

# Temperature and Density Dependence of the Viscosity of Cyclopentane

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New measurements have been made for the viscosity of cyclopentane between 258 K and 298 K at pressures up to approximately 380 MPa with a self-centering falling-body viscometer. These extend earlier high-pressure measurements made below 25 MPa by Assael and Dalaouti. A correlation function is used to represent the results as a function of temperature and molar volume with a standard deviation of  $\pm 0.3\%$ . The uncertainty in the measurements is estimated at  $\pm 1\%$ .

## Introduction

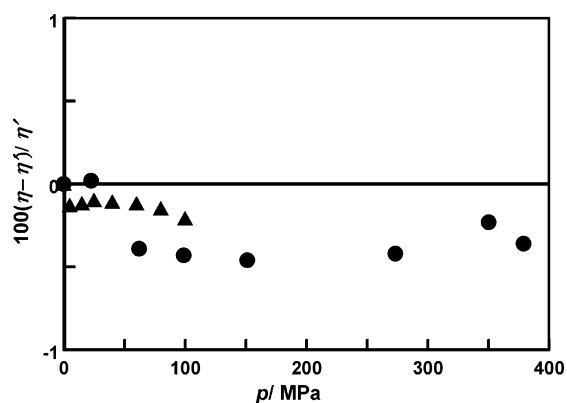
New measurements have been made for the viscosity of cyclopentane between 258 K and 298 K at pressures up to approximately 380 MPa using a self-centering falling-body viscometer. The work forms part of a project of the International Association for Transport Properties (<http://transp.eng.auth.gr/iatp.html>) to provide high-quality viscosity data for substances that are liquid over broad ranges of temperature and pressure that can be used as reference fluids, particularly where it might not be possible to use water. To this end, measurements have been made for toluene with several different types of viscometer and a correlation was derived from them.<sup>1</sup> The cyclopentane viscosity data presented here complement recent high-pressure vibrating wire measurements made to 25 MPa by Assael and Dalaouti<sup>2</sup> and will be used similarly.

## Experimental Section

The cyclopentane was Aldrich 99+% dried over sodium wire. Analysis by GCMS (using a Shimadzu GC17A gas chromatograph fitted with a J.W. Scientific DB5-MS 30 m  $\times$  0.25 mm column and employing a Shimadzu QP5000 mass spectroscopic detector) detected an impurity, 2,2-dimethylbutane. By using the method of standard additions, doping cyclopentane with 2,2-dimethylbutane (Chemical Samples Co., 99%), the purity was estimated at 99.89%.

Densities at atmospheric pressure were obtained using an Anton-Paar model DMNA5000 vibrating tube densimeter calibrated with dry air (BOC Gases, Instrument grade,  $\leq 25$  ppm water) and purified water (MilliQ ion exchange system, Waters-Millipore Ltd.). The density of the cyclopentane sample at 25 °C was 0.739 92<sub>2</sub> g/cm<sup>3</sup>. The reproducibility is  $\pm 10$   $\mu$ g/cm<sup>3</sup>. From the density of 2,2-dimethylbutane,<sup>3</sup> 0.657 02 g/cm<sup>3</sup>, and that recommended for cyclopentane,<sup>4</sup> 0.740 39<sub>8</sub> g/cm<sup>3</sup>, one obtains a purity of 99.95 mol %. The molar mass was taken as 70.1329 g/mol.

Viscosities ( $\eta$ ) at atmospheric pressure were determined with a reproducibility of  $\pm 0.2\%$  in a glass Ubbelohde viscometer mounted in a water thermostat controlled to  $\pm 1$  mK. This viscometer was calibrated at 25 °C using a



**Figure 1.** Relative deviations of the viscosity of water at 25 °C ( $\eta$ ) reported by Harlow (ref 18) (●, uncertainty of 1.4%) and those recommended in the 1985 IAPS tables (ref 19) (▲, standard uncertainty of 1%) from the results of this work,  $\eta'$ .  $\eta'/(mPa \cdot s) = 0.8909 - 2.263\ 027 \times 10^{-4}(p/MPa) + 2.683\ 453 \times 10^{-6}(p/MPa)^2 - 4.055\ 610 \times 10^{-9}(p/MPa)^3 + 3.168\ 239 \times 10^{-12}(p/MPa)^4$ .

