Densities of Water + **Diethanolamine** + **Methanol and Water** + *^N***-Methyldiethanolamine** + **Methanol at Temperatures Ranging from (283.15 to 353.15) K**

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Two vibrating tube densimeters have been used to measure the densities of two mixtures—water $+$ diethanolamine + methanol and water $+ N$ -methyldiethanolamine $+$ methanol-in the temperature range (283 to 353) K. The alkanolamines and methanol contents are respectively (between 20 and 50 and between 20 and 60) mass %. The experimental results have been correlated using the Redlich-Kister equation for the excess volume. A set of parameters for the Redlich-Kister equation has been determined using the densities of pure compounds and of binary systems available in the literature. The methodology has been extended to density calculations dealing with hybrid solvents.

Introduction

Aqueous alkanolamine solutions are of great interest as chemical solvents used in natural gas sweetening processes. A wide variety of alkanolamines such as monoethanolamine (MEA), diethanolamine (DEA), diisopropanolamine (DIPA), or methyldiethanolamine (MDEA) have been used industrially for a number of years.¹ MDEA and DEA are widely used in gas treatment because of their chemical properties. MDEA is generally used for selective removal of H_2S in the presence of CO_2 , while DEA is a common solvent for total deacidification. These aqueous alkanolamine solutions have however generally quite low efficiencies when used for the removal of other sulfur species, especially mercaptans.

Moreover, when the acid gas impurities represent an appreciable fraction of the total gas stream, the cost for removing them by heat regenerable solvent absorption may be out of proportion to the value of the treated gas. This consideration has provided the major impetus for the development of processes employing nonreactive organic solvents as a treating agent. These materials dissolve physically the acid gases and are partially regenerated by merely reducing the pressure. Moreover, minor gas impurities such as carbonyl sulfide and mercaptans are quite soluble in most organic solvents and can be removed to a large extent together with the acid gases by a physical solvent.2

In contrast to the solvents mentioned previously, mixtures of chemical and physical solvents, often referred to as "mixed" or "hybrid" solvents, have been developed.3-⁶ The absorption process resembles a conventional alkanolamine treating unit, but the presence of the physical solvent enhances the solution capacity, especially when the gas stream to be treated is at high pressure with large quantities of acid compounds and/or minor gas impurities such as carbonyl sulfide and mercaptans present.

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As the gas reserves that natural gas field exploration and production have now to deal with are increasingly sour, Rojey et al.⁷ have proposed a new sour gas treatment technology integrating dehydration, natural gas liquids (NGL) extraction, and acid gas removal steps with a single hybrid solvent (a mixture of methanol, water, and amine). This patented process produces sweet dry pipeline gas, sweet NGL, and dry pressurized acid gases. The process will be applicable to most sour to very sour, hydrocarbonrich natural or associated gases.

This process is composed of two parts: a dew point section (used for dehydration and NGL extraction) and a sweetening section (used for acid gas removal). The solvent used in the sweetening section is a mixture of methanol, water, and an alkanolamine such as diethanolamine (DEA), which combines some of the advantages of physical solvent processes (high acid gas loadings, important affinity for COS and mercaptans) with those of chemical solvent processes (stringent specifications on H_2S and CO_2 in the treated gas easily achieved).

The physicochemical data of solvents required for the design of acid gas treatment equipment are generally solubility data, kinetic data, and additional data such as density, viscosity, and so forth. In the context of the development of this new process, particular attention was accorded here to the solvent density. In this work, densities of two different solvents, water + DEA + methanol and water $+$ MDEA $+$ methanol, were measured with two vibrating tube densimeters in the temperature range (283 to 353) K, for various compositions ranging from (20 to 50) wt % alkanolamine and from (20 to 60) mass % methanol. A simplified form of the Redlich-Kister equation was applied to represent excess molar volumes.

Experimental Section

Apparatus and Procedure. Numerous experimental data for alkanolamine aqueous mixtures densities have been reported in the literature.⁸⁻¹⁴ Most of these previous works have used atmospheric apparatus, pycnometers, or vibrating tube densimeters.

