

Liquid-Phase Thermodynamic Properties for Propane (1), *n*-Butane (2), and Isobutane (3)

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Hydrocarbons (HCs) are environmentally friendly natural refrigerants and are expected to be promising alternative candidates to replace some currently used halogenated hydrocarbon refrigerants. Some available data sets for HCs used to formulate the equations of state (EoS) for them are relatively old, so we point out that new data with less uncertainty are expected to play an essential role in updating the EoS for HCs. Therefore, a set of *PVT* property measurements for hydrocarbon refrigerants including propane, *n*-butane, and isobutane was conducted in the present study. A newly developed vibrating-tube densimeter was employed for the measurements, and then a total of 430 liquid *PVT* properties were obtained, including those at the saturation boundaries. The measurement range is (240 to 380) K for temperature and up to 7 MPa for pressure. The measurement uncertainty is about 3 mK for temperature, 0.26 kPa + 0.022% for pressure, and $0.1 \text{ kg}\cdot\text{m}^{-3} + 0.024\%$ for density. The present data were compared with available thermodynamic models that are currently considered to be the most reliable. A set of modified Tait equations of state for the liquid phase are also discussed.

Introduction

Hydrocarbons (HCs) are expected to be promising alternative candidates to replace some fluorinated hydrocarbon refrigerants such as CFCs (chlorofluorocarbons), HCFCs (hydrochlorofluorocarbons), and HFCs (hydrofluorocarbons). Because their global warming potential (GWP) is negligible, they are regarded as environmentally friendly and good cost-performance refrigerants, despite their flammability. Some household refrigerators from manufacturers in Europe and even Japan have already been developed.

However, it is needless to say that the thermodynamic models for HCs play an essential role in cycle-performance prediction, various kinds of design for equipment, and the selection of refrigerants. Recently, Miyamoto and Watanabe developed a set of multiproperty equations of state (EoS) for propane,¹ *n*-butane,² and isobutane.³ These EoS were employed by the latest version of the thermodynamic-property calculation software REFPROP (version 7.0)⁴ to supersede those developed earlier by Younglove and Ely.⁵ Concerning the input data used for these models, however, some of them are relatively old.

Hence, we point out that an additional set of *PVT* data for these hydrocarbons are important to confirm the reproducibility and soundness of the available thermodynamic models. In the present study, we have intended to measure *PVT* properties for propane, *n*-butane, and isobutane with a newly developed density-measurement system with the aid of a vibrating-tube densimeter. More than 400 data points including liquid-phase *PVT* properties, vapor

pressures, and saturated-liquid densities were obtained in this study. These were compared with the above-mentioned EoS by Miyamoto and Watanabe^{1–3} to examine the representation of the EoS. On the basis of the present measurements, the modified Tait EoS was also developed to interpolate the present data.

Experimental Section

Setup. The density-measurement system used in the present study was developed by us.⁶ A detailed description of the apparatus has been given.^{6,7}

Figure 1 illustrates a schematic diagram of the present measurement system. The main part of the system is a pressure–density measurement unit, and its outlook is shown in Figure 2. A vibrating-tube densimeter (VD) is suspended by four springs from the L-shaped frame. A digital pressure gauge (PT, 31 K, Paroscientific, Co.) is also supported by the frame and directly connected to the upper port of the densimeter. There were four valves (V1–V4) within the pressure–density-measurement system. The variable-volume vessel (VB) is placed between valves V1 and V2 and connected to the lower port of the densimeter. The sample fluid was discharged from the upper port of the densimeter through the expansion space between valves V3 and V4.

We have employed a commercially available densimeter (DMA512, Anton Paar, K. G.). Its densimeter cell was removed, however, from the densimeter box and attached to a balance weight (5.5 kg) made of stainless steel.

The sample pressure and density are regulated by changing the inner volume of the unit by means of the variable-volume vessel and measured by the densimeter and the pressure gauge.

Measurements were made by immersing the pressure–density measurement system into the bath fluid (silicone oil) of the thermostatic bath (LB). It should be noted that only the pressure gauge (PT) is located above the meniscus of the bath fluid in order to protect the pressure gauge from

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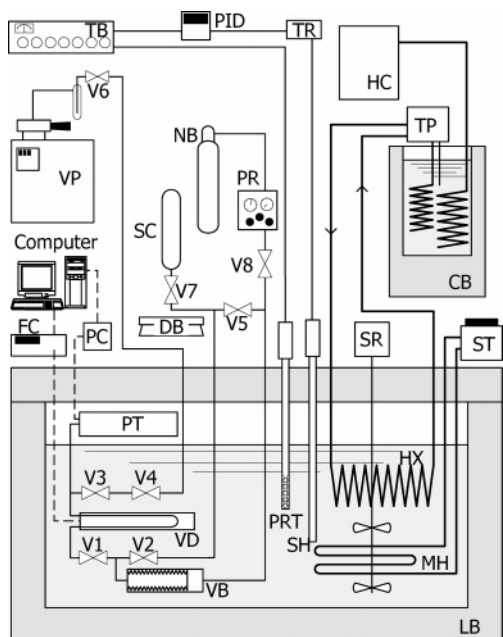


Figure 1. Schematic diagram of the experimental apparatus: VD, vibrating-tube densimeter cell; FC, frequency counter; PT, digital pressure gauge; PC, pressure computer; VB, variable-volume vessel with metallic bellows; PR, pressure regulator; NB, nitrogen gas bomb; SC, sample-supplying cylinder; DB, digital balance; VP, vacuum pump; PRT, standard platinum resistance thermometer; TB, thermometer bridge; LB, liquid bath; PID, PID controller; TR, thyristor regulator; SH, subheater; MH, main heater; ST, slide transformer; SR, stirrer; HX, heat exchanger; TP, temperature regulator pump; CB, cooling bath; HC, handy cooler; V1–7, valves.

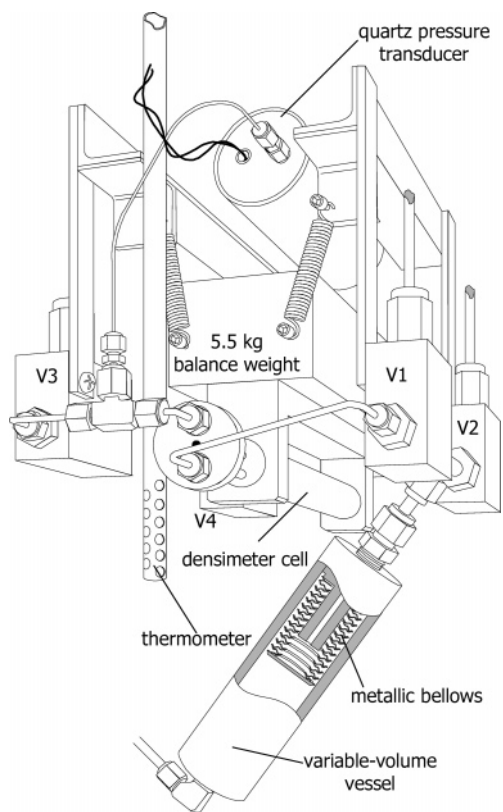


Figure 2. Drawing of the pressure–density measurement unit.

the bath fluid. The sample temperature was regarded as being equivalent to the bath-fluid temperature, and it was feedback controlled by means of a PID-controlled subheater (SH) associated with a PID controller (PID), a thermometer

bridge (TB), and a standard platinum resistance thermometer (PRT) inserted in the vicinity of the densimeter.

Calibration and Uncertainty. It should be noted that, in the present study, measurement uncertainties were evaluated along the ISO guideline⁸ where the coverage factor was $k = 2$.

The standard platinum resistance thermometer used in the present measurement was calibrated against ITS-90. The bath-fluid temperature was kept within a fluctuation of ± 1 mK so that the temperature-measurement uncertainty becomes 3 mK for temperatures less than 360 K. At temperatures above 360 K, the uncertainty approaches 7 mK.

