# Measurement and Correlation of Excess Molar Enthalpies of Carbon Dioxide + 2-Butanol and 2-Propanol Systems at the Temperatures 303.15 K and 308.15 K and at Pressures from 7.0 to 8.5 MPa 

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#### Abstract

The excess molar enthalpies of carbon dioxide + 2-butanol and 2-propanol systems were measured in the vicinity of the critical point of carbon dioxide using a flow-type isothermal microcalorimeter at the temperatures 303.15 K and 308.15 K and at pressures from 7.0 to 8.5 MPa . A strong dependence of $\mathrm{H}^{\mathrm{E}}$ on pressure at this area was observed. The correlation of the excess molar enthalpies was made using a composition-dependent equation composed of two polynomial expressions.


## Introduction

In our previous paper, we constructed a database for excess molar enthalpy data of binary systems containing a supercritical fluid, and some characteristic phenomena have been analyzed (Dai et al., 1998a). Among several supercritical fluids, carbon dioxide has been widely used as a solvent in extraction processes. The chemical, petrochemical, food, and pharmaceutical industries have mostly benefited from these new extraction technologies. Supercritical carbon di oxide also can be used for the development of heat pumps and other energy-saving processes in heat exchange, heat transport, and heat storage. This is because, under conditions exceeding the critical point of carbon dioxide, the excess molar enthal py of binary systems often shows large deviations in comparison with the normalpressure behavior. The critical temperature of carbon dioxide is close to ambient temperature, and carbon dioxide has no smell or taste and is unburnable. Therefore, we focused on the excess molar enthal pies of binary systems containing supercritical carbon dioxide. Some attempts were made to study the carbon dioxide + methanol system (Dai et al., 1998b; Dai et al., 1999). This work is a continuation of our previous studies.

In this study, we measured excess molar enthalpies of carbon dioxide +2 -butanol and +2 -propanol systems in the vicinity of the critical point of carbon dioxide to examine the pressure dependence of their thermal behavior in detail. The measurement was carried out using a flow isothermal microcal orimeter at the temperatures 303.15 K and 308.15 K and at pressures from 7.0 to 8.5 MPa . For those binary systems, there are no excess molar enthal py data available in the literature. The high-pressure vaporliquid equilibria for those binary systems have been measured by other authors (Stevens et al., 1997; Suzuki et al., 1991).

## Experimental Section

The high-pressure flow isothermal microcalorimeter (Calorimetry Sciences Corp.) was used for the measurement. It mainly consists of a mixing unit, a constant-

[^0]Table 1. Densities of Materials Used in This Study To Convert Flow Rates from Cubic Centimeters per Minute to Mole Fractions

|  |  | $\rho / \mathrm{g} \mathrm{cm}^{-3}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~T} / \mathrm{K}$ | P/MPa | carbon dioxide | 2-butanol | 2-propanol |
| 293.15 | 7.0 | 0.7977 | 0.7911 | 0.8119 |
|  | 7.5 | 0.7981 | 0.7914 | 0.8123 |
|  | 8.0 | 0.7985 | 0.7918 | 0.8127 |
|  | 8.5 | 0.7990 | 0.7922 | 0.8130 |

temperature water bath, two high-pressure ISCO syringe pumps for sample supply, a cooling circulation system, a pressure adjustment device, and a personal computer for signal collection and data processing. Measurement is possible from 273 K to 473 K and from 0.1 MPa to 14 MPa . The experimental apparatus and procedure have been described in detail elsewhere (Dai et al., 1998b; Dai et al., 1999). In the present study, the reproducibility is within $\pm 0.8 \%$ (absolute accuracy is $10 \mathrm{~J} \mathrm{~mol}{ }^{-1}$ ), the uncertainty being due primarily to the high sensitivity of the $\mathrm{H}^{\mathrm{E}}$ values to small changes in temperature and pressure. The range of total flow rate was $0.05-0.20 \mathrm{~cm}^{3} \mathrm{~min}^{-1}$ for all temperatures and pressures studied.

The 2-butanol and 2-propanol used in this study were special grade pure reagents (Wako Pure Chemical Industry, Ltd., J apan) and were used after removing trace water with molecular sieves. The purity of the 2-butanol and the 2-propanol was checked by gas chromatography and found to be better than $99.9 \mathrm{~mol} \%$. The purity of the carbon dioxide was 99.99 vol \% (Showa Carbonic Acid Company Ltd., J apan). Prior to use, the carbon dioxide was filtered through a $0.5 \mu \mathrm{~m}$ in-line filter (NUPRO Company).