**Table 1. Viscosity and Density of Cyclopentane at 0.1 MPa**

<i>TK</i>	$\rho/(g/cm^3)^a$	$\eta/(mPa \cdot s)^b$	<i>TK</i>	$\rho/(g/cm^3)^a$	$\eta/(mPa \cdot s)^b$
278.15	0.759 64	0.5230	293.15	0.744 90	0.4405
283.15	0.754 76	0.4932	298.15	0.739 92	0.4173
288.15	0.749 85	0.4657			

<sup>a</sup> Measured with vibrating tube densimeter. <sup>b</sup> Measured with Ubbelohde viscometer.

set of calibration standards from the Cannon Instrument Co. (State College, PA). The results were found to fit the working equation

$$\eta/\rho = At + B/t \quad (1)$$

(where  $\rho$  is the density and  $t$  is the flowtime) with the classical kinetic energy correction as the second term ( $A$  and  $B$  are fitted constants).<sup>5</sup> The alternative equation

$$\eta/\rho = At + B/t^2 \quad (2)$$

recommended by Bauer and Meurlender<sup>6</sup> for long capillary Ubbelohde viscometers was tested but resulted in a poor fit.

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Table 2. Viscosity of Cyclopentane from 258 K to 298 K

<i>T</i> /K	<i>t</i> /s	<i>p</i> /MPa	<i>V</i> /(cm <sup>3</sup> /mol)	$\rho$ /(g/cm <sup>3</sup> )	$\eta$ /(mPa·s)	<i>Re</i> <sup>a</sup>	<i>T</i> /K	<i>t</i> /s	<i>p</i> /MPa	<i>V</i> /(cm <sup>3</sup> /mol)	$\rho$ /(g/cm <sup>3</sup> )	$\eta$ /(mPa·s)	<i>Re</i> <sup>a</sup>
258.01	21.98	0.1	89.9819	0.77941	0.6851	514	268.01	69.92	200.7	80.9918	0.86593	2.1508	57
257.87	22.04	0.1	89.9667	0.77954	0.6871	511	268.01	79.13	225.6	80.2765	0.87364	2.4315	45
257.86	22.07	0.1	89.9660	0.77955	0.6878	510	268.01	89.32	250.8	79.6080	0.88098	2.7419	36
							268.01	100.19	275.3	79.0036	0.88772	3.0726	29
262.99	20.47	0.1	90.5254	0.77473	0.6384	588	268.01	112.52	301.0	78.4112	0.89443	3.4474	23
262.99	20.49	0.1	90.5254	0.77473	0.6388	587	268.01	125.22	325.3	77.8853	0.90046	3.8332	19
262.99	21.05	3.1	90.2605	0.77700	0.6562	558	268.01	140.04	351.2	77.3571	0.90661	4.2832	15
262.99	21.53	5.6	90.0449	0.77887	0.6709	535	268.01	155.96	378.0	76.8430	0.91268	4.7659	12
262.99	22.01	8.1	89.8316	0.78071	0.6858	513							
262.99	22.55	10.8	89.6055	0.78269	0.7025	490	273.15	17.94	0.1	91.6698	0.76506	0.5601	756
262.99	25.54	25.8	88.4602	0.79282	0.7943	388	273.15	17.97	0.1	91.6698	0.76506	0.5610	753
262.99	30.86	50.8	86.8352	0.80765	0.9576	271	273.15	18.44	3.1	91.3807	0.76748	0.5756	717
262.99	36.68	75.7	85.4712	0.82054	1.1362	195	273.15	18.87	5.6	91.1444	0.76947	0.5886	688
262.99	43.01	100.5	84.2987	0.83196	1.3301	144	273.15	19.31	8.1	90.9124	0.77143	0.6022	658
262.99	49.97	125.5	83.2532	0.84240	1.5429	108	273.15	19.74	10.6	90.6866	0.77335	0.6155	632
