# Densities of 1-Propanol and 2-Propanol via a Vibrating Tube Densimeter from 313 to 363 K and up to 25 MPa 

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PvT properties were determined in the liquid phase for 1-propanol and 2-propanol from 313 to 363 K and up to 25 MPa with an uncertainty lower than $\pm 0.05 \%$. The calibration method of the vibrating tube densimeter was performed with $\mathrm{N}_{2}$ and $\mathrm{H}_{2} \mathrm{O}$ as reference fluids. The 1-propanol and 2-propanol liquid densities reported in this work are correlated with an eleven-parameter equation of state of Starling and Han (BWRS) and the Tait equation using a least-squares optimization, with a relative deviation lower than $\pm 0.05 \%$ for both fluids. The density values calculated by the BWRS equation of state and the Tait equation agree within $0.05 \%$ with data reported by Yaginuma et al. ${ }^{15}$ for 1-propanol and within 0.09\% with data reported by Yaginuma et al. ${ }^{16}$ for 2-propanol.

## Introduction

PVT properties of pure compounds, PvT properties and phase equilibria (vapor-liquid, vapor-liquid-liquid, and liquid-liquid equilibria), and mixtures at high pressures are required in the development of supercritical fluid extraction processes. Supercritical fluids containing $\mathrm{CO}_{2}$ and alcohols are interesting from both theoretical and practical points of view, especially for the processing of pharmaceutical and natural products. ${ }^{1,2}$

Our research is focused on a systematic study to obtain experimental VLE and PVT data of the $\mathrm{CO}_{2}$-alcohol mixtures for knowledge, development, and application of techniques directed toward supercritical extraction processes. The main objective is to perform systematic studies of PVT and phase equilibria ${ }^{3-11}$ of binary mixtures containing $\mathrm{CO}_{2}$ and alcohol (from ethanol to decanol) in order to select the best supercritical operating conditions required for industrial applications, such as extraction of carotenes from the chili Poblano of Mexico (Capsicum annum).

Compressed liquid densities, for 1-propanol and 2-propanol, from 313 to 363 K and from 0.5 MPa to 25 MPa , are reported here. The reliability of the measurements has been checked by comparing the data calculated through the Starling and Han equation of state (BRWS EOS) and the Tait equation fitted on data reported in this work and data from other authors.

## Experimental Section

Apparatus and Procedure. A detailed description of the apparatus used in this work has been given by ZuñigaM oreno and Galicia-Luna. ${ }^{3}$ The measuring cell (see Figure 1) is composed of a vibrating tube (H astelloy C-276 U-tube) with a $1 \mathrm{~cm}^{3}$ internal volume. The experimental procedure used here is that already described by Galicia-Luna et al. ${ }^{4}$ and Zuñiga-Moreno and Galicia-Luna. ${ }^{3}$ In this work, estimated uncertainties are $\pm 0.03 \mathrm{~K}$ for temperatures, $\pm 0.008 \mathrm{MPa}$ for pressures, and $\pm 0.05 \%$ for liquid densities.

[^0]

Figure 1. Simplified flow diagram of the apparatus: $A B$, air bath; B and C, caps in titanium; DMA 60, period meter; EC, equilibrium cell; FV, feeding valve; GC, gas compressor; LB, liquid bath; MC, measurement cell; MR, magnetic rod; PI, I sco pump; PT, pressure transducer; PTPi, platinum probe i; ST, sapphire tube; TD, digital indicator of temperature F250; VSE, variable speed engine; VP, vacuum pump; VTD, vibrating tube densimeter.

The experimental procedure consists of four steps: 1, sensor calibration; 2, cell loading; 3, setting up of the experimental conditions; and 4, measurements at equilibrium. A detailed calibration procedure of the platinum temperature probes and of the pressure transducer is given elsewhere by Galicia-Luna et al.,3,5
The platinum probes Pt $100\left(\mathrm{PTP}_{1}, \mathrm{PTP}_{2}\right.$, and $\mathrm{PTP}_{3}$, Specitec, France; see Figure 1) connected to a digital indicator (Automatic Systems F 250, USA) were calibrated against a calibration system (Automatic Systems F 300S, USA) connected to a $25-\Omega$ reference probe (model 162CE of $\pm 0.005 \mathrm{~K}$ certified accuracy on the ITS-90 scale, from Rosemount, England).