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Figure 1. Experimental apparatus: 1, DMA45 densimeter; 2, DMA512 remote cell; 3, measuring cell; 4, solvent reserve; 5, stop valve; 6, thermostated bath.

In this work, two apparatuses in two different laboratories have been used to measure liquid densities. Both are vibrating tube densimeter type. The first one allows density measurement under pressure by using a special remote cell; the second one was a standard atmospheric apparatus similar to those described in the open literature. The consistency of the different experimental results was checked against any systematic error.

The first apparatus, manufactured by Anton Paar, is a vibrating tube densimeter type DMA512, which is a special remote cell for density measurement under pressure. The sample tube, made of stainless steel, was housed in a thermostated brass jacket. The measuring cell temperature was regulated to within 0.05 K with a HAAKE K15/DC30 liquid bath. The cell temperature was measured with a platinum probe calibrated within 0.01 K against a 25-Ω platinum probe type 1/622C manufactured by Rosemount. This remote cell was connected to an Anton Paar DMA45 densimeter used as a processing unit. Densities ρ were calculated from the period of vibration *τ*:

$$
\rho = A + Bt^2 \tag{1}
$$

The constants *A* and *B* were determined as a function of temperature by calibrating the apparatus with reference fluids of known densities, taking into account the conclusions of Bouchot and Richon.15 The DMA45 + DMA512 set was calibrated within 0.001 g \cdot cm⁻³ with pure water and pure alcohol with the same process in the temperature range (293 to 353) K.

The following procedure was applied to apparatus calibration and density measurements. The liquid sample from the solvent supply was introduced into the vibrating tube of the DMA512 densimeter (Figure 1). All the tubing was filled with the liquid. The stop valve was closed. The liquid sample was then pressurized to 0.7 MPa with nitrogen. This procedure was used to prevent the appearance of gas bubbles in the measuring cell, which occurs at high temperatures. The gas-solvent interface was located in the solvent reserve, and the tubing length avoids the introduction of N_2 into the measuring cell by diffusion through the solvent during the time of the experiment.

For each sample, the vibration period was then measured at temperatures ranging from (303 to 353) K by successive temperature increments. This operation was performed with increasing and decreasing temperatures to prove that no hysteresis effects need to be considered with temperature changes. Densities are then calculated, and each

Table 1. Experimental Conditions for Density Measurements

solvent	77K	W ₂	W_3	experimental method			
Water (1) + DEA (2) + Methanol (3)							
solvent 1	$293 - 353$	0.200	0.200	$DMA45 + DMA512$			
solvent 2	$293 - 353$	0.200	0.400	$DMA45 + DMA512$			
solvent 3	$293 - 353$	0.300	0.200	$DMA45 + DMA512$			
solvent 4	$293 - 353$	0.300	0.300	$DMA45 + DMA512$			
solvent 5	$293 - 353$	0.300	0.500	$DMA45 + DMA512$			
solvent 6	$293 - 353$	0.300	0.600	$DMA45 + DMA512$			
solvent 7	$293 - 353$	0.400	0.400	$DMA45 + DMA512$			
solvent 8	$278 - 353$	0.301	0.199	DMA5000			
solvent 9	$278 - 353$	0.400	0.200	DMA5000			
solvent 10	$278 - 353$	0.401	0.397	DMA5000			
	Water (1) + MDEA (2) + Methanol (3)						
solvent 11	$293 - 353$	0.200	0.200	$DMA45 + DMA512$			
solvent 12	$293 - 353$	0.200	0.400	$DMA45 + DMA512$			
solvent 13	$293 - 353$	0.300	0.300	$DMA45 + DMA512$			
solvent 14	$293 - 353$	0.300	0.500	$DMA45 + DMA512$			
solvent 15	$293 - 353$	0.400	0.200	$DMA45 + DMA512$			
solvent 16	$293 - 353$	0.400	0.400	$DMA45 + DMA512$			
solvent 17	$283 - 353$	0.200	0.401	DMA5000			
solvent 18	$283 - 353$	0.302	0.396	DMA5000			
solvent 19	$283 - 353$	0.303	0.495	DMA5000			
solvent 20	$283 - 353$	0.398	0.301	DMA5000			
solvent 21	$283 - 353$	0.400	0.398	DMA5000			
solvent 22	$283 - 353$	0.399	0.495	DMA5000			
solvent 23	$283 - 353$	0.496	0.300	DMA5000			
solvent 24	$283 - 353$	0.498	0.397	DMA5000			
solvent 25	$283 - 353$	0.399	0.301	DMA5000			

reported value is the average of at least three measurements within an uncertainty of ± 0.001 g.cm⁻³.