The digital pressure gauge was calibrated against a dead-weight piston gauge. The difference in the displayed pressure was corrected as a function of temperature and pressure. Because that difference does not change very much with absolute pressure but primarily depends on temperature, the approximate error in the digital pressure gauge is known by measuring under vacuum. The repeatability of the digital pressure gauge is about $\pm 0.01\%$, whereas the pressure-measurement uncertainty of the dead-weight piston gauge is $\pm 0.005\%$. By summing these uncertainties, the present pressure-measurement uncertainty was evaluated to be

$$U = 0.26 \text{ kPa} + 0.00022P \quad (1)$$

where the coverage factor is $k = 2$.

In the present study, the density was evaluated from the vibrational period of the U tube of the densimeter on the basis of the calibration function developed. This function was determined by measuring the vibrational period of water. The non-linearity of the relation between τ^2 and ρ is corrected by introducing a nonlinear calibration model. Along the present calibration function, density, ρ , is evaluated as

$$\rho = A \frac{(1 + \mu)x}{1 - \mu x} \quad (2)$$

$$x = \left(\frac{\tau^2}{\tau_0^2} \right) - 1 \quad (3)$$

$$A = (a_1 + a_2 T^{*0.75} + a_3 T^{*3})(1 - a_4 P^*) \quad (4)$$

$$P^* = \frac{P/\text{kPa}}{7000} \quad (5)$$

$$T^* = \frac{T/\text{K}}{400} \quad (6)$$

where the periodical parameter, x , was obtained from the vibrational period, τ , and that under vacuum, τ_0 , was defined in eq 3. Parameter τ_0 was obtained in the same experiment for the sample by evacuating the sample from the measurement system. However, A is a proportional parameter and was determined by calibration with a fluid (water) of known density. We have correlated this parameter as a function of temperature and pressure given in eq 4. Parameter μ is a device-dependent constant that denotes the nonlinearity of the relation between τ^2 and ρ and was determined to be $\mu = 0.0030 \pm 0.0005$ by comparing the density of water and isooctane at the same temperature and pressure. The density measurement uncertainty was evaluated as

$$U = 0.1 \text{ kg}\cdot\text{m}^{-3} + 0.00024\rho \quad (7)$$

Table 1. Experimental PVT Data for Propane

| T K | P kPa | ρ kg·m ⁻³ | T K | P kPa | ρ kg·m ⁻³ | T K | P kPa | ρ kg·m ⁻³ |
|----------|------------|------------------------------|----------|------------|------------------------------|----------|------------|------------------------------|
| 240.000 | 147.9 | 570.28 ^a | 240.000 | 7043.3 | 578.91 | 240.000 | 6523.2 | 578.30 |
| 240.000 | 6018.3 | 577.69 | 240.000 | 5475.7 | 577.04 | 240.000 | 4957.8 | 576.41 |
| 240.000 | 4504.5 | 575.85 | 240.000 | 4045.7 | 575.29 | 240.000 | 3513.0 | 574.62 |
| 240.000 | 2999.9 | 573.98 | 240.000 | 2477.9 | 573.32 | 240.000 | 1978.3 | 572.68 |
| 240.000 | 1522.4 | 572.08 | 240.000 | 1044.8 | 571.46 | 240.000 | 527.3 | 570.78 |
| 240.000 | 147.9 | 570.28 ^a | 250.000 | 7010.3 | 567.78 | 250.000 | 6543.5 | 567.17 |
| 250.000 | 5999.9 | 566.46 | 250.000 | 5495.4 | 565.78 | 250.000 | 5045.1 | 565.17 |
| 250.000 | 4478.5 | 564.40 | 250.000 | 3993.1 | 563.74 | 250.000 | 3503.7 | 563.05 |
| 250.000 | 3016.9 | 562.38 | 250.000 | 2524.1 | 561.67 | 250.000 | 2008.3 | 560.93 |
| 250.000 | 1508.3 | 560.20 | 250.000 | 1008.1 | 559.47 | 250.000 | 513.8 | 558.73 |
| 250.000 | 217.7 | 558.29 ^a | 260.000 | 310.3 | 545.77 ^a | 260.000 | 7048.9 | 556.40 |
| 260.000 | 6522.8 | 555.62 | 260.000 | 6028.2 | 554.89 | 260.000 | 5513.9 | 554.12 |
| 260.000 | 5014.5 | 553.38 | 260.000 | 4498.9 | 552.58 | 260.000 | 4020.0 | 551.84 |
| 260.000 | 3513.3 | 551.04 | 260.000 | 3012.1 | 550.24 | 260.000 | 2504.5 | 549.42 |
| 260.000 | 1999.7 | 548.60 | 260.000 | 1503.5 | 547.77 | 260.000 | 1013.8 | 546.96 |
| 260.000 | 506.6 | 546.10 | 270.000 | 429.6 | 532.67 ^a | 270.000 | 7024.1 | 544.55 |
| 270.000 | 6525.8 | 543.74 | 270.000 | 6021.1 | 542.91 | 270.000 | 5504.7 | 542.05 |
| 270.000 | 5023.8 | 541.26 | 270.000 | 4488.2 | 540.32 | 270.000 | 4018.8 | 539.50 |
| 270.000 | 3497.1 | 538.57 | 270.000 | 3017.5 | 537.70 | 270.000 | 2499.6 | 536.75 |
| 270.000 | 2005.4 | 535.83 | 270.000 | 1510.4 | 534.87 | 270.000 | 1012.9 | 533.91 |
| 270.000 | 504.7 | 532.93 | 280.000 | 7034.7 | 532.51 | 280.000 | 6522.6 | 531.56 |
| 280.000 | 5982.8 | 530.51 | 280.000 | 5443.4 | 529.45 | 280.000 | 4963.1 | 528.50 |
| 280.000 | 4527.5 | 527.65 | 280.000 | 4049.7 | 526.68 | 280.000 | 3519.3 | 525.60 |
| 280.000 | 3032.9 | 524.61 | 280.000 | 2513.0 | 523.49 | 280.000 | 1964.2 | 522.28 |
| 280.000 | 1466.1 | 521.15 | 280.000 | 1000.0 | 520.10 | 290.000 | 768.6 | 504.75 ^a |
| 290.000 | 7049.2 | 519.81 | 290.000 | 6525.4 | 518.70 | 290.000 | 5957.4 | 517.46 |
| 290.000 | 5531.4 | 516.52 | 290.000 | 5036.3 | 515.41 | 290.000 | 4476.9 | 514.12 |
| 290.000 | 4018.1 | 513.03 | 290.000 | 3484.0 | 511.74 | 290.000 | 2998.9 | 510.56 |
| 290.000 | 2510.0 | 509.33 | 290.000 | 2004.4 | 508.04 | 290.000 | 1499.4 | 506.71 |
| 300.000 | 7004.4 | 506.54 | 300.000 | 6496.7 | 505.29 | 300.000 | 6063.5 | 504.20 |
| 300.000 | 5518.9 | 502.75 | 300.000 | 4937.0 | 501.23 | 300.000 | 4462.1 | 499.91 |
| 300.000 | 4036.8 | 498.73 | 300.000 | 3486.3 | 497.18 | 300.000 | 3032.3 | 495.86 |
| 300.000 | 2519.2 | 494.32 | 300.000 | 2015.2 | 492.77 | 300.000 | 1517.7 | 491.19 |
| 300.000 | 997.6 | 489.48 ^a | 310.000 | 6991.8 | 492.41 | 310.000 | 6510.1 | 491.02 |
| 310.000 | 6046.3 | 489.64 | 310.000 | 5299.3 | 488.08 | 310.000 | 5029.4 | 486.52 |
| 310.000 | 4528.9 | 484.91 | 310.000 | 4040.6 | 483.29 | 310.000 | 3515.0 | 481.48 |
| 310.000 | 3012.9 | 479.70 | 310.000 | 2491.2 | 477.78 | 310.000 | 2018.8 | 475.98 |
| 310.000 | 1514.4 | 473.96 | 310.000 | 1272.1 | 472.96 ^a | 320.000 | 7008.9 | 477.63 |
| 320.000 | 6523.4 | 475.95 | 320.000 | 6024.8 | 474.19 | 320.000 | 5536.8 | 472.40 |
| 320.000 | 5017.9 | 470.44 | 320.000 | 4519.6 | 468.46 | 320.000 | 4025.8 | 466.44 |
| 320.000 | 3495.1 | 464.17 | 320.000 | 3002.1 | 461.96 | 320.000 | 2512.8 | 459.66 |
| 320.000 | 2011.4 | 457.17 | 320.000 | 1600.7 | 455.00 ^a | 330.000 | 6985.1 | 461.52 |
| 330.000 | 6499.8 | 459.50 | 330.000 | 6010.6 | 457.38 | 330.000 | 5488.6 | 455.01 |
| 330.000 | 4996.1 | 452.66 | 330.000 | 4495.8 | 450.17 | 330.000 | 3995.4 | 447.53 |
| 330.000 | 3909.1 | 447.05 | 330.000 | 3546.3 | 445.00 | 330.000 | 3032.0 | 441.91 |
| 330.000 | 2537.4 | 438.74 | 330.000 | 2033.9 | 435.23 | 330.000 | 1988.8 | 434.90 ^a |
| 340.000 | 6964.1 | 444.10 | 340.000 | 6494.7 | 441.64 | 340.000 | 5985.0 | 438.83 |
| 340.000 | 5516.7 | 436.10 | 340.000 | 5027.1 | 433.06 | 340.000 | 4501.8 | 429.56 |
| 340.000 | 4014.0 | 426.05 | 340.000 | 3507.8 | 422.07 | 340.000 | 3024.2 | 417.87 |
| 340.000 | 2429.7 | 411.92 ^a | 350.000 | 6978.1 | 424.88 | 350.000 | 6491.4 | 421.59 |
| 350.000 | 6027.1 | 418.22 | 350.000 | 5521.6 | 414.24 | 350.000 | 5024.8 | 409.94 |
| 350.000 | 4505.9 | 404.94 | 350.000 | 4011.9 | 399.51 | 350.000 | 3541.2 | 393.49 |
| 350.000 | 2948.0 | 384.39 ^a | 360.000 | 6953.8 | 402.50 | 360.000 | 6529.9 | 398.56 |
| 360.000 | 6048.5 | 393.63 | 360.000 | 5524.7 | 387.51 | 360.000 | 5043.0 | 380.99 |
| 360.000 | 4527.8 | 372.52 | 360.000 | 4043.5 | 362.08 | 360.000 | 3552.2 | 347.97 ^a |
| 370.000 | 2783.7 | 55.36 ^b | 370.000 | 2081.6 | 37.08 ^b | 370.000 | 1515.9 | 25.15 ^b |
| 370.000 | 1089.1 | 17.21 ^b | 370.000 | 779.8 | 11.91 ^b | 370.000 | 4325.4 | 287.46 |
| 370.000 | 7066.4 | 377.66 | 370.000 | 6504.8 | 369.98 | 370.000 | 5998.0 | 361.65 |
| 370.000 | 5527.4 | 352.01 | 370.000 | 4996.9 | 336.94 | 370.000 | 4521.7 | 312.65 |
| 380.000 | 7012.1 | 344.89 | 380.000 | 6541.5 | 333.99 | 380.000 | 6044.5 | 318.37 |
| 380.000 | 5530.3 | 291.64 | 380.000 | 5335.4 | 273.87 | 380.000 | 4556.5 | 131.82 ^b |
| 380.000 | 4060.6 | 97.22 ^b | 380.000 | 4059.9 | 97.18 ^b | 380.000 | 4059.0 | 97.16 ^b |
| 380.000 | 3340.1 | 67.96 ^b | 380.000 | 2630.4 | 47.90 ^b | 380.000 | 2032.0 | 34.39 ^b |
| 380.000 | 1564.3 | 25.22 ^b | 380.000 | 1223.8 | 19.12 ^b | 380.000 | 813.8 | 12.27 ^b |

