Liquid-Phase Thermodynamic Properties of New Refrigerants: Pentafluoroethyl Methyl Ether and Heptafluoropropyl Methyl Ether[†]

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In the present paper, we report an experimental study on the liquid-phase thermodynamic properties of the new-generation alternative refrigerants, pentafluoroethyl methyl ether, $CF_3CF_2OCH_3$ (245cbE $\beta\gamma$), and heptafluoropropyl methyl ether, $CF_3CF_2CF_2OCH_3$ (347sEy δ). The measurements of vapor pressures and saturated- and compressed-liquid densities were performed by means of a magnetic densimeter coupled with a variable-volume cell mounted with a metallic bellows for temperatures from 260 to 370 K (for CF₃CF₂OCH₃) and from 250 to 370 K (for CF₃CF₂CF₂OCH₃) and pressures up to 3 MPa. The experimental uncertainties of the temperature, pressure, and density measurements were estimated to be within ± 8 mK, ± 1.9 kPa (single-phase measurements) and ± 2.5 kPa (two-phase vapor pressure measurements), and ± 2 kg·m⁻³, respectively. The purities of the samples used throughout the measurements were 99.99 mass % for CF₃CF₂CF₂OCH₃ and 99.9 mass % for CF₃CF₂CF₂OCH₃. On the basis of these measurements and the available data reported by other investigators, the thermodynamic behaviors with respect to vapor pressures and saturated- and compressed-liquid densities are discussed in terms of vapor pressure and saturated liquid density correlations optimized and a liquid-phase equation of state. By examining the thermodynamic behavior of the derived properties such as the specific isochoric and isobaric heat capacities, speeds of sound, and Joule-Thomson coefficients, the range of validity for the optimized simple correlations and their physical soundness will be discussed.

Introduction

In accord with the increasing concerns about the global warming impact of released hydrofluorocarbon (HFC) refrigerants, several hydrofluoroether (HFE) refrigerants recently developed are considered as promising long-term replacements for some HFCs. HFE refrigerants, pentafluoroethyl methyl ether, $CF_3CF_2OCH_3$ (245cbE $\beta\gamma$), and heptafluoropropyl methyl ether, $CF_3CF_2CF_2OCH_3$ (347sE $\gamma\delta$), have vapor pressures similar to those of dichlorotetrafluoroethane (R-114) and trichlorofluoromethane (R-11), respectively. These HFE refrigerants have lower global warming potential than R-114 and R-11, respectively. So they are expected as a promising alternative to replace R-114 and R-11. The present study, therefore, aims to investigate the vapor pressures and the saturated- and compressed-liquid densities of CF₃CF₂OCH₃ and CF₃CF₂-CF₂OCH₃.

Experimental Section

All experimental measurements in the present work were performed with a magnetic densimeter coupled with a variable volume cell, which enabled measurements either at the saturated-liquid or compressed-liquid conditions. The experimental apparatus is shown in Figure 1. The magnetic densimeter (A) consists of a buoy equipped with a perma-

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Figure 1. Experimental apparatus: (A) magnetic densimeter; (B) variable volume cell; (C) digital quartz pressure transducer; (D) damper; (E) thermostated fluid bath; (F) personal computer; (G) vacuum pump; (H) vacuum gauge; (I) nitrogen gas; (J) digital quartz pressure computer; (K) main heater; (L) subheater; (M) cooler; (N) stirrer; (O) standard resistor; (P) PID controller; (Q1, 2) thyristor transformer; (R) 25 Ω standard platinum resistance thermometer; (S) pressure gauge; (T) digital multimeter; (U) current controller; (V1–10) valves; (W) DC power supply; (X) galvanometer; (Y) thermometer bridge; (Z) pen recorder.

nent magnet, a sample cell, an electromagnetic coil, and a search coil. The sample density was measured by the

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magnetic densimeter immersed in a thermostated fluid bath (E). The sample pressure was directly measured by a digital quartz pressure transducer (Paroscientific, Model 31K-101) (C) with the aid of a digital quartz pressure computer (J). The temperature was measured by means of a 25 Ω standard platinum resistance thermometer (R) placed in the vicinity of the magnetic densimeter. By controlling the pressure of the nitrogen gas in the outer space of the metallic bellows within a variable-volume cell (B), it is possible to create a saturated- and/or a compressedliquid condition. The saturated-liquid condition was determined from careful visual observation of the appearance and disappearance of a bubble in the liquid sample.

