

# Excess Enthalpies for the Systems *o*-Xylene + Cyclohexanol + Phenol and *o*-Xylene + Cyclohexanol + 1,3-Butanediol at 318.15 K

Mati Kuus, Helle Kirss, Enn Siimer, and Ludmilla Kudryavtseva\*

Institute of Chemistry, EE-0026 Tallinn, Estonia

Excess molar enthalpies ( $H^E$ ) at 318.15 K are reported for two ternary systems, *o*-xylene + cyclohexanol + phenol and *o*-xylene + cyclohexanol + 1,3-butanediol, and for two constituent binaries formed by *o*-xylene with phenol and 1,3-butanediol. The ternary system containing phenol exhibits regions of both exothermic and endothermic mixing,  $H^E$  for the other ternary system are endothermic. Owing to partial miscibility in the *o*-xylene + 1,3-butanediol system, the ternary system containing 1,3-butanediol includes a region with two coexisting liquid phases. A modified Redlich–Kister equation fitted to experimental results provides a satisfactory mathematical representation of  $H^E$  data for the *o*-xylene + cyclohexanol + 1,3-butanediol system.

## Introduction

Very little information on excess enthalpies ( $H^E$ ) in ternary systems containing phenols and diols is available. In our earlier works (Kirss et al., 1995, 1997; Kuus et al., 1996, Siimer et al., 1997), we reported  $H^E$  data for some ternary systems composed of phenols and diols with alcohols and alkanes. A continuing development of solution models for describing the thermodynamic properties of ternary systems requires a large experimental database.

The present paper reports our results on  $H^E$  in the ternary systems *o*-xylene + cyclohexanol + phenol and *o*-xylene + cyclohexanol + 1,3-butanediol. There appears to be no data for excess enthalpies of these systems in the literature.

Additionally, no  $H^E$  data have been previously reported for the binary systems *o*-xylene + phenol and *o*-xylene + 1,3-butanediol at 318.15 K. *o*-Xylene + phenol is completely miscible, but *o*-xylene + 1,3-butanediol is a partially miscible system. Existing measurements of mutual solubilities in binary glycols + aromatic hydrocarbons systems are limited to systems containing benzene, *p*-xylene, and toluene (Mandik and Lešek, 1982). Our measurements were used to further test the descriptive abilities of the modified Redlich–Kister equation reported earlier (Siimer et al., 1997).

## Experimental Section

A Calvet-type microcalorimeter DAK-1-1 and the static apparatus for mutual solubility measurements as well as experimental procedures have been fully described (Kuus et al., 1996) and were unchanged for this work. All mixtures were prepared by mass. The possible errors in mole fraction and excess enthalpy are estimated to be less than 0.0005 and  $\pm 2\%$ , respectively. The last value is a result of the chemical and electrical calibration procedures (Kirss et al., 1996).

The purities of chemicals supplied by Reakhim (Ukraine) were tested chromatographically, and they were found to be more than 99.5%. The densities were measured by

\* To whom correspondence should be addressed. E-mail: siimer@argus.chemnet.ee.

Table 1. Densities ( $d$ ) of Pure Compounds

compound	$T/K$	$d/\text{kg}\cdot\text{m}^{-3}$	
		obsvd	lit.
<i>o</i> -xylene	293.15	880.1	880.1 <sup>a</sup>
cyclohexanol	303.15	941.5	941.6 <sup>b</sup>
phenol	314.15	1057.1	1057.6 <sup>b</sup>
1,3-butanediol	293.15	1005.3	1005.3 <sup>b</sup>

<sup>a</sup> TRC d-3290, 1996. <sup>b</sup> Dean, 1992.

Table 2. Measured Excess Enthalpy for Binary Systems *o*-Xylene (1) + Phenol (2) and *o*-Xylene (1) + 1,3-Butanediol (2) at 318.15 K

$x_1$	$H^E/\text{J}\cdot\text{mol}^{-1}$	$x_1$	$H^E/\text{J}\cdot\text{mol}^{-1}$
<i>o</i> -Xylene (1) + Phenol (2)			
0.154	407	0.746	1026
0.268	650	0.795	929
0.383	890	0.878	752
0.508	1051	0.906	625
0.640	1089		
<i>o</i> -Xylene (1) + 1,3-Butanediol (2)			
0.055	290	0.640 <sup>a</sup>	383
0.104	484	0.729 <sup>a</sup>	359
0.212 <sup>a</sup>	508	0.815 <sup>a</sup>	335
0.313 <sup>a</sup>	461	0.871 <sup>a</sup>	313
0.400 <sup>a</sup>	443	0.945 <sup>a</sup>	280
0.496 <sup>a</sup>	430		

<sup>a</sup> Total mole fraction of two liquids.

means of a capillary pycnometer with an accuracy of  $\pm 2.0 \times 10^{-1} \text{ kg}\cdot\text{m}^{-3}$ . As seen from Table 1, the measured densities are in good agreement with the literature data.