The Sedeme ( 25 MPa , France) pressure transducer connected to a $6 \frac{1}{2}$ digital multimeter (HP-34401A, USA) is calibrated at temperatures from 313 to 363 K against a dead weight balance (Desgranges \& Huot, France, Model

Table 1. Purity and Origin of Pure Compounds

| compound | certified purity (\%) | max. water <br> content (\%) | supplier |
| :--- | :--- | :---: | :--- |
| 1-propanol | 99.5 | 0.05 | Merck |
| 2-propanol | 99.5 | 0.05 | Merck |
| CO2 | 99.995 |  | Air Products-I nfra |
| water | 99.95 (HPLC) |  | Fisher |
| nitrogen | 99.995 |  | Air Products-I nfra |

Table 2. Densities of Pure Liquids and Comparison with Literature ${ }^{17}$ Values at Different Temperatures

| T/K | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 1-propanol |  | 2-propanol |  |
|  | expt\| ${ }^{\text {a }}$ |  | exptI ${ }^{\text {a }}$ |  |
| 298.07 | 799.33 |  | 781.07 |  |
| 303.26 | 795.45 |  | 776.69 |  |
| 313.23 | 788.08 |  | 768.69 |  |
| 321.74 | 779.32 |  | 761.10 |  |
|  | cal ${ }^{\text {b }}$ | lit. ${ }^{17}$ | cal ${ }^{\text {c }}$ | lit. ${ }^{17}$ |
| 298.15 | 799.20 | 799.58 | 780.92 | 781.23 |
| 303.15 | 795.99 | 795.48 | 776.94 | 776.95 |
| 308.15 | 792.24 | 791.38 | 772.84 | 772.46 |
| 313.15 | 787.96 | 787.37 | 768.63 | 767.98 |

${ }^{\text {a }}$ Experimental data in this work. ${ }^{\mathrm{b}}$ Equation for 1-propanol: $\rho_{1}=-\left(1.069086 \times 10^{-02}\right) T^{2}+5.785885 T+24.48764$. Standard deviation $/ \mathrm{kg} \cdot \mathrm{m}^{-3}=0.222$. ${ }^{\text {c }}$ Equation for 2-propanol: $\rho_{2}=$ $-\left(2.272116 \times 10^{-03}\right) \mathrm{T}^{2}+\left(5.69641 \times 10^{-01}\right) \mathrm{T}+813.0550$. Standard deviation/kg $\cdot \mathrm{m}^{-3}=0.223$.

5304; accuracy $\pm 0.005 \%$ full scale). The calibration was done by both increasing and decreasing the pressure at a constant temperature to check for hysteresis.

The vibrating tube was calibrated using water and nitrogen. The reference density values for the $\mathrm{H}_{2} \mathrm{O}$ and $\mathrm{N}_{2}$ compounds were computed using the equations of state (EoS) of Harr et al. ${ }^{12}$ and Span et al. ${ }^{13}$

The density of the fluid inside the U -tube, $\rho_{\mathrm{F}}$, is given by

$$
\begin{equation*}
\rho_{\mathrm{F}}(\mathrm{P}, \mathrm{~T})=\rho_{\mathrm{H}_{2} \mathrm{O}}(\mathrm{P}, \mathrm{~T})+\frac{1}{\mathrm{~A}}(\mathrm{P}, \mathrm{~T})\left(\tau_{\mathrm{F}}^{2}(\mathrm{P}, \mathrm{~T})-\tau_{\mathrm{H}_{2} \mathrm{O}}^{2}(\mathrm{P}, \mathrm{~T})\right) \tag{1}
\end{equation*}
$$

where $\rho_{F}(\mathrm{P}, \mathrm{T})$ and $\tau_{\mathrm{F}}^{2}(\mathrm{P}, \mathrm{T})$ are the density and vibration period, respectively, of 1-propanol or 2-propanol and

$$
\begin{equation*}
\frac{1}{\mathrm{~A}}=\frac{\rho_{\mathrm{H}_{2} \mathrm{O}}-\rho_{\mathrm{N}_{2}}}{\tau_{\mathrm{H}_{2} \mathrm{O}}^{2}-\tau_{\mathrm{N}_{2}}^{2}} \tag{2}
\end{equation*}
$$

The purity and origin of chemicals used in this work are given in Table 1. The purities of the liquid samples were tested using a gas chromatograph (HP 5890 Series II ) fitted with a flame ionization detector and a packed col umn. The verified guaranteed purities are in both cases >99.5\%. Alcohols were stored over 3A molecular sieves to avoid any moisture and were used without any further purification except for a careful degassing.