The second apparatus used in this study is an Anton-Paar digital vibrating glass tube densimeter (model DMA5000), with a precision of 10^{-5} g \cdot cm⁻³. The temperature was determined with a platinum resistance thermometer with an accuracy of 0.001 K. The DMA5000 was calibrated with bidistilled and degassed water, and air. Uncertainty has been estimated to within ± 0.0002 g \cdot cm⁻³.

The sample density was measured at thermal equilibrium after changing the temperature from (283 to 353) K following successive increments. This operation is performed twice for each solution. Then each reported density is the average of two measurements.

Solutions Preparation. Mixed solvents were prepared from water, methanol, and DEA/MDEA. Water was distilled and degassed under a vacuum. Methanol (99.8 mass % purity) from Merck was also degassed under a vacuum. DEA (99 mass % purity) was purchased from Aldrich, and MDEA (98 mass % purity) was purchased from Fluka. All chemicals were used without any further purification.

The solutions were prepared gravimetrically at ambient temperature in initially evacuated 20 cm3 glass bottles (the resulting pressure is the vapor pressure of the mixed

343.05 0.911 313.15 0.9884 352.95 0.902 318.15 0.9851 3 293.15 1.001 323.15 0.9818 298.15 0.998 328.14 0.9783 303.15 0.995 333.15 0.9748 308.15 0.992 338.14 0.9712 313.15 0.988 343.15 0.9674 323.05 0.981 348.15 0.9636 333.05 0.973 353.15 0.9597 343.05 0.966 358.14 0.9557 352.95 0.958 9 278.15 1.0162 4 293.15 0.980 293.15 1.0101 298.15 0.977 303.15 1.0037 303.15 0.974 308.15 1.0004 308.15 0.971 323.15 0.9901

> 323.05 0.958 333.15 0.9829 333.05 0.950 338.15 0.9792 343.05 0.942 343.15 0.9754 352.95 0.934 348.15 0.9715

> 298.15 0.928 10 278.15 0.9736 303.15 0.924 283.15 0.9700 308.15 0.920 288.18 0.9664 313.15 0.916 293.15 0.9628

333.05 0.898 303.15 0.9554 343.05 0.892 308.15 0.9517
352.95 0.883 313.15 0.9479 352.95 0.883 313.15 0.9479 $\begin{array}{cccccc} 6 & & 293.15 & & 0.903 & & 323.15 & & 0.9401 \\ & & 298.15 & & 0.900 & & & 338.15 & & 0.9281 \end{array}$ 298.15 0.900 338.15 0.9281 303.15 0.895 343.15 0.9239 308.15 0.892 353.15 0.9155

323.05 0.907 298.15
333.05 0.898 303.15

328.15

Table 3. Density of (Water + **MDEA** + **Methanol) Solvents**

^a See Table 1 for solvent composition.

+ DMA512 and DMA5000) used in this study. As shown in Figure 2 the densities obtained through the two sets of equipment are in good agreement. Some differences appear at the higher temperatures. However, they generally remain within the uncertainties of the experimental methods. Moreover, they can be explained by the slight differences in the solvent compositions and by the different operating pressures, 0.7 MPa for the DMA45 + DMA512 and atmospheric pressure for the DMA5000.

Discussion

The density of water $+$ alkanolamine $+$ methanol systems was represented with a similar approach to those previously used by Rinker et al.¹³ and Hsu and Li¹⁶ for

^a See Table 1 for solvent composition.

