# Densities, Isothermal Compressibilities, and Isobaric Thermal Expansivities of Hexan-2-ol, Octan-1-ol, and Decan-1-ol from (313 to 363) K and Pressures up to 22 MPa 

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#### Abstract

Compressed liquid densities of hexan-2-ol, octan-1-ol, and decan-1-ol were measured from (313 to 363) K and pressures up to 22 MPa . A vibrating tube densimeter was used to obtain the experimental densities. The uncertainty is estimated to be better than $\pm 0.20 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$ for the experimental compressed liquid densities in the whole range of reported data. The experimental data were correlated using a short volume explicit equation of 5 parameters and the 11-parameter Benedict-Webb-Rubin-Starling equation of state (BWRS EoS). Comparisons with literature data were made for octan-1-ol and decan-1-ol. Densities of hexan-2-ol at high pressure were not found in the literature. Isothermal compressibilities and isobaric thermal expansivities were calculated using the 5 -parameter equation.


## Introduction

Compressed liquid densities of 1 -alcohols and their corresponding isomers are of interest in the chemical industry. ${ }^{1-8}$ Alcohols are used in a wide range of industrial applications involving hydrocarbon or petroleum fluids. ${ }^{1}$ For example, they are used as cosurfactants in oil-in-water emulsions, ${ }^{2}$ as additives in gasoline to reduce pollution effect, ${ }^{3}$ as inhibitors to prevent the precipitation of gas hydrates in pipelines, ${ }^{4}$ and as cosolvent in supercritical fluid technology. ${ }^{5-8}$ This last application has been used from the extraction of valuable products from natural products. ${ }^{9}$ The use of mixtures composed by a supercritical fluid and a liquid solvent is commonly used to manipulate the solubility and selectivity of the supercritical fluid. ${ }^{5-8}$ To study and understand the performance of these fluids under operating conditions, experimental property measurements of pure compound and mixtures can offer valuable information from a modeling and fundamental point of view. One of these properties is the density, which is required in many engineering disciplines and to obtain other thermophysical properties. The present work is part of a systematic study ${ }^{10-15}$ to obtain density data of alcohols and $\mathrm{CO}_{2}+$ alcohol mixtures having as the main goal the development of supercritical fluid technology, such as the extraction of capsaicin from Capsicum annum. ${ }^{16}$ Extensive reviews of published density data sets for 1 -alcohols and 2-alcohols at elevated pressures were made by Cibulka et al. ${ }^{17,18}$ Their review covers papers up to $1993{ }^{17}$ for 1-alcohols and up to $1997^{18}$ for 2-alcohols. The characteristics of the different sets of data reported in the literature ${ }^{19-30}$ covering papers published up to now for octan-1-ol and decan-1-ol are listed in Table 1. No experimental data were found for hexan-2-ol at high pressure. The experimental measurements obtained in this work are correlated using a short empirical equation ${ }^{31-32}$ and the Benedict-Webb-Rubin-Starling equation of state (BWRS EoS). ${ }^{33}$ Comparisons with literature data were made using density values calculated from the 5-parameter equation using

[^0]the parameters fitted to our experimental data. Our density measurements were also compared with the correlations for octan-1-ol and decan-1-ol reported by Cibulka and Zikova. ${ }^{17}$ The isothermal compressibility and isobaric thermal expansion are determined using the 5 -parameter equation with the parameters obtained for each alcohol studied in this work.

## Experimental Section

Materials. Hexan-2-ol $\left(\mathrm{C}_{6} \mathrm{H}_{14} \mathrm{O}, 102.17 \mathrm{~g} \cdot \mathrm{~mol}^{-1}\right.$, Chemical Abstracts Service Registry No. (CASRN) 626-93-7) was from Aldrich (U.S.A.) with a stated purity of $x=0.99$. Octan-1-ol $\left(\mathrm{C}_{8} \mathrm{H}_{18} \mathrm{O}, 130.23 \mathrm{~g} \cdot \mathrm{~mol}^{-1}\right.$, CASRN 111-87-5) was from Aldrich with a stated purity better than $x=0.99$. Decan-1-ol $\left(\mathrm{C}_{10} \mathrm{H}_{22} \mathrm{O}\right.$, $158.28 \mathrm{~g} \cdot \mathrm{~mol}^{-1}$, CASRN $112-30-1$ ) was from Aldrich with a stated purity of $x=0.99$. The reference fluids for the calibration of the vibrating tube densimeter were water and nitrogen. Water was HPLC grade and was from Aldrich with a stated purity of $x=0.9995$. Nitrogen was chromatographic grade with a certified volume fraction purity of 0.99998 , and it was from Air-Products Infra (México). The three alcohols were stored over a molecular sieve of $3 \AA$ to avoid any moisture. The purities of the three alcohols samples were tested using a gas chromatograph (HP 5890 series II) fitted with a flame ionization detector and a $0.9144 \mathrm{~m} \times 0.003175 \mathrm{~m}$ diameter column packed with Chromosorb 101. After drying and distillation of the alcohols, the purities of hexan-2-ol, octan-1-ol, and decan-1-ol were $x=$ $0.994,0.995$, and 0.993 , respectively. Liquid compounds were degassed under vacuum and vigorous stirring before they were used to perform density measurements.

Apparatus and Procedure. Densities were measured with an Anton Paar DMA 60/512P vibrating tube densimeter (VTD). The full scale in temperature is from ( 263.15 to 423.15 ) K and in pressure from ( 0 to 70 ) MPa. The manufacturer specifications about resolution, repeatability, and uncertainty of density are $1 \cdot 10^{-6}, 1 \cdot 10^{-5}$, and $1 \cdot 10^{-4} \mathrm{~g} \cdot \mathrm{~cm}^{-3}$. The VTD requires build and setup of special peripherals. In our case, it was built to determine densities from ( 313 to 363 ) K and pressures up to 25 MPa . Details of the apparatus and experimental procedure

Table 1. Characteristics of Density Data Sets Reported in the Literature for Octan-1-ol and Decan-1-ol at High Pressure

| reference | $N_{\text {p }}$ | $T_{\text {min }} / \mathrm{K}$ | $T_{\text {max }} / \mathrm{K}$ | $P_{\text {min }} / \mathrm{MPa}$ | $P_{\text {max }} / \mathrm{MPa}$ | sample purity/\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| octan-1-ol |  |  |  |  |  |  |
| Apaev et al. ${ }^{19}$ | 138 | 283.15 | 623.15 | 5.0 | 78.8 | 99.62 |
| Altunin and Konikevich ${ }^{20}$ | 13 | 298.15 | 298.15 | 0.5 | 200.0 |  |
| Matsuo and Makita ${ }^{21}$ | 34 | 298.15 | 348.15 | 0.1 | 40.2 | 97 |
| Uosaki et al. ${ }^{22}$ | 4 | 298.15 | 298.15 | 50.0 | 200.0 |  |
| Garg et al. ${ }^{23}$ | 50 | 323.15 | 373.15 | 0.1 | 10.0 | >99.5 |
| Lee et al. ${ }^{24}$ | 24 | 298.15 | 338.15 | 5.0 | 30.0 |  |
| Dzida ${ }^{25}$ | 66 | 293.15 | 318.15 | 0.1 | 50 | 99 |
| decan-1-ol |  |  |  |  |  |  |
| Kuss ${ }^{26}$ | 22 | 298.15 | 353.15 | 19.60 | 137.30 |  |
| Mamedov et al. ${ }^{27}$ | 42 | 283.00 | 473.00 | 9.80 | 147.00 |  |
| Shelkovenko et al. ${ }^{28}$ | 75 | 292.29 | 573.30 | 1.09 | 49.14 | 98 |
| Matsuo and Makita ${ }^{21}$ | 28 | 298.15 | 348.15 | 1.00 | 40.20 | >99 |
| Apaev and Gylmanov ${ }^{29}$ | 112 | 298.15 | 623.15 | 5.00 | 78.80 | 98.2 |
| Shakverdiev et al. ${ }^{30}$ | 49 | 448.15 | 573.15 | 0.16 | 58.41 | 99 |
| Dzida ${ }^{25}$ | 47 | 293.15 | 318.15 | 0.1 | 70 | 99 |

