

# Density, Refractive Index, Speed of Sound at 298.15 K, and Vapor–Liquid Equilibria at 101.3 kPa for Binary Mixtures of Methanol + 2-Methyl-1-butanol and Ethanol + 2-Methyl-1-butanol

José M. Resa,\* Cristina González, and José M. Goenaga

Departamento de Ingeniería Química, Universidad del País Vasco, Apartado 450, 01006, Vitoria, Spain

Densities, refractive indices, and speeds of sound at 298.15 K and isobaric vapor–liquid equilibria (VLE) data at 101.3 kPa were reported for the binary mixtures methanol + 2-methyl-1-butanol and ethanol + 2-methyl-1-butanol. Excess molar volumes, refractive index deviations, and changes of speed of sound on mixing were calculated from the measurement results that were fitted with Redlich–Kister polynomials. VLE experimental data were tested for thermodynamic consistency by means of a modified Dechema test and were demonstrated to be consistent. The activity coefficients were correlated with the Margules, van Laar, UNIQUAC, NRTL, and Wilson equations. The ASOG model also was used for prediction.

## Introduction

This work is part of a research project whose objective is to measure thermodynamic properties and concentration in equilibrium for binary systems involved in wine distillation processes for further simulation.<sup>1,2</sup> In this process, multicomponent mixtures are seen. The main components are water and ethanol, and several minor compounds such as alcohols, aldehydes, and acetates are also present. These minor compounds are called congeners. For modeling and process simulation in which mixtures appear, binary data are needed. By this, it is very important to have available vapor–liquid equilibrium (VLE) data of mixtures formed by water + congeners, ethanol + congeners, and congeners + congeners. From the measurements, parameters of some classic correlations such as Wilson, NRTL, and UNIQUAC would be calculated, and results can be applied to study the distillation of wine.

## Experimental Section

**Materials.** Methanol (99.8 mol %) was supplied by Fluka. Ethanol (99.5 %) was supplied by Panreac. Both were used without further purification. 2-Methyl-1-butanol (99 mol %) from Aldrich was purified by distillation in a laboratory column of 100 plates; the purity of the material was checked by gas liquid chromatography and was higher than 99.6 %. All products were degassed using ultrasound and dried on molecular sieves (pore diameter 3.10(E–10) m from Fluka) before use. Densities, refractive indexes, and normal boiling points of the pure substances are given in Table 1 and compared with literature values of Riddick et al.<sup>3</sup> and Tojo et al.<sup>4</sup>

**Apparatus and Procedure.** The still used to measure VLE data was a dynamic recirculating apparatus described by Resa et al.<sup>5</sup> The equilibrium temperature was measured with a digital platinum 100  $\Omega$  resistance thermometer with an accuracy of  $\pm 0.01$  K. For the pressure measurement, a digital manometer regulator (Divatron DT1 model) manufactured by Leybold with an accuracy of  $\pm 0.1$  kPa was used. Both vapor- and liquid-phase compositions for the

two systems were determined by densimetry, refractometry, and speed of sound. Densities were measured at 298.15 K by using an Anton Paar DMA 58 vibrating tube densimeter with an accuracy of  $\pm 0.00001$  g·cm<sup>-3</sup>, which had been calibrated at atmospheric pressure with twice distilled water and dry air. The temperature of the densimeter was maintained at 298.15 K with a precision of  $\pm 0.01$  K by means of a semiconductor Peltier element and measured by a calibrated platinum resistance thermometer. Refractive indices were measured with a Mettler RE50 refractometer with an accuracy of  $\pm 0.00001$ , and temperature was controlled like the densimeter, with a temperature precision of  $\pm 0.01$  K. Speeds of sound were measured with an Anton Paar DSA 48 sound analyzer with an accuracy of  $\pm 0.1$  m·s<sup>-1</sup>, and temperature was controlled by a Peltier cooler to a precision of  $\pm 0.1$  K. Prior to measurements, density-calibration, refractive index, and speed of sound curves for these systems were obtained to calculate the compositions of the vapor and liquid phases. The binary mixtures were prepared by directly weighing the constituent components with an electronic balance (Salter model ER-182A) that has an accuracy of  $\pm 0.0001$  g. Precautions were taken in order to minimize evaporation losses during storage and preparation of the solutions. The estimated uncertainty in the determination of both liquid- and vapor-phase mole fractions is  $\pm 0.001$ .

## Results and Discussion

**Density, Refractive Index, and Speed of Sound.** Table 2 lists the measured density ( $\rho$ ), refractive index ( $n_D$ ), and speed of sound ( $u$ ) data at 298.15 K with the corresponding excess molar volume ( $V^E$ ), refractive index deviation ( $\delta n_D$ ), and speed of sound deviation ( $\delta u$ ) for the binary mixtures of methanol + 2-methyl-1-butanol and ethanol + 2-methyl-1-butanol.

The excess molar volumes of binary mixtures were calculated from density measurements by applying

$$V^E = x_1 M_1 (1/\rho - 1/\rho_1) + x_2 M_2 (1/\rho - 1/\rho_2) \quad (1)$$

where  $\rho$  is the density of the mixture,  $\rho_1$  and  $\rho_2$  are the densities of the pure substances,  $M_1$  and  $M_2$  are the molar

\* Corresponding author e-mail: iqpredij@vc.ehu.es.