Flow rates measured in cubic centimeters per minute at a constant temperature of 293.15 K were converted to moles per minute and to mole fractions using the densities of the pure materials estimated as follows. The densities of carbon dioxide at 293.15 K and different pressures were from the values of the literature (NIST, 1998). The densities of 2-butanol and 2-propanol at 293.15 K and different pressures were obtained by interpolating the values of the literature (K ubota et al., 1987). The calculated densities of materials are given in Table 1.

Table 2. Experimental Excess Molar Enthalpies of the Carbon Dioxide (1) + 2-Butanol (2) System

| $\mathrm{P}=7.5 \mathrm{MPa}$ |  | $\mathrm{P}=8.0 \mathrm{MPa}$ |  | $\mathrm{P}=8.5 \mathrm{MPa}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{X}_{1}$ | $\mathrm{H}^{\mathrm{E}} / \mathrm{J} \cdot \mathrm{mol}^{-1}$ | $\mathrm{X}_{1}$ | $\mathrm{H}^{\mathrm{E}} / \mathrm{J} \cdot \mathrm{mol}^{-1}$ | $\mathrm{X}_{1}$ | $\mathrm{H}^{\mathrm{E}} \mathrm{J} \cdot \mathrm{mol}^{-1}$ |
| $\mathrm{T}=303.15 \mathrm{~K}$ |  |  |  |  |  |
| 0.0417 | 94 | 0.0422 | 105 | 0.0425 | 81 |
| 0.0821 | 247 | 0.0829 | 279 | 0.0836 | 253 |
| 0.1211 | 443 | 0.1222 | 442 | 0.1232 | 450 |
| 0.1588 | 548 | 0.1602 | 583 | 0.1614 | 663 |
| 0.2306 | 683 | 0.2325 | 752 | 0.2342 | 874 |
| 0.2981 | 791 | 0.3003 | 881 | 0.3022 | 958 |
| 0.3615 | 835 | 0.3640 | 948 | 0.3661 | 1021 |
| 0.4213 | 846 | 0.4239 | 988 | 0.4261 | 1047 |
| 0.4777 | 845 | 0.4803 | 984 | 0.4827 | 1052 |
| 0.5311 | 798 | 0.5337 | 959 | 0.5360 | 1033 |
| 0.5816 | 738 | 0.5841 | 910 | 0.5864 | 1000 |
| 0.6295 | 660 | 0.6319 | 853 | 0.6341 | 944 |
| 0.6749 | 580 | 0.6772 | 785 | 0.6793 | 875 |
| 0.7182 | 485 | 0.7203 | 697 | 0.7221 | 793 |
| 0.7593 | 359 | 0.7612 | 610 | 0.7629 | 702 |
| 0.7985 | 242 | 0.8002 | 514 | 0.8017 | 607 |
| 0.836 | 138 | 0.8374 | 418 | 0.8387 | 510 |
| 0.8717 | 17 | 0.8729 | 329 | 0.8739 | 423 |
| 0.9059 | -74 | 0.9068 | 236 | 0.9076 | 328 |
| 0.9386 | -175 | 0.9392 | 151 | 0.9397 | 231 |
| 0.9544 | -164 | 0.9703 | 75 | 0.9705 | 107 |
| 0.9699 | -125 |  |  |  |  |
| 0.9851 | -32 |  |  |  |  |
| $\mathrm{T}=308.15 \mathrm{~K}$ |  |  |  |  |  |
| 0.0821 | -97 | 0.0422 | 132 | 0.0425 | 129 |
| 0.1588 | -185 | 0.0829 | 280 | 0.0836 | 340 |
| 0.2306 | -322 | 0.1222 | 407 | 0.1232 | 499 |
| 0.2981 | -433 | 0.1602 | 485 | 0.1614 | 600 |
| 0.3615 | -591 | 0.2325 | 565 | 0.2342 | 739 |
| 0.4213 | -735 | 0.3003 | 616 | 0.3022 | 808 |
| 0.4777 | -901 | 0.3640 | 637 | 0.3661 | 831 |
| 0.5311 | -1064 | 0.4239 | 618 | 0.4261 | 833 |
| 0.5816 | -1255 | 0.4803 | 571 | 0.4827 | 816 |
| 0.6295 | -1435 | 0.5337 | 505 | 0.5360 | 766 |
| 0.6749 | -1677 | 0.5841 | 419 | 0.5864 | 713 |
| 0.7182 | -1929 | 0.6319 | 309 | 0.6341 | 633 |
| 0.7593 | -2249 | 0.6772 | 199 | 0.6793 | 534 |
| 0.7985 | -2607 | 0.7203 | 88 | 0.7221 | 444 |
| 0.836 | -2899 | 0.7612 | -29 | 0.7629 | 345 |
| 0.8717 | -2895 | 0.8002 | -165 | 0.8017 | 249 |
| 0.9059 | -2530 | 0.8374 | -267 | 0.8387 | 137 |
| 0.9386 | -1381 | 0.8729 | -408 | 0.8739 | 9 |
| 0.9596 | -669 | 0.9068 | -456 | 0.9076 | -142 |
|  |  | 0.9392 | -420 | 0.9397 | -134 |
|  |  |  |  | 0.9553 | -125 |
|  |  |  |  | 0.9705 | -71 |

