# Liquid Densities of Propane + Linear Low-Density Polyethylene Systems at (354-378) K and (4.00-7.00) MPa 

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#### Abstract

Liquid densities have been measured with a variable volume cell for propane + linear low-density polyethylene systems. The temperature and pressure ranges studied are (354-378) K and (4.00-7.00) MPa, and polyethylene mass fractions in the mixtures vary between 0 and 0.0355 . Altogether, 107 liquid density data points are reported. The results obtained for pure propane agree well with literature values. Results show that densities increase almost linearly with increasing mass fraction of the polymer.


## Introduction

Phase equilibria of polyethylene + hydrocarbon systems has been widely investigated over the past few decades. In some investigations, long-chain al kanes have been used as model components for small polyethylene molecules. However, the liquid densities of the systems are rarely reported. Liquid density is nevertheless a fundamental physical property, thus being interesting in the theoretical sense, and al so a property that is often needed in practical engineering calculations and process control.

Earlier phase equilibrium studies on related systems include the papers by Peters et al. (1989, 1992, 1993) on the phase equilibria of propane + long-chain alkane systems and by Condo et al. (1992) on propane + polyethylene systems. Liquid densities on similar mixtures have been previously published by Nieuwoudt (1996), who reported both vapor-liquid equilibria and densities for the system butane + hexacontane, and by Aalto and Liukkonen (1996), who reported density and bubble point pressure measurements in propane + long-chain alkane systems.

In this work, liquid densities for propane + linear lowdensity polyethylene mixtures have been measured using a variable volume optical cell. The temperature and pressure regions studied are in the vicinity of the critical point of propane. The reported data points are located in the one-phase region, i.e., above the cloud point pressure.

## Experimental Section

Materials. The propane used in these measurements was supplied by AGA Oy (purity $99.95 \mathrm{~mol} \%$ ). Linear Iowdensity pol yethylene was obtained from Borealis Pilot Plant and subsequently fractionated using propane as the solvent. The fraction that had been dissolved in propane, which had a number average molecular weight $\mathrm{M}_{\mathrm{n}}$ of 300 $\mathrm{g} / \mathrm{mol}$ (weight average molecular weight $\mathrm{M}_{\mathrm{w}}=490 \mathrm{~g} / \mathrm{mol}$ ), was used in the reported measurements.

Apparatus. Measurements were performed using a DB Robinson J efri sapphire glass cell apparatus. This apparatus, as well as the procedure, were described in more detail in an earlier paper (Aalto and Liukkonen, 1996). In brief, the glass cylinder is thermostated within an air bath,

[^0]and the volume of the sample (and therefore pressure as well) can be varied by moving the piston inside the cylinder. The maximum volume of the cylinder is approximately 56 $\mathrm{cm}^{3}$. Temperature and pressure can be measured with sensors located in the top of the cylinder. Sample volume can be calculated from the cylinder cross-sectional area and the positions of the piston and the upper end of the cylinder, which are determined with a cathetometer. Because the cylinder is transparent, it is possible to see the experimental fluid and make sure the system is in one phase.

Procedure. A known mass of the polymer sample is loaded into the cylinder. The amount of propane added into the cylinder is determined by measuring the volume of the propane in the liquid state (at known temperature T and pressure P). The density of propane at those conditions is estimated from the HBT correlation (Thomson et al., 1982), which is known to be highly accurate. The amount of propane is corrected for the volume taken by the pol yethylene sample. This volume is obtained from the known mass of PE and by approximating the PE density with the density of the unfractionated polymer, which is $0.937 \mathrm{~g} / \mathrm{cm}^{3}$ (gradient col umn). The sample is now heated to the first experimental temperature, and the system is given approximately 1 h timeto reach equilibrium. Sample volumes are then measured at all experimental pressures while the temperature is kept constant. The measurements are then continued following the same steps: heating, equilibration time, and determination of sample volumes at experimental pressures.

