

# Critical Properties of 1,2,2,2-Tetrafluoroethyl Trifluoromethyl Ether (HFE-227me) + Trifluoromethoxymethane (HFE-143m) and + Methyl Pentafluoroethyl Ether (HFE-245mc)

Masahiko Yasumoto,<sup>†</sup> Yuko Uchida,<sup>‡</sup> Kenji Ochi,<sup>‡</sup> Takeshi Furuya,<sup>§</sup> Atsushi Shono,<sup>†</sup> and Katsuto Otake<sup>\*,†</sup>

Department of Industrial Chemistry, Faculty of Engineering, Tokyo University of Science, Ichigaya Funakawaramachi 12-1, Shinjyuku-ku, Tokyo 162-0826, Japan, College of Science & Technology, Nihon University, Kanda-Surugadai 1-8-14, Chiyoda-ku, Tokyo 101-8308, Japan, and Nanotechnology Research Institute, National Institute of Advanced Industrial Science and Technology (AIST), Higashi 1-1-1, Tsukuba Central 5, Tsukuba, Ibaraki 305-8565, Japan

Critical properties of binary mixtures of 1,2,2,2-tetrafluoroethyl trifluoromethyl ether (HFE-227me) with two hydrofluoroethers, trifluoromethoxymethane (HFE-143m) and methyl pentafluoroethyl ether (HFE-245mc), were measured. The uncertainties were  $\pm 10$  mK in temperature,  $\pm 0.5$  kPa in pressure, and  $\pm 1.0$  kg·m<sup>-3</sup> in density. The experimental data were correlated with equations proposed by Higashi.

## Introduction

Hydrofluoroethers (HFEs) are environmentally benign compounds having zero ODP and low GWP and are expected to be the new refrigerants.<sup>1,2</sup> The Research Institute of Innovative Technology for the Earth (RITE) synthesized and evaluated about 150 HFEs.<sup>3,4</sup> Of these, trifluoromethoxymethane (CF<sub>3</sub>OCH<sub>3</sub>, HFE-143m) and pentafluoromethoxyethane (CF<sub>3</sub>CF<sub>2</sub>OCH<sub>3</sub>, HFE-245mc) were found to be possible alternatives for dichlorodifluoromethane (CCl<sub>2</sub>F<sub>2</sub>, CFC-12) and 1,2-dichloro-1,1,2,2-tetrafluoroethane (CClF<sub>2</sub>CClF<sub>2</sub>, CFC-114), respectively. Unfortunately, they are slightly combustible (ASHRAE class 2).<sup>5,6</sup> Thus, for safety reasons, the HFEs are expected to be used in binary mixtures with inflammable compounds.

The critical properties (critical temperature, pressure, and density) are the most important physical properties for the development of an equation of state to calculate and estimate the thermodynamic properties of fluids in industry. However, reliable information on the thermophysical properties of these mixtures has not been reported. In previous papers, we described the construction of an apparatus for the precise measurement of critical properties<sup>7</sup> and its application to the newly synthesized compounds and their mixtures.<sup>5,8,9</sup> In the present article, using this apparatus, we have measured the critical properties of binary mixtures of 1,2,2,2-tetrafluoroethyl trifluoromethyl ether (HFE-227me) with two HFEs, HFE-143m and HFE-245mc.

## Experimental

**Materials.** Table 1 summarizes the properties of samples used in this study. They were all supplied by RITE. The mole fraction based purities were analyzed by gas chromatography

(Hewlett-Packard, model HP-6890; thermal conductivity detector).

**Apparatus and Procedures.** The critical points of HFE-227me and its mixtures were measured by observing the behavior of the meniscus at the vapor–liquid interface in an optical cell. The apparatus used in this study is the same as that in the previous papers.<sup>5,7–10</sup> Briefly, the apparatus is composed of a rectangular-shaped optical cell (ca. 5 cm<sup>3</sup> in volume) and two variable-volume vessels to control the inner volume of the apparatus and a differential null-pressure detector. The optical cell was connected to the two variable-volume vessels and the differential null-pressure detector by a valve. The central axis of these vessels and the detector were adjusted to be at the same level. They were immersed in a constant temperature oil bath. The temperature of the oil bath was controlled to within  $\pm 3$  mK in the range of (300 to 450) K. Under these conditions, the uncertainty in the critical temperature was estimated to be  $\pm 10$  mK. The uncertainty in pressure was estimated to be less than  $\pm 0.5$  kPa.