262.99	57.66	150.5	82.3200	0.85195	1.7779	82	273.15	22.42	25.9	89.4362	0.78417	0.6979	497
262.99	65.98	175.5	81.4794	0.86074	2.0319	64	273.15	27.10	50.8	87.7056	0.79964	0.8418	348
262.99	75.00	200.2	80.7196	0.86885	2.3071	50	273.15	32.17	75.8	86.2575	0.81306	0.9972	251
							273.15	37.69	100.7	85.0199	0.82490	1.1663	186
262.93	20.50	0.1	90.5187	0.77479	0.6392	587	273.15	43.66	125.5	83.9357	0.83556	1.3491	141
262.93	20.50	0.1	90.5187	0.77479	0.6393	587	273.15	50.25	150.5	82.9634	0.84535	1.5505	108
262.93	21.09	3.1	90.2531	0.77707	0.6574	556	273.15	57.39	175.5	82.0905	0.85434	1.7685	84
262.93	21.56	5.6	90.0384	0.77892	0.6719	534	273.15	65.19	200.5	81.2915	0.86273	2.0065	65
262.93	22.01	7.9	89.8388	0.78065	0.6858	513	273.15	73.72	225.3	80.5671	0.87049	2.2665	52
262.93	22.43	10.1	89.6612	0.78220	0.6987	495	273.15	83.08	250.6	79.8841	0.87793	2.5516	41
262.93	25.56	25.8	88.4548	0.79287	0.7950	387	273.15	93.35	275.8	79.2534	0.88492	2.8641	33
262.93	30.88	50.8	86.8336	0.80767	0.9583	271	273.15	104.31	300.7	78.6699	0.89148	3.1977	27
262.93	36.71	75.7	85.4697	0.82056	1.1371	195	273.15	116.23	325.9	78.1167	0.89780	3.5597	22
262.93	43.11	100.7	84.2840	0.83210	1.3330	144	273.15	128.97	350.7	77.6032	0.90374	3.9467	18
262.93	50.08	125.8	83.2390	0.84255	1.5462	108	273.15	145.21	379.2	77.0490	0.91024	4.4399	14
262.93	57.79	150.8	82.3083	0.85208	1.7819	82							
262.93	66.25	175.8	81.4667	0.86088	2.0402	63	278.16	16.93	0.1	92.2540	0.76022	0.5288	843
262.93	75.48	200.8	80.6987	0.86907	2.3219	49	278.16	16.94	0.1	92.2540	0.76022	0.5290	842
262.93	85.58	225.9	79.9926	0.87674	2.6295	39	278.16	17.39	2.9	91.9731	0.76254	0.5430	801
262.93	96.65	250.9	79.3391	0.88396	2.9667	31	278.16	17.74	5.0	91.7607	0.76430	0.5539	772
262.93	108.69	275.8	78.7342	0.89076	3.3330	24	278.16	18.26	8.1	91.4636	0.76679	0.5697	732
262.93	121.58	300.6	78.1713	0.89717	3.7251	20	278.16	18.71	10.8	91.2115	0.76890	0.5838	698
							278.16	21.25	25.9	89.9307	0.77986	0.6618	550
263.03	20.48	0.1	90.5294	0.77470	0.6386	588	278.16	25.68	50.8	88.1454	0.79565	0.7981	385
263.03	20.49	0.1	90.5294	0.77470	0.6390	587	278.16	30.49	75.8	86.6573	0.80931	0.9456	279
263.03	22.49	10.6	89.6245	0.78252	0.7005	493	278.16	35.69	100.6	85.3884	0.82134	1.1048	207
263.03	24.45	20.6	88.8455	0.78938	0.7608	421	278.16	41.40	125.7	84.2688	0.83225	1.2796	156
263.03	26.47	30.6	88.1297	0.79579	0.8231	362	278.16	47.59	150.7	83.2772	0.84216	1.4689	120
263.03	28.57	40.5	87.4720	0.80177	0.8873	314	278.16	54.33	175.8	82.3825	0.85131	1.6746	93
263.03	30.79	50.5	86.8589	0.80743	0.9555	272	278.16	61.56	200.7	81.5743	0.85974	1.8953	73