Theory. The experimental data have been correlated using the Starling and Han equation of state (BWRS E oS): ${ }^{14}$

$$
\begin{align*}
P= & \frac{R T}{v}+\left(B_{0} R T-A_{0}-\frac{C_{0}}{T^{2}}+\frac{D_{0}}{T^{3}}-\frac{E_{0}}{T^{4}}\right) / v^{2}+(b R T-a- \\
& d) / v^{3}+\alpha\left(a+\frac{d}{T}\right) / v^{6}+c\left(1+\frac{u}{v^{2}}\right) \exp \left(-\frac{u}{v^{2}}\right) /\left(v^{3} T^{2}\right) \tag{3}
\end{align*}
$$

where $v$ is the molar volume.
And using the Tait equation ${ }^{15}$

$$
\begin{equation*}
\rho=\rho_{0}\left[1-\mathrm{C} \ln \left(\frac{\mathrm{~B}_{\mathrm{T}}+\mathrm{P}}{\mathrm{~B}_{\mathrm{T}}+\mathrm{P}_{0}}\right)\right] \tag{4}
\end{equation*}
$$

Both equations are useful for the description of compressed liquid densities.

Table 3. Densities of 1-Propanol at Different Temperatures

| T/K = 313.15 |  | T/K $=323.10$ |  | T/K $=332.99$ |  | $\mathrm{T} / \mathrm{K}=342.95$ |  | $\mathrm{T} / \mathrm{K}=352.88$ |  | $\mathrm{T} / \mathrm{K}=362.77$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |
| 0.500 | 788.29 | 0.511 | 779.97 | 0.507 | 771.54 | 0.511 | 762.53 | 0.509 | 753.47 | 0.513 | 743.92 |
| 1.005 | 788.71 | 1.022 | 780.44 | 1.005 | 772.03 | 1.008 | 763.04 | 1.026 | 754.05 | 1.013 | 744.53 |
| 2.010 | 789.57 | 2.009 | 781.33 | 2.015 | 772.99 | 2.008 | 764.07 | 2.014 | 755.14 | 2.016 | 745.73 |
| 3.033 | 790.45 | 3.014 | 782.25 | 3.005 | 773.96 | 3.012 | 765.09 | 3.001 | 756.22 | 3.010 | 746.90 |
| 4.002 | 791.26 | 4.014 | 783.14 | 4.016 | 774.90 | 4.024 | 766.12 | 3.998 | 757.30 | 4.006 | 748.06 |
| 5.007 | 792.10 | 5.002 | 784.02 | 5.017 | 775.85 | 5.031 | 767.12 | 5.004 | 758.39 | 5.010 | 749.20 |
| 6.006 | 792.93 | 6.025 | 784.91 | 6.027 | 776.79 | 6.007 | 768.10 | 6.005 | 759.44 | 6.010 | 750.33 |
| 7.004 | 793.76 | 7.013 | 785.77 | 7.024 | 777.72 | 7.018 | 769.08 | 7.015 | 760.48 | 7.015 | 751.46 |
| 8.010 | 794.58 | 8.016 | 786.66 | 8.010 | 778.61 | 8.011 | 770.05 | 8.003 | 761.51 | 8.007 | 752.55 |
| 8.998 | 795.39 | 9.023 | 787.52 | 9.016 | 779.52 | 9.015 | 771.02 | 9.030 | 762.56 | 9.013 | 753.64 |
| 10.006 | 796.20 | 9.998 | 788.35 | 10.028 | 780.42 | 10.007 | 771.95 | 10.001 | 763.53 | 10.003 | 754.71 |
| 11.004 | 796.99 | 11.041 | 789.22 | 11.010 | 781.29 | 11.008 | 772.88 | 11.019 | 764.54 | 10.999 | 755.76 |
| 12.004 | 797.78 | 12.002 | 790.02 | 12.027 | 782.17 | 12.025 | 773.82 | 12.002 | 765.50 | 12.019 | 756.81 |
| 12.997 | 798.57 | 13.017 | 790.85 | 12.999 | 783.01 | 13.013 | 774.72 | 13.021 | 766.49 | 12.988 | 757.82 |
| 14.008 | 799.34 | 14.007 | 791.65 | 14.050 | 783.90 | 14.016 | 775.61 | 13.997 | 767.42 | 14.016 | 758.84 |
| 14.990 | 800.08 | 15.002 | 792.45 | 15.017 | 784.72 | 14.992 | 776.49 | 15.016 | 768.38 | 15.006 | 759.84 |
| 16.024 | 800.85 | 16.011 | 793.24 | 15.994 | 785.53 | 16.028 | 777.39 | 16.004 | 769.29 | 16.008 | 760.82 |
| 16.994 | 801.58 | 17.038 | 794.04 | 17.030 | 786.38 | 17.000 | 778.24 | 16.997 | 770.21 | 17.026 | 761.81 |
| 18.005 | 802.32 | 17.999 | 794.80 | 18.005 | 787.17 | 18.029 | 779.12 | 18.027 | 771.14 | 18.006 | 762.75 |
| 19.000 | 803.05 | 19.023 | 795.57 | 19.021 | 787.99 | 19.013 | 779.95 | 19.009 | 772.02 | 19.009 | 763.71 |
| 20.019 | 803.79 | 20.036 | 796.33 | 20.006 | 788.78 | 20.002 | 780.78 | 20.026 | 772.94 | 20.031 | 764.66 |
| 20.986 | 804.49 | 21.002 | 797.08 | 21.026 | 789.59 | 21.034 | 781.64 | 21.002 | 773.79 | 21.045 | 765.61 |
| 22.024 | 805.23 | 22.016 | 797.82 | 22.018 | 790.38 | 22.046 | 782.48 | 22.006 | 774.67 | 21.992 | 766.49 |
| 22.993 | 805.93 | 23.037 | 798.60 | 23.024 | 791.17 | 23.000 | 783.28 | 23.082 | 775.60 | 23.029 | 767.45 |
| 24.040 | 806.70 | 23.994 | 799.34 | 24.007 | 791.95 | 24.036 | 784.14 | 24.059 | 776.45 | 24.020 | 768.34 |
| 25.003 | 807.40 | 25.049 | 800.13 | 25.015 | 792.76 | 25.090 | 784.99 | 25.032 | 777.29 | 25.007 | 769.24 |
| $14.006^{1}$ | 799.29 |  |  |  |  |  |  |  |  |  |  |
| $5.008^{1}$ | 792.02 |  |  |  |  |  |  |  |  |  |  |
| $1.008{ }^{1}$ | 788.67 |  |  |  |  |  |  |  |  |  |  |
| $0.49{ }^{1}$ | 788.23 |  |  |  |  |  |  |  |  |  |  |