Table 2. $(p, \rho, T)$ Data of Hexan-2-ol at Six Different Temperatures

| $T / \mathrm{K}=313.13$ |  | $T / \mathrm{K}=323.09$ |  | $T / \mathrm{K}=333.04$ |  | $T / \mathrm{K}=342.98$ |  | $T / \mathrm{K}=352.86$ |  | $T / \mathrm{K}=362.73$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |
| 1.010 | 799.26 | 1.037 | 791.00 | 1.055 | 782.56 | 1.032 | 774.05 | 1.053 | 765.06 | 1.075 | 754.97 |
| 2.006 | 800.05 | 2.000 | 791.79 | 2.007 | 783.43 | 2.015 | 775.01 | 2.014 | 766.05 | 2.006 | 756.02 |
| 2.999 | 800.83 | 3.010 | 792.63 | 3.005 | 784.28 | 3.012 | 775.95 | 3.019 | 767.09 | 3.018 | 757.16 |
| 4.008 | 801.59 | 4.029 | 793.48 | 4.007 | 785.21 | 4.017 | 776.87 | 4.033 | 768.08 | 4.034 | 758.26 |
| 4.999 | 802.35 | 5.004 | 794.27 | 5.015 | 786.06 | 5.013 | 777.79 | 4.996 | 769.01 | 5.016 | 759.29 |
| 5.986 | 803.12 | 6.020 | 795.10 | 6.009 | 786.93 | 6.012 | 778.72 | 6.006 | 770.06 | 6.066 | 760.41 |
| 7.000 | 803.86 | 7.007 | 795.84 | 7.006 | 787.77 | 7.025 | 779.62 | 7.013 | 771.02 | 6.998 | 761.37 |
| 8.010 | 804.64 | 8.009 | 796.68 | 7.998 | 788.61 | 8.000 | 780.47 | 8.004 | 771.95 | 8.041 | 762.44 |
| 9.026 | 805.38 | 9.017 | 797.48 | 9.006 | 789.47 | 9.000 | 781.35 | 9.035 | 772.93 | 9.014 | 763.43 |
| 10.004 | 806.09 | 10.003 | 798.25 | 10.004 | 790.32 | 9.996 | 782.25 | 10.009 | 773.84 | 10.001 | 764.37 |
| 11.005 | 806.84 | 11.001 | 799.00 | 11.007 | 791.11 | 11.020 | 783.12 | 11.007 | 774.75 | 11.026 | 765.39 |
| 12.001 | 807.56 | 12.000 | 799.77 | 12.012 | 791.93 | 11.999 | 783.92 | 12.007 | 775.66 | 12.000 | 766.35 |
| 13.010 | 808.28 | 13.021 | 800.56 | 13.003 | 792.72 | 12.996 | 784.76 | 12.999 | 776.54 | 13.010 | 767.31 |
| 14.002 | 808.98 | 14.001 | 801.30 | 14.008 | 793.51 | 14.007 | 785.60 | 14.012 | 777.47 | 13.999 | 768.28 |
| 14.998 | 809.67 | 15.002 | 802.00 | 15.005 | 794.30 | 15.003 | 786.41 | 15.010 | 778.33 | 15.006 | 769.21 |
| 16.001 | 810.39 | 16.000 | 802.74 | 16.001 | 795.06 | 16.005 | 787.17 | 16.003 | 779.21 | 16.006 | 770.12 |
| 17.006 | 811.08 | 17.004 | 803.48 | 17.006 | 795.85 | 17.002 | 787.98 | 17.002 | 780.07 | 17.005 | 771.02 |
| 18.000 | 811.70 | 18.008 | 804.21 | 18.010 | 796.61 | 18.010 | 788.76 | 18.017 | 780.92 | 18.000 | 771.92 |
| 19.005 | 812.39 | 19.001 | 804.90 | 19.002 | 797.35 | 19.005 | 789.49 | 19.005 | 781.75 | 19.003 | 772.82 |
| 20.015 | 813.10 | 20.011 | 805.62 | 20.000 | 798.08 | 20.010 | 790.27 | 20.014 | 782.58 | 20.017 | 773.70 |
| 21.029 | 813.74 | 21.003 | 806.31 | 21.000 | 798.82 | 21.006 | 791.00 | 21.013 | 783.39 | 21.006 | 774.56 |
| 22.004 | 814.40 | 22.004 | 807.01 | 22.004 | 799.56 | 22.005 | 791.75 | 22.010 | 784.18 | 22.010 | 775.42 |

used in this work have been described previously. ${ }^{10-15}$ The reliability of the experimental density determinations and of the apparatus has been demonstrated in previous papers. ${ }^{10-15,31,32,34}$ The measurement circuit consists of the vibrating tube (Hastelloy C-276 U-tube) containing a sample of approximately $1 \mathrm{~cm}^{3}$. It is connected to a sapphire tube cell, which is used to feed the fluids to the VTD. The experimental procedure has been previously described. ${ }^{10,11}$ Temperature calibrations were made using a calibration system (Automatic Systems F300S, U.S.A.) using a $25 \Omega$ reference probe (Rosemount, England, model 162CE; $\pm 0.005 \mathrm{~K}$ certified accuracy traceable to the ITS-90 scale). The uncertainty of temperature measurements by the platinum probes was estimated to be $\pm 0.03 \mathrm{~K}$. The pressure measurements were made directly in the equilibrium cell by means of a 25 MPa Sedeme pressure transducer (France). It was calibrated at temperatures from ( 313 to 363 ) K at the same conditions of measurements against a dead weight balance (Desgranges \& Huot, France, model 5304; accuracy $\pm 0.005$ \% full scale). The uncertainty in the pressure measurements is estimated to be $\pm 0.008 \mathrm{MPa}$. Water and nitrogen were used as the reference fluids as described in the classical method. ${ }^{35}$ The reference densities of water and nitrogen were obtained using the equations of state proposed by Wagner and Pruss. ${ }^{36}$ and Span et al., ${ }^{37}$ respectively. Calibration procedures of the platinum temperature probes, the pressure transducer, and the VTD are described in previous papers. ${ }^{10,38}$ The uncertainty of the
experimental liquid densities presented in this work was estimated to be $\pm 0.20 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$. The estimation of the uncertainty for the experimental densities was made according to a previous paper. ${ }^{32}$

## Results and Discussion

Density Measurements. Densities of hexan-2-ol, octan-1-ol, and decan-1-ol were determined at six temperatures from (313 to 363 ) K and pressures up to 22 MPa , and they are reported in Tables 2, 3, and 4. Densities of hexan-2-ol cover the density range between ( 754 to 815 ) $\mathrm{kg} \cdot \mathrm{m}^{-3}$, densities of octan-1-ol cover the density range between ( 795 to 824 ) $\mathrm{kg} \cdot \mathrm{m}^{-3}$, while densities of decan-1-ol cover the density range between ( 781 to 830 ) $\mathrm{kg} \cdot \mathrm{m}^{-3}$.

For each component the measured densities were correlated with two different models. Because excellent results were obtained for liquid densities in previous papers, ${ }^{31,32}$ a short equation of five parameters was used to correlate the densities reported here. This equation is expressed as

$$
\begin{equation*}
v / \mathrm{m}^{3} \cdot \mathrm{~kg}^{-1}=\frac{c_{1}+c_{2} P}{c_{3}-\left(c_{4} / T+c_{5} / T^{1 / 3}\right)+P} \tag{1}
\end{equation*}
$$

where $v$ is the specific volume, and $c_{i}$ is fitted to experimental ( $p, \rho, T$ ) data.