## Results and Discussion

The experimental excess molar enthal py data are listed in Tables 2 and 3. A graphical representation of the experimental $\mathrm{H}^{\mathrm{E}}$ data is given in Figures 1-4. The critical temperature and critical pressure of carbon dioxide are 304.2 K and 7.38 M Pa (Reid et al., 1987), respectively. As can be seen from different diagrams, large changes in $\mathrm{H}^{\mathrm{E}}$ with temperature and pressure, especially with pressure, are observed. When the system pressure is decreased, the measurement of $\mathrm{H}^{\mathrm{E}}$ becomes difficult at a high concentration of carbon dioxide and the reproducibility of $\mathrm{H}^{\mathrm{E}}$ values also becomes poor.

The large changes in $\mathrm{H}^{\mathrm{E}}$ near the critical region can be estimated by the changes in the heat capacity at constant pressure ( $\mathrm{C}_{\mathrm{p}}$ ) of the components and the mixture in this region (Christensen et al., 1987). We examined the Cp of carbon dioxide near the critical point. Figure 5 is a $\mathrm{C}_{\mathrm{p}}-$ $\mathrm{T}-\mathrm{P}$ plot of carbon dioxide near the critical point which has been drawn from the available $C_{p}$ data in the literature (Vargaftik, 1975). In Figure 5, it shows the maximum $C_{p}$ values of carbon dioxide at the different temperatures and


Figure 1. Experimental excess molar enthalpy data for the system carbon dioxide (1) +2 -butanol (2) at 303.15 K : ( O ) 7.5 MPa ; (ロ) 8.0 MPa ; ( $\Delta$ ) 8.5 MPa . Solid lines are correlated with eqs 2 and 3.


Figure 2. Experimental excess molar enthalpy data for the system carbon dioxide (1) + 2-butanol (2) at 308.15 K : (O) 7.5 MPa ; (■) 8.0 MPa ; ( $\Delta$ ) 8.5 MPa . Solid lines are correlated with eqs 2 and 3.
pressures (points A to G). As can be seen in Figure 5, the constant-pressure heat capacity changes sharply in the vicinity of the critical point, and it becomes infinite at the critical point $A$. We also made a $\ln \left(P_{s}\right)$ versus $1 / T$ plot of carbon dioxide, shown in Figure 6, using the literature data (Vargaftik, 1975). The points A to G in Figure 6 correspond to the maximum values of the constant-pressure heat capacities in Figure 5. All of the points (A to G) are on the extension line of the vapor pressure curve of carbon dioxide beyond the critical point. It means that when temperature and pressure are on the vapor pressure curve or its extension line beyond the critical point, the value of $C_{p}$ will change rapidly. At constant pressure, the excess molar enthalpy changes with the temperature can be expressed as eq 1 .

$$
\begin{equation*}
\left(\frac{\partial H^{E}}{\partial T}\right)_{P}=C_{P}^{E}=C_{P}-\left(x_{1} C_{P, 1}+x_{2} C_{P, 2}\right) \tag{1}
\end{equation*}
$$

Table 3. Experimental Excess Molar Enthalpies of the Carbon Dioxide (1) + 2-Propanol (2) System


Figure 3. Experimental excess molar enthalpy data for the system carbon dioxide (1) + 2-propanol (2) at 303.15 K: ( $\nabla$ ) 7.0 MPa; (O) 7.5 MPa; (ㅁ) 8.0 MPa ( $\Delta$ ) 8.5 MPa . Solid lines are correlated with eqs 2 and 3.