^a Datum in the saturated liquid phase. ^b Datum in the supercritical state.

Materials. We have used research-grade samples of propane, *n*-butane, and isobutane with a purity of 99.99 mol %. This purity information was provided by the chemical manufacturer, Nippon Sanso Co., and we did not conduct any further purification except degassing.

Results and Discussion

A total of 192, 128, and 110 *PVT* properties were obtained for propane, *n*-butane, and isobutane, respectively. These data widely range from (240 to 380) K, up to 7 MPa, in the liquid phase including data along the saturation curves. Tables 1, 2, and 3 tabulate the present measured data. Figures 3, 4, and 5 illustrate the distribu-

Table 2. Experimental PVT Data for *n*-Butane

| T K | P kPa | ρ kg·m ⁻³ | T K | P kPa | ρ kg·m ⁻³ | T K | P kPa | ρ kg·m ⁻³ |
|----------|------------|------------------------------|----------|------------|------------------------------|----------|------------|------------------------------|
| 240.000 | 26.2 | 634.72 ^a | 240.000 | 23.9 | 634.79 ^a | 240.000 | 7115.6 | 642.22 |
| 240.000 | 6517.3 | 641.67 | 240.000 | 5990.8 | 641.21 | 240.000 | 5540.8 | 640.78 |
| 240.000 | 5029.0 | 640.31 | 240.000 | 4487.8 | 639.80 | 240.000 | 4001.2 | 639.35 |
| 240.000 | 3512.2 | 638.87 | 240.000 | 3029.5 | 638.41 | 240.000 | 2570.2 | 637.97 |
| 240.000 | 2000.1 | 637.42 | 240.000 | 1510.1 | 636.95 | 240.000 | 1007.3 | 636.47 |
| 240.000 | 486.0 | 635.96 | 260.000 | 59.9 | 615.48 ^a | 260.000 | 6989.2 | 623.08 |
| 260.000 | 6478.7 | 622.54 | 260.000 | 6003.3 | 622.01 | 260.000 | 5503.1 | 621.46 |
| 260.000 | 5004.2 | 620.91 | 260.000 | 4494.6 | 620.36 | 260.000 | 3997.0 | 619.80 |
| 260.000 | 3506.9 | 619.26 | 260.000 | 3039.4 | 618.72 | 260.000 | 2488.3 | 618.09 |
| 260.000 | 2020.3 | 617.55 | 260.000 | 1521.8 | 616.98 | 260.000 | 998.4 | 616.36 |
| 260.000 | 481.0 | 615.74 | 280.000 | 131.5 | 593.89 ^a | 280.000 | 7020.0 | 603.37 |
| 280.000 | 6499.1 | 602.71 | 280.000 | 5929.2 | 601.98 | 280.000 | 5428.9 | 601.30 |
| 280.000 | 4975.0 | 600.69 | 280.000 | 4513.6 | 600.07 | 280.000 | 3974.9 | 599.34 |
| 280.000 | 3516.7 | 598.71 | 280.000 | 2985.5 | 597.98 | 280.000 | 2465.8 | 597.26 |
| 280.000 | 1987.6 | 596.59 | 280.000 | 1472.7 | 595.86 | 280.000 | 992.0 | 595.16 |
| 280.000 | 493.9 | 594.44 | 280.000 | 173.2 | 593.97 | 280.000 | 144.7 | 593.92 |
| 300.000 | 256.4 | 571.03 ^a | 300.000 | 7089.3 | 582.62 | 300.000 | 6459.3 | 581.65 |
| 300.000 | 5951.1 | 580.88 | 300.000 | 5543.6 | 580.23 | 300.000 | 4990.4 | 579.31 |
| 300.000 | 4525.1 | 578.55 | 300.000 | 3992.8 | 577.66 | 300.000 | 3499.9 | 576.83 |
| 300.000 | 2964.0 | 575.92 | 300.000 | 2499.1 | 575.12 | 300.000 | 2013.4 | 574.26 |
| 300.000 | 1491.3 | 573.35 | 300.000 | 992.8 | 572.45 | 300.000 | 493.4 | 571.55 |
| 300.000 | 315.1 | 571.23 | 300.000 | 268.9 | 571.14 | 320.000 | 6982.1 | 560.62 |
| 320.000 | 6510.5 | 559.67 | 320.000 | 6031.0 | 558.74 | 320.000 | 5473.8 | 557.60 |
| 320.000 | 4992.8 | 556.63 | 320.000 | 4513.3 | 555.64 | 320.000 | 4015.6 | 554.60 |
| 320.000 | 4017.2 | 554.60 | 320.000 | 3523.1 | 553.55 | 320.000 | 3010.6 | 552.45 |
| 320.000 | 2517.1 | 551.36 | 320.000 | 2011.8 | 550.22 | 320.000 | 1502.7 | 549.06 |
| 320.000 | 1002.9 | 547.89 | 320.000 | 515.9 | 546.74 | 320.000 | 454.8 | 546.56 ^a |
| 340.000 | 750.5 | 520.07 ^a | 340.000 | 751.0 | 519.84 ^a | 340.000 | 7014.5 | 537.36 |
| 340.000 | 6451.2 | 535.97 | 340.000 | 5975.4 | 534.78 | 340.000 | 5471.0 | 533.51 |
| 340.000 | 4964.4 | 532.19 | 340.000 | 4437.7 | 530.79 | 340.000 | 4034.7 | 529.70 |
| 340.000 | 3504.4 | 528.23 | 340.000 | 3012.7 | 526.82 | 340.000 | 2514.4 | 525.36 |
| 340.000 | 1975.7 | 523.74 | 340.000 | 1519.5 | 522.33 | 340.000 | 989.9 | 520.64 |
| 340.000 | 791.7 | 519.97 | 340.000 | 761.5 | 519.87 | 360.000 | 1168.5 | 490.27 ^a |
| 360.000 | 7012.4 | 512.64 | 360.000 | 6486.7 | 510.96 | 360.000 | 5979.4 | 509.32 |
| 360.000 | 5504.8 | 507.65 | 360.000 | 4984.1 | 505.83 | 360.000 | 4488.7 | 504.06 |
| 360.000 | 3993.1 | 502.23 | 360.000 | 3489.7 | 500.29 | 360.000 | 2995.1 | 498.32 |
| 360.000 | 2493.7 | 496.23 | 360.000 | 2006.4 | 494.12 | 360.000 | 1507.5 | 491.85 |
| 360.000 | 1215.8 | 490.48 | 360.000 | 1181.7 | 490.31 | 360.000 | 1168.1 | 490.24 ^a |
| 380.000 | 6978.0 | 484.82 | 380.000 | 6534.9 | 482.88 | 380.000 | 6013.8 | 480.51 |
| 380.000 | 5511.1 | 478.12 | 380.000 | 5015.7 | 475.66 | 380.000 | 4508.9 | 473.00 |
| 380.000 | 3999.9 | 470.18 | 380.000 | 3502.0 | 467.25 | 380.000 | 3010.6 | 464.17 |
| 380.000 | 2503.7 | 460.77 | 380.000 | 2007.2 | 457.14 | 380.000 | 1925.7 | |