Table 3. $(p, \rho, T)$ Data of Octan-1-ol at Six Different Temperatures

| $T / \mathrm{K}=313.14$ |  | $T / \mathrm{K}=323.09$ |  | $T / \mathrm{K}=333.05$ |  | $T / \mathrm{K}=343.03$ |  | $T / \mathrm{K}=352.89$ |  | $T / \mathrm{K}=362.77$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| p/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | p/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | p/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | p/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | p/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | p/MPa | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |
| 1.004 | 811.26 | 1.007 | 804.26 | 1.038 | 797.31 | 1.049 | 790.60 | 1.023 | 782.71 | 1.051 | 775.67 |
| 2.019 | 811.95 | 2.016 | 804.97 | 2.029 | 798.03 | 2.003 | 791.16 | 2.011 | 783.55 | 2.025 | 776.41 |
| 3.000 | 812.59 | 3.019 | 805.70 | 2.999 | 798.76 | 2.981 | 791.93 | 3.032 | 784.42 | 3.016 | 777.19 |
| 4.020 | 813.22 | 4.025 | 806.40 | 4.033 | 799.51 | 4.017 | 792.68 | 4.022 | 785.42 | 4.009 | 778.05 |
| 4.995 | 813.89 | 5.012 | 807.07 | 5.020 | 800.25 | 5.000 | 793.37 | 5.005 | 786.18 | 4.974 | 778.77 |
| 6.000 | 814.53 | 6.093 | 807.82 | 6.014 | 800.97 | 6.005 | 794.05 | 6.026 | 787.13 | 6.005 | 779.51 |
| 7.007 | 815.21 | 7.143 | 808.56 | 7.029 | 801.69 | 7.018 | 794.88 | 7.003 | 787.90 | 7.006 | 780.30 |
| 8.012 | 815.83 | 8.009 | 809.12 | 8.011 | 802.44 | 8.104 | 795.68 | 8.016 | 788.71 | 8.011 | 780.95 |
| 8.994 | 816.51 | 8.989 | 809.77 | 9.005 | 803.11 | 9.014 | 796.44 | 9.007 | 789.47 | 9.008 | 781.79 |
| 10.014 | 817.19 | 10.014 | 810.47 | 10.022 | 803.83 | 10.022 | 797.10 | 10.003 | 790.22 | 10.034 | 782.62 |
| 11.007 | 817.79 | 11.031 | 811.14 | 11.011 | 804.55 | 11.028 | 797.87 | 11.022 | 791.00 | 11.013 | 783.32 |
| 12.000 | 818.42 | 12.010 | 811.82 | 12.021 | 805.23 | 11.997 | 798.58 | 12.170 | 791.78 | 11.987 | 784.03 |
| 12.997 | 819.05 | 13.005 | 812.44 | 13.022 | 805.92 | 13.030 | 799.30 | 13.015 | 792.51 | 13.015 | 784.77 |
| 14.001 | 819.67 | 14.003 | 813.11 | 14.031 | 806.61 | 14.005 | 800.00 | 14.018 | 793.24 | 14.006 | 785.51 |
| 14.997 | 820.27 | 15.012 | 813.76 | 15.010 | 807.28 | 15.002 | 800.66 | 15.009 | 794.00 | 14.997 | 786.30 |
| 16.002 | 820.89 | 16.009 | 814.40 | 16.023 | 807.92 | 16.032 | 801.38 | 16.023 | 794.74 | 16.001 | 787.03 |
| 17.001 | 821.48 | 17.005 | 815.04 | 17.012 | 808.59 | 17.016 | 801.99 | 17.010 | 795.48 | 17.013 | 787.79 |
| 17.997 | 822.10 | 18.013 | 815.66 | 18.035 | 809.23 | 18.012 | 802.68 | 18.002 | 796.16 | 17.997 | 788.55 |
| 19.004 | 822.69 | 19.003 | 816.26 | 19.009 | 809.87 | 19.005 | 803.29 | 19.029 | 796.90 | 19.000 | 789.33 |
| 20.007 | 823.28 | 20.025 | 816.90 | 20.002 | 810.51 | 20.018 | 803.98 | 20.046 | 797.63 | 20.023 | 790.04 |
| 21.004 | 823.86 | 21.081 | 817.56 | 21.011 | 811.15 | 21.014 | 804.61 | 21.023 | 798.30 | 21.004 | 790.83 |
|  |  | 22.009 | 818.09 | 22.019 | 811.82 | 22.004 | 805.23 |  |  |  |  |

Table 4. ( $p, \rho, T$ ) Data of Decan-1-ol at Six Different Temperatures

| $T / \mathrm{K}=313.12$ |  | $T / \mathrm{K}=323.09$ |  | $T / \mathrm{K}=333.04$ |  | $T / \mathrm{K}=342.98$ |  | $T / \mathrm{K}=352.86$ |  | $T / \mathrm{K}=362.89$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | $p / \mathrm{MPa}$ | $\rho / \mathrm{kg} \cdot \mathrm{m}^{-3}$ |
| 1.025 | 816.79 | 1.002 | 809.87 | 1.046 | 802.82 | 1.058 | 795.63 | 1.069 | 788.44 | 1.077 | 781.02 |
| 2.002 | 817.46 | 2.011 | 810.59 | 2.018 | 803.50 | 2.045 | 796.40 | 2.043 | 789.24 | 2.027 | 781.83 |
| 2.995 | 817.98 | 3.019 | 811.21 | 3.008 | 804.21 | 3.022 | 797.12 | 3.040 | 790.04 | 3.089 | 782.69 |
| 4.013 | 818.58 | 4.014 | 811.83 | 4.012 | 804.88 | 4.035 | 797.90 | 4.048 | 790.78 | 4.047 | 783.49 |
| 5.004 | 819.21 | 5.006 | 812.47 | 5.059 | 805.62 | 5.028 | 798.63 | 5.038 | 791.59 | 5.061 | 784.29 |
| 5.994 | 819.86 | 6.012 | 813.18 | 6.016 | 806.29 | 6.030 | 799.37 | 6.043 | 792.34 | 6.060 | 785.12 |
| 7.003 | 820.47 | 7.002 | 813.80 | 7.022 | 807.00 | 7.023 | 800.07 | 7.038 | 793.09 | 7.041 | 785.91 |
| 7.997 | 821.19 | 8.003 | 814.42 | 8.014 | 807.64 | 8.028 | 800.78 | 8.039 | 793.84 | 8.049 | 786.70 |
| 9.000 | 821.73 | 9.008 | 815.10 | 9.015 | 808.34 | 9.062 | 801.51 | 9.040 | 794.57 | 9.049 | 787.47 |
| 9.994 | 822.38 | 10.006 | 815.70 | 10.015 | 808.97 | 10.035 | 802.22 | 10.038 | 795.32 | 10.052 | 788.25 |
| 10.995 | 823.02 | 11.000 | 816.38 | 11.019 | 809.64 | 11.029 | 802.92 | 11.032 | 796.04 | 11.045 | 788.99 |
| 11.995 | 823.67 | 12.002 | 816.97 | 12.007 | 810.31 | 12.064 | 803.64 | 12.032 | 796.74 | 12.044 | 789.75 |
| 12.997 | 824.20 | 13.002 | 817.64 | 13.019 | 810.96 | 13.023 | 804.31 | 13.040 | 797.47 | 13.054 | 790.54 |
| 13.996 | 824.82 | 14.000 | 818.21 | 14.019 | 811.60 | 14.042 | 805.00 | 14.046 | 798.18 | 14.053 | 791.25 |
| 14.998 | 825.42 | 15.017 | 818.84 | 15.014 | 812.24 | 15.022 | 805.66 | 15.043 | 798.89 | 15.052 | 792.00 |
| 15.990 | 826.01 | 16.003 | 819.40 | 16.021 | 812.88 | 16.022 | 806.36 | 16.037 | 799.59 | 16.056 | 792.77 |
| 16.995 | 826.61 | 17.015 | 820.02 | 17.026 | 813.50 | 17.021 | 807.00 | 17.040 | 800.26 | 17.063 | 793.47 |
| 17.986 | 827.14 | 18.006 | 820.61 | 18.023 | 814.11 | 18.034 | 807.70 | 18.046 | 800.95 | 18.062 | 794.20 |
| 18.992 | 827.76 | 19.007 | 821.24 | 19.018 | 814.72 | 19.025 | 808.35 | 19.040 | 801.63 | 19.062 | 794.91 |
| 19.993 | 828.31 | 20.007 | 821.84 | 20.025 | 815.35 | 20.038 | 808.98 | 20.064 | 802.32 | 20.068 | 795.64 |
| 20.999 | 828.88 | 21.002 | 822.41 | 21.020 | 815.94 | 21.018 | 809.62 | 21.048 | 802.96 | 21.072 | 796.35 |
| 21.509 | 829.19 | 22.014 | 823.01 | 22.032 | 816.58 | 22.035 | 810.28 | 22.049 | 803.62 | 22.063 | 797.03 |