 $\begin{array}{ccc} 313.15 & \quad \ \ \, 0.887 \\ 323.05 & \quad \ \ \, 0.879 \end{array}$ 323.05 0.879 $\begin{array}{ccc} 333.05 & \quad 0.869 \\ 343.05 & \quad 0.861 \end{array}$ 343.05 0.861
352.95 0.851 352.95

 $\frac{5}{298.15}$ $\frac{0.931}{0.928}$ 10

solvent) using a Mettler AT 200 balance with an accuracy of 10^{-4} g.

The procedure was the following: (1) the bottles were first evacuated with a vacuum pump; (2) the empty bottles were weighed; (3) degassed DEA or MDEA was introduced in the bottles by means of a syringe; (4) the bottles loaded with DEA or MDEA were weighed; (5) degassed water and degassed methanol were added successively, and the bottles were weighed after each addition. Finally, the composition of the solution was determined from the different masses. The solution was then transferred into the solvent reserve for DMA45 + DMA512 equipment (measurement under pressure) or directly introduced into the DMA5000 densimeter cell (measurement under atmospheric pressure). The compositions for each solvent, and the corresponding density measurement method, are reported in Table 1.

Results. The densities of the different solvents, water + DEA + methanol and water + MDEA + methanol, are reported in Tables 2 and 3, respectively, at several compositions and for temperatures ranging from (283 to 353) K.

We have compared for the similar solvent compositions the densities obtained with both sets of equipment (DMA45

Figure 2. Comparison of the two experimental techniques: \blacklozenge , $(50-30-20)$ mass % H₂O + DEA + MeOH; \Diamond , (50-30-20) mass % H₂O + DEA + MeOH; \bullet , (20-40-40) mass % H₂O + DEA + MeOH; O, $(20-40-40)$ mass % H₂O + DEA + MeOH.

Table 4. Density of Pure DEA and Pure MDEA

ref	77K	no. of points	deviation ^{<i>a</i>} (%)		
DEA					
20	$293.15 - 353.15$	4	0.11		
21	$298.15 - 333.15$	8	0.03		
22	$298.15 - 393.15$	6	0.09		
23	$293.15 - 361.15$	$\overline{5}$	0.09		
13	$298.15 - 363.15$	5	0.24		
$18*$	$283.15 - 363.15$	18	0.04		
$14*$	$183.15 - 373.15$	10	0.03		
$8*$	$298.15 - 353.15$	7	0.03		
MDEA					
22	$296.15 - 398.15$	5	0.12		
24	$303.15 - 353.15$	8	0.08		
23	$293.15 - 361.15$	5	0.06		
13	$298.15 - 366.15$	6	0.31		
$18*$	$283.15 - 363.15$	17	0.06		
$14*$	$293.15 - 393.15$	9	0.27		
$8*$	$298.15 - 353.15$	7	0.05		

a Deviation $U = (100/n) \Sigma((U_{exp} - U_{cal})/U_{exp})$.

water $+$ alkanolamines binary and ternary systems:

$$
\rho = \frac{M_{\rm m}}{V_{\rm m}} = \frac{\sum x_i M_i}{V_{\rm m}}\tag{2}
$$

where M_m was the molar mass of the mixture, M_i was the molar mass of the pure compound i , and x_i was the mole fraction of component *i*. The molar volume of the liquid mixture V_m was calculated from eq 3:

$$
V_{\rm m} = \sum x_i V_i + V^E \tag{3}
$$

where V^E is the excess volume and V_i is the molar volume of component *i*.

