# Vapor Pressure Measurements of 1,1,1,2,3,3,3-Heptafluoropropane from 233.15 to $\mathbf{3 7 5 . 1 5}$ K 

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#### Abstract

The vapor pressures of 1,1,1,2,3,3,3-heptafluoropropane (HFC-227ea) were measured in the temperature range from 233.15 to 375.15 K . The uncertainties of the measurements were estimated to be within $\pm 1.5$ kPa for pressure and within $\pm 5 \mathrm{mK}$ for temperature. The purity of the HFC-227ea sample used in the present measurements was $99.9 \mathrm{~mol} \%$. A Wagner-type vapor pressure equation for HFC-227ea was developed. The critical pressure was calculated from the vapor pressure equation at the critical temperature. The normal boiling point and acentric factor were also determined.


## Introduction

The Montreal Protocol establishes schedules for phasing out the manufacture of chlorine-containing refrigerants, chlorofluorocarbons (CFC) and hydrochlorofluorocarbons (HCFC), which have been implicated in stratospheric ozone depletion. The compound 1,1,1,2,3,3,3-heptafluoropropane (HFC-227ea), which is chlorine-free, could be considered as a possible alternative refrigerant. It is intended as a potential alternative for CFC12 and CFC114 for units with high condensing temperatures, and blends containing HFC227 ea are potential alternatives to HCFC22 and R502. The atmospheric lifetime, ozone-depletion potential relative to CFC11, and global-warming potential relative to $\mathrm{CO}_{2}$ at 100 years of HFC-227ea are 36.5 years, 0, and 2900, respectively. ${ }^{1}$

Vapor pressures are among the most fundamental thermophysical properties for pure substances. To our knowledge, only a few measurements of thevapor pressure of HFC-227ea have been published in the literature, those of Salvi-Narkhede et al. ${ }^{2}$ and Lin Shi et al. ${ }^{3}$ Weber also measured 31 vapor pressure data. ${ }^{4}$ In this paper, 145 vapor pressure data for HFC-227ea were measured in the temperature range from 233.15 to 375.15 K , and a Wagnertype vapor pressure equation for HFC-227ea was developed.

## Experimental Section

Reagent. The sample of HFC-227ea was obtained from Zhejiang Chemical Industry Research Institute, with a stated purity of $99.9 \mathrm{~mol} \%$, and the water content was $<0.0006 \mathrm{~mol} \%$. It was used without further purification.
Apparatus. Figure 1 shows the schematic of the experimental apparatus used. It is composed of a thermostatic bath, a temperature measurement and control system, a pressure measurement system, a vacuum system, and an optical sample cell.

The thermostatic bath has two glass windows with inner dimensions of $350 \times 350 \times 500 \mathrm{~mm}$. The temperature can be varied from 233 to 453 K . The bath fluid used is al cohol,

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Figure 1. Experimental apparatus: (A) optical sample cell; (B) platinum resistance thermometer; (C) differential pressure detector; (D) HP34970A data acquisition/switch unit; (E) personal computer; (F) silicon-controlled switch; (G) stirrer; (H1, H2) heaters; (I) cooler; (J) thermostatic bath; (K) nitrogen gas; (L) oilpiston type dead-weight pressure gauge; (M) oil-gas separator; (N) sample bottle; (O) vacuum gauge; (P) vacuum pump; (V1-V8) valves.
distilled water, or silicon oil depending on the temperature range. Its temperature-controlling uncertainty is $\pm 2 \mathrm{mK}$. The temperature measurement and control system are made with a four-wire $25-\Omega$ platinum resistance thermometer (Y unnan Instrument) with an uncertainty of $\pm 2 \mathrm{mK}$ (ITS-90), which was calibrated by the water's triple-point temperature before experiment, and an HP34970A data acquisition/switch unit (Hewlett-Packard Co.) with an uncertainty of $< \pm 1 \mathrm{mK}$. The overall temperature uncertainty is $\sim \pm 5 \mathrm{mK}$. We programmed temperature measurement control software on the basis of an incremental digital PID algorithm. The temperature of the thermostatic bath can be measured and controlled by a personal computer automatically at the same time, which controls the siliconcontrolled on/off switch to change the electric power of the heaters.