**Table 1. Physical Properties of Pure Compounds: Densities ( $\rho$ ) Refractive Indices ( $n_D$ ), Speeds of Sound ( $u$ ) at 298.15 K, and Normal Boiling Points ( $T_b$ )**

	$\rho/(\text{kg}\cdot\text{m}^{-3})$		$n_D$		$u/(\text{m}\cdot\text{s}^{-1})$		$T_b/\text{K}$	
	obs	lit. <sup>a</sup>	obs	lit. <sup>a</sup>	obs	lit. <sup>b</sup>	obs	lit. <sup>a</sup>
methanol	0.78714	0.78637	1.32667	1.32652	1102	1102	337.65	337.696
ethanol	0.78536	0.78493	1.35916	1.35941	1143	1142	351.50	351.44
2-methyl-1-butanol	0.81487	0.8150	1.40872	1.4086	1253	na <sup>c</sup>	401.86	401.9

<sup>a</sup> Ref 1. <sup>b</sup> Ref 4. <sup>c</sup> na, not available.

**Table 2. Densities, Refractive Indices, and Speed of Sounds for Methanol (1) + 2-Methyl-1-butanol (2) and Ethanol (1) + 2-Methyl-1-butanol (2) at 298.15 K with Excess Molar Volume ( $V^E$ ), Refractive Index Deviation ( $\delta n_D$ ), and Speeds of Sound Deviation ( $\delta u$ )**

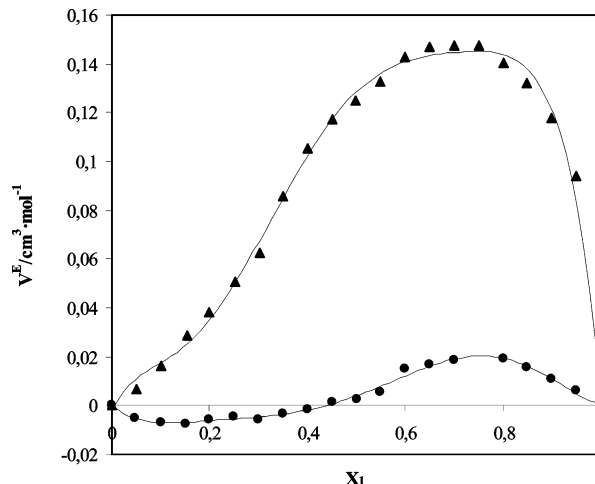
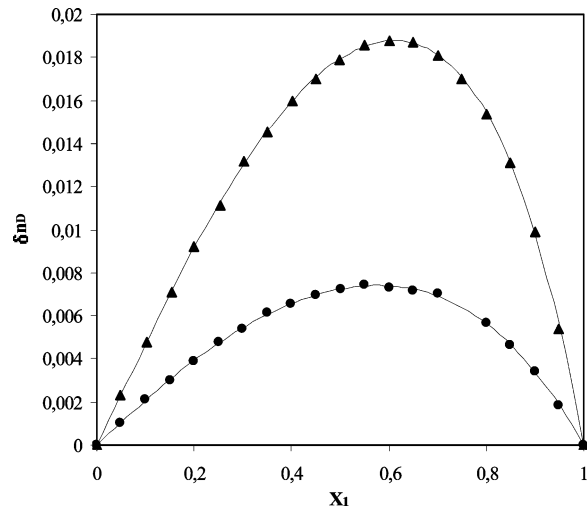
$x_1$	$\rho$		$n_D$	$\delta n_D$	$u$		$\delta u$
	$\text{g}\cdot\text{cm}^{-3}$	$\text{cm}^3\cdot\text{mol}^{-1}$			$\text{m}\cdot\text{s}^{-1}$	$\text{m}\cdot\text{s}^{-1}$	
Methanol (1) + 2-Methyl-1-butanol (2)							
0.0485	0.81430	0,007	1.40702	0.003	1250.7		4.8
0.1016	0.81363	0,016	1.40511	0.005	1246.7		8.8
0.1543	0.81290	0,029	1.40324	0.007	1242.6		12.5
0.1987	0.81222	0,038	1.40162	0.010	1238.7		15.6
0.2528	0.81135	0,051	1.39907	0.012	1233.9		18.9
0.3017	0.81050	0,062	1.39712	0.013	1229.0		21.4
0.3496	0.80949	0,086	1.39461	0.015	1223.0		22.6
0.4005	0.80836	0,106	1.39181	0.016	1217.0		24.5
0.4506	0.80725	0,117	1.38875	0.018	1210.7		25.7
0.4987	0.80612	0,125	1.38569	0.019	1204.2		26.5
0.5502	0.80484	0,133	1.38222	0.019	1197.2		27.1
0.6003	0.80340	0,143	1.37832	0.019	1188.8		26.4
0.6487	0.80191	0,147	1.37416	0.019	1180.7		25.7
0.7003	0.80027	0,147	1.36946	0.019	1171.5		24.1
0.7504	0.79844	0,147	1.36420	0.018	1162.7		23.0
0.8002	0.79650	0,140	1.35846	0.016	1151.4		19.2
0.8503	0.79435	0,132	1.35214	0.014	1142.2		17.6
0.9004	0.79196	0,118	1.34482	0.010	1131.5		14.4
0.9503	0.78939	0,094	1.33618	0.006	1120.5		11.0
Ethanol (1) + 2-Methyl-1-butanol (2)							
0.0486	0.81411	-0.005	1.40734	0.001	1247.7		1.6
0.1013	0.81323	-0.007	1.40583	0.002	1245.0		4.5
0.1523	0.81231	-0.007	1.40424	0.003	1241.4		6.4
0.1987	0.81139	-0.006	1.40277	0.004	1237.6		7.8
0.2503	0.81038	-0.005	1.40112	0.005	1233.6		9.2
0.3004	0.80933	-0.006	1.39926	0.005	1229.6		10.7
0.3486	0.80822	-0.003	1.39756	0.006	1225.3		11.7
0.4003	0.80702	-0.002	1.39549	0.007	1221.0		12.9
0.4502	0.80574	0.002	1.39341	0.007	1215.9		13.3
0.5004	0.80441	0.003	1.39120	0.007	1210.5		13.3
0.5502	0.80301	0.006	1.38899	0.007	1205.4		13.5
0.6004	0.80143	0.015	1.38636	0.007	1199.4		12.9
0.6503	0.79981	0.017	1.38373	0.007	1193.1		12.2
0.7000	0.79810	0.019	1.38109	0.007	1186.9		11.3
0.8009	0.79432	0.019	1.37475	0.006	1173.0		8.4
0.8503	0.79234	0.016	1.37134	0.005	1166.0		6.6
0.9002	0.79013	0.011	1.36758	0.003	1158.2		4.3
0.9503	0.78777	0.0059	1.36358	0.002	1150.2		1.7