In experiments, critical properties were measured by the appearance and disappearance of the meniscus at the critical density with changing temperature, whereas the density was maintained at the critical value by the two variable-volume vessels.

After the critical property measurements, the samples inside the optical cell and the null-pressure detector were trapped in a cold trap separately and weighed. The critical density was then determined from the mass of the sample and the known internal volume of the optical cell. The composition of the samples in the null-pressure detector and the optical cell was analyzed by gas chromatography. The uncertainties in the density and the mole fractions both in the optical cell and in the null-pressure gauge were  $\pm 1.0$  kg·m<sup>-3</sup> and  $\pm 0.5$  %, respectively.

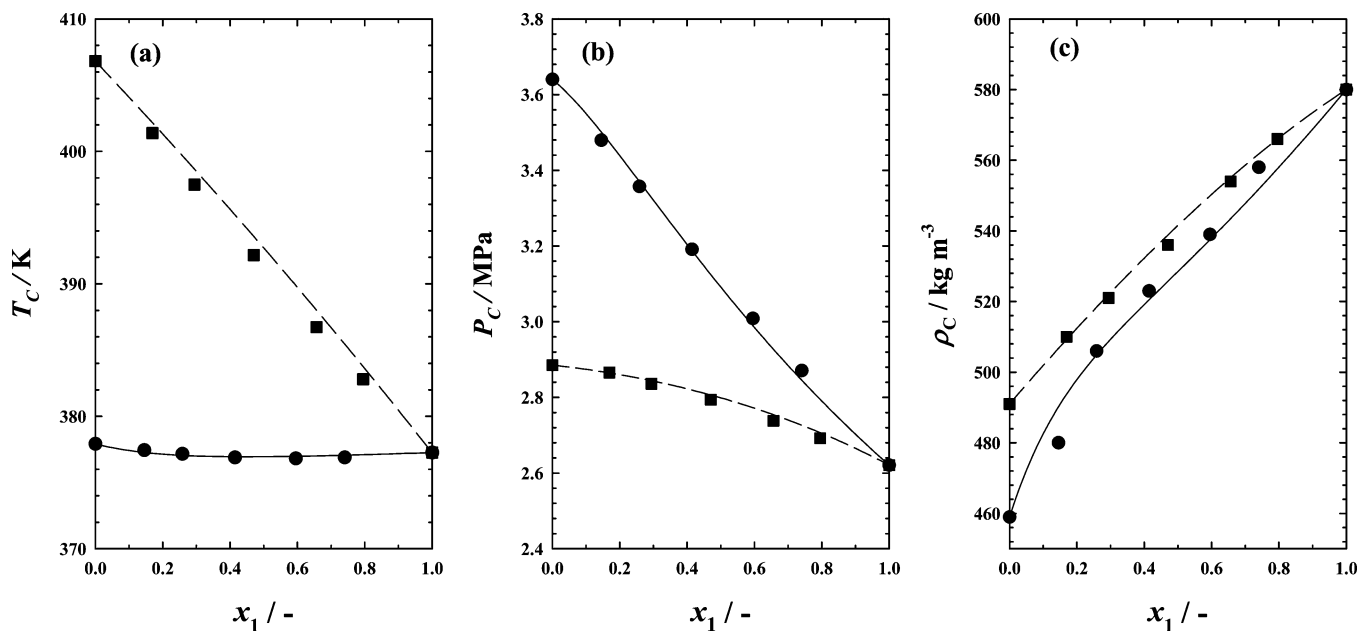
A detailed description of the experimental apparatus and procedures including the sample preparation were given in the previous papers.<sup>5,7–10</sup>

\* Corresponding author. Phone/Fax: +81-3-5228-8052. E-mail: k-otake@ci.kagu.tus.ac.jp.

<sup>†</sup> Tokyo University of Science.

<sup>‡</sup> Nihon University.

<sup>§</sup> National Institute of Advanced Industrial Science and Technology (AIST).



**Figure 1.** Critical properties of the binary mixtures of HFE-227me (1) and HFEs (2). (a) Critical temperature, (b) critical pressure, and (c) critical density for: ●, HFE-143m; ■, HFE-245mc. Lines are the correlated results of eqs 1 to 6: —, HFE-143m; ---, HFE-245mc.