A Redlich-Kister type equation was applied for the excess molar volume:

$$
V_{12}^{E}/\text{cm}^{3}\cdot\text{mol}^{-1} = x_{1}x_{2}(A_{0} + A_{1}T/(\text{K}) + A_{2}x_{1})
$$
 (4)

T is the temperature and A_0 , A_1 , and A_2 are binary parameters; cf. Table 6. The excess volume *V*^E of the liquid mixture for a ternary system was obtained from the excess molar volume of each binary system:

$$
V^{E} = V_{12}^{E} + V_{13}^{E} + V_{23}^{E}
$$
 (5)

The method was based on the molar volumes of each pure compound, as well as on the representation of the two water $+$ alkanolamine and water $+$ methanol binary

Table 5. Density of Binary Systems

H_2O-DEA					
		DEA	no. of	deviation ^a	
ref	T/K	mass %	points	(%)	
20	$293.15 - 353.15$	$20 - 100$	20	0.60	
25	$293.15 - 303.15$	$0 - 100$	33	0.07	
26	298.15	$0 - 30$	10	0.15	
$8*$	$298.15 - 353.15$	$0 - 100$	119	0.05	
12	298.15	$10 - 40$	4	0.06	
16	$313.15 - 353.15$	$20 - 30$	12	0.06	
13	$293.15 - 373.15$	$10 - 100$	22	0.11	
$14*$	$283.15 - 363.15$	$0 - 100$	171	0.04	
$H_2O-MDEA$					
		MDEA	no. of	deviation ^a	
ref	T/K	mass %	points	(%)	
27	$288.15 - 308.15$	$10 - 20$	12	0.78	
28	$288.15 - 333.15$	$0 - 50$	53	0.05	
24	$303.15 - 353.15$	30	8	0.06	
9	$303.15 - 333.15$	$20 - 30$	8	0.06	
$8*$	$298.15 - 353.15$	$0 - 100$	126	0.10	
29	$303.15 - 323.15$	$30 - 40$	5	0.05	
11	$283.15 - 353.15$	50	5	0.06	
12	298.15	$30 - 60$	4	0.24	
13	$333.15 - 373.15$	$10 - 100$	18	0.16	
$14*$	$283.15 - 373.15$	$0 - 100$	135	0.17	
H ₂ O-Methanol					
		methanol	no. of	deviation ^a	
ref	T/K	mass %	points	(%)	
open lit.	$273.15 - 353.15$	$0 - 100$	>700	0.19	

a Deviation $U = (100/n) \Sigma ((U_{exp} - U_{cal})/U_{exp})$.

Table 6. Binary Parameters of the Redlich-**Kister Equation**

binary pairs		A_0 /cm ³ ·mol ⁻¹ A_1 /cm ³ ·mol ⁻¹ ·K ⁻¹ A_2 /cm ³ ·mol ⁻¹	
$DEA + H2O$	-5.39820	6.321 9 \times 10 ⁻³	1.942 42
$MDEA + H2O$	-10.4622	0.011 22	4.079 36
$DEA + MeOH$	2.551 49	-1.94842×10^{-2}	0.521 99
$MDEA + MeOH$	4.989 25	-0.01138	-30.15951
$H_2O-MeOH$	-0.43707	-0.01066	-0.32874
DEA-MDEA	-11.15259	0.034 82	Ω

systems. The binary parameters for these two systems were determined from experimental data. The representation of the ternary systems was then realized by fitting the $parameters$ alkanolamine $+$ methanol from the experimental data obtained for the ternary systems. Therefore, the developed model will not allow representing the density of the binary systems alkanolamine + methanol.

Representation of Molar Volumes of Pure Compounds. The molar volumes of water and methanol were obtained from the correlations of Rinker et al.13 and DIPPR:17

$$
V_{\text{methanol}}/\text{cm}^3 \cdot \text{mol}^{-1} = 1000 \times \frac{0.27073^{(1+(1-[T(\text{K})]/512.5)^{0.24713})}}{2.3267}
$$
 (6)

$$
V_{\text{H}_2\text{O}}/\text{cm}^3 \cdot \text{mol}^{-1} = \frac{18.02}{0.753597 + (1.877465 \times 10^{-3})T}
$$
 (7)
(K) - (3.563982 × 10⁻⁶) T²/(K²)

For DEA and MDEA, we have selected the literature data which appear to be the most consistent with the temperature and composition ranges studied and according to the consistency of these data between each other. $8,14,18$ These data are identified with an asterisk in Table 4. They have been obtained by means of a vibrating glass tube

Table 7. Density of Ternary Systems

a Deviation $U = (100/n) \Sigma((U_{exp} - U_{cal})/U_{exp})$.