[^1]Table 4. Densities of 2-Propanol at Different Temperatures

| T/K = 313.16 |  | T/K = 323.11 |  | T/K = 333.02 |  | T/K = 342.97 |  | T/K = 352.93 |  | $\mathrm{T} / \mathrm{K}=362.81$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | P/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |
| 0.498 | 769.30 | 0.510 | 760.23 | 0.498 | 751.84 | 0.509 | 741.69 | 0.523 | 731.18 | 0.507 | 719.60 |
| 1.011 | 769.80 | 1.003 | 760.73 | 1.006 | 752.40 | 1.004 | 742.30 | 1.011 | 731.83 | 1.011 | 720.34 |
| 2.008 | 770.76 | 2.014 | 761.78 | 2.008 | 753.53 | 2.016 | 743.51 | 2.008 | 733.15 | 2.013 | 721.78 |
| 3.013 | 771.70 | 2.999 | 762.80 | 3.010 | 754.62 | 3.006 | 744.68 | 3.016 | 734.45 | 3.003 | 723.19 |
| 4.004 | 772.64 | 4.015 | 763.81 | 3.995 | 755.68 | 4.013 | 745.87 | 4.004 | 735.70 | 4.008 | 724.58 |
| 5.007 | 773.59 | 5.008 | 764.82 | 5.018 | 756.79 | 5.017 | 747.04 | 5.007 | 736.96 | 5.005 | 725.95 |
| 6.009 | 774.52 | 6.003 | 765.80 | 6.008 | 757.84 | 6.012 | 748.18 | 6.016 | 738.20 | 6.012 | 727.30 |
| 7.016 | 775.44 | 7.007 | 766.80 | 7.009 | 758.89 | 7.009 | 749.30 | 7.005 | 739.42 | 7.010 | 728.62 |
| 8.011 | 776.36 | 8.014 | 767.77 | 8.026 | 759.93 | 8.021 | 750.42 | 8.014 | 740.63 | 8.004 | 729.92 |
| 9.024 | 777.27 | 9.019 | 768.74 | 9.004 | 760.94 | 9.013 | 751.50 | 9.010 | 741.80 | 9.018 | 731.21 |
| 10.025 | 778.16 | 10.003 | 769.67 | 10.013 | 761.95 | 10.029 | 752.60 | 10.007 | 742.96 | 10.011 | 732.46 |
| 11.000 | 779.02 | 11.052 | 770.64 | 11.016 | 762.94 | 11.027 | 753.66 | 11.022 | 744.11 | 10.997 | 733.66 |
| 12.017 | 779.90 | 12.005 | 771.54 | 12.003 | 763.91 | 12.003 | 754.68 | 11.997 | 745.22 | 12.013 | 734.90 |
| 13.015 | 780.76 | 13.021 | 772.44 | 13.023 | 764.89 | 13.026 | 755.73 | 13.004 | 746.33 | 12.993 | 736.07 |
| 13.999 | 781.58 | 14.000 | 773.33 | 14.003 | 765.83 | 14.052 | 756.77 | 14.018 | 747.43 | 14.024 | 737.27 |
| 15.016 | 782.44 | 15.033 | 774.23 | 15.025 | 766.77 | 15.005 | 757.72 | 15.011 | 748.49 | 14.997 | 738.38 |
| 16.003 | 783.26 | 16.000 | 775.07 | 16.000 | 767.69 | 16.028 | 758.74 | 16.029 | 749.56 | 16.021 | 739.55 |
| 17.006 | 784.06 | 17.011 | 775.95 | 17.026 | 768.61 | 16.998 | 759.68 | 16.998 | 750.56 | 17.001 | 740.66 |
| 18.001 | 784.86 | 18.023 | 776.80 | 17.997 | 769.50 | 18.025 | 760.67 | 18.026 | 751.64 | 18.031 | 741.78 |
| 19.019 | 785.67 | 18.994 | 777.63 | 19.038 | 770.43 | 19.003 | 761.60 | 18.999 | 752.62 | 19.013 | 742.85 |
| 20.000 | 786.45 | 20.037 | 778.48 | 19.994 | 771.27 | 19.993 | 762.54 | 20.029 | 753.64 | 19.998 | 743.92 |
| 21.030 | 787.25 | 21.000 | 779.30 | 21.003 | 772.14 | 21.021 | 763.49 | 20.991 | 754.60 | 21.023 | 744.99 |
| 21.997 | 788.01 | 22.019 | 780.13 | 22.048 | 773.06 | 21.999 | 764.40 | 22.028 | 755.63 | 21.996 | 746.00 |
| 23.050 | 788.83 | 23.036 | 780.97 | 22.999 | 773.89 | 23.033 | 765.34 | 22.999 | 756.57 | 23.020 | 747.07 |
| 24.003 | 789.60 | 23.995 | 781.77 | 24.025 | 774.78 | 23.998 | 766.23 | 24.038 | 757.58 | 24.020 | 748.10 |
| 25.005 | 790.39 | 25.036 | 782.62 | 25.118 | 775.71 | 25.046 | 767.18 | 25.020 | 758.52 | 24.998 | 749.12 |