masses, and  $x_1$  and  $x_2$  are the mole fractions. The uncertainty in the calculation of  $V^E$  from density measurements was estimated to be  $\pm 0.001 \text{ cm}^3\cdot\text{mol}^{-1}$ . Figure 1 illustrates the excess molar volumes of the two binary systems at 298.15 K.

The changes of refractive index ( $\delta n_D$ ) at 298.15 K from the linear additive value of the mole fraction is obtained by

$$\delta n_D = n_D - (x_1 n_{D1} + x_2 n_{D2}) \quad (2)$$

where  $n_D$  is the refractive index of the mixture, and  $n_{D1}$  and  $n_{D2}$  are the refractive indices of the pure compounds. The plot of  $\delta n_D$  versus the mole fraction  $x_1$  of the most volatile compound of each binary system is given in Figure 2.

**Figure 1.** Excess molar volumes of mixtures of  $\blacktriangle$ , methanol (1) + 2-methyl-1-butanol (2);  $\bullet$ , ethanol (1) + 2-methyl-1-butanol (2). —, Redlich–Kister fit curves at 298.15 K.**Figure 2.** Change of refractive indices on  $\blacktriangle$ , methanol (1) + 2-methyl-1-butanol (2);  $\bullet$ , ethanol (1) + 2-methyl-1-butanol (2). —, Redlich–Kister fit curves at 298.15 K.

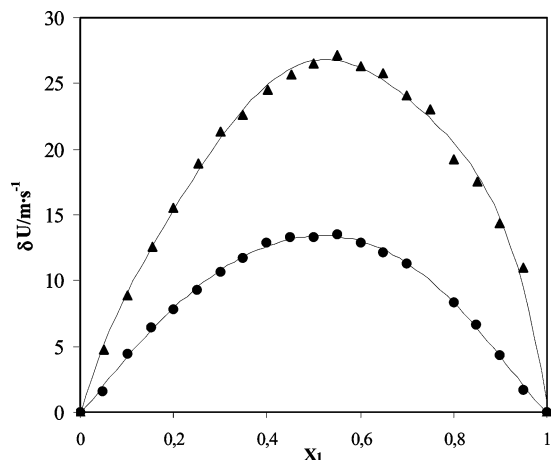
In the same way, the changes of speed of sound on mixing were calculated by

$$\delta u = u - (x_1 u_1 + x_2 u_2) \quad (3)$$

where  $u$  is the speed of sound of the mixture, and  $u_1$  and  $u_2$  are the speeds of sound of the pure compounds. The plot of  $\delta u$  versus the mole fraction  $x_1$  of the more volatile compound of each binary system is given in Figure 3.

Excess molar volumes, changes of refractive index, and speeds of sound on mixing of the binary systems were fitted to Redlich–Kister polynomials of the form:

$$(V^E \text{ or } \delta_D \text{ or } \delta u) = x_1 x_2 \sum_{k=0}^k a_k (x_1 - x_2)^k \quad (4)$$



**Figure 3.** Change of speed of sounds on mixing ▲, methanol (1) + 2-methyl-1-butanol (2); ●, ethanol (1) + 2-methyl-1-butanol (2). —, Redlich–Kister fit curves at 298.15 K.