The experimental apparatus used for the present measurements was originally constructed by Maezawa et al.¹ and modified by Widiatmo et al.² Since then, we have completed a series of similar measurements with respect to HCFC and HFC refrigerants and their mixtures.^{3,4}

The sample purities, as analyzed by the chemical manufacturer, are 99.99 mass % for $CF_3CF_2OCH_3$ and 99.9 mass % for $CF_3CF_2CF_2OCH_3$. These samples were provided by the Research Institute of Innovative Technology for the Earth (RITE), Tsukuba, Japan.

We estimated the uncertainties of the present measurements according to the ISO recommendation⁵ in terms of the expanded uncertainties with a coverage factor of 2. The experimental uncertainties of temperature, pressure, and density measurements were estimated to be within ± 8 mK, ± 1.9 kPa (single-phase measurements) and ± 2.5 kPa (two-phase vapor pressure measurements), and ± 2.2 kg·m⁻³, respectively.

Results and Discussion

Fifteen vapor pressures and saturated-liquid densities, and 49 compressed-liquid densities of $CF_3CF_2OCH_3$ have been measured at temperatures from 260 to 370 K in 10 K intervals and pressures up to 3 MPa. The numerical experimental results are summarized in Table 1. For CF_3 - $CF_2CF_2OCH_3$, 22 vapor pressures and saturated-liquid densities, and 80 compressed-liquid densities have been measured for temperatures from 250 to 370 K and pressures up to 3 MPa. The obtained data are tabulated in Table 2.

Widiatmo and Watanabe⁶ correlated the vapor pressure correlations for both $CF_3CF_2OCH_3$ and $CF_3CF_2CF_2OCH_3$ by using the present data added with the data by Tsuge et al.^{7,8} and Uchimura et al.,⁹ in a functional form given in eq 1.

$$\ln P_{\rm r} = \frac{T_{\rm c}}{T} (a_1 \tau + a_2 \tau^{1.5} + a_3 \tau^3 + a_4 \tau^6) \tag{1}$$

where P_r and τ are defined as P/P_c and $1 - (T/T_c)$, respectively. The critical temperature, T_c , used in eq 1 for CF₃CF₂OCH₃ is that reported by Yoshii et al.,¹⁰ while that of CF₃CF₂CF₂OCH₃ is that reported by Sako et al.¹¹ The critical pressures, P_c , in eq 1 are those determined by Widiatmo and Watanabe⁶ for both compounds. The critical temperatures and pressures are given in Table 3, while coefficients a_1 to a_4 are given in Table 4.

The vapor pressure deviation of $CF_3CF_2OCH_3$ from eq 1, as illustrated in Figure 2, shows that the present measured vapor pressures agree satisfactorily with the data by Tsuge et al.^{7,8} within our claimed uncertainty. On the other hand, the vapor pressures calculated from the vapor pressure correlation developed by Sako et al.¹⁴ show a significant deviation from both the present data and the