Cyclohexanol, 1,3-butanediol, and phenol were stored in a drybox and protected from light.

The binodal curve in the ternary system *o*-xylene + cyclohexanol + 1,3-butanediol was measured by titrating *o*-xylene + 1,3-butanediol with cyclohexanol. *o*-Xylene + 1,3-butanediol mixtures were prepared by adding known masses of components into the vessel. The accuracy of cloud points was estimated to be about 0.35 mass %. The temperature of the water bath was controlled at 318.15 K within  $\pm 0.1$  K.

We could not determine cloud points in the *o*-xylene + 1,3-butanediol system in the *o*-xylene-rich region.

**Table 3. Coefficients  $A_i$  of the Redlich–Kister (Eq 2) and Standard Deviations  $\sigma(H^E)$  for Binary Systems at 318.15 K**

system	$A_0$	$A_1$	$A_2$	$A_3$	$A_4$	$A_5$	$\sigma(H^E)/J\cdot\text{mol}^{-1}$
<i>o</i> -xylene + phenol	4185.916	1823.77	-88.97	1167.48	2709.92	0	12.1
<i>o</i> -xylene + 1,3-butanediol	1735.56	320.27	645.48	-6661.63	5241.77	7594.02	24.0

**Table 4. Experimental Excess Enthalpies for the Ternary Systems *o*-Xylene (1) + Cyclohexanol (2) + Phenol (3) and *o*-Xylene (1) + Cyclohexanol (2) + 1,3-Butanediol (3) at 318.15 K**

$x_1$	$x_2$	$x_3$	$H^E/J\cdot\text{mol}^{-1}$	$x_1$	$x_2$	$x_3$	$H^E/J\cdot\text{mol}^{-1}$
<b><i>o</i>-Xylene (1) + Cyclohexanol (2) + Phenol (3)</b>							
$x_1/x_2 = 1.00$				$x_1/x_3 = 2.00$			
0.444	0.444	0.112	763	0.581	0.129	0.290	395
0.384	0.384	0.232	90	0.480	0.280	0.240	155
0.287	0.287	0.426	-449	0.379	0.432	0.189	236
0.150	0.150	0.700	-465	0.142	0.787	0.071	280
$x_1/x_2 = 0.33$				$x_2/x_3 = 1.00$			
0.206	0.617	0.177	-82	0.906	0.047	0.047	510
0.154	0.462	0.384	-908	0.798	0.101	0.101	577
0.093	0.279	0.628	-1058	0.660	0.170	0.170	483
0.050	0.149	0.801	-690	0.102	0.449	0.449	-1175
$x_1/x_2 = 2.00$				$x_2/x_3 = 0.67$			
0.546	0.273	0.181	419	0.808	0.077	0.115	561
0.449	0.224	0.327	40	0.655	0.138	0.207	486
0.203	0.102	0.695	-83	0.522	0.191	0.287	230
0.097	0.048	0.855	-37	0.133	0.347	0.520	-1005
$x_1/x_3 = 1.00$				$x_2/x_3 = 2.00$			
0.434	0.133	0.433	229	0.849	0.101	0.050	713
0.358	0.284	0.358	-268	0.756	0.163	0.081	769
0.278	0.445	0.277	-327	0.610	0.260	0.130	619
0.124	0.752	0.124	-78	0.516	0.323	0.161	452
$x_1/x_3 = 0.50$				$x_2/x_3 = 0.295$			
0.286	0.142	0.572	-46	0.115	0.590	0.295	-877
0.257	0.230	0.513	-470				
0.216	0.351	0.433	-715				
0.055	0.834	0.111	-304				
<b><i>o</i>-Xylene (1) + Cyclohexanol (2) + 1,3-Butanediol (3)</b>							
$x_1/x_2 = 1.00$				$x_2/x_3 = 1.00$			
0.442	0.442	0.116	1598	0.844	0.078	0.078	1035
0.346	0.345	0.309	1455	0.742	0.129	0.129	1360
0.250	0.249	0.501	1242	0.716	0.142	0.142	1423
0.096	0.096	0.808	631	0.670	0.165	0.165	1491
$x_1/x_2 = 4.00$				$x_2/x_3 = 2.00$			
0.700	0.175	0.125	1530	0.602	0.199	0.199	1526
0.698	0.175	0.127	1548	0.234	0.383	0.383	1191
0.609	0.152	0.239	1486	0.105	0.448	0.447	774
0.525	0.131	0.344	1358 <sup>a</sup>				
0.386	0.097	0.517	1057 <sup>a</sup>	0.751	0.166	0.083	1431
0.232	0.058	0.710	765 <sup>a</sup>	0.560	0.293	0.147	1509
$x_1/x_2 = 2.00$				$x_2/x_3 = 0.25$			
0.584	0.292	0.124	1644	0.128	0.581	0.291	819
0.474	0.237	0.289	1545				
0.341	0.171	0.488	1339	0.779	0.044	0.177	794 <sup>a</sup>
0.139	0.069	0.792	782	0.559	0.088	0.353	1008 <sup>a</sup>
$x_1/x_2 = 0.50$				$x_2/x_3 = 0.565$			
0.300	0.601	0.099	1346	0.293	0.142	0.565	1235 <sup>a</sup>
0.241	0.482	0.277	1241	0.259	0.149	0.592	1180
0.171	0.342	0.487	1060	0.191	0.162	0.647	1005
0.110	0.221	0.669	780				