Table 3. Experimental PVT Data for Isobutane

| T K | P kPa | ρ kg·m ⁻³ | T K | P kPa | ρ kg·m ⁻³ | T K | P kPa | ρ kg·m ⁻³ |
|----------|------------|------------------------------|----------|------------|------------------------------|----------|------------|------------------------------|
| 240.000 | 40.1 | 617.17 ^a | 240.000 | 7010.9 | 624.66 | 240.000 | 6540.8 | 624.19 |
| 240.000 | 5987.3 | 623.62 | 240.000 | 5522.1 | 623.14 | 240.000 | 5022.8 | 622.62 |
| 240.000 | 4542.1 | 622.10 | 240.000 | 4038.4 | 621.58 | 240.000 | 3501.9 | 621.00 |
| 240.000 | 3029.3 | 620.49 | 240.000 | 2522.8 | 619.95 | 240.000 | 2037.8 | 619.41 |
| 240.000 | 1538.4 | 618.86 | 240.000 | 1027.4 | 618.30 | 240.000 | 484.1 | 617.68 |
| 260.000 | 94.6 | 595.32 ^a | 260.000 | 7031.7 | 604.37 | 260.000 | 6532.0 | 603.75 |
| 260.000 | 5953.7 | 603.05 | 260.000 | 5481.6 | 602.44 | 260.000 | 4915.7 | 601.73 |
| 260.000 | 4464.7 | 601.16 | 260.000 | 4015.9 | 600.60 | 260.000 | 3472.2 | 599.90 |
| 260.000 | 3005.3 | 599.28 | 260.000 | 2532.0 | 598.66 | 260.000 | 1984.7 | 597.94 |
| 260.000 | 1503.8 | 597.28 | 260.000 | 947.4 | 596.52 | 260.000 | 517.1 | 595.93 |
| 280.000 | 197.8 | 572.74 ^a | 280.000 | 6980.4 | 583.64 | 280.000 | 6507.2 | 582.93 |
| 280.000 | 5986.9 | 582.16 | 280.000 | 5494.5 | 581.39 | 280.000 | 4938.8 | 580.54 |
| 280.000 | 4460.5 | 579.80 | 280.000 | 4015.2 | 579.09 | 280.000 | 3506.0 | 578.27 |
| 280.000 | 2999.4 | 577.44 | 280.000 | 2508.1 | 576.64 | 280.000 | 2000.6 | 575.80 |
| 280.000 | 1532.9 | 575.01 | 280.000 | 996.0 | 574.10 | 280.000 | 512.2 | 573.26 |
| 300.000 | 368.6 | 548.27 ^a | 300.000 | 7025.2 | 561.79 | 300.000 | 6460.3 | 560.72 |
| 300.000 | 5953.2 | 559.79 | 300.000 | 5467.8 | 558.87 | 300.000 | 4980.2 | 557.93 |
| 300.000 | 4482.8 | 556.96 | 300.000 | 3965.8 | 555.93 | 300.000 | 3526.2 | 555.05 |
| 300.000 | 3021.3 | 554.01 | 300.000 | 2533.3 | 552.99 | 300.000 | 1999.9 | 551.86 |
| 300.000 | 1462.4 | 550.70 | 300.000 | 1017.6 | 549.71 | 300.000 | 476.5 | 548.51 |
| 320.000 | 632.5 | 521.48 ^a | 320.000 | 6995.3 | 538.27 | 320.000 | 6511.5 | 537.15 |
| 320.000 | 5960.5 | 535.86 | 320.000 | 5450.3 | 534.62 | 320.000 | 4946.7 | 533.39 |
| 320.000 | 4496.4 | 532.26 | 320.000 | 4027.5 | 531.05 | 320.000 | 3521.6 | 529.72 |
| 320.000 | 3037.4 | 528.43 | 320.000 | 2548.7 | 527.08 | 320.000 | 2072.9 | 525.74 |
| 320.000 | 1503.5 | 524.10 | 320.000 | 1063.0 | 522.78 | 340.000 | 1013.7 | 491.87 ^a |
| 340.000 | 6962.7 | 513.39 | 340.000 | 6512.9 | 512.03 | 340.000 | 5998.3 | 510.42 |
| 340.000 | 5520.7 | 508.89 | 340.000 | 5017.1 | 507.23 | 340.000 | 4507.3 | 505.51 |
| 340.000 | 4023.8 | 503.83 | 340.000 | 3503.8 | 501.94 | 340.000 | 3002.8 | 500.07 |
| 340.000 | 2499.6 | 498.13 | 340.000 | 2007.1 | 496.16 | 340.000 | 1494.6 | 493.98 |
| 360.000 | 1541.6 | 457.33 ^a | 360.000 | 6987.7 | 486.08 | 360.000 | 6485.4 | 484.01 |
| 360.000 | 6006.8 | 481.96 | 360.000 | 5482.2 | 479.63 | 360.000 | 5024.7 | 477.51 |
| 360.000 | 4532.2 | 475.11 | 360.000 | 4027.6 | 472.55 | 360.000 | 3502.9 | 469.71 |
| 360.000 | 2997.5 | 466.82 | 360.000 | 2503.6 | 463.81 | 360.000 | 2008.5 | 460.57 |
| 380.000 | 2250.4 | 413.34 ^a | 380.000 | 6952.1 | 454.64 | 380.000 | 6503.3 | 451.96 |
| 380.000 | 6019.7 | 448.91 | 380.000 | 5519.1 | 445.53 | 380.000 | 4990.6 | 441.69 |
| 380.000 | 4487.2 | 437.71 | 380.000 | 4014.9 | 433.63 | 380.000 | 3511.0 | 428.79 |
| 380.000 | 3027.5 | 423.54 | 380.000 | 2517.9 | 417.11 | | | |

^a Datum at the saturated liquid phase.