**Table 3.** Adjustable Parameters ( $a_k$ ) with Standard Deviations ( $\sigma$ ) for Excess Molar Volumes ( $V^E$ ), Refractive Index Deviations ( $\delta n_D$ ), and Speeds of Sound Deviations ( $\delta u$ )

	$V^E/(\text{cm}^3 \cdot \text{mol}^{-1})$	$\delta n_D$	$\delta u/(\text{m} \cdot \text{s}^{-1})$
Methanol (1) + 2-Methyl-1-butanol (2)			
$a_0$	0.514	0.072	-22.2
$a_1$	0.375	0.029	5.8
$a_2$	-0.227	0.014	-0.6
$a_3$	0.541	0.010	0.0
$a_4$	0.984	-0.001	0.0
$\sigma$	0.004	0.000	8.7
Ethanol (1) + 2-Methyl-1-butanol (2)			
$a_0$	0.133	0.029	53.6
$a_1$	0.204	0.009	4.4
$a_2$	0.115	0.003	-3.4
$a_3$	0.354	0.001	-5.9
$a_4$	0.411	-0.002	-11.8
$\sigma$	0.004	0.000	0.2

where  $a_k$  are the adjustable parameters obtained by a least-squares fit method, and  $k$  is the degree of the polynomial expansion. Table 3 lists the parameters with their standard deviations ( $\sigma$ ). The coefficients  $a_k$  were used to calculate the solid curves (see Figures 1 to 3). The standard deviations ( $\sigma$ ) are defined as follows:

$$\sigma = \sqrt{\frac{\sum (Z_{\text{cal}} - Z_{\text{exp}})_i^2}{N - m}} \quad (5)$$

where  $N$  is the number of experimental data,  $m$  is the number of equation parameters, and  $Z$  is the considered property ( $V^E$ ,  $\delta n_D$ , or  $\delta u$ ).

**VLE Data.** Vapor–liquid equilibrium data ( $T$ ,  $x_1$ ,  $y_1$ ) for methanol (1) + 2-methyl-1-butanol (2) and ethanol (1) + 2-methyl-1-butanol (2) binary systems at 101.3 kPa are presented in Table 4. The  $T$ - $x_1$ - $y_1$  phase diagrams are shown in Figures 4 and 5.

The activity coefficients  $\gamma_i$  of the components were calculated from

$$\gamma_i = \frac{y_i \Phi_i P}{x_i P_i^0} \quad (6)$$

where  $x_i$  and  $y_i$  are the liquid and vapor mole fractions in equilibrium,  $\Phi_i$  is a vapor-phase correction factor,  $P$  is the total pressure, and  $P_i^0$  is the vapor pressure of pure

**Table 4.** Vapor–Liquid Equilibrium Data for for Methanol (1) + 2-Methyl-1-butanol (2) and Ethanol (1) + 2-Methyl-1-butanol (2) Systems<sup>a</sup>

$x_1$	$y_1$	$T/\text{K}$	$\gamma_1$	$\gamma_2$	$\phi_1$	$\phi_2$	$\phi_1^s$	$\phi_2^s$
Methanol (1) + 2-Methyl-1-butanol (2)								
0.000	0.000	401.58						
0.012	0.098	398.75	1.105	1.011	1.018	0.962	0.989	0.965
0.038	0.273	393.59	1.138	0.998	1.008	0.962	0.991	0.969
0.064	0.393	389.25	1.090	1.002	1.002	0.963	0.992	0.973
0.090	0.474	385.55	1.044	1.024	0.998	0.965	0.993	0.975
0.122	0.572	381.02	1.054	1.028	0.994	0.967	0.994	0.978
0.155	0.634	377.68	1.013	1.045	0.991	0.969	0.995	0.980
0.167	0.663	376.22	1.027	1.034	0.990	0.971	0.995	0.981
0.212	0.737	371.44	1.043	1.041	0.988	0.974	0.996	0.983
0.247	0.777	368.67	1.031	1.043	0.986	0.976	0.996	0.985
0.307	0.827	364.51	1.010	1.057	0.985	0.979	0.997	0.987
0.351	0.856	361.64	1.006	1.065	0.984	0.981	0.997	0.988
0.389	0.883	358.71	1.031	1.061	0.983	0.983	0.998	0.989
0.446	0.900	356.29	0.996	1.120	0.982	0.984	0.998	0.990
0.474	0.915	354.56	1.012	1.092	0.982	0.985	0.998	0.991
0.638	0.965	347.70	1.013	0.915	0.980	0.990	0.999	0.993
0.698	0.967	345.73	0.999	1.142	0.979	0.999	0.999	0.993
0.787	0.980	343.04	0.992	1.126	0.979	0.991	0.999	0.994
0.833	0.985	341.81	0.988	1.129	0.978	0.992	0.999	0.994
0.905	0.993	339.90	0.985	1.090	0.978	0.993	0.999	0.995
0.956	0.997	338.64	0.983	0.905	0.977	0.993	0.999	0.995
0.975	0.999	338.23	0.981	0.813	0.977	0.993	0.999	0.995
0.000	0.000	337.65						
Ethanol (1) + 2-Methyl-1-butanol (2)								
0.000	0.000	401.86						
0.021	0.118	398.77	1.194	1.106	0.987	0.962	0.922	0.965
0.062	0.286	393.79	1.127	1.111	0.985	0.960	0.929	0.969
0.102	0.405	389.90	1.089	1.112	0.984	0.959	0.934	0.972
0.141	0.488	386.61	1.047	1.130	0.983	0.957	0.938	0.974
0.175	0.559	383.66	1.053	1.132	0.982	0.956	0.942	0.976
0.216	0.624	380.78	1.041	1.138	0.981	0.955	0.945	0.978
0.274	0.692	377.18	1.022	1.160	0.980	0.954	0.950	0.980
0.328	0.755	373.73	1.041	1.148	0.980	0.953	0.953	0.982
0.385	0.795	371.02	1.024	1.174	0.979	0.952	0.956	0.984
0.416	0.817	369.67	1.017	1.174	0.978	0.951	0.958	0.984
0.446	0.837	368.20	1.021	1.176	0.978	0.951	0.959	0.985
0.476	0.852	366.72	1.024	1.205	0.978	0.950	0.960	0.986
0.516	0.871	365.22	1.018	1.213	0.977	0.949	0.962	0.986
0.550	0.887	363.97	1.019	1.209	0.979	0.949	0.963	0.987
0.580	0.898	362.95	1.012	1.227	0.977	0.948	0.964	0.987
0.695	0.937	359.39	1.002	1.222	0.976	0.947	0.967	0.989
0.817	0.967	355.97	0.998	1.251	0.975	0.945	0.970	0.990
0.922	0.987	353.32	0.996	1.358	0.974	0.944	0.972	0.991
0.972	0.997	352.08	1.000	1.046	0.974	0.943	0.973	0.991
0.993	0.999	351.61	1.000	1.171	0.973	0.943	0.973	0.992
1.000	1.000	351.50						