**Table 1.** Compounds Used in This Study

| sample code<br>(molecular formula)                               | name  | CAS No.    | purity | boiling point<br>K | $T_C$<br>K    | $P_C$<br>MPa   | $\rho_C$<br>kg·m <sup>-3</sup> | ref       |
|--|---|------------|--------|--------------------|---------------|----------------|--------------------------------|-----------|
| HFE-143m<br>(CF <sub>3</sub> OCH <sub>3</sub> )                  | trifluoromethoxymethane                           | 421-14-7   | 99.9   | 249.15             | 377.92 ± 0.01 | 3.640 ± 0.0005 | 459 ± 1.0                      | 5         |
| HFE-227me<br>(CF <sub>3</sub> CHFOCF <sub>3</sub> )              | 1,2,2,2-tetrafluoroethyl<br>trifluoromethyl ether | 2356-62-9  | 99.9   | 263.41             | 377.26 ± 0.01 | 2.621 ± 0.0005 | 580 ± 1.0                      | this work |
| HFE-245mc<br>(CF <sub>3</sub> CF <sub>2</sub> OCH <sub>3</sub> ) | methylpentafluoroethylether                       | 22410-44-2 | 99.9   | 278.66             | 406.82 ± 0.01 | 2.885 ± 0.0005 | 491 ± 1.0                      | 8         |

**Correlation.** Critical data measured in this study were correlated by equations proposed by Higashi:<sup>11,12</sup>

$$T_{Cm} = \theta_1 T_{C1} + \theta_2 T_{C2} + 2\theta_1\theta_2\Delta_T \quad (1)$$

$$V_{Cm} = \theta_1 V_{C1} + \theta_2 V_{C2} + 2\theta_1\theta_2\Delta_V \quad (2)$$

$$P_{Cm} = \theta_1 P_{C1} + \theta_2 P_{C2} + 2\theta_1\theta_2\Delta_P \quad (3)$$

$$V_{Cm} = M_m / \rho_{Cm} \quad (4)$$

$$M_m = x_1 M_1 + (1 - x_1) M_2 \quad (5)$$

$$\theta_i = \frac{x_i V_{Ci}^{2/3}}{\sum_{j=1}^2 x_j V_{Cj}^{2/3}} \quad i = 1, 2 \quad (6)$$

where  $T_{Ci}$ ,  $V_{Ci}$ , and  $P_{Ci}$  are the critical temperature, critical volume, and critical pressure of component  $i$ , respectively;  $x$  is the mole fraction;  $M_i$  is the molecular weight of component  $i$ ;  $\vartheta_i$  is the surface ratio of component  $i$  given by eq 6; and  $\Delta_T$ ,  $\Delta_V$ , and  $\Delta_P$  are the fitting properties for critical temperature, volume, and pressure, respectively. Subscript m means mixture.

## Results and Discussion

**Critical Properties of Mixtures.** Figure 1 shows the critical loci of the two binary systems investigated in this study. Numerical values are tabulated in Tables 2 and 3. Similar to the mixtures previously reported,<sup>5,8</sup> the critical density data

**Table 2.** Critical Properties of HFE-227me (1) + HFE-143m (2) Binary Systems

| $x_1^a$ | $T_C$  | $P_C$ | $\rho_C$           | $x_1^b$   | $x_1^c$   |
|---------|--------|-------|--------------------|---|---|
|         | K      | MPa   | kg·m <sup>-3</sup> | (optical cell<br>base deviation/%) <sup>d</sup> | (optical cell<br>base deviation/%) <sup>e</sup> |
| 0       | 377.92 | 3.640 | 459                | 0.0000  | 0.0000  |
| 0.1455  | 377.45 | 3.480 | 480                | 0.1437 (1.24)                                   | 0.1441 (0.96)                                   |
| 0.2585  | 377.16 | 3.357 | 506                | 0.2578 (0.27)                                   | 0.2585 (0.00)                                   |
| 0.4147  | 376.89 | 3.191 | 523                | 0.4091 (1.35)                                   | 0.4151 (-0.10)                                  |
| 0.5954  | 376.82 | 3.009 | 539                | 0.5932 (0.37)                                   | 0.5948 (0.10)                                   |
| 0.7403  | 376.89 | 2.871 | 558                | 0.7378 (0.34)                                   | 0.7393 (0.14)                                   |
| 1       | 377.26 | 2.621 | 580                | 1.0000  | 1.0000  |
|         |        | AAD/% |                    | 0.71  | 0.26  |