263.03	33.03	60.5	86.2841	0.81281	1.0243	238	278.16	69.48	225.8	80.8289	0.86767	2.1366	58
263.03	35.35	70.5	85.7422	0.81795	1.0955	210	278.16	77.96	250.8	80.1448	0.87508	2.3951	47
263.03	37.81	80.6	85.2285	0.82288	1.1709	184	278.16	87.30	275.9	79.5048	0.88212	2.6793	37
263.03	40.26	90.4	84.7592	0.82744	1.2457	164	278.16	97.57	300.8	78.9129	0.88874	2.9917	30
263.03	42.89	100.4	84.3055	0.83189	1.3265	145	278.16	108.47	325.9	78.3559	0.89506	3.3230	25
263.03	45.61	110.5	83.8685	0.83622	1.4097	129	278.16	120.33	350.9	77.8310	0.90109	3.6833	20
263.03	48.43	120.5	83.4563	0.84035	1.4959	115	278.16	135.51	380.1	77.2557	0.90780	4.1439	16
263.03	51.35	130.5	83.0623	0.84434	1.5851	103							
263.03	54.36	140.4	82.6893	0.84815	1.6770	92	287.93	15.06	0.1	93.4306	0.75064	0.4710	1050
263.03	57.52	150.4	82.3261	0.85189	1.7737	83	287.93	15.07	0.1	93.4306	0.75064	0.4712	1049
263.03	60.81	160.5	81.9783	0.85550	1.8742	74	287.93	15.50	3.0	93.1064	0.75326	0.4845	995
263.03	64.17	170.5	81.6450	0.85900	1.9766	67	287.93	15.86	5.4	92.8527	0.75531	0.4955	954
263.03	67.65	180.4	81.3261	0.86237	2.0830	61	287.93	16.28	8.1	92.5747	0.75758	0.5084	908
263.03	71.25	190.3	81.0194	0.86563	2.1927	55	287.93	16.70	10.8	92.3007	0.75983	0.5216	865
263.03	73.81	200.2	80.7226	0.86881	2.2705	51	287.93	19.00	25.9	90.9217	0.77135	0.5923	680
							287.93	23.00	50.9	89.0138	0.78789	0.7153	475
268.01	19.28	0.1	91.0842	0.76998	0.6016	659	287.93	27.28	75.8	87.4405	0.80206	0.8468	344
268.01	19.21	0.1	91.0842	0.76998	0.5994	663	287.93	31.91	100.8	86.1048	0.81451	0.9885	256
268.01	19.70	3.0	90.8136	0.77227	0.6145	633	287.93	36.95	125.7	84.9428	0.82565	1.1428	194
268.01	20.16	5.5	90.5844	0.77423	0.6285	606	287.93	42.36	150.6	83.9123	0.83579	1.3083	150
268.01	20.62	8.1	90.3601	0.77615	0.6428	581	287.93	48.24	175.7	82.9835	0.84514	1.4879	117
268.01	21.08	10.6	90.1467	0.77799	0.6569	557	287.93	54.57	200.6	82.1443	0.85378	1.6810	92
268.01	23.95	25.9	88.9372	0.78857	0.7450	439	287.93	61.53	225.7	81.3754	0.86184	1.8932	73
268.01	28.90	50.9	87.2588	0.80374	0.8969	308	287.93	69.00	250.7	80.6673	0.86941	2.1208	59
268.01	34.36	75.9	85.8512	0.81691	1.0645	222	287.93	76.89	275.7	80.0087	0.87657	2.3608	48
268.01	40.20	100.7	84.6459	0.82854	1.2433	164	287.93	85.50	300.8	79.3963	0.88333	2.6228	39
268.01	46.65	125.7	83.5802	0.83911	1.4405	124	287.93	94.66	325.5	78.8302	0.88967	2.9013	32
268.01	53.75	150.6	82.6330	0.84873	1.6574	95	287.93	104.38	349.5	78.3123	0.89555	3.1964	27
268.01	61.55	175.7	81.7727	0.85766	1.8956	73	287.93	116.44	376.9	77.7545	0.90198	3.5626	22