Table 5. Tait and Rackett Equations: Adjusted Parameters for 1-Propanol and 2-Propanol

| range | 1-propanol | 2-propanol |
| :---: | :---: | :---: |
| $\mathrm{T}_{\text {min }} / \mathrm{K}$ | 313.15 | 313.16 |
| $\mathrm{T}_{\text {max }} / \mathrm{K}$ | 362.77 | 362.80 |
| $\mathrm{P}_{\text {min }} / \mathrm{MPa}$ | 0.500 | 0.498 |
| $\mathrm{P}_{\text {max }} / \mathrm{MPa}$ | 25.090 | 25.118 |
| $\rho_{\text {min }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | 743.92 | 719.60 |
| $\rho_{\text {max }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | 807.40 | 790.39 |
| no. data points | 160 | 156 |
| Tait parameters | 1-propanol | 2-propanol |
| C | 0.087295461 | 0.083655791 |
| $\mathrm{B}_{0}$ | 234.9514 | 217.71334 |
| $\mathrm{b}_{1}$ | -50.274 305 | -49.319 841 |
| E | 100 | 100 |
| STD/kg $\cdot \mathrm{m}^{-3}$ | $7.24 \times 10^{-2}$ | $2.22 \times 10^{-1}$ |
| $\mathrm{P}_{\text {ref }} / \mathrm{MPa}$ | 0.1 | 0.1 |
| Rackett parameters ${ }^{\text {a }}$ | 1-propanol | 2-propanol |
| $\mathrm{A}_{\mathrm{R}}$ | 0.082166243 | 0.16235064 |
| $\mathrm{B}_{\mathrm{R}}$ | 0.29008731 | 0.41872676 |
| $\mathrm{C}_{\mathrm{R}}$ | 507.26176 | 428.78187 |
| $\mathrm{D}_{\mathrm{R}}$ | 0.19825205 | 0.18361664 |

a Parameters to calculate densities are in $\mathrm{g} \cdot \mathrm{cm}^{-3}$.
We have used the M arquardt-Levenberg least squares optimization using the following objective function, S:

$$
\begin{equation*}
\mathrm{S}=\sum_{i}\left[\frac{\left(\rho_{i, \exp }-\rho_{\mathrm{i}, \text { cal }}\right.}{\rho_{i, \exp }}\right]^{2} \tag{5}
\end{equation*}
$$

to correlate the parameters of both models. The units used for the adjustment of parameters are bar, kelvin, and cubic centimeters per mole.