<sup>a</sup> Mole fraction in the optical cell. <sup>b</sup> Mole fraction calculated from the mass ratio. <sup>c</sup> Mole fraction in the null-pressure detector and variable-volume vessels. <sup>d</sup> Deviation =  $(x_{\text{optical cell}} - x_{\text{feed}})/x_{\text{optical cell}}$ . <sup>e</sup> deviation =  $(x_{\text{optical cell}} - x_{\text{null-pressure detector}})/x_{\text{optical cell}}$ .

showed a wider spread compared with the critical temperature and pressure. The larger the difference in boiling point and critical temperature, the wider the data spread. This is presumably due to the characteristics of the critical point where the density changes sharply with only minute changes in temperature and/or pressure.

From the tables, it is also clear that there are composition differences between samples recovered from the optical cell and the null pressure detector. The larger the boiling point and critical temperature difference, the larger the average absolute deviation (AAD) of the composition. As reported previously,<sup>5,8</sup> this fact suggests that there was a temperature difference between the optical cell and the null pressure detector. However,

**Table 3. Critical Properties of HFE-227me (1) + HFE-245mc (2) Binary Systems**

| $x_1^a$ | $T_C$  | $P_C$ | $\rho_C$                      | $x_1^b$   | $x_1^c$   |
|---------|--------|-------|-------------------------------|---|---|
|         | K      | MPa   | $\text{kg}\cdot\text{m}^{-3}$ | (optical cell<br>base deviation/%) <sup>d</sup> | (optical cell<br>base deviation/%) <sup>e</sup> |
| 0.0000  | 406.82 | 2.885 | 491                           | 0.0000  | 0.0000  |
| 0.1694  | 401.38 | 2.866 | 510                           | 0.1715 (-1.24)                                  | 0.1710  |
| 0.2941  | 397.49 | 2.836 | 521                           | 0.2578 (-1.84)                                  | 0.2948  |
| 0.4706  | 392.17 | 2.794 | 536                           | 0.4753 (-1.00)                                  | 0.4715  |
| 0.6565  | 386.73 | 2.738 | 554                           | 0.6592 (-0.41)                                  | 0.6587  |
| 0.7952  | 382.80 | 2.692 | 566                           | 0.7965 (-0.16)                                  | 0.7948  |
| 1.0000  | 377.26 | 2.621 | 580                           | 1.0000  | 1.0000  |
|         |        | AAD/% |                               | 0.93  | 0.35  |

<sup>a</sup> Mole fraction in the optical cell. <sup>b</sup> Mole fraction calculated from the mass ratio. <sup>c</sup> Mole fraction in the null-pressure detector and variable-volume vessels. <sup>d</sup> Deviation =  $(x_{\text{optical cell}} - x_{\text{feed}})/x_{\text{optical cell}}$ . <sup>e</sup> Deviation =  $(x_{\text{optical cell}} - x_{\text{null-pressure detector}})/x_{\text{optical cell}}$ .

**Table 4. Correlated Results**

| system                | parameters               | AAD/% |
|-----------------------|--------------------------|-------|
| HFE-227ea + HFE-143m  | $\Delta_T = -1.2005$     | 0.04  |
|                       | $\Delta_p = 0.3441$      | 0.53  |
|                       | $\Delta_\rho = -40.8037$ | 0.84  |
| HFE-227ea + HFE-245mc | $\Delta_T = -0.0887$     | 0.00  |
|                       | $\Delta_p = 0.0786$      | 0.06  |
|                       | $\Delta_\rho = -4.9893$  | 0.12  |

as the AADs are smaller than 1 % for the two systems investigated, there will be only minor effects on the critical property measurements.

**Correlation of the Critical Properties.** The correlated results are shown as lines in Figure 1 and are summarized in Table 4. As shown in the table, the AADs of the critical properties are less than  $\pm 1$  %. The AAD of the critical density is larger than that of critical temperature as described above.

## Conclusion

We have measured the critical properties of binary mixtures of HFE-227me with two hydrofluoroethers, HFE-143m and HFE-245mc, with uncertainties of  $\pm 10$  mK in temperature,  $\pm 0.5$  kPa in pressure, and  $\pm 1.0$   $\text{kg}\cdot\text{m}^{-3}$  in density. The data spread in the critical density was larger than that of critical temperature and pressure data. This is presumably due to the difficulty in measuring the density close to the critical point where it changes sharply with only minimal changes in temperature and pressure.