The other equation used to correlate the experimental density data was the BWRS EoS, expressed as ${ }^{33}$

$$
\begin{align*}
& p / \mathrm{bar}=\frac{R T}{V_{\mathrm{m}}}+\frac{\left(B_{0} R T-A_{0}-C_{0} / T^{2}+D_{0} / T^{3}-E_{0} / T^{4}\right)}{V_{\mathrm{m}}{ }^{2}}+ \\
& \quad \frac{(b R T-a-d / T)}{V_{\mathrm{m}}^{3}}+\frac{\alpha(a+d / T)}{V_{\mathrm{m}}{ }^{6}}+\frac{c\left(1+u / V_{\mathrm{m}}^{2}\right) \exp \left(-u / V_{\mathrm{m}}{ }^{2}\right)}{V_{\mathrm{m}}^{3} T^{2}} \tag{2}
\end{align*}
$$

where $V_{\mathrm{m}}$ is the molar volume.
The values for the parameters of eqs 1 and 2 were obtained by minimizing the deviations between the model and the experimental densities of the pure fluid using the MarquardtLevenberg least-squares optimization with the following objective function, $S$ :

$$
\begin{equation*}
S=\sum_{i}\left[\frac{\rho_{i}(\operatorname{expt})-\rho_{i}(\mathrm{calc})}{\rho_{i}(\operatorname{expt})}\right]^{2} \tag{3}
\end{equation*}
$$

The number of data points $\left(N_{\mathrm{p}}\right)$, ranges of temperature, pressure, and density used in the correlations, along with the optimized parameters and statistical values ${ }^{31,32,34}$ to evaluate the correlations are presented in Table 5 for the three alcohols studied in this work.

Relative deviations of experimental densities ( $\rho$ (exptl)) with values calculated ( $\rho($ calc)) using the BWRS EoS for hexan-2ol are plotted in Figure 1. The maximum relative deviations are $\pm 0.05 \%$ for the BWRS EoS as depicted in Figure 1. The same maximum deviations were obtained for the 5-parameter equation. Both equations represent the experimental density data of hexan-2-ol with a standard deviation (SDV) of $0.03 \%$; this value is consistent with the experimental uncertainty declared in this work. The relative deviations of experimental densities of octan-1-ol ( $\rho($ exptl)) with values calculated ( $\rho($ calc $)$ ) with the 5-parameter equation are illustrated in Figure 2. The maximum deviation is $+0.052 \%$ and the minimum deviation is -0.042 \% as can bee seen in Figure 2. For the BWRS EoS, the maximum deviation was +0.048 and the minimum deviation was -0.044 . Two equations represent the experimental densities


Figure 1. Relative deviations of experimental densities from this work ( $\rho$ (expt)) and values calculated ( $\rho$ (calc)) with the BWRS EoS using the parameters reported in Table 5 for hexan-2-ol at the following temperatures: $\bigcirc, 313.13 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond, 342.98 \mathrm{~K} ; \Delta, 352.86 \mathrm{~K}$; *, 362.73 K .
of octan-1-ol within the experimental uncertainty with the SDV being $0.02 \%$. In Figure 3, the relative deviations between experimental densities of decan-1-ol and values calculated with the BWRS EoS are shown. The maximum and minimum relative deviations from Figure 3 are -0.017 and +0.014 , respectively. Similar deviations were obtained for the 5-parameter equation. These two equations represent the experimental densities of decan-1-ol with a SDV of $0.01 \%$. In general, the two equations used in this work represent the experimental density within the declared experimental uncertainty.

The consistency of the experimental densities was done by comparing our experimental data (or the correlations obtained)


Figure 2. Relative deviations of experimental densities from this work ( $\rho$ (expt)) and values calculated ( $\rho$ (calc)) with the 5-parameter equation using the parameters reported in Table 5 for octan-1-ol at the following temperatures: $\bigcirc, 313.14 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.05 \mathrm{~K} ; \diamond, 343.03 \mathrm{~K} ; \Delta$, 352.89 K ; «, 362.77 K .
with density data and correlations reported in the literature. No background exists of densities in the literature for hexan-2-ol; the data set presented here represent the first reported at high pressure. Densities of octan-1-ol and of decan-1-ol have been studied before, and the characteristics of the data sets published are summarized in Table 1.

Because no comparison of densities at high pressure was possible, density values of hexan-2-ol at atmospheric pressure calculated with the 5-parameter equation were compared with experimental data reported in the literature. ${ }^{39-42}$ The relative deviations of experimental densities from literature ( $\rho$ (lit)) with calculated values $(\rho($ calc $))$ is depicted in Figure 4. The best

Table 5. Temperature T, Pressure $p$, and Density $\rho$ Ranges, Data Points $N_{\mathrm{p}}$, and Parameters for the Two Correlation Models for Hexan-2-ol, Octan-1-ol, and Decan-1-ol along with Statistical Values: AAD, Mean Deviation Bias, SDV, and rms

|  | hexan-2-ol | octan-1-ol | decan-1-ol |
| :---: | :---: | :---: | :---: |
| $T_{\text {min }} / \mathrm{K}$ | 313.13 | 313.14 | 313.12 |
| $T_{\text {max }} / \mathrm{K}$ | 362.73 | 362.77 | 362.89 |
| $p_{\text {min }} / \mathrm{MPa}$ | 1.010 | 1.004 | 1.002 |
| $p_{\text {max }} / \mathrm{MPa}$ | 22.010 | 22.019 | 22.063 |
| $\rho_{\text {min }} / \mathrm{kg} \cdot \mathrm{m}^{-3}$ | 754.97 | 775.67 | 781.02 |
| $\rho_{\max } / \mathrm{kg} \cdot \mathrm{~m}^{-3}$ | 814.40 | 823.86 | 829.19 |
| $N_{\mathrm{p}}$ | 132 | 129 | 132 |
| 5-parameters equation |  |  |  |
| $c_{1} / \mathrm{MPa} \cdot \mathrm{kg}^{-1} \cdot \mathrm{~m}^{3}$ | 0.16583 | 0.24011 | 0.21512 |
| $c_{2} / \mathrm{kg}^{-1} \cdot \mathrm{~m}^{3}$ | 0.001081 | 0.001028 | 0.001049 |
| $c_{3 /} \mathrm{MPa}$ | -437.548 | -400.559 | -265.660 |
| $c 4 / \mathrm{K} \cdot \mathrm{MPa}$ | 70257.1 | 70048.2 | 47261.2 |
| $c_{5} / \mathrm{MPa} \cdot \mathrm{K}^{1 / 3}$ | -5393.7 | -5560.4 | -4021.0 |
| AAD/\% | 0.03 | 0.02 | 0.005 |
| bias/\% | -0.0002 | -0.002 | 0.005 |
| SDV/\% | 0.03 | 0.02 | 0.01 |
| rms/\% | 0.03 | 0.02 | 0.01 |
| BWRS EoS |  |  |  |
| $B_{0} / \mathrm{cm}^{3} \cdot \mathrm{~mol}^{-1}$ | 664.01 | 237.78 |  |
| $A_{0} / \mathrm{bar} \cdot \mathrm{cm}^{6} \cdot \mathrm{~mol}^{-2}$ | $4.1900 \cdot 10^{7}$ | $6.0067 \cdot 10^{7}$ | $7.4694 \cdot 10^{7}$ |
| $C_{0} / \mathrm{bar} \cdot \mathrm{K}^{2} \cdot \mathrm{~cm}^{6} \cdot \mathrm{~mol}^{-2}$ | $1.3345 \cdot 10^{12}$ | $3.5131 \cdot 10^{12}$ | $4.6815 \cdot 10^{12}$ |
| $D_{0} / \mathrm{bar} \cdot \mathrm{K}^{3} \cdot \mathrm{~cm}^{6} \cdot \mathrm{~mol}^{-2}$ | $-2.0618 \cdot 10^{14}$ | $-4.3430 \cdot 10^{14}$ | $-5.5842 \cdot 10^{14}$ |
| $E_{0} / \mathrm{bar} \cdot \mathrm{K}^{4} \cdot \mathrm{~cm}^{6} \cdot \mathrm{~mol}^{-2}$ | $-1.1622 \cdot 10^{17}$ | $-2.5917 \cdot 10^{17}$ | $-2.9681 \cdot 10^{17}$ |
| $b / \mathrm{cm}^{6} \cdot \mathrm{~mol}^{-2}$ | $5.9113 \cdot 10^{4}$ | $2.0213 \cdot 10^{5}$ | $2.8979 \cdot 10^{5}$ |
| a/bar $\cdot \mathrm{cm}^{9} \cdot \mathrm{~mol}^{-3}$ | $2.6693 \cdot 10^{8}$ | $9.5285 \cdot 10^{8}$ | $2.0085 \cdot 10^{9}$ |
| $\mathrm{d} / \mathrm{bar} \cdot \mathrm{K} \cdot \mathrm{cm}^{9} \cdot \mathrm{~mol}^{-3}$ | $5.2406 \cdot 10^{10}$ | $4.5534 \cdot 10^{10}$ | $2.0765 \cdot 10^{11}$ |
| $c / \mathrm{bar} \cdot \mathrm{K}^{2} \cdot \mathrm{~cm}^{9} \cdot \mathrm{~mol}^{-3}$ | $-3.8020 \cdot 10^{14}$ | $-6.985 \cdot 10^{14}$ | $-1.2529 \cdot 10^{15}$ |
| $\alpha / \mathrm{cm}^{9} \cdot \mathrm{~mol}^{-3}$ | $2.3461 \cdot 10^{7}$ | $3.9899 \cdot 10^{7}$ | $5.7066 \cdot 10^{7}$ |
| $u / \mathrm{cm}^{6} \cdot \mathrm{~mol}^{-2}$ | $2.4210 \cdot 10^{4}$ | $4.9619 \cdot 10^{4}$ | $5.7597 \cdot 10^{4}$ |
| AAD/\% | 0.02 | 0.02 | 0.01 |
| bias/\% | -0.0004 | -0.0002 | -0.0005 |
| SDV/\% | 0.03 | 0.02 | 0.01 |
| rms/\% | 0.03 | 0.02 | 0.01 |