For 1-propanol and 2-propanol a reference pressure $\mathrm{P}_{0}$ $=0.1 \mathrm{MPa}$ was chosen. The corresponding liquid densities at atmospheric pressure can be described with a modified Rackett equation, ${ }^{15}$

$$
\begin{equation*}
\rho_{0}=\mathrm{A}_{\mathrm{R}} / \mathrm{B}_{\mathrm{R}}{ }^{\left[1+\left(1-\mathrm{T} / \mathrm{C}_{\mathrm{R}}\right)_{\mathrm{R}}\right]} \tag{6}
\end{equation*}
$$

The parameters for this equation were extrapolated from
Table 6. BWRS EoS Adjusted Parametersa for 1-Propanol and 2-Propanol

| parameter $^{1}$ | 1-propanol | 2-propanol |
| :--- | ---: | ---: |
| $\mathrm{B}_{0}$ | $1.9829332 \times 10^{2}$ | $3.6553646 \times 10^{2}$ |
| $\mathrm{~A}_{0}$ | $1.7514201 \times 10^{7}$ | $2.0066518 \times 10^{7}$ |
| $\mathrm{C}_{0}$ | $-2.6081751 \times 10^{11}$ | $-4.0416841 \times 10^{11}$ |
| $\mathrm{D}_{0}$ | $-3.8964521 \times 10^{14}$ | $-2.5047135 \times 10^{14}$ |
| $\mathrm{E}_{0}$ | $-6.6558650 \times 10^{16}$ | $-7.9757661 \times 10^{16}$ |
| b | $1.2491951 \times 10^{4}$ | $7.5203862 \times 10^{3}$ |
| a | $3.2966452 \times 10^{7}$ | $3.7009389 \times 10^{7}$ |
| d | $3.2446284 \times 10^{9}$ | $6.1168966 \times 10^{9}$ |
| c | $-6.0884670 \times 10^{13}$ | $-9.9629653 \times 10^{13}$ |
| $\alpha$ | $9.1344935 \times 10^{6}$ | $9.4287012 \times 10^{6}$ |
| u | $1.6122470 \times 10^{4}$ | $3.0915146 \times 10^{3}$ |
| ${\text { STD } / \mathrm{cm}^{3} \cdot \mathrm{~mol}^{-1}}$ | $1.02 \times 10^{-2}$ | $2.63 \times 10^{-1}$ |

a The units used for the adjustment of parameters are bar, K , and $\mathrm{cm}^{3} \cdot \mathrm{~mol}^{-1}$.

Table 7. Densities of Pure Components from the Literature ${ }^{16}$ and Comparison with Calculated Values from the BWRS EoS

| T/K | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 1-propanol |  | 2-propanol |  |
|  | lit. ${ }^{16}$ | BWRS | lit. ${ }^{16}$ | BWRS |
| 298.15 | 799.58 | 799.93 | 781.23 | 779.83 |
| 303.15 | 795.48 | 796.07 | 776.95 | 776.40 |
| 308.15 | 791.38 | 792.11 | 772.46 | 772.73 |
| 313.15 | 787.37 | 788.07 | 767.98 | 768.83 |

high-pressure experiments. Prof. Gmehling's group provided the correlated parameters ${ }^{15}$ reported in Table 5 for 1-propanol and 2-propanol. To consider the temperature dependence in the Tait equation, the following function is used:

$$
\begin{equation*}
B_{T}=b_{0}+b_{1} \frac{T}{E}+b_{2}\left(\frac{T}{E}\right)^{2}+b_{3}\left(\frac{T}{E}\right)^{3}+b_{4}\left(\frac{T}{E}\right)^{4} \tag{7}
\end{equation*}
$$

In the process to correlate the compressed liquid densities for both fluids, eq 7 was used, but it was found that similar results were obtained only retaining his linear terms. This approach is described in detail by I hmels and Gmehling. ${ }^{15}$

Table 8. Comparison of Calculated Values Using the BWRS EoS and the Tait Equation with Literature ${ }^{19}$ Density Values of 1-Propanol at 298.15 K