densimeter, and they present experimental uncertainties lower than 0.001 g \cdot cm⁻³ and a good consistency between the various sources. The following correlations were obtained from these data:

$$
V_{\text{DEA}}/\text{cm}^3 \cdot \text{mol}^{-1} = \frac{105.16}{1.2968 - (6.8008 \times 10^{-4}) T / (\text{K})} \tag{8}
$$

$$
V_{\text{MDEA}}/\text{cm}^3 \cdot \text{mol}^{-1} = \frac{119.16}{1.27462 - (7.9703 \times 10^{-4}) T / (\text{K})} \tag{9}
$$

Table 4 shows the deviation between these correlations and the literature data and contains the regressed data sources.

Representation of Water + **Alkanolamine and Water** + **Methanol Binary Systems.** The binary parameters for DEA + water and MDEA + water, were determined from literature data. As for the pure components, consistent data (displayed with an asterisk in Table 5) were selected in the open literature for the determination of the correlation parameters. The representation of the consistent data was achieved within an average absolute percentage deviation of 0.04% and 0.14%, respectively, for the water $+$ DEA and water $+$ MDEA systems.

More than 800 experimental data points are available in the open literature for the water $+$ methanol system, over a large range of temperatures (163 to 353 K) and compositions. All of them are collected in the Dortmund Data Bank.19 We have retained the more consistent data for the identification of the water $+$ methanol binary parameters, in the temperature range (273.15 to 353.15) K (Table 5). All the determined binary parameters are reported in Table 6.

Representation of Water + *Alkanolamine* + *Methanol Ternary Systems.* As mentioned above, the representation of the ternary system was obtained by fitting the alkanolamine + methanol binary parameters from density data of ternary systems. This approach ensured a good representation of the water $+$ alkanolamine $+$ methanol system, within (0.07 and 0.16)% deviation for water + DEA + methanol and water + MDEA + methanol ternary systems, respectively, as shown in Table 7 and Figures 3 and 4.

Conclusion

The densities of the solvent systems (water + DEA + methanol) and (water + MDEA + methanol) have been measured using two apparatuses, the first one for density measurement under pressure and the second one for density measurement under atmospheric pressure. Measurements were performed for temperatures ranging from (283 to 353) K and for several compositions. We obtained good reproducibility, and at temperatures below 353 K, we have observed an excellent agreement between the two

Figure 3. Density of the water $+$ DEA $+$ methanol system: \Box , $(10-30-60)$ mass % H₂O + DEA + MeOH; small box, $(40-20-$ 40) mass % $H_2O + DEA + MeOH$; \triangle , (20-30-50) mass % $H_2O +$ DEA + MeOH; $*$, (40-30-30) mass % H₂O + DEA + MeOH; \triangle , (20−40−40) mass % H₂O + DEA + MeOH; ♦, (50-30-20) mass % H₂O + DEA + MeOH; \Diamond , (40-20-20) mass % H₂O + DEA + MeOH; +, $(60-20-20)$ mass % H₂O + DEA + MeOH; -, calculated values.

Figure 4. Density of the water $+$ DEA $+$ methanol system: \blacksquare , $(20-30-50)$ mass % H₂O + DEA + MeOH; \Diamond , (20-40-40) mass % H₂O + DEA + MeOH; \times , (40-30-30) mass % H₂O + DEA + MeOH; \bullet , (40-40-20) mass % H₂O + DEA + MeOH; \triangle , (60-20-20) mass % $H_2O + DEA + MeOH$; -, calculated values.

methods within their estimated uncertainties. The densities of liquid mixtures have been correlated using a Redlich-Kister equation for the excess volume. On the basis of the densities of pure compounds and of binary systems available in the literature, a set of parameters in the Redlich-Kister equation was determined. The methodology has been extended to the density calculations for the hybrid solvents. Satisfactory results were obtained for the (water $+$ DEA $+$ methanol) and (water $+$ MDEA $+$ methanol) solvents, within an overall average absolute percentage deviation of 0.12%.

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