<sup>a</sup> Liquid-phase mole fraction,  $x_1$ ; vapor-phase mole fraction,  $y_1$ ; boiling temperature,  $T$ ; activity coefficients,  $\gamma_1$  and  $\gamma_2$ ; fugacity coefficients,  $\phi_1$  and  $\phi_2$ ; fugacity coefficients at saturation,  $\phi_1^s$  and  $\phi_2^s$  at 101.3 kPa.

component  $i$ . These vapor pressures were calculated from the Antoine equation:

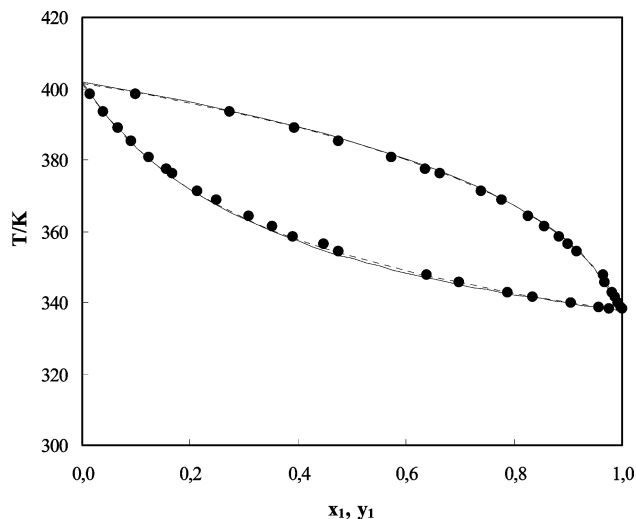
$$\log(P_i^0/\text{kPa}) = A_i - \frac{B_i}{(T/\text{K}) + C_i} \quad (7)$$

The constants  $A_i$ ,  $B_i$ , and  $C_i$  are reported in Table 5, and their values were obtained from Riddick et al.<sup>3</sup>

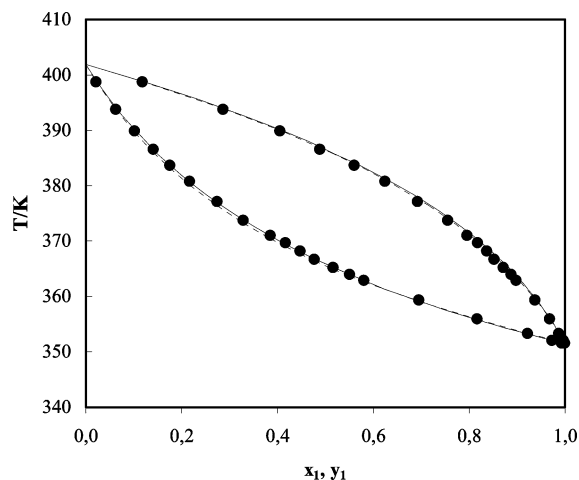
The vapor-phase correction factor is given by

$$\phi_i = \frac{\phi_i}{\phi_i^{\text{sat}}} \exp\left[-\frac{V_i(P - P_i^0)}{RT}\right] \quad (8)$$

where  $\phi_i$  is the fugacity coefficient of component  $i$  in the mixture,  $\phi_i^{\text{sat}}$  is the fugacity coefficient at saturation, and  $V_i$  is the molar volume of component  $i$  in the liquid phase.



**Figure 4.**  $T$ - $x_1$ - $y_1$  diagram for methanol (1) + 2-methyl-1-butanol (2) at 101.3 kPa: ●, experimental data; --, Wilson correlation; —, ASOG prediction.