Fab	le	1.	Measure	l P	-ρ-	T	Properties	for	CF ₃ CF ₂ OCH ₃
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		r r	- 1		2 0
<i>T</i> /K	<i>P</i> /kPa	$ ho/(kg\cdot m^{-3})$	<i>T</i> /K	₽⁄kPa	ρ/(kg•m ^{−3})
259.984	43.5	1373.8 ^a	319.986	2499.1	1210.7
			319.986	3001.6	1213.7
269.986	69.0	1347.7 ^a			
269.986	69.0	1346.3 ^a	329.985	535.1	1163.0 ^a
			329.985	997.0	1167.1
279.989	104.8	1319.5 ^a	329.985	1496.8	1170.9
279.989	104.7	1319.1 ^a	329.985	1993.8	1174.7
279.989	502.4	1320.5	329.985	2503.2	1178.7
279.989	1003.9	1322.5	329.985	3005.5	1182.4
279.989	1501.8	1324.4			
279.989	1998.7	1326.3	339.985	694.9	1126.2 ^a
279.989	2504.2	1328.3	339.985	1007.3	1129.6
279.989	3007.4	1330.0	339.985	1498.9	1134.3
			339.985	1999.3	1139.2
289.988	153.3	1290.9 ^a	339.985	2501.2	1143.6
289.988	504.7	1292.3	339.985	2994.4	1148.3
289.988	996.1	1294.6			
289.988	1496.4	1296.8	349.984	888.0	1086.4 ^a
289.988	1996.3	1299.0	349.984	1494.3	1094.3
289.988	2503.8	1300.9	349.984	1999.3	1100.3
289.988	2997.7	1303.0	349.984	2496.3	1105.8
			349.984	2998.4	1111.2
299.987	217.3	1260.8 ^a			
299.987	218.2	1260.9 ^a	359.984	1119.0	1042.4 ^a
299.987	501.2	1262.4	359.984	1502.0	1048.8
299.987	1001.5	1264.9	359.984	1997.0	1056.8
299.987	1501.1	1267.3	359.984	2500.0	1064.0
299.987	2000.5	1269.5	359.984	2996.3	1070.9
299.987	2501.2	1272.2			
299.987	2998.4	1274.2	369.983	1393.0	992.9 ^a
			369.983	1993.2	1006.5
309.986	300.1	1229.8 ^a	369.983	2498.6	1016.4
309.986	999.8	1233.7	369.983	2996.4	1025.5
309.986	1498.7	1236.7			
309.986	2000.1	1239.6			
309.986	2501.9	1242.3			
309.986	2998.2	1244.7			
319.986	404.5	1196.6 ^a			
319.986	1006.4	1201.0			
319.986	1502.3	1205.9			
319.986	2002.1	1207.7			

^a Observed values at two-phase conditions.

data by Tsuge et al.^{7,8} This may reflect the existence of a systematic error in the development of the vapor pressure correlation by Sako et al.¹⁴

Figure 3 depicts the vapor pressure deviation of CF₃CF₂-CF₂OCH₃ from eq 1. As also seen in Figure 2, the vapor pressures calculated from the vapor pressure correlation developed by Sako et al.¹⁴ deviate systematically to greater values with increasing temperature. On the contrary, the present vapor pressure data and those by Tsuge et al.^{7,8} are in agreement within ± 2 kPa. From Figures 2 and 3, it can be concluded that those vapor pressure correlations by Sako et al.¹⁴ were developed on the basis of less reliable vapor pressure data. Since there is no numerical data available in their report, detailed discussion about the measurements by Sako et al.¹⁴ cannot be done.

For the purpose of data comparison, the saturated-liquid density correlation optimized by Widiatmo and Watanabe⁶ and given in eq 2 is referred to in the present study.

$$\rho' = \rho_{\rm c} [1 + B(1 - T_{\rm r})^{\beta} + \sum_{i=1}^{3} B_i (1 - T_{\rm r})^{b/3}] \qquad (2)$$

The critical density, ρ_c , used in eq 2 for CF₃CF₂OCH₃ is that reported by Yoshii et al.,¹⁰ while that for CF₃CF₂CF₂-OCH₃ is reported by Sako et al.¹¹ The numerical values of critical densities are given in Table 3, while the coefficients