Accuracy. The uncertainties in the measured temperatures and pressures are $\pm 0.05 \mathrm{~K}$ and $\pm 0.001 \mathrm{MPa}$, respectively. The location of the piston and the upper end of the cylinder can be determined within $\pm 0.001 \mathrm{~cm}$ each, which results in $\pm 0.01 \mathrm{~cm}^{3}$ uncertainty in the volume (typically $30-40 \mathrm{~cm}^{3}$ at the experimental conditions). The mass of polyethylene is known within $\pm 0.0001 \mathrm{~g}$, while the determined mass of propane has an uncertainty of $\pm 0.010$ g. The typical mass of propane used in the measurements is $13-14 \mathrm{~g}$, and the mass of polyethylene is $0.130-0.500 \mathrm{~g}$ depending on the intended mass fraction. Consequently, the relative error in the mass fraction of PE becomes $\pm 0.15 \%$. The reported density values should be accurate within $\pm 0.19 \%$.

Table 1. Measured Densities for Propane (1) + LLDPE (2)

| T/K | P/MPa | $\rho /\left(\mathrm{kg} \cdot \mathrm{m}^{-3}\right)$ | T/K | P/MPa | $\rho /\left(\mathrm{kg} \cdot \mathrm{m}^{-3}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{w}_{2}=0$ |  |  |  |  |  |
| 358.7 | 3.999 | 366.5 | 368.4 | 4.151 | 292.1 |
| 358.7 | 5.001 | 384.1 | 368.7 | 4.998 | 342.6 |
| 358.8 | 5.501 | 391.0 | 368.7 | 5.498 | 356.1 |
| 358.8 | 5.998 | 395.6 | 368.7 | 5.999 | 365.1 |
| 358.8 | 6.403 | 399.7 | 368.7 | 6.498 | 373.7 |
| 358.8 | 7.003 | 405.6 | 368.7 | 7.000 | 380.5 |
| 363.5 | 4.004 | 340.3 | 373.2 | 4.549 | 244.2 |
| 363.6 | 4.996 | 366.7 | 373.5 | 4.996 | 308.7 |
| 363.7 | 5.506 | 375.9 | 373.6 | 5.490 | 331.7 |
| 363.7 | 6.006 | 383.1 | 373.6 | 5.994 | 347.3 |
| 363.7 | 6.402 | 387.8 | 373.6 | 6.405 | 355.2 |
| 363.7 | 7.001 | 394.0 | 373.6 | 7.004 | 366.1 |
| $\mathrm{w}_{2}=0.0094$ |  |  |  |  |  |
| 358.5 | 4.998 | 388.1 | 363.5 | 6.197 | 387.3 |
| 358.6 | 5.502 | 395.1 | 363.5 | 6.399 | 389.2 |
| 358.6 | 5.998 | 399.0 | 363.5 | 6.603 | 392.5 |
| 358.6 | 6.197 | 400.8 | 363.6 | 6.995 | 395.6 |
| 358.6 | 6.406 | 402.3 | 368.3 | 6.004 | 369.6 |
| 358.6 | 6.596 | 404.5 | 368.4 | 6.201 | 372.7 |
| 358.6 | 7.000 | 407.0 | 368.4 | 6.399 | 375.5 |
| 363.5 | 5.502 | 378.2 | 368.4 | 6.599 | 378.9 |
| 363.5 | 5.998 | 384.6 | 368.4 | 7.001 | 382.6 |
| $\mathrm{w}_{2}=0.0097$ |  |  |  |  |  |
| 353.8 | 3.999 | 389.4 | 373.5 | 6.198 | 356.0 |
| 353.9 | 4.994 | 401.8 | 373.5 | 6.399 | 361.5 |
| 353.9 | 5.498 | 407.0 | 373.5 | 6.603 | 364.7 |
| 353.9 | 5.998 | 411.5 | 373.5 | 6.998 | 370.8 |
| 353.9 | 6.200 | 413.1 | 378.2 | 6.202 | 337.5 |
| 353.9 | 6.400 | 414.9 | 378.2 | 6.400 | 342.2 |
| 353.9 | 6.603 | 415.7 | 378.2 | 6.600 | 346.9 |
| 353.9 | 7.004 | 419.9 | 378.2 | 6.999 | 354.9 |
| $\mathrm{w}_{2}=0.0101$ |  |  |  |  |  |
| 358.5 | 4.996 | 387.7 | 363.5 | 6.200 | 387.4 |
| 358.5 | 5.502 | 393.7 | 363.5 | 6.398 | 390.1 |
| 358.5 | 5.997 | 398.4 | 363.5 | 6.599 | 392.2 |
| 358.5 | 6.203 | 400.6 | 363.5 | 6.998 | 397.0 |
| 358.5 | 6.400 | 403.3 | 368.3 | 5.997 | 369.4 |
| 358.5 | 6.602 | 405.0 | 368.3 | 6.202 | 372.8 |
| 358.5 | 7.000 | 409.0 | 368.3 | 6.402 | 375.9 |
| 363.5 | 5.497 | 379.2 | 368.3 | 6.602 | 378.1 |
| 363.5 | 6.003 | 385.4 | 368.3 | 6.999 | 383.7 |
| $w_{2}=0.0232$ |  |  |  |  |  |
| 358.7 | 5.000 | 393.7 | 363.7 | 6.203 | 394.7 |
| 358.7 | 5.498 | 400.5 | 363.7 | 6.401 | 396.7 |
| 358.7 | 6.000 | 404.7 | 363.7 | 6.603 | 399.4 |
| 358.7 | 6.204 | 407.2 | 363.7 | 7.000 | 403.3 |
| 358.7 | 6.398 | 409.2 | 368.6 | 5.997 | 377.0 |
| 358.7 | 6.601 | 411.2 | 368.6 | 6.202 | 379.9 |
| 358.8 | 7.000 | 414.8 | 368.6 | 6.399 | 382.9 |
| 363.7 | 5.501 | 385.3 | 368.6 | 6.602 | 385.6 |
| 363.7 | 6.001 | 392.3 | 368.6 | 6.999 | 389.7 |
| $\mathrm{w}_{2}=0.0355$ |  |  |  |  |  |
| 358.7 | 5.001 | 396.6 | 368.5 | 6.001 | 381.1 |
| 358.7 | 5.500 | 402.7 | 368.5 | 6.199 | 384.2 |
| 358.7 | 6.001 | 407.9 | 368.5 | 6.399 | 387.1 |
| 358.7 | 6.202 | 410.1 | 368.5 | 6.600 | 389.5 |
| 358.7 | 6.401 | 411.5 | 368.5 | 6.997 | 393.7 |
| 358.7 | 6.601 | 413.1 | 368.5 | 7.097 | 395.0 |
|  | 6.999 |  |  |  |  |