The pressure measurement system includes an oil-piston type dead-weight pressure gauge (Xi'an Instrument, YS60), a differential pressure detector (Xi'an Instrument, 1151DP), and a mercury atmosphere gauge (Ningbo Instrument, DYM-1). The accuracy of the oil-piston type deadweight pressure gauge is $0.02 \%$ in the range from 0.1 to 6.0 MPa, and its maximum uncertainty is 1.2 kPa . The

Table 1. Experimental Vapor Pressure Data of HFC-227ea

| T/K | P/kPa | T/K | P/kPa | T/K | P/kPa | T/K | P/kPa | T/K | P/kPa | T/K | P/kPa |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 233.149 | 32.316 | 258.151 | 107.505 | 283.149 | 279.532 | 308.155 | 610.988 | 332.150 | 1147.493 | 356.150 | 1982.182 |
| 234.150 | 34.089 | 259.150 | 112.142 | 284.150 | 289.373 | 309.148 | 628.737 | 333.150 | 1174.997 | 357.150 | 2024.761 |
| 235.150 | 36.004 | 260.150 | 117.247 | 285.149 | 299.626 | 310.148 | 646.395 | 334.150 | 1203.975 | 358.150 | 2068.828 |
| 236.153 | 38.004 | 261.149 | 122.107 | 286.149 | 309.991 | 311.149 | 664.932 | 335.150 | 1234.747 | 359.151 | 2112.981 |
| 237.150 | 40.040 | 262.149 | 127.270 | 287.150 | 320.330 | 312.000 | 681.342 | 336.151 | 1264.065 | 360.150 | 2157.528 |
| 238.157 | 42.149 | 263.151 | 132.506 | 288.150 | 330.674 | 312.150 | 683.200 | 337.150 | 1293.774 | 361.150 | 2203.239 |
| 239.150 | 44.460 | 264.150 | 138.087 | 289.150 | 341.956 | 313.150 | 702.836 | 338.150 | 1324.554 | 362.148 | 2249.814 |
| 240.150 | 46.823 | 265.150 | 143.807 | 290.150 | 353.494 | 314.150 | 722.165 | 339.150 | 1355.410 | 363.151 | 2297.573 |
| 241.150 | 49.203 | 266.150 | 149.695 | 291.150 | 364.970 | 315.150 | 742.183 | 340.151 | 1387.639 | 364.150 | 2345.386 |
| 242.154 | 51.562 | 267.150 | 155.876 | 292.149 | 376.870 | 316.151 | 762.043 | 341.150 | 1420.223 | 365.149 | 2394.993 |
| 243.149 | 54.255 | 268.151 | 161.800 | 293.150 | 389.450 | 317.149 | 783.395 | 342.150 | 1454.043 | 366.149 | 2444.628 |
| 244.150 | 57.068 | 269.150 | 167.977 | 294.150 | 401.783 | 318.149 | 804.495 | 343.001 | 1482.927 | 367.150 | 2495.090 |
| 245.150 | 59.776 | 270.150 | 174.663 | 295.150 | 414.391 | 319.150 | 825.755 | 343.151 | 1487.027 | 368.150 | 2547.268 |
| 246.150 | 62.698 | 271.150 | 181.599 | 296.150 | 427.631 | 320.150 | 848.456 | 344.148 | 1521.227 | 369.151 | 2599.253 |
| 247.150 | 65.619 | 272.150 | 188.458 | 297.150 | 441.234 | 321.150 | 870.404 | 345.150 | 1556.224 | 370.150 | 2653.351 |
| 248.150 | 68.953 | 273.152 | 195.337 | 298.152 | 455.013 | 322.150 | 892.726 | 346.149 | 1590.884 | 371.150 | 2706.665 |
| 249.150 | 72.175 | 274.150 | 202.987 | 299.150 | 469.138 | 323.150 | 915.998 | 347.150 | 1626.366 | 372.149 | 2763.159 |
| 250.151 | 75.789 | 275.150 | 210.889 | 300.150 | 483.140 | 324.150 | 940.172 | 348.151 | 1664.489 | 373.150 | 2820.940 |
| 251.149 | 79.168 | 276.150 | 218.852 | 301.150 | 498.048 | 325.151 | 964.789 | 349.152 | 1701.423 | 374.151 | 2877.705 |
| 252.150 | 82.791 | 277.150 | 226.733 | 302.150 | 513.654 | 326.150 | 989.522 | 350.150 | 1739.897 | 375.150 | 2937.158 |
| 253.149 | 86.737 | 278.149 | 235.054 | 303.148 | 528.626 | 327.150 | 1013.611 | 351.151 | 1778.492 |  |  |
| 254.150 | 90.634 | 279.149 | 243.844 | 304.150 | 544.494 | 328.150 | 1039.059 | 352.148 | 1817.834 |  |  |
| 255.150 | 94.720 | 280.149 | 252.400 | 305.150 | 560.771 | 329.150 | 1065.613 | 353.151 | 1857.444 |  |  |
| 256.150 | 98.888 | 281.150 | 261.473 | 306.172 | 577.156 | 330.150 | 1092.352 | 354.149 | 1898.573 |  |  |
| 257.150 | 103.049 | 282.149 | 270.331 | 307.156 | 593.928 | 331.151 | 1119.279 | 355.150 | 1939.553 |  |  |



Figure 2. Absolute deviation of the vapor pressure data from eq 1: ■, this work; $\nabla$, Salvi-Narkhede et al.; ${ }^{2} \square$, Lin Shi et al.; ${ }^{3} \Delta$, Weber. ${ }^{4}$
accuracy of the differential pressure detector is $0.5 \%$ in the range from 0 to 50 kPa , its maximum uncertainty is 0.25 kPa , and the mercury atmosphere gauge is $\pm 50 \mathrm{~Pa}$. The overall maximum experimental uncertainty in the pressure measurements can be estimated to be within $\pm 1.5 \mathrm{kPa}$.

