.0000 \\ 0.0123 \\ 0.0357 \\ 0.0644 \\ 0.1216 \\ 0.2027 \\ 0.2806 \\ 0.3604 \\ 0.4352 \\ \hline r = 333.35 \\ \hline x_1 \\ \text{uran (2)} \\ 0.0000 \\ 0.0260 \\ 0.0452 \\ 0.0914 \\ 0.1588 \\ 0.2452 \end{array}$	$\begin{array}{c} y_1 \\ \hline \\ 0.0000 \\ 0.0076 \\ 0.0073 \\ 0.0143 \\ 0.0350 \\ 0.0922 \\ 0.1734 \\ 0.2771 \\ 0.2771 \\ 0.3976 \\ \hline \\ \hline \\ \hline \\ y_1 \\ \hline \\ 0.0000 \\ 0.0123 \\ 0.0245 \\ 0.0508 \\ 0.0926 \\ 0.1439 \\ \end{array}$	P/kPa           31.180           32.340           33.930           35.810           37.490           39.100           40.000           40.230           7           P/kPa           57.800           54.030           50.250           47.090           44.160           42.000	$\begin{array}{c} x_1 \\ 0.5099 \\ 0.6067 \\ 0.6955 \\ 0.7988 \\ 0.8739 \\ 0.9408 \\ 0.9740 \\ 1.0000 \\ \hline \end{array}$	<i>y</i> <sub>1</sub> 0.519 <del>0</del> 0.6701 0.7780 0.8737 0.9338 0.9716 0.9844 1.0000 K

data could only be correlated with a five-parameter Legendre polynomial expansion. The VLE phase envelope of the pyrrolidine + water mixture has a peculiar shape, which is not fit well by existing excess Gibbs free energy models. It is interesting to compare the shape of the VLE phase envelope for this mixture with that of diethylamine + methanol mixture measured by Srivastava and Smith (14). They found a double azeotrope in the diethylamine + methanol mixture at one isotherm and only a single azeotrope at another isotherm; the pyrrolidine + water mixture shows incipient azeotropic behavior. The reason why we compare these two systems is because of their similar molecular interactions. Pyrrolidine and diethylamine are both secondary amines; the former is cyclic and the latter noncyclic. Water and methanol, the second components, are both hydrogen-bonding molecules. Consequently, these two mixtures should have a similar phase behavior. Although there is no azeotrope in the pyrrolidine + water mixture in the temperature range we measured, the shape of the phase envelope suggests the mixture may form an azeotrope at different temperatures. Thus, while the shape of the pyrrolidine + water phase envelope is unusual, the behavior is plausible. The data for this system, and indeed for all the systems studied, satisfy the point-to-point consistency test.

The predictive UNIFAC model with parameters reported in the literature (15) results in poor predictions for all the mixtures studied here. This confirms our suspicion and the findings of

Table IV. Second Molar Virial Coefficients  $B_{ij}$  and Liquid Molar Volumes  $V_i$  (cm<sup>3</sup> mol<sup>-1</sup>) as a Function of Temperature T

component	T/K	$V_i$	B <sub>ii</sub>	B <sub>12</sub>
pyrrolidine $(i = 1)$	313.15	84.7	-1235	
	313.35	84.7	-1233	
	333.15	86.6	-1054	
	333.35	86.6	-1052	
	353.15	88.4	-914	
cyclohexane $(i = 2)$	313.15	111.9	-1691	-1278
	333.15	114.6	-1423	-1081
water $(i = 2)$	333.15	18.4	-912	-479
	353.15	18.8	-637	-415
ethanol $(i = 2)$	313.15	59.2	-1652	-985
	333.35	60.9	-1201	-847
tetrahydrofuran ( $i = 2$ )	313.35	83.4	-1118	-1101
-	222.25	84.8	_958	-937



**Figure 5**. Molar excess enthalpy,  $H^{\text{E}}$ , for the pyrrolidine (1) + cyclohexane (2) system. The points are direct calorimetric measurements (13), and the lines resulted from the values of  $G^{\text{E}}$  generated from our vapor-liquid equilibrium measurements.

Tine and Kehiaian (16) that the cyclic secondary amine group in pyrrolidine may have to be considered a different functional group from the noncyclic secondary amine group in future improvements of the UNIFAC model. It is also worth noting that our VLE data reported here can be reproduced by the DISQ-UAC model with reported parameters (*17*), with average deviations in pressure of the order of 0.5 kPa and in composition of 0.01 or better.

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Registry No. Pyrrolidine, 123-75-1; cyclohexane, 110-82-7; ethanol, 64-17-5; tetrahydrofuran, 109-99-9.

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# Thermodynamics of Binary Mixtures Containing Alkanenitriles. 1. Excess Enthalpies of Some n-Alkanenitrile + n-Alkane or + Cyclohexane Mixtures

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A Tian-Calvet-type calorimeter was used to determine excess enthalples,  $H^{E}$ , as a function of concentration at atmospheric pressure and 298.15 K for some binary liquid mixtures containing linear alkanenitriles of the general formula  $CH_3(CH_2)_{n-2}CN$  (n = 2, 3, 4, 5) with *n*-alkanes (hexane, heptane) or cyclohexane.

#### Introduction

This work is part of a systematic study of the thermodynamic properties of organic mixtures, TOM Project (1-16), with the purpose of characterizing the type and magnitude of molecular interactions in binary liquid mixtures and to improve the group contribution models currently used to predict thermodynamic