## Results and Discussion

The results of the density measurements are shown in Table 1. Measurements were made at temperatures from 354 to 378 K with 5 K intervals. The pressures start at 4.00 MPa and go up to 7.00 MPa . Mass fractions $\mathrm{w}_{2}$ of the polymer are 0.0, 0.0094, 0.0097, 0.0101, 0.0232, and 0.0355. The results listed are all in the one-phase (liquid or supercritical fluid) region, which is the reason values are not given at lower pressures for all isotherms.


Figure 1. Deviations of measured densities and literature values of pure propane from the BWR-type equation of state by Younglove and Ely (1987). Data sources: - this work; $\square$ Dittmar et al. (1962); $\diamond$ Defibaugh and Moldover (1997); $\Delta$ Vargaftik (1975).


Figure 2. Isotherms obtained for the mixtures where the mass fraction of PE $\left(w_{2}\right)$ is approximately 0.01 . The mixture will separate into two liquid phases at low pressures, which is illustrated by sketching the two-phase region boundary. Symbols: ■ 354 K , $359 \mathrm{~K}, \diamond 359 \mathrm{~K}, \Delta 364 \mathrm{~K}, \Delta 364 \mathrm{~K}, ~ \bullet 368 \mathrm{~K}, ~ ○$ 368 K, $\times 374$ K, +378 K .

In Figure 1, the measured densities and literature values for pure propane are compared to the BWR-type equation of state by Younglove and Ely (1987), which is based on critically evaluated data, and it is one of the most accurate models available for pure propane. The comparison shows that there is scatter in the literature values, and the results obtained in this work agree well with the BWR equation of state. The average relative deviation between this work and the BWR EOS is $0.45 \%$, which is larger than the accuracy of $\pm 0.19 \%$ stated in the previous section. However, according to Younglove and Ely (1987), typical uncertainties in propane densities obtained from the BWR EOS are $0.1 \%$ (liquid density below $\mathrm{T}_{\mathrm{c}}$ ) and $1.5 \%$ (critical region), and all the data obtained in this work are at reduced temperatures $\mathrm{T}_{\mathrm{r}} \geqslant 0.97$.