Figure 3. Relative deviations of experimental densities from this work ( $\rho($ expt $)$ ) and values calculated ( $\rho$ (calc)) with the BWRS EoS using the parameters reported in Table 5 for decan-1-ol at the following temperatures: $O, 313.12 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond, 342.98 \mathrm{~K} ; \Delta, 352.86 \mathrm{~K} ;$ A, 362.89 K .


Figure 4. Comparison of experimental densities at atmospheric pressure for hexan-2-ol reported by different authors in the literature ( $\rho($ lit)) with the values calculated from the 5-parameter equation ( $\rho$ (calc)) fitted to data reported in this work; O, Ortega; ${ }^{39} \nabla$, TRC Tables; ${ }^{40} \square$, Iloukhani et al.; ${ }^{41}$ $\diamond$, Weng and Chen. ${ }^{42}$
agreement was found with the data reported by Ortega ${ }^{39}$ and Weng and Chen. ${ }^{42}$ The 5 -parameter equation represents their data with an average absolute deviation (AAD) of $0.04 \%$. Larger deviations were founded with the data from ref 40 and Iloukhani et al. ${ }^{41}$ The deviations increased as the temperature decreases as can be seen in Figure 4.

Cibulka and Zikova ${ }^{17}$ reported two different correlations for octan-1-ol. The first correlation was obtained using data reported by Matsuo and Makita, ${ }^{21}$ Uoasaki et al., ${ }^{22}$ and Garg et al. ${ }^{23}$ (named 1-Octanol (I)), and the second one (1-Octanol (II)) was obtained using the above data along with those reported by Apaev et al. ${ }^{19}$ Density values at the same conditions reported herein were calculated with the two mentioned correlations. The relative deviation of experimental data from this work and values calculated with both correlations are shown in Figure 5. The maximum deviations are $\pm 0.08 \%$ for both correlations. No difference is observed for both correlations by observing Figure 5; however, to evaluate this comparison the absolute (rmsd) and relative (rmsdr) root-mean-square deviation, and bias, as defined in ref 17, were calculated for our set of data for both correlations. The results are $0.353 \mathrm{~kg} \cdot \mathrm{~m}^{-3}, 0.044 \%$, and $0.002 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$, respectively, for 1-Octanol (I) correlation, and $0.316 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$,


Figure 5. Relative deviations of experimental densities of octan-1-ol from this work ( $\rho($ expt)) and values calculated ( $\rho$ (calc)) using the correlations reported by Cibulka and Zikova ${ }^{17}$ for octan-1-ol at the following temperatures: $O, 313.14 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.05 \mathrm{~K} ; \diamond, 343.03 \mathrm{~K} ; \Delta, 352.89$ $\mathrm{K} ; \star, 362.77 \mathrm{~K}$. Open and closed symbols are for 1-Octanol (I) and 1-Octanol (II) correlations from ref 17, respectively.


Figure 6. Comparison of the experimental densities at high pressure of octan-1-ol reported by different authors ( $\rho($ lit $)$ ) with values calculated from the 5-parameter equation ( $\rho$ (calc)) fitted to data reported in this work; $\bigcirc$, Apaev et al. $;^{19} \nabla$, Matsuo and Makita; ${ }^{21} \square$, Garg et al.;23 $\diamond$, Lee et al.; ${ }^{24} \Delta$, Dzida. ${ }^{25}$
$0.039 \%$, and $-0.005 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$, respectively, for 1-Octanol (II) correlation. The second correlation represents with better accuracy our experimental data, and the statistical values obtained are lower than those obtained for the 1-Octanol (II) correlation. ${ }^{17}$ Additionally to this comparison, the 5-parameter equation with the parameters obtained here for octan-1-ol was used to calculate densities at the same temperature and pressure of the data reported in the literature; however, only those data reported in the same range of temperature and pressure measured here were considered. The relative deviations for the different sets of data considered are plotted in Figure 6. The average absolute deviations for individual sets of data compared are 0.04 \% (Apaev et al. ${ }^{19}$ ), $0.08 \%$ (Matsuo and Makita ${ }^{21}$ ), $0.03 \%$ (Garg et al. ${ }^{23}$ ), $0.06 \%$ (Lee et al. ${ }^{24}$ ), and $0.07 \%\left(\right.$ Dzida $\left.^{25}\right)$. Comparisons of density at atmospheric pressure are shown in Figure 7 for octan-1-ol. Relative deviations of values calculated with the 5-parameter equation for octan-1-ol with density data reported in the literature. ${ }^{21,23,25,43-46}$ The maximum deviation is $+0.1 \%$ and the minimum deviation is $-0.34 \%$ as can be seen in Figure 7. The average absolute deviations for each set of data used in the comparison are as follows: $0.20 \%$ (Diaz-Peña and


Figure 7. Comparison of experimental densities at atmospheric pressure for octan-1-ol reported in the literature ( $\rho($ lit)) with the values calculated from the 5-parameter equation ( $\rho(\mathrm{calc})$ ) fitted to data reported in this work; O, Diaz-Peña and Tardajos; ${ }^{43} \nabla$, Ortega; $;{ }^{44} \square$, Rauf et al.; ${ }^{45} \diamond$, Matsuo and Makita; ${ }^{21} \Delta$, Liew et al. ${ }^{46} \star$, Garg et al.; ${ }^{23} \times$, Dzida. ${ }^{25}$


Figure 8. Relative deviations of experimental densities of decan-1-ol from this work ( $\rho($ expt)) and values calculated ( $\rho($ calc)) using the correlation reported by Cibulka and Zikova ${ }^{17}$ for decan-1-ol at the following temperatures: $\bigcirc, 313.12 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond, 342.98 \mathrm{~K} ; \Delta, 352.86$ K; ※, 362.89 K.

Tardajos ${ }^{43}$ ), 0.16 \% (Ortega ${ }^{44}$ ), 0.13 \% (Rauf et al. ${ }^{45}$ ), 0.17 \% (Matsuo and Makita ${ }^{21}$ ), 0.12 \% (Liew et al. ${ }^{46}$ ), 0.07 \% (Garg et al. ${ }^{23}$ ), and $0.16 \% ~\left(\right.$ Dzida $^{25}$ ).