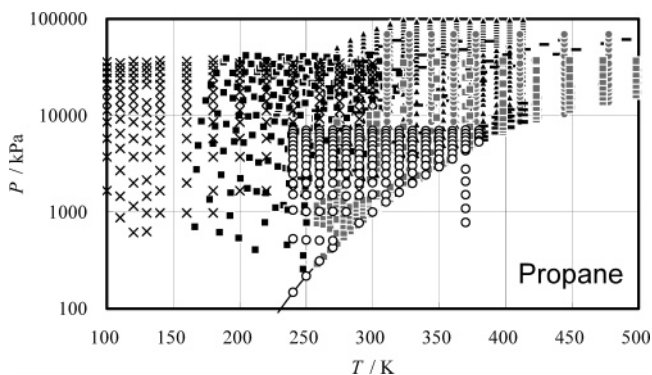


Figure 3. PVT data distribution for propane: ○, this work; ▲, Dittmar et al.;²³ ■, Ely and Kobayashi;²¹ ×, Haynes;²⁰ —, Kratzke and Mueller;²⁴ ● (in gray), Reamer et al.;²⁵ ■ (in gray), Thomas and Harrison.²⁶

to be set in $\pm 0.15\%$ from the baseline. Although there are slight fluctuations for liquid-density data by Beattie,¹⁵ Kay,⁹ and Olds et al.,¹⁰ it is considered that those data satisfactorily agree with the baseline as long as the date of measurements of these data around the 1940s is considered.

It was also found from Figure 8 that the present liquid-density data show an S-shaped systematic deviation from the MWEoS. The density difference becomes large at higher temperatures to a maximum of 0.4%. At temperatures of (300 to 380) K, there are no data other than piezometry data by Morris et al.,¹¹ Sage and Lacey,¹² and our data. Therefore, it is considered to be unreasonable to require high reproducibility to the EoS. It may also be said that the present data provide important information about liquid-phase PVT properties for isobutane.

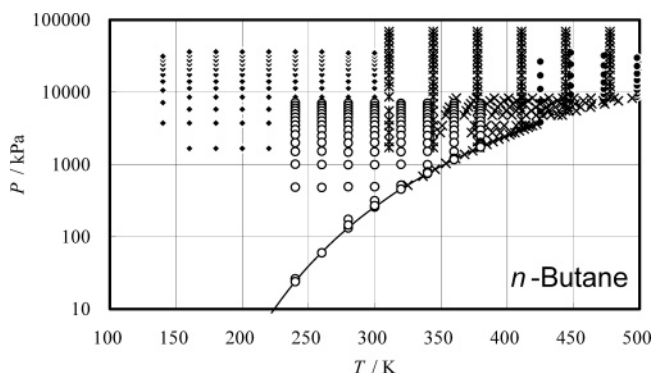


Figure 4. PVT data distribution for *n*-butane: ○, this work; ●, Beattie et al.;¹⁵ ◆, Haynes;¹⁴ ×, Kay;⁹ *, Olds et al.¹⁰

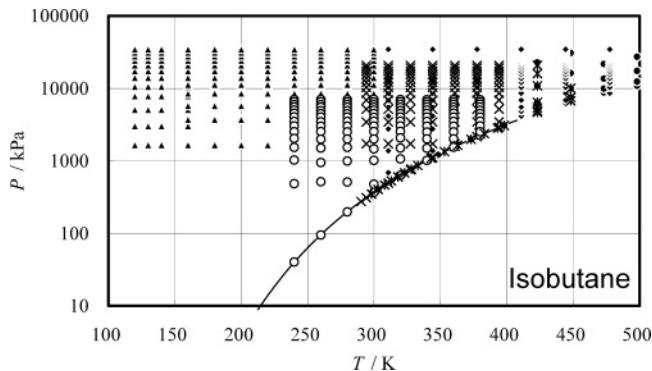


Figure 5. PVT data distribution for isobutane: ○, this work; ●, Beattie et al.;²⁷ ▲, Haynes;²² ◆, Morris et al.;¹¹ ×, Sage and Lacey;¹² *, Waxman et al.²⁸

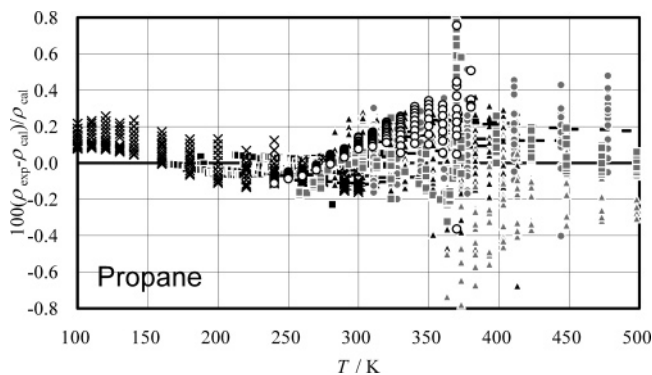


Figure 6. Relative density deviation of the liquid-density data for propane from the Miyamoto and Watanabe EoS:¹ ○, this work; ▲, Dittmar et al.;²³ ■, Ely and Kobayashi;²¹ ×, Haynes;²⁰ —, Kratzke and Mueller;²⁴ ● (in gray), Reamer et al.;²⁵ ▲ (in gray), Straty and Palavra;²⁹ ■ (in gray), Thomas and Harrison;²⁶ ◆ (in gray), Warowny et al.³⁰

In the present study, vapor pressures for propane, *n*-butane, and isobutane were also measured in the temperature range from 240 K to 380 K or the critical temperature for propane. These data and available literature data were also compared with the MWEoS in Figures 9, 10, and 11, respectively.

From Figure 9, it is found that most of the present data agree well with the MWEoS within a scatter of ± 3 kPa. The vapor-pressure data for *n*-butane obtained in the present study have a similar negative deviation of about -3.5 kPa maximum. Concerning the present vapor-pressure data for isobutane, it was found that they were well reproduced by the MWEoS only within ± 1.5 kPa. The available vapor-pressures for isobutane have relatively large scatter of ± 10 kPa. Hence, it can be said that the

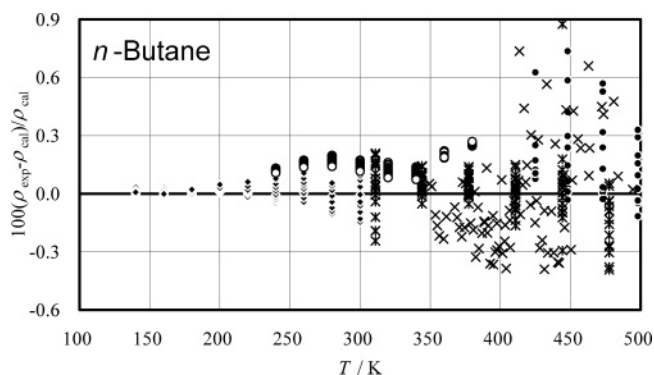


Figure 7. Relative density deviation of the liquid-density data for *n*-butane from the Miyamoto and Watanabe EoS:² ○, this work; ●, Beattie et al.;¹⁵ ▲, Haynes;¹⁴ ×, Kay;⁹ *, Olds et al.¹⁰