The experimental results were correlated with equations proposed by Higashi.<sup>11,12</sup> The maximum average absolute deviation was less than 1 % for all critical properties. A minute

composition difference less than 1 % was observed between the optical cell and the null-pressure detector for both the binary systems.

## Acknowledgment

We thank members of the Research Institute of Innovative Technology for the Earth (RITE), Tsukuba, for their help. Further, we are grateful to our technician Mr. Aso, for his help in the construction of the optical cell and the variable-volume vessels.

## Literature Cited

- (1) Sekiya, A.; Misaki, S. The potential of hydrofluoroethers to replace CFCs, HCFCs, and PFCs. *J. Fluorine Chem.* **2000**, *101*, 215–221.
- (2) Ravishankara, A. R.; Tunipseed, A. A.; Jensen, N. R.; Barone, S.; Mills, M.; Howard, C. J.; Solomon, S. Do Hydrofluorocarbons Destroy Stratospheric Ozone? *Science* **1994**, *263*, 71–75.
- (3) RITE *Survey of Alternative Methods and Molecular Design of New Candidate Compounds*; 1996–2002.
- (4) RITE *Development of an Advanced Refrigerant for Compression Heat Pumps*; 1990–1995.
- (5) Uchida, Y.; Yasumoto, M.; Yamada, Y.; Ochi, K.; Furuya, T.; Otake, K. Critical Properties of Four HFE + HFC Binary Systems: Trifluoromethoxyethane (HFE-143m) + Pentafluoroethane (HFC-125), + 1,1,1,2-Tetrafluoroethane (HFC-134a), + 1,1,1,2,3,3,3-Heptafluoropropane (HFC-227ea), and + 1,1,1,2,3,3,3-Hexafluoropropane (HFC-236ea). *J. Chem. Eng. Data* **2004**, *49*, 1615–1621.
- (6) Sekiya, A.; Yamada, Y. Perspective of the development of new generation refrigerants. *Koatsu-gasu* **2001**, *38*, 27–31.
- (7) Yasumoto, M.; Yamada, Y.; Murata, J.; Urata, S.; Otake, K. Critical Parameters and Vapor Pressure Measurements of Hydrofluoroethers at High Temperatures. *J. Chem. Eng. Data* **2003**, *48*, 1368–1379.
- (8) Otake, K.; Uchida, Y.; Yasumoto, M.; Yamada, Y.; Furuya, T.; Ochi, K. Critical Parameters Measurements of Four HFE + HFC Binary Systems: Pentafluoromethoxyethane (HFE-245Mc) + Pentafluoroethane (HFC-125), + 1,1,1,2-Tetrafluoroethane (HFC-134a), + 1,1,1,2,3,3,3-Heptafluoropropane (HFC-227ea), and + 1,1,1,2,3,3-Hexafluoropropane (HFC-236ea). *J. Chem. Eng. Data* **2004**, *49*, 1643–1647.
- (9) Otake, K.; Yasumoto, M.; Yamada, Y.; Murata, J.; Urata, S. Critical Parameters and Vapor Pressure Measurements of Potential Replacements for Chlorofluorocarbons-Four Hydrofluoroketones and a Hydrofluoroamine. *J. Chem. Eng. Data* **2003**, *48*, 1380–1383.
- (10) Yasumoto, M.; Uchida, Y.; Ochi, K.; Furuya, T.; Otake, K. Critical Properties of Three Dimethyl Ether Binary Systems: Dimethyl Ether (RE-170) + Propane (HC-290), Butane (HC-600), and 2-Methyl Propane (HC-600A). *J. Chem. Eng. Data* **2005**, *50*, 596–602.
- (11) Higashi, Y. Vapor-Liquid Critical Surface of Ternary HFC-32(CH<sub>2</sub>F<sub>2</sub>) + HFC-125(CF<sub>3</sub>CHF<sub>2</sub>) + HFC-134a(CF<sub>3</sub>CH<sub>2</sub>F). *Int. J. Thermophys.* **1999**, *20*, 1485.
- (12) Higashi, Y. Vapor-Liquid Equilibria, Coexistence Curve, and Critical Locus for Difluoromethane + Pentafluoroethane (R-32 + R-125). *J. Chem. Eng. Data* **1997**, *42*, 1269–1273.

Received for review March 7, 2007. Accepted May 31, 2007. This work was financially supported by the New Energy and Industrial Technology Development Organization (NEDO).

JE700123Q