**Table 2 (Continued)**

<i>T</i> /K	<i>t</i> /s	<i>p</i> /MPa	<i>V</i> /(cm <sup>3</sup> /mol)	$\rho$ /(g/cm <sup>3</sup> )	$\eta$ /(mPa·s)	<i>Re</i> <sup>a</sup>	<i>T</i> /K	<i>t</i> /s	<i>p</i> /MPa	<i>V</i> /(cm <sup>3</sup> /mol)	$\rho$ /(g/cm <sup>3</sup> )	$\eta$ /(mPa·s)	<i>Re</i> <sup>a</sup>
298.03	13.38	0.1	94.7018	0.74057	0.4190	1311	298.00	13.39	0.1	94.6979	0.74060	0.4191	1310
298.03	13.38	0.1	94.7018	0.74057	0.4190	1310	298.00	13.40	0.1	94.6979	0.74060	0.4196	1307
298.03	13.38	0.1	94.7018	0.74057	0.4190	1310	298.00	13.77	3.0	94.3457	0.74336	0.4308	1244
298.03	14.10	5.5	94.0554	0.74566	0.4410	1190	298.00	14.08	5.3	94.0814	0.74545	0.4404	1193
298.03	14.40	7.8	93.8012	0.74768	0.4505	1143	298.00	14.47	8.1	93.7585	0.74802	0.4526	1133
298.03	14.83	10.8	93.4647	0.75037	0.4637	1083	298.00	14.86	10.9	93.4587	0.75042	0.4644	1079
298.03	16.91	25.9	91.9690	0.76257	0.5276	848	298.00	16.95	26.0	91.9617	0.76263	0.5288	844
298.03	20.50	50.9	89.9336	0.77983	0.6379	592	298.00	20.53	50.8	89.9316	0.77985	0.6390	590
298.03	24.30	75.8	88.2673	0.79455	0.7549	430	298.00	24.38	75.8	88.2654	0.79457	0.7572	427
298.03	28.41	100.8	86.8585	0.80744	0.8807	320	298.00	28.52	100.8	86.8585	0.80744	0.8842	318
298.03	32.83	125.8	85.6400	0.81893	1.0159	244	298.00	32.98	125.8	85.6376	0.81895	1.0207	241
298.03	37.64	150.7	84.5642	0.82935	1.1633	188	298.00	37.76	150.7	84.5638	0.82935	1.1669	187
298.03	42.84	175.7	83.6010	0.83890	1.3221	147	298.00	42.91	175.7	83.6012	0.83890	1.3241	147
298.03	48.39	200.7	82.7308	0.84772	1.4914	117	298.00	48.51	200.7	82.7292	0.84774	1.4951	116
298.03	54.34	225.6	81.9380	0.85593	1.6729	93	298.00	54.52	225.7	81.9336	0.85597	1.6784	93
298.03	60.85	250.6	81.2068	0.86363	1.8711	75	298.00	60.95	250.7	81.2031	0.86367	1.8743	75
298.03	67.74	275.6	80.5294	0.87090	2.0809	61	298.00	67.89	275.7	80.5248	0.87095	2.0854	61
298.03	75.12	300.4	79.9028	0.87773	2.3054	50	298.00	75.29	300.6	79.8953	0.87781	2.3106	50
298.03	83.01	325.3	79.3153	0.88423	2.5452	42	298.00	82.89	324.9	79.3222	0.88415	2.5415	42
298.03	91.38	350.1	78.7639	0.89042	2.7995	35	298.00	91.17	349.6	78.7730	0.89032	2.7929	35
298.03	101.68	378.0	78.1834	0.89703	3.1121	28	298.00	100.78	375.7	78.2277	0.89652	3.0845	29