All instruments were calibrated by their manufacturer before measurement.

The optical sample cell is a cylindrical vessel made of stainless steel with two quartz glass windows ( $\sim 13 \mathrm{~cm}^{3}$ in inner volume). Before the experiment, the sample cell was rinsed with acetone to remove any residue from previous experiments and vacuumed. The extremely high vacuum is $1 \times 10^{-4} \mathrm{~Pa}$.

## Results and Discussion

A total of 145 points were measured at temperatures from 233 to 375 K, and the pressures varied from 32 to 2937 kPa . The temperatures are given on the ITS-90 scale. The experimental vapor pressures of HFC-227ea are given in Table 1.


Figure 3. Relative deviation of the vapor pressure data from eq 1: ■, this work; $\nabla$, Salvi-Narkhede et al.; ${ }^{2} \square$, Lin Shi et al.; ${ }^{3} \Delta$, Weber. ${ }^{4}$

On the basis of the present vapor pressure measurements, we devel oped a Wagner-type equation ${ }^{5}$ to correlate the vapor pressures:

$$
\begin{equation*}
\ln (\mathrm{P} / \mathrm{kPa})=\mathrm{A}_{1}+\left(\mathrm{A}_{2} \mathrm{t}+\mathrm{A}_{3} \mathrm{t}^{1.5}+\mathrm{A}_{4} \mathrm{t}^{2.5}+\mathrm{A}_{5} 5^{5}\right) \mathrm{T}_{d} T \tag{1}
\end{equation*}
$$

In eq 1, $\mathrm{t}=1-\mathrm{T} / \mathrm{T}_{\mathrm{c}}, \mathrm{T}_{\mathrm{c}}=375.95 \mathrm{~K}^{6}$ is the critical temperature, $\mathrm{A}_{1}=8.001231, \mathrm{~A}_{2}=-7.717082, \mathrm{~A}_{3}=$ 1.682182, $\mathrm{A}_{4}=-2.644382$, and $\mathrm{A}_{5}=-4.210056$. The equation is effective for the range of temperatures from 233 K to the critical temperature. The critical pressure $\mathrm{P}_{\mathrm{c}}$ was calculated to be 2984.6 kPa . The normal boiling point was also determined to be $\mathrm{T}_{\mathrm{b}}=256.454 \mathrm{~K}$ with an uncertainty of $\pm 5 \mathrm{mK}$.

Using eq 1, with the above-calculated critical pressure, the value of the acentric factor obtained was $\omega=0.352$.

The absolute and relative deviations from eq 1 of all the measured values including the present study and those by Salvi-Narkhede et al., ${ }^{2}$ Lin Shi et al., ${ }^{3}$ and Weber ${ }^{4}$ are shown in Figures 2 and 3, respectively. The present measurements show that the maximum absol ute deviation
is $\sim 1.4 \mathrm{kPa}$ at 347.15 K from eq 1, and the absolute average deviation is $0.054 \%$. Figure 2 shows that the data of Lin Shi et al. ${ }^{3}$ agree well with our data; the experimental results of Salvi-Narkhede et al. ${ }^{2}$ are $\sim 7 \mathrm{kPa}$ higher than our data in thetemperature range from 300 K to the critical point. Figure 3 shows that Weber's ${ }^{4}$ data are $\sim 0.15 \%$ higher than our data. The data of Lin Shi et al. ${ }^{3}$ agree with eq 1 within $\pm 0.1 \%$ at most temperatures; however, in the temperature range from 243 to 258 K, their results are $\sim 0.2 \%$ higher than our data.

## Conclusion

We have measured 145 vapor pressures of HFC-227ea at temperatures from 233 to 375 K and corresponding pressures from 32 to 2937 kPa . The uncertainties of the measurements were estimated to be within $\pm 1.5 \mathrm{kPa}$ for pressure and within $\pm 5 \mathrm{mK}$ for temperature. A Wagnertype vapor pressure equation was developed. The critical pressure was calculated by using the developed vapor pressure equation at the critical temperature, and the normal boiling point and acentric factor were also determined.

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