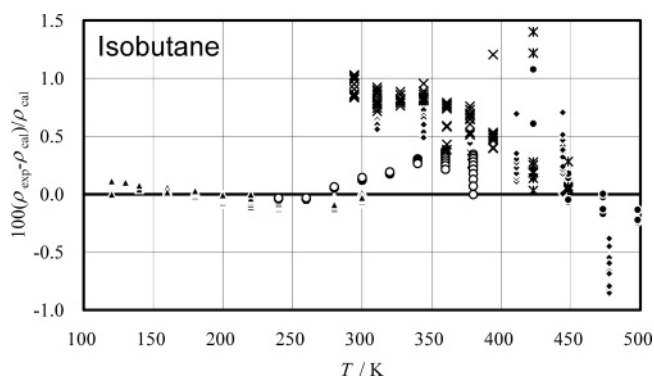


Figure 8. Relative density deviation of the liquid-density data for isobutane from the Miyamoto and Watanabe EoS:³ ○, this work; ●, Beattie et al.;²⁷ ▲, Haynes;²² ◆, Morris et al.;¹¹ ×, Sage and Lacey;¹² *, Waxman et al.²⁸

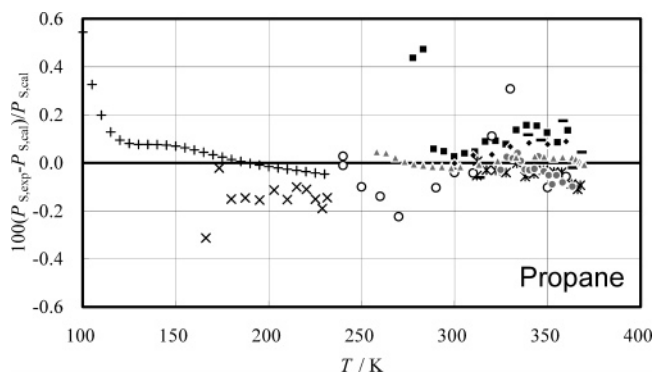


Figure 9. Relative deviation of the vapor-pressure data for propane from the Miyamoto and Watanabe EoS:¹ ○, this work; ■, Helgeson and Sage;³¹ ◆, Hondo et al.;³² ×, Kemp and Egan;³³ *, Kratzke;³⁴ +, Magee;³⁵ -, Reamer et al.;²⁵ ● (in gray), Teichmann;³⁶ ▲ (in gray), Thomas and Harrison.²⁶

soundness of the prediction of the MWEoS for isobutane was confirmed by the present measurements.

The saturated liquid densities for propane, *n*-butane, and isobutane were also compared with the MWEoS in Figures 12, 13, and 14, respectively.

Excellent agreement of the present data with the MWEoS appears in Figure 12. In the temperature range below 350 K, it is confirmed that all of the data obtained in the present study agree well with the EoS within $\pm 0.1\%$. At higher temperatures, the data deviate to 0.6%, as do other reported data, because they are close to the critical temperature.

Concerning the saturated liquid densities for *n*-butane, the present data have a positive systematic deviation by

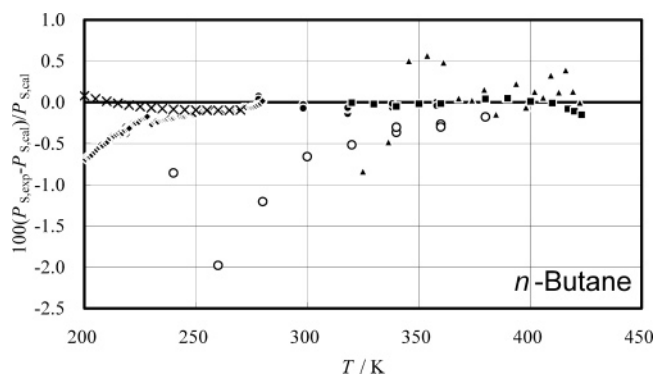


Figure 10. Relative deviation of the vapor-pressure data for *n*-butane from the Miyamoto and Watanabe EoS:² ○, this work; ●, Flebbe et al.;³⁷ ▲, Kay;⁹ ■, Kratzke;³⁴ ◆, Machin and Golding;³⁸ ×, Magee.³⁵

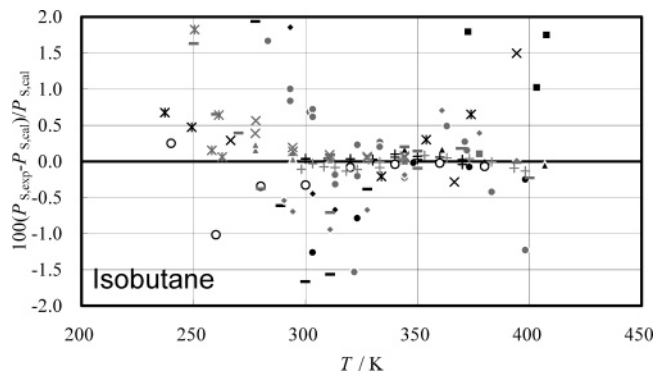


Figure 11. Relative deviation of the vapor-pressure data for isobutane from the Miyamoto and Watanabe EoS:³ ○, this work; ●, Beattie et al.;³⁹ ▲, Connolly;⁴⁰ ■, Gilliland and Scheeline;⁴¹ ◆, Higashi et al.;⁴² ×, Hipkin;⁴³ *, Hirata and Suda;⁴⁴ +, Hondo et al.;³² -, Kahre;⁴⁵ ● (in gray), KIST;⁴⁶⁻⁵⁰ ▲ (in gray), Martinez-Ortiz and Manley;⁵¹ ■ (in gray), Morris et al.;¹¹ ◆ (in gray), Sage and Lacey;¹² × Steele et al.;⁵² * (in gray), Wackher et al.;⁵³ + (in gray), Waxman et al.;²⁸ - (in gray), Weber.⁵⁴⁻⁵⁶

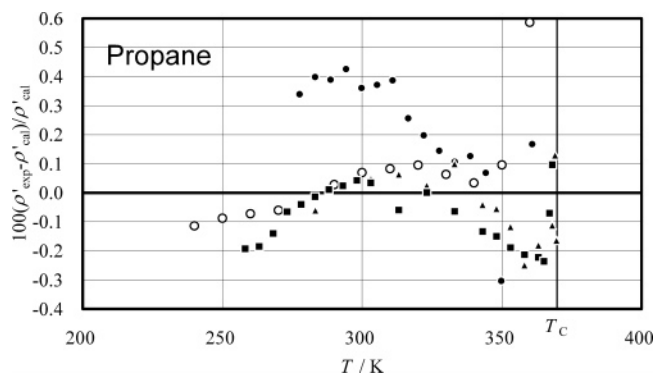


Figure 12. Relative deviation of the saturated-liquid density data for propane from the Miyamoto and Watanabe EoS:¹ ○, this work; ●, Helgeson and Sage;³¹ ▲, Sliwinski;⁵⁷ ■, Thomas and Harison.²⁶

about +0.07% to +0.26% from the baseline. This trend is different from those for the majority of the available data by Haynes,¹⁴ Orrit and Laupretre,¹⁶ and Sliwinski.¹⁷

From Figure 14, the present data were found to have a systematic deviation from the prediction of the MWEoS, but they are still within $\pm 0.3\%$. It is interesting that this behavior is similar to that for the data by Sliwinski.¹⁷

Liquid-Density Equation

To represent the thermodynamic properties in the liquid phase of propane, *n*-butane, and isobutane obtained in the

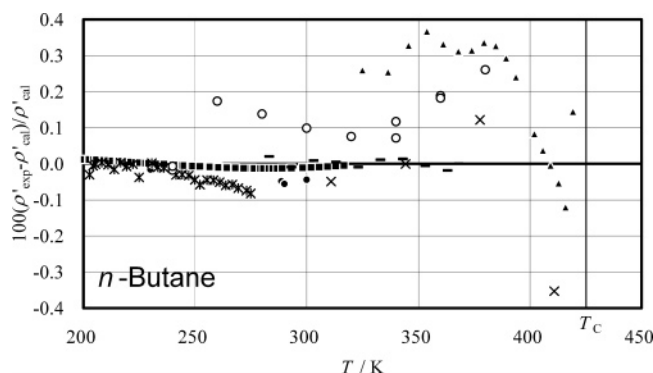


Figure 13. Relative deviation of the saturated-liquid density data for *n*-butane from the Miyamoto and Watanabe EoS:² ○, this work; ●, Haynes;¹⁴ ▲, Kay;⁹ ■, Magee;³⁵ ×, Olds et al.;¹⁰ *, Orrit and Laupretre;¹⁶ −, Sliwinski.¹⁷