Table 4. Parameters and Deviations of Correlation by Using Eqs 2 and $3^{a}$

|  | $\mathrm{T} / \mathrm{K}=303.15$ |  |  | $\mathrm{T} / \mathrm{K}=308.15$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{Pb}^{\mathrm{b}}=7.5$ | $\mathrm{P}^{\mathrm{b}}=8.0$ | $\mathrm{P}^{\mathrm{b}}=8.5$ | $\mathrm{P}^{\mathrm{b}}=7.5$ | $\mathrm{P}^{\mathrm{b}}=8.0$ | $\mathrm{P}^{\mathrm{b}}=8.5$ |
| $\mathrm{a}_{1}$ | $2.89127 \times 10^{7}$ | $4.16512 \times 10^{7}$ | $7.05807 \times 10^{7}$ | $-1.2484 \times 10^{9}$ | $-1.31909 \times 10^{8}$ | $3.62844 \times 10^{7}$ |
| $\mathrm{a}_{2}$ | $9.92134 \times 10^{7}$ | $9.20847 \times 10^{7}$ | $1.45602 \times 10^{8}$ | $-2.41919 \times 10^{9}$ | $-2.28244 \times 10^{8}$ | $1.30952 \times 10^{8}$ |
| $a_{3}$ | $6.89579 \times 10^{7}$ | $5.12848 \times 10^{7}$ | $7.63411 \times 10^{7}$ | $-1.16575 \times 10^{9}$ | $-1.01103 \times 10^{8}$ | $9.52039 \times 10^{7}$ |
| $\mathrm{b}_{1}$ | 3310.36 | 3941.37 | 4283.33 | -3737.98 | 2170.41 | 3186.16 |
| $\mathrm{b}_{2}$ | 1662.13 | 934.621 | 904.786 | 4428.41 | 2444.43 | 1854.75 |
| $\mathrm{b}_{3}$ | -1236.93 | -1016.19 | -1053.73 | -1331.29 | -765.066 | -335.817 |
| $\delta_{1}$ | 16 | 10 | 8 | 36 | 10 | 13 |
| $\delta_{2}$ | 1.9 | 1.0 | 0.7 | 1.5 | 1.6 | 1.6 |
|  | Carbon Dioxide + 2-Propanol |  |  |  |  |  |


|  | $\mathrm{T} / \mathrm{K}=303.15$ |  |  |  | T/K = 308.15 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{Pb}^{\mathrm{b}}=7.0$ | $\mathrm{Pb}^{\mathrm{b}}=7.5$ | $\mathrm{Pb}^{\mathrm{b}}=8.0$ | $\mathrm{Pb}^{\mathrm{b}}=8.5$ | $\mathrm{Pb}=7.5$ | $\mathrm{Pb}=8.0$ | $\mathrm{Pb}=8.5$ |
| $\mathrm{a}_{1}$ | $-1.26419 \times 10^{9}$ | $-4.04562 \times 10^{7}$ | $-1.87453 \times 10^{7}$ | $1.47014 \times 10^{7}$ | $-1.09362 \times 10^{9}$ | $-2.69217 \times 10^{8}$ | $-5.9184 \times 10^{7}$ |
| $\mathrm{a}_{2}$ | $-2.65297 \times 10^{9}$ | $-7.14283 \times 10^{7}$ | $-4.28111 \times 10^{7}$ | $2.43789 \times 10^{7}$ | $-2.27615 \times 10^{9}$ | $-5.43147 \times 10^{8}$ | $-9.36276 \times 10^{7}$ |
| $a_{3}$ | $-1.48345 \times 10^{9}$ | $-3.49524 \times 10^{7}$ | $-2.5911 \times 10^{7}$ | $9.51481 \times 10^{6}$ | $-1.25155 \times 10^{9}$ | $-2.97161 \times 10^{8}$ | $-3.82568 \times 10^{7}$ |
| $\mathrm{b}_{1}$ | -5351.70 | 927.875 | 1486.87 | 2741.46 | -7830.19 | -2365.41 | 500.746 |
| $\mathrm{b}_{2}$ | 9143.01 | 849.674 | -22.1120 | -63.8613 | 10640.30 | 4188.56 | 1084.54 |
| $\mathrm{b}_{3}$ | -3704.48 | -1601.12 | -961.019 | -494.999 | -6544.86 | -1976.02 | -1315.98 |
| $\delta_{1}$ | 19 | 3 | 3 | 3 | 20 | 16 | 9 |
| $\delta_{2}$ | 0.4 | 1.8 | 0.8 | 0.8 | 0.8 | 1.2 | 2.5 |

${ }^{\text {a }} \delta_{1}$ : average absolute deviation $=\left\{\sum_{i=1}^{\mathrm{N}}\left|\left(\mathrm{H}_{\text {cal }}^{\mathrm{E}}-\mathrm{H}_{\text {exp }}^{\mathrm{E}}\right)_{i}\right|\right\} / \mathrm{N}\left(J \cdot \mathrm{~mol}^{-1}\right)$, where N is the number of data points. $\delta_{2}$ : average relative deviation $=\left\{\sum_{i=1}^{N}\left|\left(H_{\text {cal }}^{\mathrm{E}}-\mathrm{H}_{\text {exp }}^{\mathrm{E}}\right) / \mathrm{H}_{\text {(exp)max }}^{\mathrm{E}}\right| \times 100 \%\right\} / \mathrm{N}(\%)$, where N is the number of data points. ${ }^{\mathrm{b}}$ Units $=\mathrm{MPa}$.