<sup>a</sup> Reynolds number for annular flow:  $Re = 2r_1^2\rho v/(r_2 - r_1)\eta$  where  $v$  is the terminal velocity of the sinker and  $r_1$  and  $r_2$  are the radii of the sinker and tube, respectively (ref 9).

The effect of the impurity on the viscosity was checked by adding 0.5 and 1% 2,2-dimethylbutane by mass. There was no discernible effect within the experimental error of  $\pm 0.2\%$ : the composition dependence of the viscosity of the mixture is therefore very flat in this composition range.

The high-pressure viscometer and its operation and calibration have been described elsewhere.<sup>7,8</sup> It was also calibrated with the Cannon standards.<sup>8</sup> Platinum resistance thermometers newly recalibrated by the National Measurement Laboratory (CSIRO, West Lindfield, NSW) between  $(-65$  and  $100)$  °C on the ITS-90 to a tolerance of  $\pm 8$  mK were employed. The viscometer oil-bath temperature was controlled<sup>8</sup> to within  $\pm 0.01$  K between  $(-10$  and  $25)$  °C and to  $\pm 0.02$  K below  $-10$  °C. The primary pressure gauge (400 MPa Heise CM) was calibrated<sup>7</sup> against a deadweight tester to  $\pm 0.05\%$ , and pressures have an overall uncertainty of  $\pm 0.2$  MPa.

The working equation for the falling-body viscometer is<sup>7,9,10</sup>

$$\eta(p, T) = \frac{t(1 - \rho/\rho_s)}{A[1 + 2\alpha(T - T_{\text{ref}})][1 - 2\beta(p - p_{\text{ref}})/3]} \quad (3)$$

where  $t$  is the fall time at temperature  $T$  and pressure  $p$ ,  $\rho$  is the density of the fluid,  $\rho_s$  is that of the sinker,  $\alpha$  is the coefficient of thermal expansion ( $1.6 \times 10^{-5}$  K<sup>-1</sup>), and  $\beta$  is the bulk compressibility ( $2 \times 10^{-6}$  MPa<sup>-1</sup>) of the sinker and tube material, in this case 316 stainless steel.  $A$  is the calibration constant,  $28\,707$  Pa<sup>-1</sup> ( $\pm 0.17\%$ ), obtained at temperature  $T_{\text{ref}}$  and pressure  $p_{\text{ref}}$ , valid for  $Re < 1000$ .<sup>8</sup> The sinker density was corrected for changes in temperature and pressure from the calibration state point,  $T_{\text{ref}} \equiv 298.15$  K and  $p_{\text{ref}} \equiv 0.1$  MPa, using the relation<sup>11</sup>

$$\rho_s = \frac{\rho_s(T_{\text{ref}}, p_{\text{ref}})}{[1 + 3\alpha(T - T_{\text{ref}})][1 - \beta(p - p_{\text{ref}})]} \quad (4)$$

The overall uncertainty in the viscosity, based on replicate measurements and the sum of the uncertainty in the calibration ( $\pm 0.2\%$ ) and that in the fit to the function of temperature and density described below ( $\pm 0.25\%$ ), is estimated at  $\pm 1\%$ .