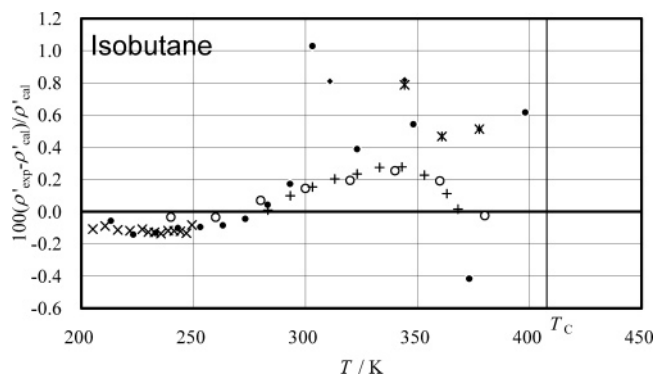


Figure 14. Relative deviation of the saturated-liquid density data for isobutane from the Miyamoto and Watanabe EoS:³ ○, this work; ●, Beattie et al.;³⁹ ◆, Morris et al.;¹¹ ×, Orrit and Laupretre;¹⁶ *, Sage and Lacey;¹² +, Sliwinski.¹⁷

present study, we have developed an empirical equation of state. The original basic function of the EoS was proposed by Sato¹⁸ to represent the thermodynamic properties of water as a modified form of the van der Waals equation of state. We have employed this basic function to represent the liquid-phase thermodynamic properties for light hydrocarbons. The functional form of the EoS is given by

$$\rho_r = \frac{(P_r + A(T_r))^{C(T_r)}}{D(T_r)} \quad (8)$$

$$A(T) = \sum_{k=0}^2 a_k T_r^k \quad (9)$$

$$C(T) = \sum_{k=0}^2 c_k T_r^k \quad (10)$$

$$D(T) = \sum_{k=0}^2 d_k T_r^k \quad (11)$$

T_r , P_r , and ρ_r are the reduced temperature, pressure, and density, respectively. They are nondimensionalized by the critical parameters (e.g., $T_r = T/T_c$). As for the critical parameters for propane and isobutane used in the present EoS, we have employed those reported by Yoshii.¹³ As for *n*-butane, those by Haynes and Goodwin¹⁹ were employed. It should be noted that the critical pressure values for propane and isobutane were originally optimized from the

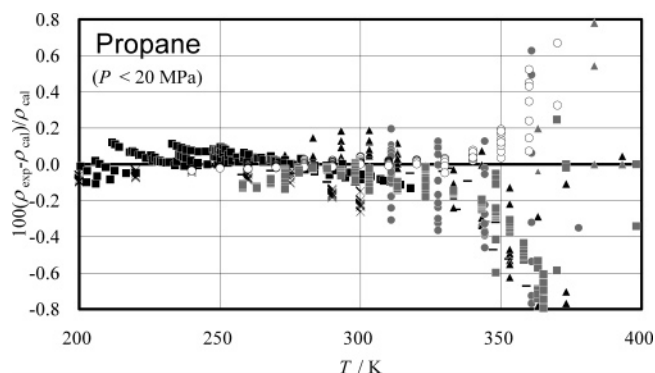


Figure 15. Relative density deviation of the liquid-density data for propane from eq 8: ○, this work; ▲, Dittmar et al.;²³ ■, Ely and Kobayashi;²¹ ×, Haynes;²⁰ −, Kratzke and Mueller;²⁴ ● (in gray), Reamer et al.;²⁵ ▲ (in gray), Straty and Palavra;²⁹ ■ (in gray), Thomas and Harrison;²⁶ ◆ (in gray), Warowny et al.³⁰

Table 4. Numerical Constants for Equations 8–11

| substance | propane | <i>n</i> -butane | isobutane |
|--------------------------|-----------|------------------|-----------|
| T_c/K | 369.811 | 425.125 | 407.761 |
| P_c/kPa | 4248 | 3796 | 3631 |
| $\rho_c/kg \cdot m^{-3}$ | 222 | 227.84 | 233 |
| a_0 | 51.5282 | 39.0313 | 40.0811 |
| a_1 | −90.2975 | −63.6158 | −66.0010 |
| a_2 | 37.8007 | 23.5672 | 24.9675 |
| c_0 | 0.102351 | 0.072934 | 0.077124 |
| c_1 | −0.077820 | −0.075024 | −0.078421 |
| c_2 | 0.087578 | 0.109702 | 0.113271 |
| d_0 | 0.404740 | 0.352283 | 0.369925 |
| d_1 | 0 | −0.000028 | −0.000241 |
| d_2 | 0.160565 | 0.208062 | 0.213270 |

vapor-pressure correlation. These parameters are summarized in Table 4.

This equation of state is valid in the liquid phase; however, the temperature range is up to the reduced temperature, $T_r = 0.95$, where the isothermal compressibility moderately changes. At higher temperatures, the EoS may not be effective because of the steep curvature of the P – ρ isotherm.

In the present study, numerical constants a_0 through d_2 were determined by a nonlinear regression of the EoS to the present data obtained by the vibrating-tube densimeter apparatus. Concerning the input data for propane, we did not use data at temperatures higher than $T_r = 0.95$. Thus-determined numerical constants are summarized in Table 4.

Concerning the valid range of the EoS that was fitted to the present data for (240 to 380) K, up to 7 MPa, it is expected to be valid down to 200 K. However, the pressure limit of the present EoS for the liquid phase is not strictly restricted by the input data range, but it is expected to be effective at pressures up to 20 MPa.

The relative density deviation of the reported data at pressures up to 20 MPa from eq 8 is illustrated in Figure 15. The EoS is in good agreement with the present data within $\pm 0.08\%$ at temperatures up to 340 K. As the temperature rises, the deviation increases to 0.5%. It is found from Figure 15 that eq 8 represents the reported liquid-density data with good reproducibility. The maximum deviation of the data for temperatures between 240 K and 350 K is less than $\pm 0.2\%$. Equation 8 has the best reproducibility among the available representations at lower temperatures from 210 K to 290 K, although all of them agree well with eq 8 within $\pm 0.15\%$. The data at lower temperatures down to 100 K reported by Haynes²⁰ and by Ely and Kobayashi²¹ have slight systematic devia-

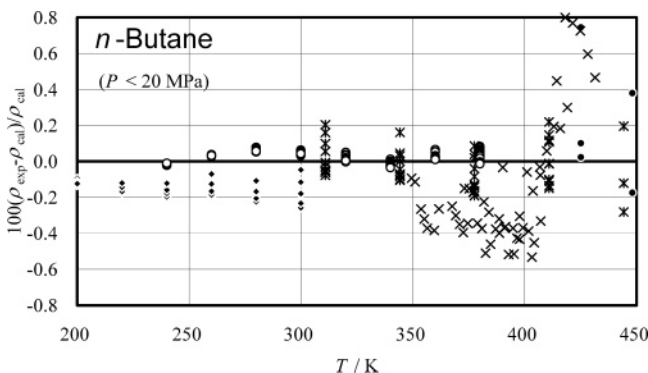


Figure 16. Relative density deviation of the liquid-density data for *n*-butane from eq 8: ○, this work; ●, Beattie et al.;¹⁵ ◆, Haynes;¹⁴ ×, Kay;⁹ *, Olds et al.¹⁰

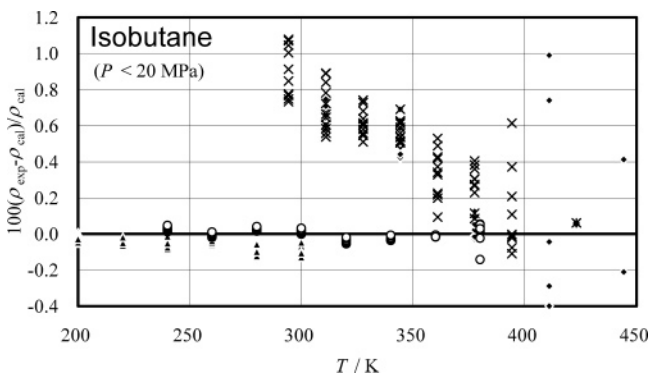


Figure 17. Relative density deviation of the liquid-density data for isobutane from eq 8: ○, this work; ●, Beattie et al.;²⁷ ▲, Haynes;²² ◆, Morris et al.;¹¹ ×, Sage and Lacey;¹² *, Waxman et al.²⁸

tions, but they are not greater than -1.0% even at 120 K. Although the reproducibility of eq 8 also decreases in the vicinity of the critical point, all of the data are reproduced within $\pm 1.0\%$ at temperatures up to 360 K. Judging from these facts, the lowest-temperature limit for eq 8 to be valid is expected to be down to 200 K, whereas the highest-temperature limit is about 360 K because of the effectiveness of the EoS.