For decan-1-ol, we compare our data with the correlation reported by Cibulka and Zikova. ${ }^{17}$ This correlation was done using the density data sets reported by Kuss, ${ }^{26}$ Matsuo and Makita, ${ }^{21}$ and Apaev and Gylmanov. ${ }^{29}$ The relative deviations between the experimental data and the model are plotted in Figure 8. The maximum deviations are $\pm 0.04 \%$. As for the case of octan-1-ol, the rmsd, rmsdr, and bias were calculated for our set of data, and the results are $0.144 \mathrm{~kg} \cdot \mathrm{~m}^{-3}, 0.018 \%$, and $0.097 \mathrm{~kg} \cdot \mathrm{~m}^{-3}$. These values are lower compared to the values reported for the correlation. ${ }^{17}$ This demonstrates good agreement with the correlation reported by Cibulka and Zikova. ${ }^{17}$ The 5-parameter equation with the parameters reported in Table 5 for decan-1-ol was used to calculate density values at the same conditions of temperature and pressure reported in the literature, considering only data reported in the same range of temperature and pressure used in this work. The relative deviations of calculated densities and literature data ${ }^{21,25,27,29}$ are shown in Figure 9. The maximum deviations are $\pm 0.6 \%$, and


Figure 9. Comparison of the experimental densities at high pressure of decan-1-ol reported by different authors ( $\rho$ (lit)) with values calculated from the 5-parameter equation ( $\rho(\mathrm{calc})$ ) fitted to data reported in this work; $\bigcirc$, Mamedov and Aliev; ${ }^{27} \nabla$, Matsuo and Makita; ${ }^{21} \square$, Apaev and Gylmanov; ${ }^{29}$ $\diamond$, Dzida. ${ }^{25}$


Figure 10. Comparison of experimental densities at atmospheric pressure for decan-1-ol reported by different authors ( $\rho($ lit)) and values calculated with the 5-parameter equation ( $\rho(\mathrm{calc})$ ) fitted to data reported in this work; O, Diaz-Peña and Tardajos; ${ }^{43} \nabla$, Mamedov and Aliev; ${ }^{27} \square$, Ortega; ${ }^{44} \diamond$, Rauf et al. ${ }^{45} \Delta$, Matsuo and Makita; ${ }^{21}$, Apaev and Gylmanov; ${ }^{29} \times$, Liew et al.;46 ${ }^{4 \prime}$, Dzida. ${ }^{25}$
the best agreement was found with the data reported by Matsuo and Makita, ${ }^{21}$ having an AAD of $0.02 \%$ with respect to the model. The AAD values for the remaining sets of data are as follows: 0.31 \% (Mamedov and Aliev ${ }^{27}$ ), $0.26 \%$ (Apaev and Gylmanov ${ }^{29}$ ), and $0.56 \%$ (Dzida ${ }^{25}$ ). Comparisons for decan-1-ol at atmospheric pressure were also done, and the relative deviations of density values calculated with the 5-parameter equation with literature data ${ }^{21,25,27,29,43-46}$ are shown in Figure 10. Excellent agreement was found with the data reported by Ortega ${ }^{44}$ and Dzida ${ }^{25}$ having both sets of data with AAD values of $0.01 \%$ with respect to the model. For the other sets of data, the AAD values are $0.12 \%$ (Diaz-Peña and Tardajos ${ }^{43}$ ), 0.11 \% (Mamedov and Aliev ${ }^{27}$ ), 0.04 \% (Rauf et al. ${ }^{45}$ ), $0.05 \%$ (Matsuo and Makita ${ }^{21}$ ), $0.25 \%$ (Apaev and Gylmanov ${ }^{29}$ ), and $0.05 \%$ (Liew et al. ${ }^{46}$ ). The different comparisons show the reliability of our experimental data.

Derived Properties. The experimental densities can be used to obtain some thermodynamic properties, such as the isothermal compressibility ( $K_{\mathrm{T}}$ ) and the isobaric thermal expansivity ( $\alpha_{\mathrm{p}}$ ). The effect of pressure in density can be described by the

Table 6. Calculated Values of Isothermal Compressibility, $K_{T}$, and Isobaric Thermal Expansivity, $\alpha_{p}$, for Hexan-2-ol

| $T=313.13 \mathrm{~K}$ |  |  | $T=323.09 \mathrm{~K}$ |  |  | $T=333.04 \mathrm{~K}$ |  |  | $T=342.98 \mathrm{~K}$ |  |  | $T=352.86 \mathrm{~K}$ |  |  | $T=362.73 \mathrm{~K}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{\mathrm{p}} \cdot 10^{3}$ | $p$ | $K_{\mathrm{T}}$ | $\alpha_{p} \cdot 10^{3}$ |
| MPa | $\overline{\mathrm{GPa}^{-1}}$ | $\mathrm{K}^{-1}$ | MPa | $\overline{\mathrm{GPa}^{-1}}$ | $\mathrm{K}^{-1}$ | MPa | $\overline{\mathrm{GPa}^{-1}}$ | $\mathrm{K}^{-1}$ | MPa | $\overline{\mathrm{GPa}^{-1}}$ | $\mathrm{K}^{-}$ | MPa | $\overline{\mathrm{GPa}^{-1}}$ | K | MPa | $\overline{\mathrm{GPa}^{-1}}$ | $\mathrm{K}^{-1}$ |
| . 010 | 1.021 | 0.967 | 1.037 | 1.096 | 1.044 | 1.055 | 1.178 | 1.113 | 1.032 | 1.266 | 1.174 | 1.053 | 1.358 | 1.228 | 1.075 | 1.455 | 1.277 |
| 2.006 | 1.007 | 0.960 | 2.000 | 1.082 | 1.037 | 2.007 | 1.162 | 1.104 | 2.015 | 1.248 | 1.165 | 2.014 | 1.339 | 1.219 | 2.006 | 1.435 | 1.267 |
| 2.999 | 0.993 | 0.953 | 3.010 | 1.067 | 1.029 | 3.005 | 1.146 | 1.096 | 3.012 | 1.231 | 1.156 | 3.019 | 1.320 | 1.209 | 3.018 | 1.415 | 1.257 |
| 4.008 | 0.980 | 0.946 | 4.029 | 1.052 | 1.021 | 4.007 | 1.130 | 1.088 | 4.017 | 1.214 | 1.147 | 4.033 | 1.302 | 1.200 | 4.034 | 1.395 | 1.247 |
| 4.999 | 0.967 | 0.939 | 5.004 | 1.038 | 1.014 | 5.015 | 1.115 | 1.080 | 5.013 | 1.197 | 1.139 | 4.996 | 1.284 | 1.191 | 5.016 | 1.376 | 1.238 |
| 5.986 | 0.954 | 0.932 | 6.020 | 1.023 | 1.006 | 6.009 | 1.100 | 1.072 | 6.012 | 1.181 | 1.130 | 6.006 | 1.266 | 1.182 | 6.066 | 1.356 | 1.228 |
| 7.000 | 0.941 | 0.926 | 7.007 | 1.010 | 0.999 | 7.006 | 1.085 | 1.064 | 7.025 | 1.164 | 1.122 | 7.013 | 1.249 | 1.173 | 6.998 | 1.338 | 1.219 |
| 8.010 | 0.928 | 0.919 | 8.009 | 0.996 | 0.992 | 7.998 | 1.070 | 1.056 | 8.000 | 1.149 | 1.114 | 8.004 | 1.232 | 1.164 | 8.041 | 1.319 | 1.210 |
| 9.026 | 0.916 | 0.912 | 9.017 | 0.983 | 0.985 | 9.006 | 1.056 | 1.049 | 9.000 | 1.134 | 1.106 | 9.035 | 1.215 | 1.156 | 9.014 | 1.302 | 1.201 |
| 10.004 | 0.904 | 0.906 | 10.003 | 0.970 | 0.978 | 10.004 | 1.042 | 1.041 | 9.996 | 1.119 | 1.098 | 10.009 | 1.199 | 1.147 | 10.001 | 1.284 | 1.192 |
| 11.005 | 0.892 | 0.900 | 11.001 | 0.958 | 0.971 | 11.007 | 1.028 | 1.034 | 11.020 | 1.104 | 1.089 | 11.007 | 1.183 | 1.139 | 11.026 | 1.267 | 1.183 |
| 12.001 | 0.881 | 0.894 | 12.000 | 0.945 | 0.964 | 12.012 | 1.015 | 1.026 | 11.999 | 1.089 | 1.082 | 12.007 | 1.168 | 1.131 | 12.000 | 1.250 | 1.175 |
| 13.010 | 0.869 | 0.887 | 13.021 | 0.933 | 0.957 | 13.003 | 1.002 | 1.019 | 12.996 | 1.075 | 1.074 | 12.999 | 1.152 | 1.123 | 13.010 | 1.234 | 1.166 |
| 14.002 | 0.858 | 0.881 | 14.001 | 0.921 | 0.951 | 14.008 | 0.989 | 1.012 | 14.007 | 1.061 | 1.067 | 14.012 | 1.137 | 1.115 | 13.999 | 1.218 | 1.158 |
| 14.998 | 0.848 | 0.875 | 15.002 | 0.909 | 0.944 | 15.005 | 0.976 | 1.005 | 15.003 | 1.047 | 1.059 | 15.010 | 1.123 | 1.107 | 15.006 | 1.202 | 1.150 |
| 16.001 | 0.837 | 0.869 | 16.000 | 0.898 | 0.938 | 16.001 | 0.964 | 0.998 | 16.005 | 1.034 | 1.052 | 16.003 | 1.108 | 1.099 | 16.006 | 1.186 | 1.142 |
| 17.006 | 0.826 | 0.864 | 17.004 | 0.886 | 0.932 | 17.006 | 0.951 | 0.992 | 17.002 | 1.021 | 1.045 | 17.002 | 1.094 | 1.092 | 17.005 | 1.171 | 1.133 |
| 18.000 | 0.816 | 0.858 | 18.008 | 0.875 | 0.925 | 18.010 | 0.939 | 0.985 | 18.010 | 1.008 | 1.037 | 18.017 | 1.080 | 1.084 | 18.000 | 1.156 | 1.126 |
| 19.005 | 0.806 | 0.852 | 19.001 | 0.865 | 0.919 | 19.002 | 0.928 | 0.978 | 19.005 | 0.995 | 1.030 | 19.005 | 1.066 | 1.077 | 19.003 | 1.141 | 1.118 |
| 20.015 | 0.796 | 0.847 | 20.011 | 0.854 | 0.913 | 20.000 | 0.916 | 0.972 | 20.010 | 0.983 | 1.023 | 20.014 | 1.053 | 1.069 | 20.017 | 1.127 | 1.110 |
| 21.029 | 0.786 | 0.841 | 21.003 | 0.843 | 0.907 | 21.000 | 0.905 | 0.965 | 21.006 | 0.971 | 1.017 | 21.013 | 1.040 | 1.062 | 21.006 | 1.113 | 1.102 |
| 22.004 | 0.777 | 0.836 | 22.004 | 0.833 | 0.901 | 22.004 | 0.894 | 0.959 | 22.005 | 0.959 | 1.010 | 22.010 | 1.027 | 1.055 | 22.010 | 1.099 | 1.095 |