Table	2.	Measured	$P-\rho-7$	Properties	fo
CF ₃ CI	F2C	F ₂ OCH ₃			

<i>T</i> /K	<i>P</i> /kPa	$ ho/(kg\cdot m^{-3})$	<i>T</i> /K	<i>P</i> /kPa	ρ/(kg•m ⁻³)
249.981	4.8	1528.3 ^a	319.986	155.8	1341.2 ^a
			319,986	746.8	1344.1
259.984	10.2	1504.0 ^a	319,986	1001.3	1345.4
2001001	1012	100110	319 986	1503.0	1347.8
269 986	18.9	1 /178 0 a	319 986	2084 5	1351.0
200.000	10.5	1470.5	319 986	2450 5	1353.0
279 989	31.7	1452 7a	319 986	2003 6	1355.6
270 088	31.7	1452 Qa	515.500	2000.0	1555.0
270 088	500 4	1452.5	320 085	2146	1311 7a
270.000	1005 2	1456.0	220.085	214.0 912.0	1911.7 1911 5a
270.000	1506 5	1450.0	220.005	£13.0 919.0	1919 48
270.000	1000.0	1457.9	329.900	£13.9	1012.4-
279.988	2003.3	1409.0	329.983	505.4 000.0	1313.3
279.988	2499.0	1461.2	329.985	999.0	1310.4
279.988	3004.2	1462.6	329.985	1497.8	1319.3
	10.0	1.105.00	329.985	1999.1	1322.3
289.989	49.8	1425.8 ^a	329.985	2499.9	1325.4
289.989	550.1	1428.7			
289.989	1011.5	1429.9	329.985	2995.6	1327.9
289.989	1502.9	1432.2	329.985	504.5	1314.7
289.989	2007.0	1433.6	329.985	998.8	1317.4
289.989	2504.8	1435.5	329.985	1500.2	1320.3
289.989	2998.9	1437.2	329.985	2010.3	1323.7
			329.985	2505.8	1327.0
299.987	75.5	1399.6 ^a	329.985	2989.8	1329.0
299.987	534.7	1400.4			
299.987	996.3	1403.3	339.985	288.7	1281.0 ^a
299.987	1504.4	1404.6	339.985	288.1	1280.6 ^a
299.987	2007.0	1407.0	339.985	288.2	1280.6 ^a
299.987	2499.9	1408.6	339.985	508.3	1281.9
299.987	2992.0	1410.3	339.985	1002.7	1285.5
			339.985	1503.7	1288.9
309.986	110.2	1370.5 ^a	339.985	2000.1	1292.4
309.986	557.3	1372.3	339.985	2503.7	1295.7
309.986	1008.3	1374.1	339.985	3000.6	1298.9
309.986	1501.4	1376.8	339.985	522.7	1282.3
309.986	2000.3	1379.7	339.985	998.4	1285.7
309.986	2502.3	1381.6	339.985	1493.5	1288.9
309.986	2992.0	1383.6	339.985	2007.9	1292.5
			339,985	2505.4	1296.0
			339,985	3006.3	1299.2
349 985	381.9	1247 8 ^a	359 984	494 7	1211 4
349 985	380.4	1247 2 ^a	359 984	493 7	1212.1
349.985	380.7	1246.2 ^a	359.984	493.9	1210.6
349 985	501.8	1248 2	359 984	1010.0	1217.3
349 985	1000.6	1252 4	359 984	1505.6	1222 2
349 985	1502.5	1256 /	359 984	2002 4	1226.7
340.085	2000 8	1260.4	350 084	2506 1	1221 2
240.085	2500.6	1264.9	250 094	2006 1	1225.2
240.085	2008 5	1204.2	250 094	1000.0	1215 6
349.985	2008 3	1251 /	350 084	1505.3	1220.8
349.905	1504 6	1255 8	350.004	2001 7	1225 7
343.303	2001.0	1250.2	350.004	2507 C	1920 /
343.303	2507 7	1200.0	350.004	2002 C	1220.4
343.303 210 005	2000 0	1203.3	555.904	3002.0	1204.0
349.900	2990.2	1207.1	260 002	691.9	1179 64
			309.903 360 000	1002.0	1170 0
			309.903	1400 7	11/0.2
			309.983	1498./	1103.9
			309.903	2004.0 2501 7	1109.9
			309.903	2002 C	1194.9
			JUJ.JOJ	2993.U	1200.2

^a Observed values at two-phase conditions.