Figure 2 shows isotherms obtained for the mixtures where the mass fraction of the polymer $\left(w_{2}\right)$ is approximately 0.01 . By looking at the two-phase region in Figure 2, it is clear that the higher the temperature, the higher the pressure has to be in order to keep the mixture in one phase. Phase separation occurs because propane is close to its critical point and propane density decreases


Figure 3. Comparison of this work (black symbols) to earlier results (white symbols) obtained for the propane (1) + pentacontane (2) system (Aalto and Liukkonen, 1996). Three isobars (5.5 MPa , $6.0 \mathrm{MPa}, 7.0 \mathrm{MPa}$ ) are shown at 364 K . Notations PE and c50 refer to the heavier component in the mixture. Symbols: PE, 5.5 MPa; $\square \mathrm{c} 50,5.5 \mathrm{MPa} ; ~ P E, 6.0 \mathrm{MPa} ; \diamond \mathrm{c} 50,6.0 \mathrm{MPa}$; $\boldsymbol{\Delta}$ $\mathrm{PE}, 7.0 \mathrm{MPa} ; \Delta \mathrm{c} 50,7.0 \mathrm{MPa}$.
rapidly with increasing temperature (at constant pressure), which results in a substantial increase in the freevolume difference between the components (Folie and Radosz, 1995). In Figure 3, the measured mixture density is shown as a function of $w_{2}$, and compared to earlier results on the propane + pentacontane system (Aalto and Liukkonen, 1996). Figure 3 shows that the mixture densities are almost linearly dependent of $w_{2}$, and they are not very sensitive to the molecular weight of the heavy component.

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## Literature Cited

Aalto, M.; Liukkonen, S. Bubble Point Pressures and Densities for the Binary Systems of Propane with Triacontane, Hexatriacontane, Tetracontane, Pentacontane, and Squalane at 353-373 K and 4.007.00 MPa. J. Chem. Eng. Data 1996, 41, 79-83.

Condo, P. D.; Colman, E. J.; Ehrlich, P. Phase Equilibria of Linear Polyethylene with Supercritical Propane. Macromolecules 1992, 25, 750-753.
Defibaugh, D. R.; Moldover, M. R. Compressed and Saturated Liquid Densities for 18 Halogenated Organic Compounds. J. Chem. Eng. Data 1997, 42, 160-168.
Dittmar, P.; Schulz, F.; Strese, G. Pressure/Density/TemperatureValues for Propane and Propylene. Chem.-Ing.-Tech. 1962, 34, 437441.

Folie, B.; Radosz, M. Phase Equilibria in High-Pressure Polyethylene Technology. Ind. Eng. Chem. Res. 1995, 34, 1501-1516.
Nieuwoudt, I. Vapor-Liquid Equilibria and Densities for the System Butane + H exacontane. J. Chem. Eng. Data 1996, 41, 1024-1027.
Peters, C. J.; van der Kooi, H. J.; de Roo, J. L.; de Swaan Arons, J.; Gallagher, J. S.; Levelt Sengers, J. M. H. The Search for Tricriticality in Binary Mixtures of Near-Critical Propane and Normal Paraffins. Fluid Phase Equilib. 1989, 51, 339-351.
Peters, C. J.; de Roo, J. L.; de Swaan Arons, J. Measurements and calculations of phase equilibria in binary mixtures of propane + tetratriacontane. Fluid Phase Equilib. 1992, 72, 251-266.
Peters, C. J.; de Roo, J. L.; de Swaan Arons, J. Phase equilibria in binary mixtures of propane and hexacontane. Fluid Phase Equilib. 1993, 85, 301-312.
Thomson, G. H.; Brobst, K. R.; Hankinson, R. W. An Improved Correlation for Densities of Compressed Liquids and Liquid Mixtures. AIChE J. 1982, 28, 671-676.
Vargaftik, N. B. Tables on the Thermophysical Properties of Liquids and Gases, 2nd ed.; Hemisphere Publishing Corporation: Washington, DC, 1975.
Younglove, B. A.; Ely, J. F. Thermophysical Properties of Fluids. II. Methane, Ethane, Propane, I sobutane, and Normal Butane. J . Phys. Chem. Ref. Data 1987, 16, 577-798.

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