Calculation of the viscosity from fall times requires knowledge of the density of cyclopentane as a function of  $T$  and  $p$ . There are three sets of  $pVT$  data for cyclopentane in the literature: those of Brazier and Freeman<sup>12</sup> are confined to a single isotherm (303.15 K) but extend to 450 MPa, those of Kuss and Taslimi<sup>13</sup> lie in the  $pT$  region (39.2 MPa to 196.1 MPa, 298.15 K to 353.15 K), and those of Baonza et al.<sup>4</sup> lie in the region (0.1 MPa to 104.3 MPa, 192.79 K to 298.15 K). We have used two equations of state based on these data in this work, one given by Cibulka and co-workers,<sup>14</sup> recommended for the region (0.1 MPa to 196 MPa, 192.79 K to 353.15 K), and one based on the method of Malhotra and Woolf<sup>15,16</sup> for extrapolation of modified Tait equation parameters outside the range of experimental data. For the latter method, the Tait parameter  $C$  was taken to be 0.2220<sup>13</sup> and Tait parameters  $B(T)$  were obtained from the equation

$$B(T) = -p_c + b_1(1 - T_r) + b_2(1 - T_r)^2 \quad T_r = T/T_c \quad (5)$$

The critical pressure  $p_c$  and temperature  $T_c$  are the values recommended by Kudchadker et al.<sup>17</sup> (4.508 MPa, 511.65 K), and  $b_1$  and  $b_2$ , obtained from a least-squares fit of the  $B$  parameters of refs 12 and 13, are 68.2777 MPa and 286.3729 MPa, respectively.

Measurements were made of the viscosity of water at 298.15 K as a test of the instrument and technique. Figure 1 shows a comparison with the results of Harlow<sup>18</sup> (uncertainty given as  $\pm 1.4\%$ ) and the 1985 International Association for the Properties of Steam (IAPS) recommendations (standard uncertainty,  $\pm 1\%$ ).<sup>19</sup> The agreement is well within the limits of the combined uncertainties.

## Results and Discussion

The results are presented in Tables 1 and 2.

The viscosities were fitted as a function of temperature and molar volume to the empirical Pade approximation used for toluene,<sup>8</sup>

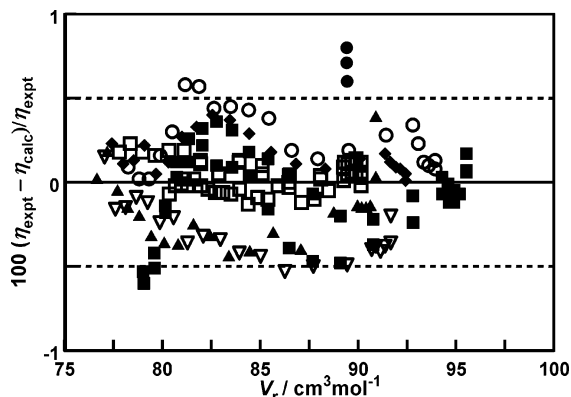
$$\sqrt{T\eta} = (\zeta_1 + \zeta_2 V_r + \zeta_3 V_r^2)/(1 + \zeta_4 V_r) \quad (6)$$

where the  $\eta$ - $V$  isotherms are mapped onto a single

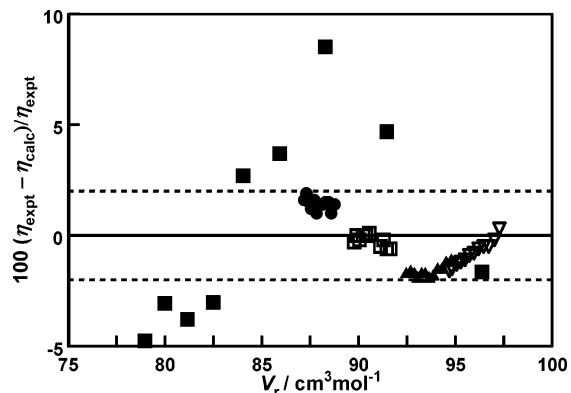
**Table 3. Coefficients of Best Fit: Equations 6 and 7**