<sup>a</sup> Total molar fraction of two liquid phases.

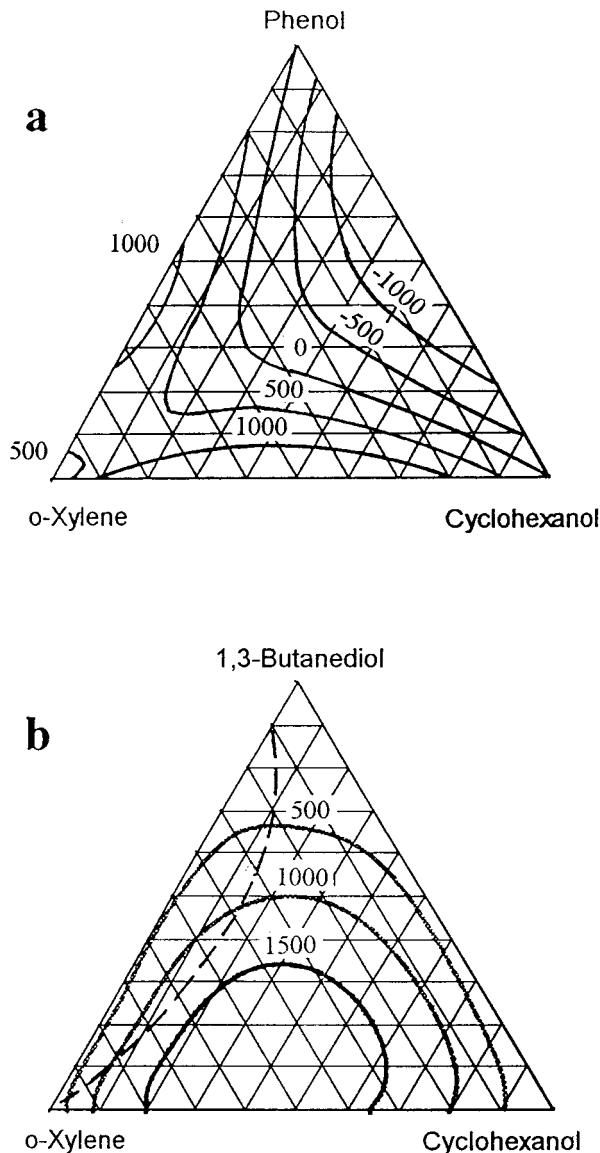
## Results

The experimental data of the excess enthalpy for the binary systems *o*-xylene + phenol and *o*-xylene + 1,3-butanediol are given in Table 2.

The binary  $H^E$  values were fitted to the Redlich–Kister equation (eq 1)

$$H^E/J\cdot\text{mol}^{-1} = x_1 x_2 \sum_{i=0}^{n-1} (x_1 - x_2)^i A_i \quad (1)$$

where  $x_1$  and  $x_2$  are the mole fractions of the first and the



**Figure 1.** Isoenthalpic curves ( $H^E = \text{const}$ ) of ternary systems at 318.15 K: (a) *o*-xylene + cyclohexanol + phenol, the graphical presentation of experimental data; (b) *o*-xylene + cyclohexanol + 1,3-butanediol, calculated by eq 4. The dashed line, drawn by the graphical interpolation of experimental data, separates the two-phase liquid system (left) from the one-phase system.