| P/MPa | $\rho^{\text {lit. }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\rho^{\text {BWRS }} / \mathrm{kg}^{\mathbf{1}} \mathrm{m}^{-3}$ | $\left(\left(\rho^{\text {lit. } .^{18}}-\rho^{\text {BWRS }}\right) / \rho^{\text {lit. }{ }^{18}}\right) \times 100$ | $\rho^{\text {Tait }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\left(\left(\rho^{\text {lit. }{ }^{18}}-\rho^{\text {Tait }}\right) / \rho^{\text {lit. }{ }^{18}}\right) \times 100$ |
| ---: | :---: | :---: | :---: | :---: | :---: |
| 2.00 | 801.00 | 801.38 | -0.047 | 801.45 | -0.057 |
| 5.99 | 803.90 | 804.38 | -0.060 | 804.61 | -0.088 |
| 7.98 | 805.30 | 805.85 | -0.068 | 806.14 | -0.104 |
| 11.97 | 808.10 | 808.74 | -0.079 | 809.13 | -0.127 |
| 15.96 | 810.90 | 811.57 | -0.083 | 812.02 | -0.138 |
| 19.95 | 813.50 | 814.34 | -0.104 | 814.81 | -0.161 |
| 23.93 | 816.10 | 817.04 | -0.116 | 817.52 | -0.174 |
| 28.92 | 819.30 | 820.37 | -0.130 | 820.80 | -0.183 |
| 33.90 | 822.40 | 823.59 | -0.145 | 823.95 | -0.189 |



Figure 2. Relative deviations between experimental data $\left(\mathrm{V}_{1}\right)$ and those calculated with the BWRS EoS and the Tait equation $\left(\mathrm{V}_{2}\right)$ fitted on data reported in this work for 1-propanol at the following temperatures: © 313.15 K ; $\mathbf{~ v}, 323.10 \mathrm{~K} ; \mathbf{■}, 332.99 \mathrm{~K} ; \mathbf{\Delta}, 352.88$ K; $\uparrow 362.77$ K. Open and closed symbols are for Tait and BRWS equations, respectively.


Figure 3. Comparison of the experimental molar volumes from ref $17\left(V_{1}\right)$ for 1-propanol with the values calculated with the BWRS EoS $\left(\mathrm{V}_{2}\right)$ fitted on data reported in this work at 313.15 K .

## Results

The densities of pure liquids reported in Table 2 and the corresponding data calculated through both correlations for both fluids were compared with the experimental data of Nikam et al. ${ }^{16}$

The obtained results at atmospheric pressure agree within $\pm 0.86 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$ for 1-propanol and $\pm 0.65 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$ for 2-propanol (se Table 2) with those reported by Nikam et al. ${ }^{16}$

The liquid densities of 1-propanol and 2-propanol were determined at six temperatures from 313 to 363 K (see Tables 3 and 4) and compared with the data of Yaginuma et al. ${ }^{17,18}$ For the comparison, the data reported in this work


Figure 4. Relative deviations between experimental data $\left(\mathrm{V}_{1}\right)$ and those calculated with the BWRS EoS and the Tait equation $\left(\mathrm{V}_{2}\right)$ fitted on data reported in this work for 2-propanol at the following temperatures: •, 313.15 K; v, 323.10 K; ■, 332.99 K; ©, 352.93 K; 362.77 K. Open and closed symbols are for Tait and BRWS equations, respectively.

Table 9. Comparison of Calculated Data at 313.15 K with the BWRS EoS for 1-Propanol with Data from ref 17

| $\mathrm{P} / \mathrm{MPa}$ | $\rho^{\text {BWRS }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\rho^{\text {exp }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\left(\left(\rho^{\text {exp }}-\rho^{\text {BWRS }}\right) / \rho^{\text {exp }}\right) \times 100$ |
| :---: | :---: | :---: | :---: |
| 1.000 | 788.73 | 788.60 | -0.017 |
| 2.000 | 789.56 | 789.50 | -0.008 |
| 3.000 | 790.39 | 790.40 | 0.001 |
| 4.000 | 791.22 | 791.20 | -0.002 |
| 5.000 | 792.03 | 791.20 | -0.105 |
| 6.000 | 79.84 | 792.10 | -0.094 |
| 7.000 | 793.65 | 793.80 | 0.019 |
| 8.000 | 794.45 | 794.40 | -0.006 |
| 9.000 | 795.25 | 795.40 | 0.019 |
| 9.500 | 795.65 | 795.80 | 0.019 |
| 9.800 | 795.88 | 796.00 | 0.015 |

were correlated for the whole range of pressures and temperatures reported using the BWRS EoS ${ }^{14}$ and the Tait equation. The obtained parameters for the different equations and their standard deviations (STDs) are given in Tables 5 and 6 . Relative deviations between experimental data ( $\mathrm{V}_{1}$ experimental molar volume) and those calculated with the BWRS EoS and the Tait equation ( $\mathrm{V}_{2}$ calculated molar volume) fitted to the data reported in this work for 1-propanol and 2-propanol are presented in Figures 2 and 4. The maximum relative deviations $100\left(\mathrm{~V}_{1}-\mathrm{V}_{2}\right) N_{1}$ from Figure 2 are $+0.032 \%$ and $-0.125 \%$ for 1-propanol, and from Figure 4 are $+0.082 \%$ and $-0.05 \%$ for 2 -propanol, and the standard deviations (STDs) are given in Tables 5 and 6.