**Figure 5.**  $T$ - $x_1$ - $y_1$  diagram for ethanol (1) + 2-methyl-1-butanol (2) at 101.3 kPa: ●, experimental data; --, Wilson correlation; —, ASOG prediction.

**Table 5. Antoine Coefficients (eq 7)**

compound	$A_i$	$B_i$	$C_i$
methanol	7.20519	1581.993	-33.439
ethanol	7.16879	1552.601	-50.731
2-methyl-1-butanol	6.19220	1195.26	-116.32

The fugacity coefficients for  $\phi_1$  and  $\phi_2$  were calculated by the expressions:

$$\ln \phi_1 = \frac{P}{RT}(B_{11} + y_2^2 \delta_{12}) \quad (9)$$

$$\ln \phi_2 = \frac{P}{RT}(B_{22} + y_1^2 \delta_{12}) \quad (10)$$

where  $P$  is the total pressure,  $T$  is the experimental temperature,  $y_1$  and  $y_2$  are the vapor mole fractions of compounds 1 and 2,  $B_{11}$  and  $B_{22}$  are the second virial coefficients of pure compounds 1 and 2, and  $\delta_{12} = 2B_{12} - B_{11} - B_{22}$ , in which  $B_{12}$  is the second cross virial coefficient.

Pitzer's correlation for the second virial coefficient was extended to mixtures by Reid et al.<sup>6</sup> to calculate  $B_{12}$  with

**Table 6. Published Parameters<sup>10</sup> Used for Calculation of Fugacity Coefficients<sup>a</sup>**

	$T_c$	$P_c$	$V_c$	$Z_c$	$\omega$
	K	Pa	$\text{m}^3 \cdot \text{kmol}^{-1}$		
methanol	512.58	8.10·E+6	0.1178	0.224	0.5656
ethanol	513.92	6.38·E+6	0.1669	0.248	0.6371
2-methyl-1-butanol	565.00	3.88·E+6	0.3270	0.270	0.6784

<sup>a</sup> Critical temperature,  $T_c$ ; critical pressure,  $P_c$ ; critical volume,  $V_c$ ; critical compression factor,  $Z_c$ ; and acentric factor,  $\omega$ , of pure compounds.

Tsonopoulos<sup>7</sup> modification for polar molecules to calculate  $B_{12}$  by

$$B_{12} = \frac{RT_{c12}}{P_{c12}}(B^0 + \omega_{12}B^1 + aT_r^{-6} - bT_r^{-8}) \quad (11)$$

where  $a$  is the polarity parameter,  $b$  is the association parameter,  $T_r$  is the reduced temperature, and  $B^0$  and  $B^1$  are functions that depend exclusively on reduced temperature that can be represented satisfactorily by

$$B^0 = 0.083 - 0.422/T_r^{1.6} \quad (12)$$

$$B^1 = 0.139 - 0.172/T_r^{4.2} \quad (13)$$

The mixing rules proposed by Prausnitz<sup>8</sup> for the calculation of  $\omega_{12}$ ,  $T_{c12}$ , and  $P_{c12}$  are

$$\omega_{12} = \frac{\omega_1 + \omega_2}{2} \quad (14)$$

where  $\omega_1$  and  $\omega_2$  are the acentric factors of compounds 1 and 2, and

$$T_{c12} = (1 - k_{ij})(T_{c1}T_{c2})^{0.5} \quad (15)$$

where  $T_{c1}$  and  $T_{c2}$  are the critical temperatures of compounds 1 and 2, and  $k_{ij}$  is the binary interaction constant proposed by Lee and Chen.<sup>9</sup> For the alcohol + alcohol mixtures,  $k_{ij} = 0.08$ .

Also

$$P_{c12} = \frac{Z_{c12}RT_{c12}}{V_{c12}} \quad (16)$$

where  $Z_{c12}$  is calculated by

$$Z_{c12} = \frac{Z_{c1} + Z_{c2}}{2} \quad (17)$$

$Z_{c1}$  and  $Z_{c2}$  are the critical compressibility factors, and  $V_{c12}$  is defined by

$$V_{c12} = \left( \frac{V_{c1}^{1/3} + V_{c2}^{1/3}}{2} \right)^3 \quad (18)$$

where  $V_{c1}$  and  $V_{c2}$  are the critical volumes of compounds 1 and 2. Values of  $P_c$ ,  $V_c$ ,  $T_c$ ,  $Z_c$ , and  $\omega$  have been obtained from the literature<sup>10</sup> and are presented in Table 6.