Figure 16 illustrates the relative density deviation of the present data and other reported density data for *n*-butane from those calculated by eq 8. The reported data above 20 MPa were not included in Figure 16 for the same reason as that discussed previously. From the deviation plot, it is apparent that eq 8 excellently represents the input data obtained in the present study within $\pm 0.06\%$. Equation 8 also shows a good representation for liquid-density data by Haynes¹⁴ within $\pm 0.15\%$. As already discussed above, other reported data have a relatively wider scatter from the baseline. However, this fact is considered to be acceptable by considering the measurement uncertainty of these data.

A similar comparison was made for isobutane, as shown in Figure 17. The present data were confirmed to agree with the baseline EoS, eq 8, excellently within $\pm 0.05\%$ except for a single datum at 380 K. To examine the extrapolation capability of eq 8 with respect to temperature, it is compared with the available liquid-density data at pressures up to 20 MPa. It is found that eq 8 has good reproducibility within $\pm 0.3\%$ of the data by Haynes²² down to 200 K. As for temperatures between 310 K and 350 K, all of the data including those by Haynes and those by Sage and Lacey¹² deviate by about $+0.5\%$ to $+1.0\%$ from eq 8. The temperature behavior of the data by Haynes shows a

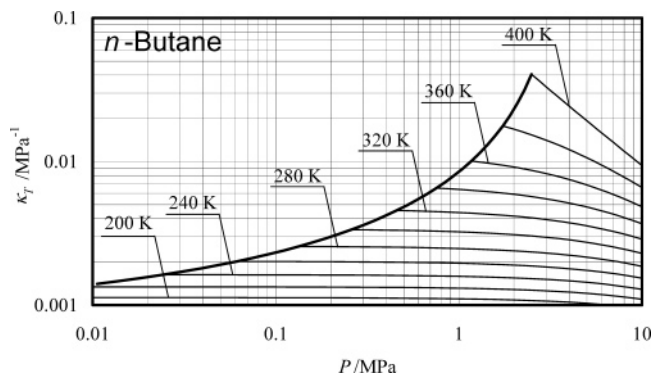


Figure 18. Pressure dependence of the isothermal compressibility for *n*-butane derived from eq 8.

certain discrepancy at temperatures between 300 K and 310 K, which is considered to be inconsistent. Regarding this temperature range, it is considered that some unknown thermodynamic behavior of isobutane may exhibit this gap. Further investigation regarding this issue is expected to be done. Although the issue that a considerable observed discrepancy for the data at temperatures between 310 K and 350 K remains unsolved, eq 8 has satisfactory effectiveness for temperatures from 200 K to 400 K and pressures up to 20 MPa.

To confirm the thermodynamic consistency of eq 8, we derived properties such as the isochoric heat capacity, c_v , isobaric heat capacity, c_p , speed of sound, w , and isothermal compressibility, κ_T from eq 8. These properties were evaluated by applying following thermodynamic relations.

$$c_v = c_p + \frac{T \left(\frac{\partial v}{\partial T} \right)_P^2}{\rho^2 \left(\frac{\partial v}{\partial P} \right)_T} \quad (12)$$

$$c_p = c_p' - \int_{P_s}^P T \left(\frac{\partial^2 v}{\partial T^2} \right)_P dP \quad (13)$$

$$w = \sqrt{\frac{c_p}{\rho \alpha_T c_v}} \quad (14)$$

$$\kappa_T = \frac{C}{A + P} \quad (15)$$

In the present paper, these properties for *n*-butane are discussed as an example because the behavior of these properties calculated from the present EoS is not very different from each other.

In eq 13, c_p' denotes the saturated-liquid isobaric heat capacity. To calculate these derived properties, the computed c_p' values were employed as the reference state. Figures 18, 19, and 20 illustrate the pressure dependences of the isothermal compressibility, isobaric heat capacity, and speed of sound for *n*-butane, respectively.

It is recognized from these Figures that eq 8 can yield a thermodynamically sound property surface within its valid temperature range (from 200 K to 409 K = $0.95T_c$). As for the same examination of eq 8 for propane, unreasonable behavior of the isochoric heat capacity was observed for an isotherm of 360 K. Because that temperature ($T_r = 0.973$) is very close to the critical point and is not valid for eq 8, the thermodynamic consistency would be lost in this temperature range. At temperatures below $T_r = 0.95$, the

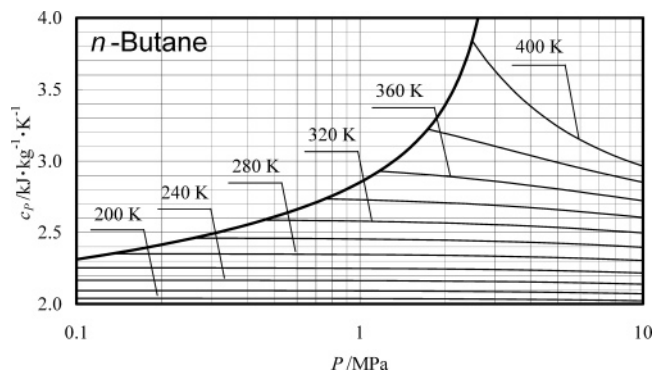


Figure 19. Pressure dependence of the isobaric heat capacity for *n*-butane derived from eq 8.

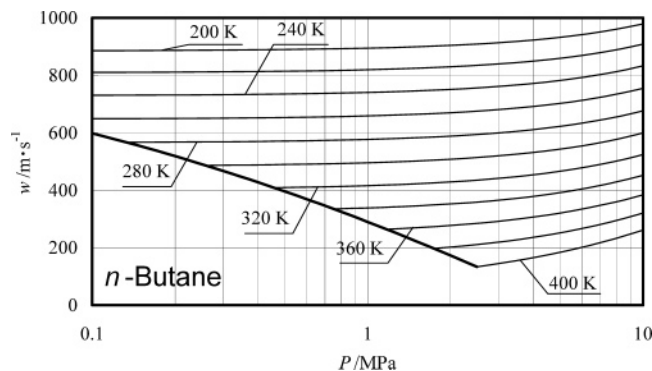


Figure 20. Pressure dependence of the speed of sound for *n*-butane derived from eq 8.

present EoS is confirmed to be reasonable by examining the behavior of these derived properties.

Conclusions

Hydrocarbon refrigerants are expected to be promising alternatives for halogenated hydrocarbon refrigerants that have a large global warming potential. Equations of state (EoS) for these three hydrocarbons have recently been updated but are still based on relatively old measured data. In the present study, a total of 192, 128, and 110 liquid PVT properties were obtained for propane, *n*-butane, and isobutane, respectively. From the comparison of these data with the EoS, a slight systematic density deviation was found. Further accurate measurements for PVT properties are expected in order to develop reliable thermodynamic models for these hydrocarbons. A modified Tait EoS proposed by Sato in 1981 was applied to correlate the present data. The EoS was exclusively fitted to the present data, and it represents these input data excellently within $\pm 0.1\%$ as far as its effective range (i.e., 200 K to $0.95T_c$) up to 20 MPa. The thermodynamic property surface of the EoS was examined in terms of essential derived properties such as heat capacities, speed of sound, and isothermal compressibility.

Acknowledgment

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