Table 3. Critical Parameters for $CF_3CF_2OCH_3$ and $CF_3CF_2CF_2OCH_3$

	CF ₃ CF ₂ OCH ₃	$CF_3CF_2CF_2OCH_3$
P _c /kPa	2887 ^a	2476^{b}
$T_{\rm c}/{ m K}$	406.83 ^a	437.7^{c}
$ ho_{ m c}/(m kg\cdot m^{-3})$	509 ^a	530 ^c

^a Yoshii et al.¹⁰ ^b Uchimura et al.⁹ ^c Sako et al.¹¹

B and B_1 through B_3 together with the respective exponents are given in Table 4.



Figure 2. Vapor pressure deviation for $CF_3CF_2OCH_3$: •, this work; \triangle , Tsuge et al.;^{7,8} –, Sako et al.¹⁴



Figure 3. Vapor pressure deviation for $CF_3CF_2CF_2OCH_3$: •, this work; ×, Uchimura et al.;⁹ –, Sako et al.¹⁴

Table 4. Coefficients and Exponents in Eqs 1-3 for $CF_3CF_2OCH_3$ and $CF_3CF_2CF_2OCH_3$

	CF ₃ CF ₂ OCH ₃	CF ₃ CF ₂ CF ₂ OCH ₃
a_1	-7.73986	-7.95132
a_2	1.52151	1.50989
a_3	-4.05631	-4.48124
a_4	-11.0921	-20.8350
В	1.43926	1.81014
\overline{B}_1	1.69075	0.98763
$\dot{B_2}$	-1.54018	
$\tilde{B_3}$	1.57395	
β	0.322	0.325
b_1	2	2.36
b_2	4	
b_3	6	
c_0	0.084716	0.074730
c_1	-0.17288	-0.11568
d_0	-0.99575	-0.99907
d_1	12.306	11.368
d_2	69.742	106.35
d_3	-359.41	-456.44
d_4	545.71	570.32
en	0.56963	0.56658
<i>e</i> 1	-0.69563	-0.71530
e2	0.49193	0.73236
<i>e</i> ₃	0.28421	-0.43312
<i>e</i> ₄	-0.71301	0.098989

Figure 4 illustrates the saturated-liquid density deviation of $CF_3CF_2OCH_3$ from eq 2. Earlier measurements by Tsuge et al.^{7,8} are also represented in Figure 4. As shown in Figure 4, the present measurements agree well with the data by Tsuge et al.^{7,8} Concerning $CF_3CF_2CF_2OCH_3$, as given in Figure 5, the present measurements also show an excellent agreement with the data by Yoshii et al.¹⁰ and a smooth extension to those by Uchimura et al.⁹



Figure 4. Saturated-liquid density deviation for $CF_3CF_2OCH_3$: •, this work; \triangle , Tsuge et al.^{7.8}



Figure 5. Saturated-liquid density deviation for $CF_3CF_2CF_2$ -OCH₃: •, this work; ×, Uchimura et al.,⁹ \Box , Nakazawa et al.¹³

Regarding the representation of thermodynamic properties of fluorinated ethers of present interest in their liquid phases including the saturated liquids, we have employed eq 3, which was successfully applied to similar representation by Fujimine et al.¹² for binary and ternary mixtures of difluoromethane (R-32), pentafluoroethane (R-125), and 1,1,1-trifluoroethane (R-143a).

$$\rho_{\rm r} = (P_{\rm r} + D)^C / E \tag{3}$$

where $\rho_{\rm r} = \rho/\rho_{\rm c}$ and $P_{\rm r} = P/P_{\rm c}$. The exponent *C* and the coefficients *D* and *E* are correlated using functional forms given in eqs 4–6.