**Table 7. Correlation Parameters for Activity Coefficients and Average Deviation for the Studied Systems**

equation	$A_{12}$	$A_{21}$	$\Delta T/K$	$\Delta y_1$
Methanol (1) + 2-Methyl-1-butanol (2)				
Margules <sup>a</sup>	0.1190	0.2341	0.28	0.005
van Laar <sup>a</sup>	0.1213	0.2963	0.27	0.005
Wilson <sup>b</sup>	2009.02	-1116.49	0.31	0.005
NRTL <sup>c</sup> ( $\alpha_{12} = 0.30$ )	3262.01	-2014.23	0.27	0.005
UNIQUAC <sup>d</sup>	2592.50	-247.02	0.29	0.003
Ethanol (1) + 2-Methyl-1-butanol (2)				
Margules <sup>a</sup>	0.0837	0.1316	0.12	0.004
van Laar <sup>a</sup>	0.0866	0.1403	0.12	0.004
Wilson <sup>b</sup>	1303.95	-843.85	0.12	0.004
NRTL <sup>c</sup> ( $\alpha_{12} = 0.30$ )	1997.92	-1380.45	0.12	0.004
UNIQUAC <sup>d</sup>	-404.12	821.13	0.13	0.004

<sup>a</sup> Margules and van Laar constants (dimensionless). <sup>b</sup> Wilson's interaction parameters ( $J \cdot \text{mol}^{-1}$ ). <sup>c</sup> NRTL's interaction parameters ( $J \cdot \text{mol}^{-1}$ ). <sup>d</sup> UNIQUAC's interaction parameters ( $J \cdot \text{mol}^{-1}$ ).

The fugacity coefficients at saturation  $\phi_1^s$  and  $\phi_2^s$  were calculated by

$$\phi_1^s = \exp \frac{B_{11} P_1^{\text{sat}}}{RT} \quad (19)$$

$$\phi_2^s = \exp \frac{B_{22} P_2^{\text{sat}}}{RT} \quad (20)$$

The activity coefficients were correlated with the Margules,<sup>11</sup> van Laar,<sup>12</sup> Wilson,<sup>13</sup> NRTL,<sup>14</sup> and UNIQUAC<sup>15</sup> equations. To determine the constants of each model, we have used the method "VLE calc" suggested by Gess et al.<sup>16</sup> Estimation of the parameters for the equation was based on the iterative solution, using the maximum likelihood regression of the objective function ( $Q_i$ ),<sup>17</sup> with the activity coefficients obtained from the consistency test as experimental values:

$$Q_i = \sum \left( \frac{\gamma_{\text{exptl}} - \gamma_{\text{calcd}}}{\gamma_{\text{exptl}}} \right)^2 \quad (21)$$

where  $\gamma_{\text{exptl}}$  are the activity coefficients calculated from experimental data and  $\gamma_{\text{calcd}}$  are the coefficients calculated with the correlations. The parameters, the average deviation in  $T$  ( $\Delta T$ ) and the average deviation in  $y$  ( $\Delta y$ ) are listed in Table 7. Also, the ASOG<sup>18</sup> method was used to obtain predictions (see Figures 4 and 5).

The thermodynamic consistency of the experimental data was checked by means of a modified Dechema test,<sup>19</sup> where the fugacity coefficients are calculated by the method of Hayden and O'Connell<sup>20</sup> and activity coefficients are calculated by using the four-suffix Margules equation:

$$\bar{g}^E/RT = x_1 x_2 [A x_2 + B x_1 - D x_1 x_2] \quad (22)$$

with the corresponding activity coefficients

$$\ln \gamma_1 = x_2^2 [A + 2(B - A - D)x_1 + 3Dx_1^2] \quad (23)$$

$$\ln \gamma_2 = x_1^2 [B + 2(A - B - D)x_2 + 3Dx_2^2] \quad (24)$$

Parameters  $A$ ,  $B$ , and  $D$  were estimated using the error-in-variables regression maximum likelihood technique. The constraint equation for the regression was

$$F = P - \left( \frac{x_1 \gamma_1^* f_1^0}{\phi_1} + \frac{x_2 \gamma_2^* f_2^0}{\phi_2} \right) \quad (25)$$

**Table 8. Results of the Thermodynamic Consistency Test**

system	avg dev $\Delta y_1$	$A$	$B$	$D$
methanol (1) + 2-methyl-1-butanol (2)	0.003	0.2221	0.3204	0.3649
ethanol (1) + 2-methyl-1-butanol (2)	0.003	0.1167	0.1593	0.1173

Here the asterisk (\*) denotes a calculated or predicted value. An experimental value has no asterisk;  $f_1^0$  and  $f_2^0$  are the standard-state fugacities. The errors in the prediction of  $y_1$  were calculated. Predicted  $y_1^*$  values were obtained using

$$y_1^* = \frac{x_1 \gamma_1^* f_1^0}{\phi_1 P^*} \quad (26)$$

An average deviation was calculated from

$$\text{average deviation} = \frac{\sum_{i=1}^n |\Delta y_i|}{n} \quad (27)$$

Here  $\Delta y = y_1 - y_1^*$  and  $n =$  number of experimental data points. To pass the consistency test, a system must have an average deviation less than 0.01. The two systems included in this work have passed this consistency test. In Table 8, we show these results and the values the  $A$ ,  $B$ , and  $D$  of eqs 22 to 24.

## Conclusions

New vapor-liquid equilibria data not previously reported in the literature have been measured for the systems methanol + 2-methyl-1-butanol and ethanol + 2-methyl-1-butanol; as well as binary parameters, values of different correlations and necessary physical properties for modeling and simulation of wine distillation.