Figure 5. Plot of $C_{P}-T-P$ for carbon dioxide near the critical point ( $\mathrm{P}_{\mathrm{c}}=7.38 \mathrm{MPa}, \mathrm{T}_{\mathrm{c}}=304.2 \mathrm{~K}$ ). $\mathrm{C}_{\mathrm{p}}$ becomes infinite at the critical point A.
where $H^{E}$ is the excess molar enthalpy, $C_{p}^{E}$ is the excess molar heat capacity at constant pressure, $\mathrm{C}_{\mathrm{p}}$ is the molar heat capacity at constant pressure of the mixture, $C_{p, i}$ is the molar heat capacity at constant pressure of pure component $i$, and $x_{i}$ is the molar fraction of component i .

In eq 1, it is usually not so easy to find the data of $C_{p}$ in the literature. Thus, for the behavior of $\mathrm{H}^{\mathrm{E}}$ as shown in Figures 1 to 4, we estimated that the excess molar enthal pies of the mixture would be affected by the strong pressure dependency of the heat capacity at constant pressure ( $C_{p}, C_{P, 1}$, and $C_{P, 2}$ ). We obtained the largest value of excess molar enthalpy at the conditions 308.15 K and 75 bar, which are closest to the critical point of carbon dioxide. When the temperature was reduced to 303.15 K , the maximum value of the excess molar enthalpy was obtained at 70 bar.


Figure 6. Vapor pressure curve for carbon dioxide extrapolated beyond the critical point. Circles indicate the temperature and pressure corresponding to the maximum values of $C_{p}$ as determined from Figure 5.

## Correlation

In this work, the experimental results of excess molar enthal pies $\mathrm{H}^{\mathrm{E}}$ were correlated by a composition-dependent equation composed of two polynomial expressions (Gruszkiewic et al., 1993):

$$
\begin{align*}
H^{E}\left(J \cdot \mathrm{~mol}^{-1}\right)=x(1-x)\{S & \sum_{i=0}^{N-1} a_{i}(1-2 x)^{i}+ \\
& \left.(1-S) \sum_{i=0}^{N-1} b_{i}(1-2 x)^{i}\right\} \tag{2}
\end{align*}
$$

where $a_{i}$ and $b_{i}$ are adjustable parameters, $x$ is the mole fraction of carbon dioxide, and N is the number of adjust-
able parameters $\mathrm{a}_{\mathrm{i}}, \mathrm{b}_{\mathrm{i}}$. In this work, N was set to $3 . \mathrm{S}$ is a switching function used to change from a polynomial fit at low molefraction to a different polynomial fit at high mole fraction (Gruszkiewicz et al., 1993). To control the value of $S$ to vary from 0 to $1, S$ is given as

$$
\begin{equation*}
S=0.5\left[\left(\frac{e^{y}-e^{-y}}{e^{y}+e^{-y}}\right)+1\right] \tag{3}
\end{equation*}
$$

where $y=10(x-1.3)$. The correlation results of the adjustable parameters $a_{i}, b_{i}$ for the mixtures are shown in Table 4, and the plots of calculated results are shown in Figures 1 to 4.

An algorithm suggested by Marquardt (Marquardt, 1963), based on an earlier suggestion of Levenberg (Levenberg, 1944), had been used in the data reduction. A suitable objective function to be minimized is

$$
\begin{equation*}
\mathrm{OF}=\sum_{\mathrm{i}=1}^{\mathrm{n}}\left[\frac{\left(\mathrm{H}_{\text {cal }}^{\mathrm{E}}-\mathrm{H}_{\text {exp }}^{\mathrm{E}}\right)_{\mathrm{i}}}{\sigma}\right]^{2} \tag{4}
\end{equation*}
$$

where

$$
\begin{equation*}
\sigma=\sqrt{\frac{\sum_{\mathrm{i}=1}^{\mathrm{n}}\left(\mathrm{H}_{\mathrm{cal}}^{\mathrm{E}}-\mathrm{H}_{\mathrm{exp}}^{\mathrm{E}}\right)_{\mathrm{i}}^{2}}{\mathrm{n}}} \tag{5}
\end{equation*}
$$

n is the point number of experimental data, and $\sigma$ is the standard deviation.

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