**Table 5. Binodal Curve for *o*-Xylene (1) + Cyclohexanol (2) + 1,3-Butanediol (3) at 318.15 K**

$x_1$	$x_2$	$x_3$	$x_1$	$x_2$	$x_3$
0.112		0.888	0.412	0.154	0.434
0.114	0.014	0.872	0.511	0.144	0.345
0.142	0.057	0.801	0.590	0.131	0.279
0.174	0.091	0.735	0.685	0.114	0.201
0.222	0.122	0.656	0.816	0.079	0.105
0.242	0.129	0.629	0.914	0.038	0.048
0.270	0.143	0.587	0.947	0.023	0.030
0.323	0.153	0.524			

second component, respectively, and  $n$  is the number of coefficients  $A_i$ .

The values of parameters  $A_i$  and standard deviations are listed in Table 3. In each case, the optimum number of

**Table 6. Mean Relative Error between Experimental and Calculated by Eq 4 Ternary Excess Enthalpies, and Values of Coefficients  $A_i$  at  $m = 4$** 

system	mean relative error, %	coefficients of eq 4			
		$A_0$	$A_1$	$A_2$	$A_3$
<i>o</i> -xylene + cyclohexanol + phenol	22.6	-16 414.36	-196 904.30	0	0
<i>o</i> -xylene + cyclohexanol + 1,3-butanediol	5.6	11 638.47	18 906.53	28 427.30	-100 480.80

coefficients was obtained through testing the standard deviation

$$\sigma(H^E) = \left[ \sum (H_{\text{calc}}^E - H_{\text{exp}}^E)^2 / (N - n) \right]^{1/2} \quad (2)$$

where  $N$  and  $n$  are the numbers of experimental points and coefficients of eq 1, respectively.

Superscript  $a$ 's of *o*-xylene + 1,3-butanediol composition (Table 2) refer to the total ("gross") mole fraction of two coexisting liquid phases. The immiscibility in the composition range (at  $x_1$  values higher than 0.11) of this system shows a linear dependence of  $H^E$  on the total mole fraction of two liquids:

$$H^E / \text{J} \cdot \text{mol}^{-1} = 563.6 - 288.0 \cdot x_1^a \quad (3)$$

with  $\sigma(H^E) = 7.4 \text{ J} \cdot \text{mol}^{-1}$ .

The experimental results for the excess enthalpies of ternary systems at 318.15 K are listed in Table 4. We used the same experimental technique described earlier (Kuus et al., 1996), starting with a homogeneous binary liquid with mole ratio of components ( $x_i/x_j$ ) shown in Table 4. The ternary system *o*-xylene + cyclohexanol + phenol exhibits regions of both exothermic and endothermic mixing, whereas the  $H^E$  values of *o*-xylene + cyclohexanol + 1,3-butanediol are endothermic over the entire composition range. The last system has both one-phase and two-phase liquids separated by a binodal curve; these measurements are given in Table 5.

The isenthalpic lines  $H^E = \text{const}$  of the systems *o*-xylene + cyclohexanol + phenol and *o*-xylene + cyclohexanol + 1,3-butanediol are compared in parts a and b of Figure 1, respectively.

The isenthalpic lines of the first system were determined by graphical interpolation of experimental data, whereas those of the second one were calculated using the equation reported and tested in our previous work (Siimer et al., 1997)

$$H^E = H_{12} + H_{23} + H_{31} + (A_0 + A_1 x_1^m + A_2 x_2^m + A_3 x_3^m) x_1 x_2 x_3 \quad (4)$$

where  $H_{ik}$  are contributions to the ternary  $H^E$  values from constituent binaries calculated by eq 1 and  $x_i$  is the mole

fraction of component  $i$  in the ternary mixture. Of course, in principle, eq 4 cannot correctly reproduce excess enthalpy in the two-phase liquid region.

The values of parameters  $A_i$  of eq 4 and mean relative errors between experimental and calculated  $H^E$  for both systems are given in Table 6. As seen from Table 6, the equation gives a quite satisfactory description of excess enthalpy for the system *o*-xylene + cyclohexanol + 1,3-butanediol only. For the second ternary system eq 4 does not give fully satisfactory results. It is very difficult to describe excess enthalpy in such systems, having both exothermic and endothermic mixing, as we have mentioned earlier (Siimer et al., 1997).

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