The ethanol + 2-methyl-1-butanol system presents a near ideal behavior, and the methanol + 2-methyl-1-butanol system presents a less ideal behavior. Correlations for both systems are very similar. The ASOG method prediction has a perfectly agreement with experimental data in both cases.

Values of excess molar volumes of the methanol + 2-methyl-1-butanol system are positive and clearly bigger than the ethanol + 2-methyl-1-butanol system due to expansive trend and bigger polarity of methanol. On the contrary, corresponding values for ethanol + 2-methyl-1-butanol are very close to zero, due to less polarity of ethanol and that the intermolecular interaction energy of the molecules is small.

In case of change of refractive indices appear positive values. The methanol + 2-methyl-1-butanol system is bigger than the ethanol + 2-methyl-1-butanol system. Finally, changes of speed of sound values are completely analogous as the change of refractive indices.

## Literature Cited

- Resa, J. M.; González, C.; Juez, M.; Ortiz de Landaluze, S. Density, refractive index, speed of sound, for mixtures of ethyl acetate with 2-butanol and 3-methyl-1-butanol. Vapor-liquid equilibrium of ethyl acetate + 3-methyl-1-butanol system. *Fluid Phase Equilib.* **2004**, *217*, 175-180.
- Resa, J. M.; González, C.; Goenaga, J. M.; Iglesias, M. Density, refractive index, speed of sound at 298.15 K and Vapor-liquid equilibria at 101.3 kPa for binary mixtures of ethyl acetate +

- 1-pentanol and ethanol + 2-methyl-1-propanol. *J. Chem. Eng. Data* **2004**, *49*, 804–808.
- (3) Riddick, J. A.; Bunger, W. B.; Sakano, T. K. *Organic Solvents*; Wiley-Interscience: New York, 1986.
- (4) Rodríguez, A.; Canosa, J.; Tojo, J. Density, refractive index, and speed of sound of binary mixtures (diethyl carbonate + alcohols) at several temperatures. *J. Chem. Eng. Data* **2001**, *46*, 1506–1515.
- (5) Resa, J. M.; González, C.; Moradillo, B.; Lanz, J. Vapour + liquid equilibria for methanol + butyl acetate, vinyl acetate + butyl acetate, methanol + isobutyl acetate and vinyl acetate + isobutyl acetate. *J. Chem. Thermodyn.* **1998**, *30*, 1207–1219.
- (6) Reid, R. C.; Prausnitz, J. M.; Poling, B. E. *The Properties of Gases and Liquids*; McGraw-Hill: New York, 1987.
- (7) Tsonopoulos, C. An empirical correlation of second virial coefficients. *AIChE J.* **1974**, *20*, 263–272.
- (8) Prausnitz, J. M. *Molecular Thermodynamics of Fluid Phase Equilibria*; Prentice Hall: Englewood Cliffs, NJ, 1969; pp 121–125.
- (9) Lee, M. J.; Chen, J. T. An improved model of second virial coefficients for polar fluids and fluid mixtures. *J. Chem. Eng. Jpn.* **1998**, *4*, 518–526.
- (10) Daubert, T. E.; Danner, R. P. *Physical and Thermodynamics Properties of Pure Chemicals. Data Compilation*; Taylor & Francis: Washington, DC, 1994.
- (11) Margules, M. S. *Akad. B. Wien. Math-Naturwiss. KI. II* **1895**, *104*, 1234–1239.
- (12) van Laar, J. J. The vapor pressure of binary mixtures. *Z. Phys. Chem.* **1910**, *72*, 723–751.
- (13) Wilson, G. M. Vapor–liquid equilibrium. XI. A new expression for the excess free energy of mixing. *J. Am. Chem. Soc.* **1964**, *86*, 127–130.
- (14) Renon, H.; Prausnitz, J. M. Estimation of parameters for the NRTL equation for excess Gibbs energies of strongly non-ideal liquid mixtures. *Ind. Eng. Chem. Process. Des. Dev.* **1969**, *8*, 413–419.
- (15) Abrams, D. S.; Prausnitz, J. M. Statistical thermodynamics of liquid mixtures: a new expression for the excess Gibbs energy of partially or completely miscible systems. *AIChE J.* **1975**, *21*, 116–128.
- (16) Gess, M. A.; Danner, R. P.; Nagvekar, M. *Thermodynamic Analysis of Vapor-Liquid Equilibria: Recommended Models and a Standard Data Base*; DIPPR, AIChE: 1991.
- (17) Patino-Leal, H.; Reilly, P. Statistical estimation of parameters in vapor–liquid equilibrium. *AIChE J.* **1982**, *28*, 580–584.
- (18) Kojima, K.; Tochigi, K. *Prediction of Vapor–Liquid Equilibria by the ASOG Method*; Kodansha Ltd.: Tokyo, 1979.
- (19) Gmehling, J.; Onken, U. *Vapor Liquid Equilibrium Data Collection, DECHEMA Chemistry Data Serie*; DECHEMA: Frankfurt, 1977; Vols. 1–8.
- (20) Hayden, J. G.; O’Connell, J. P. A generalized method for predicting second virial coefficients. *Ind. Eng. Chem. Process. Des. Dev.* **1975**, *14*, 209–216.

Received for review January 21, 2005. Accepted June 26, 2005.

JE0500330