$$C = c_0 + c_1 \tau \tag{4}$$

$$D = d_0 + d_1 \tau + d_2 \tau^2 + d_3 \tau^3 + d_4 \tau^4 \tag{5}$$

$$E = e_0 + e_1 \tau + e_2 \tau^2 + e_3 \tau^3 + e_4 \tau^4 \tag{6}$$

The numerical constants in eqs 4-6 are given in Table 4. The data used to determine the numerical constants in eq 3 are the present measurements and unpublished data by Tsuge et al.^{7.8} for CF₃CF₂OCH₃, and the present measurements and unpublished data by Uchimura et al.⁹ for CF₃CF₂CF₂OCH₃, respectively.

The range of validity of eq 3, therefore, covers the reduced range of temperatures 0.639 to 0.999, pressures up to 1.03, and the range of densities 1.34 to 2.70 for CF₃-CF₂OCH₃, whereas it covers 0.571 to 0.998 for T_r , up to 1.21 for P_r , and 1.35 to 2.88 for ρ_r for CF₃CF₂CF₂OCH₃.

It should be noted that the range of validity mentioned above was concluded on the basis of $P\rho T$ properties reported, excluding the very vicinity of the critical point of both compounds. The liquid density deviation from eq 3 is plotted in Figures 6 and 7 for CF₃CF₂OCH₃, and in Figures



Figure 6. Liquid-density deviation for $CF_3CF_2OCH_3$ at different temperatures: •, saturated-liquid densities from this work; \bigcirc , compressed-liquid densities from this work; \triangle , Tsuge et al.^{7,8}



Figure 7. Liquid-density deviation for $CF_3CF_2OCH_3$ at different pressures: \bullet , saturated-liquid densities from this work; \bigcirc , compressed-liquid densities from this work; \triangle , Tsuge et al.^{7,8}



Figure 8. Liquid-density deviation for $CF_3CF_2CF_2OCH_3$ at different temperatures: \bullet , saturated-liquid densities from this work; \bigcirc , compressed-liquid densities from this work; \times , Uchimura et al.;⁹ \Box , Nakazawa et al.¹³



Figure 9. Liquid-density deviation for $CF_3CF_2CF_2OCH_3$ at different pressures: \bullet , saturated-liquid densities from this work; \bigcirc , compressed-liquid densities from this work; \times , Uchimura et al.,⁹ \Box , Nakazawa et al.¹³

8 and 9 for $CF_3CF_2CF_2OCH_3$, respectively. As shown in those figures, eq 3 represents the present compressed-liquid densities satisfactorily within $\pm 0.2\%$.

It should be noted that the present representation, eq 3, was confirmed to provide physically sound behaviors with respect to essential thermodynamic properties such as isothermal compressibility, specific isobaric and isochoric heat capacities, speed of sound, and the Joule–Thomson coefficient for the range of pressures up to 10 MPa and temperatures up to 390 K for $CF_3CF_2OCH_3$, whereas it covers up to 10 MPa and up to 420 K for $CF_3CF_2OCH_3$.

Conclusions

Forty-nine compressed-liquid densities and fifteen vaporpressures and saturated-liquid densities of $CF_3CF_2OCH_3$ have been measured over the range of temperatures 260 to 370 K and pressures up to 3 MPa. Eighty compressedliquid densities and twenty-two vapor pressures and saturated-liquid densities of $CF_3CF_2CF_2OCH_3$ have also been obtained over the range of temperatures 250 to 370 K and pressures up to 3 MPa.

On the basis of the present measurements, a simple thermodynamic formulation to represent the compressedliquid densities has also been developed for $CF_3CF_2OCH_3$ and $CF_3CF_2CF_2OCH_3$, which enabled us to reproduce the measured data within $\pm 0.2\%$ in density.

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