Table 7. Calculated Values of Isothermal Compressibility, $K_{T}$, and Isobaric Thermal Expansivity, $\alpha_{p}$, for Octan-1-ol

| $T=313.14 \mathrm{~K}$ |  |  | $T=323.09 \mathrm{~K}$ |  |  | $T=333.05 \mathrm{~K}$ |  |  | $T=343.03 \mathrm{~K}$ |  |  | $T=352.89 \mathrm{~K}$ |  |  | $T=362.77 \mathrm{~K}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\mathrm{T}}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ |
| MPa | $\mathrm{GPa}^{-1}$ | K | MPa | $\mathrm{GPa}^{-1}$ | K | MPa | $\mathrm{GPa}^{-1}$ | $\mathrm{K}^{-1}$ | MPa | $\mathrm{GPa}^{-1}$ | $\mathrm{K}^{-1}$ | MPa | $\mathrm{GPa}^{-1}$ | $\mathrm{K}^{-1}$ | MPa | $\mathrm{GPa}^{-1}$ | $\mathrm{K}^{-1}$ |
| 1.004 | 0.850 | 0.804 | 1.007 | 0.892 | 0.851 | 1.038 | 0.937 | 0.891 | 1.049 | 0.984 | 0.926 | 1.023 | 1.033 | 0.957 | 1.051 | 1.084 | 0.984 |
| 2.019 | 0.842 | 0.800 | 2.016 | 0.884 | 0.846 | 2.029 | 0.928 | 0.886 | 2.003 | 0.975 | 0.922 | 2.011 | 1.024 | 0.952 | 2.025 | 1.074 | 0.979 |
| 3.000 | 0.834 | 0.796 | 3.019 | 0.876 | 0.842 | 2.999 | 0.920 | 0.882 | 2.981 | 0.966 | 0.917 | 3.032 | 1.014 | 0.947 | 3.016 | 1.064 | 0.974 |
| 4.020 | 0.826 | 0.792 | 4.025 | 0.867 | 0.838 | 4.033 | 0.911 | 0.877 | 4.017 | 0.957 | 0.912 | 4.022 | 1.004 | 0.942 | 4.009 | 1.054 | 0.969 |
| 4.995 | 0.819 | 0.788 | 5.012 | 0.860 | 0.833 | 5.020 | 0.903 | 0.873 | 5.000 | 0.948 | 0.908 | 5.005 | 0.995 | 0.938 | 4.974 | 1.044 | 0.964 |
| 6.000 | 0.812 | 0.784 | 6.093 | 0.851 | 0.829 | 6.014 | 0.894 | 0.868 | 6.005 | 0.939 | 0.903 | 6.026 | 0.986 | 0.933 | 6.005 | 1.034 | 0.959 |
| 7.007 | 0.804 | 0.780 | 7.143 | 0.843 | 0.824 | 7.029 | 0.886 | 0.864 | 7.018 | 0.931 | 0.898 | 7.003 | 0.977 | 0.928 | 7.006 | 1.025 | 0.954 |
| 8.012 | 0.797 | 0.776 | 8.009 | 0.836 | 0.821 | 8.011 | 0.878 | 0.860 | 8.104 | 0.921 | 0.893 | 8.016 | 0.968 | 0.923 | 8.011 | 1.015 | 0.949 |
| 8.994 | 0.790 | 0.773 | 8.989 | 0.829 | 0.817 | 9.005 | 0.870 | 0.855 | 9.014 | 0.914 | 0.889 | 9.007 | 0.959 | 0.918 | 9.008 | 1.006 | 0.944 |
| 10.014 | 0.783 | 0.769 | 10.014 | 0.821 | 0.813 | 10.022 | 0.862 | 0.851 | 10.022 | 0.905 | 0.885 | 10.003 | 0.950 | 0.914 | 10.034 | 0.996 | 0.939 |
| 11.007 | 0.776 | 0.765 | 11.031 | 0.814 | 0.809 | 11.011 | 0.854 | 0.847 | 11.028 | 0.897 | 0.880 | 11.022 | 0.941 | 0.909 | 11.013 | 0.987 | 0.935 |
| 12.000 | 0.769 | 0.761 | 12.010 | 0.807 | 0.805 | 12.021 | 0.847 | 0.843 | 11.997 | 0.889 | 0.876 | 12.170 | 0.932 | 0.904 | 11.987 | 0.979 | 0.930 |
| 12.997 | 0.762 | 0.758 | 13.005 | 0.799 | 0.801 | 13.022 | 0.839 | 0.839 | 13.030 | 0.881 | 0.872 | 13.015 | 0.924 | 0.900 | 13.015 | 0.970 | 0.925 |
| 14.001 | 0.755 | 0.754 | 14.003 | 0.792 | 0.797 | 14.031 | 0.832 | 0.835 | 14.005 | 0.873 | 0.867 | 14.018 | 0.916 | 0.896 | 14.006 | 0.961 | 0.921 |
| 14.997 | 0.749 | 0.750 | 15.012 | 0.785 | 0.793 | 15.010 | 0.824 | 0.831 | 15.002 | 0.866 | 0.863 | 15.009 | 0.908 | 0.891 | 14.997 | 0.952 | 0.916 |
| 16.002 | 0.742 | 0.747 | 16.009 | 0.778 | 0.789 | 16.023 | 0.817 | 0.827 | 16.032 | 0.858 | 0.859 | 16.023 | 0.900 | 0.887 | 16.001 | 0.944 | 0.911 |
| 17.001 | 0.736 | 0.743 | 17.005 | 0.772 | 0.786 | 17.012 | 0.810 | 0.823 | 17.016 | 0.850 | 0.855 | 17.010 | 0.892 | 0.883 | 17.013 | 0.935 | 0.907 |
| 17.997 | 0.729 | 0.740 | 18.013 | 0.765 | 0.782 | 18.035 | 0.803 | 0.819 | 18.012 | 0.843 | 0.851 | 18.002 | 0.884 | 0.878 | 17.997 | 0.927 | 0.903 |
| 19.004 | 0.723 | 0.736 | 19.003 | 0.758 | 0.778 | 19.009 | 0.796 | 0.815 | 19.005 | 0.836 | 0.847 | 19.029 | 0.876 | 0.874 | 19.000 | 0.919 | 0.898 |
| 20.007 | 0.717 | 0.733 | 20.025 | 0.752 | 0.775 | 20.002 | 0.789 | 0.811 | 20.018 | 0.828 | 0.843 | 20.046 | 0.868 | 0.870 | 20.023 | 0.911 | 0.894 |
| 21.004 | 0.711 | 0.730 | 21.081 | 0.745 | 0.771 | 21.011 | 0.782 | 0.807 | 21.014 | 0.821 | 0.839 | 21.023 | 0.861 | 0.866 | 21.004 | 0.903 | 0.889 |
|  |  |  | 22.009 | 0.739 | 0.767 | 22.019 | 0.775 | 0.803 | 22.004 | 0.814 | 0.835 |  |  |  |  |  |  |