$10^{-3}\zeta_1/(K^{0.5}/\text{mPa}\cdot\text{s})$	0.252 583 2
$10^{-1}\zeta_2/(K^{0.5} \text{ mol}/\text{mPa}\cdot\text{s}\cdot\text{cm}^3)$	-0.710 693 7
$10\zeta_3/(K^{0.5} \text{ mol}^2/\text{mPa}\cdot\text{s}\cdot\text{cm}^6)$	0.502 047 4
$10^2\zeta_4/(\text{mol}/\text{cm}^3)^2$	-0.238 253 2
$10\xi_1/(\text{cm}^3/\text{K}\cdot\text{mol})$	-0.347 809 1
$10^4 \xi_2/(\text{cm}^3/\text{K}^2\cdot\text{mol})$	0.474 140 0
standard uncertainty/mPa·s	0.004
standard percentage uncertainty	0.25
maximum percentage deviation	0.8

<sup>a</sup> Incorrect units were given in Table 3 of ref 8 for this parameter.



**Figure 2.** Residuals (experimental – calculated values) for the fit of the experimental high-pressure viscosity results of this work to eqs 6 and 7 plotted as a function of reference molar volume,  $V_r$ , for each experimental isotherm. The dashed lines represent the expanded uncertainty of the fit, or 95% confidence limits, that is, the standard uncertainty multiplied by 2. Symbols: ●, 258 K; □, 263 K; ▲, 268 K; ▽, 273 K; ◆, 278 K; ○, 288 K; ■, 298 K.



**Figure 3.** Residuals (literature data – values calculated from eqs 6 and 7 using the coefficients of Table 3) for the comparison of the viscosity results of Assael and Dalaouti (ref 2) (vibrating wire; ●, 253 K; □, 273 K; ▲, 293 K; ▽, 309 K) and of Brazier and Freeman (ref 12) (rolling ball; ■, 303 K) with those of this work as a function of reference molar volume,  $V_r$ . The dashed lines represent limits of  $\pm 2\%$  about our correlation.

isotherm,  $T_{\text{ref}}$ , taken as an arbitrary reference, by

$$V_r = V - \xi_1(T - T_{\text{ref}}) - \xi_2(T - T_{\text{ref}})^2 \quad (7)$$

In this work,  $T_{\text{ref}}$  was chosen as 273.15 K. The coefficients of the fit,  $\zeta_i$  and  $\xi_j$ , are given in Table 3. The residual plot is shown as Figure 2. For cyclopentane, this correlation is superior to those based on reduced viscosities employed in earlier studies.<sup>8,20–22</sup>

The viscosity of cyclopentane has been measured under high pressure by Brazier and Freeman<sup>12</sup> using a rolling

ball viscometer at the single temperature of 303.15 K to 400 MPa pressure and by Assael and Dalaouti<sup>2</sup> using a vibrating wire technique over the temperature range of (210 to 310) K but to only 25 MPa pressure. Figure 3 shows a comparison with the results of this work. Our results are in satisfactory agreement with those of Assael and Dalaouti (uncertainty,  $\pm 0.5$  to 1%), but much less so with those of Brazier and Freeman (uncertainty not explicitly stated but gauged at  $\pm 2\%$ ). A similar lack of agreement with the latter workers' results has been found by other groups for hexane<sup>23</sup> and hexadecane.<sup>11</sup> Lohrenz and co-workers<sup>24</sup> have made an analysis of the rolling ball viscometer showing that it is extremely sensitive to the effects of nonuniform construction and may exhibit random slip and spin that vary with density and viscosity.

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