The calculated values for 1-propanol and 2-propanol using the BRWS EoS were compared with those published by Nikam et al. ${ }^{16}$ at atmospheric pressure liquid densities, and both of them agree (see Table 7).

The densities of 1-propanol and 2-propanol correlated to the BWRS EoS ${ }^{14}$ were compared with the experimental

Table 10. Comparison of Calculated Values Using the BWRS EoS and the Tait Equation with Literature ${ }^{20}$ Density Values of 2-Propanol at Different Temperatures

| $\mathrm{T} / \mathrm{K}$ | $\mathrm{P} / \mathrm{MPa}$ | $\rho^{\text {lit. } .{ }^{19}} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\rho^{\text {BWRS }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\left(\left(\rho^{\text {lit. } .^{19}}-\rho^{\text {BWRS }}\right) / \rho^{\text {lit. } .^{19}}\right) \times 100$ | $\rho^{\text {Tait }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\left(\left(\rho^{\text {lit. } .{ }^{19}}-\rho^{\text {Tait }}\right) / \rho^{\text {lit. } .{ }^{19}}\right) \times 100$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 303.15 | 0.1 | 776.40 | 776.40 | 0.00 |  |  |
| 303.15 | 20.0 | 793.00 | 792.89 | 0.01 | 793.45 |  |
| 303.15 | 40.0 | 806.70 | 807.20 | -0.06 | 807.29 | -0.06 |
| 303.15 | 60.0 | 818.40 | 819.87 | -0.18 | 819.16 | -0.07 |
|  |  |  | -0.09 |  |  |  |



Figure 5. Percent relative deviation calculations between the experimental data of Yaginuma et al. ${ }^{18}\left(\mathrm{~V}_{1}\right)$ for 2-propanol and the values of the BWRS EoS $\left(\mathrm{V}_{2}\right)$ fitted on data reported in this work at 313.15 K .

Table 11. Comparison of Calculated Data at 313.15 K with the BWRS EoS for 2-Propanol with Experimental Data from ref 18

| $\mathrm{P} / \mathrm{MPa}$ | $\rho^{\mathrm{BWRS}} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\rho^{\exp } / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\left(\left(\rho^{\exp }-\rho^{\mathrm{BWRS}}\right) / \rho^{\exp }\right) \times 100$ |
| :---: | :---: | :---: | :---: |
| 1.000 | 769.62 | 768.7 | -0.120 |
| 2.000 | 770.56 | 769.6 | -0.125 |
| 3.000 | 771.49 | 770.6 | -0.116 |
| 4.000 | 772.41 | 771.6 | -0.105 |
| 5.000 | 773.34 | 772.5 | -0.108 |
| 6.000 | 774.24 | 773.5 | -0.096 |
| 7.000 | 775.14 | 774.4 | -0.096 |
| 8.000 | 776.03 | 775.3 | -0.095 |
| 9.000 | 776.92 | 776.2 | -0.092 |
| 9.500 | 777.36 | 776.7 | -0.085 |
| 9.800 | 777.62 | 776.9 | -0.093 |

values of data reported by Yaginuma et al. ${ }^{17-18}$ The obtained results agree quite well with those of Yaginuma et al. ${ }^{17}$ (see Figure 3 and Table 9) and Yaginuma et al. ${ }^{18}$ (see Figure 5 and Table 11). The maximum relative deviations from Figure 3 are $+0.02 \%$ and $-0.11 \%$, and that from Figure 5 is $-0.125 \%$.

To demonstrate the versatility of the models used in this study, the densities were calculated outside the range of parameters adjustment. In doing so, it was noted that the models provide excellent results, as can be observed by examining results given in Table 8 of ref 19 for 1-propanol and Table 10 of ref 20 for 2-propanol.

The temperatures were selected taking into account the intended industrial applications of $\mathrm{CO}_{2}$ and of binary mixtures containing $\mathrm{CO}_{2}$ and alcohols, as a supercritical fluid for extracting components of natural products.

## Conclusions

Experimental determinations of densities were carried out at the temperatures $313-363 \mathrm{~K}$ and at pressures up to 25 MPa for 1-propanol and 2-propanol, using a vibrating tube densimeter DTV. The reported data are consistent with those appearing in the literature, and the correlated
models are reliable for extrapolating densities at lower temperatures.

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[^1]:    a Measurement of densities on decreasing the pressure after its increment up to 25 MPa .