isothermal compressibility that is calculated using the isothermal pressure derivative of density according to the following expression:

$$
\begin{equation*}
K_{\mathrm{T}}=\frac{1}{\rho}\left(\frac{\partial \rho}{\partial p}\right)_{T} \tag{4}
\end{equation*}
$$

In this work, the isothermal compressibility of each compound has been determined analytically by differentiating eq 1 along with the parameters reported in Table 5. This results in the following expression for the isothermal compressibility:

$$
\begin{equation*}
K_{\mathrm{T}}=\frac{1}{\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)}-\frac{c_{2}}{\left(c_{1}+c_{2} p\right)} \tag{5}
\end{equation*}
$$

The isobaric thermal expansivity is defined as

$$
\begin{equation*}
\alpha_{\mathrm{p}}=-\frac{1}{\rho}\left(\frac{\partial \rho}{\partial T}\right)_{p} \tag{6}
\end{equation*}
$$

as it was done for the isothermal compressibility. Equation 1, along with the parameters reported in Table 5, is used to derive the isobaric thermal expansivity, obtaining the following expression

$$
\begin{equation*}
\alpha_{\mathrm{p}}=-\frac{3 c_{4} / T^{2}+c_{5} / T^{4 / 3}}{3\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)} \tag{7}
\end{equation*}
$$

The uncertainties of the calculated isothermal compressibilities and the calculated isobaric thermal expansivities were calculated with the law of propagation of errors. ${ }^{47}$ The uncertainty was


Figure 11. Isotherms for the isothermal compressibility of hexan-2-ol at the following temperatures: $\bigcirc, 313.13 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond$, $342.98 \mathrm{~K} ; \Delta, 352.86 \mathrm{~K}$; $\boldsymbol{\lambda}_{2}, 362.73 \mathrm{~K}$.


Figure 12. Isotherms for the isothermal compressibility of octan-1-ol at the following temperatures: $\bigcirc, 313.14 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.05 \mathrm{~K} ; \diamond$, $343.03 \mathrm{~K} ; \Delta, 352.89 \mathrm{~K}$; ث, 362.77 K .


Figure 13. Isotherms for the isothermal compressibility of decan-1-ol at the following temperatures: $\bigcirc, 313.12 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond$, $342.98 \mathrm{~K} ; \Delta, 352.86 \mathrm{~K}$; ネ, 362.89 K .
estimated to be better than $\pm 1.6 \%$ for the isothermal compressibilities, while, the uncertainty for the isobaric thermal expansivities was estimated to be better than $\pm 0.8 \%$.

The uncertainty on the calculation of the derived thermody-


Figure 14. Isotherms for the isobaric thermal expansivity of hexan-2-ol at the following temperatures: $\bigcirc, 313.13 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond$, $342.98 \mathrm{~K} ; \Delta, 352.86 \mathrm{~K}$; A九, 362.73 K .


Figure 15. Isotherms for the isobaric thermal expansivity of octan-1-ol at the following temperatures: $\bigcirc, 313.14 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.05 \mathrm{~K} ; \diamond$, $343.03 \mathrm{~K} ; \Delta, 352.89 \mathrm{~K} ; \star, 362.77 \mathrm{~K}$.


Figure 16. Isotherms for the isobaric thermal expansivity of decan-1-ol at the following temperatures: $\bigcirc, 313.12 \mathrm{~K} ; \nabla, 323.09 \mathrm{~K} ; \square, 333.04 \mathrm{~K} ; \diamond$, $342.98 \mathrm{~K} ; \Delta, 352.86 \mathrm{~K}$; „, 362.89 K .
namic properties was obtained based on the next expression for the law of propagation of errors ${ }^{47}$

$$
\begin{equation*}
\sigma_{K_{\mathrm{T}}}^{2}=\sum_{i=1}^{N_{p}}\left(\frac{\partial K_{\mathrm{T}}}{\partial X_{i}}\right)^{2} \sigma_{X_{i}}^{2} \tag{8}
\end{equation*}
$$

where the $X_{\mathrm{i}}$ values are referred to as sensitivity coefficients and $\sigma_{X_{i}}$ is the standard uncertainty associated with each $X_{i}$. For the case of the isothermal compressibility, the following expressions were used:

$$
\begin{equation*}
\sigma_{K \mathrm{~T}}^{2}=\left(\frac{\partial K_{\mathrm{T}}}{\partial T}\right)^{2} \sigma_{T}^{2}+\left(\frac{\partial K_{\mathrm{T}}}{\partial p}\right)^{2} \sigma_{p}^{2}+\left(\frac{\partial K_{\mathrm{T}}}{\partial \rho}\right)^{2} \sigma_{\rho}^{2} \tag{9}
\end{equation*}
$$

The derivates with respect to temperature, pressure, and density are given by the following equations:

$$
\begin{gather*}
\frac{\partial K_{\mathrm{T}}}{\partial T}=-\left[\frac{3 c_{4} / T^{2}+c_{5} / T^{4 / 3}}{3\left(c_{3}-c_{4} / T-c_{5} T^{1 / 3}+p\right)^{2}}\right]  \tag{10}\\
\frac{\partial K_{\mathrm{T}}}{\partial p}=\frac{-1}{\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)^{2}}+\frac{c_{2}}{\left(c_{1}+c_{2} p\right)^{2}}  \tag{11}\\
\frac{\partial K_{\mathrm{T}}}{\partial \rho}=\left[\frac{-1}{\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)^{2}}+\frac{c_{2}}{\left(c_{1}+c_{2} p\right)^{2}}\right] \\
{\left[\frac{\left(c_{1}+c_{2} p\right)^{2}}{\left(c_{1}+c_{2} p\right)-c_{2}\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)}\right]} \tag{12}
\end{gather*}
$$

On the other hand, for the isobaric thermal expansivity the following expressions were used:

$$
\begin{equation*}
\sigma_{\alpha_{\mathrm{p}}}^{2}=\left(\frac{\partial \alpha_{\mathrm{p}}}{\partial T}\right)^{2} \sigma_{T}^{2}+\left(\frac{\partial \alpha_{\mathrm{p}}}{\partial p}\right)^{2} \sigma_{p}^{2}+\left(\frac{\partial \alpha_{\mathrm{p}}}{\partial \rho}\right)^{2} \sigma_{\rho}^{2} \tag{13}
\end{equation*}
$$

The respective derivates are given by the following equations:

$$
\begin{align*}
& \frac{\partial \alpha_{\mathrm{p}}}{\partial T}= \\
& \frac{3\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)\left(6 c_{4} / T^{-3}-4 c_{5} / T^{7 / 3}\right)+\left(3 c_{4} / T^{2}+c_{5} / T^{4 / 3}\right)^{2}}{9\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)^{2}} \tag{14}
\end{align*}
$$

$$
\begin{gather*}
\frac{\partial \alpha_{\mathrm{p}}}{\partial p}=\frac{3 c_{4} / T^{2}+c_{5} / T^{4 / 3}}{3\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)^{2}}  \tag{15}\\
\frac{\partial \alpha_{\mathrm{p}}}{\partial \rho}=\left[\frac{3 c_{4} / T^{2}+c_{5} / T^{4 / 3}}{3\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)^{2}}\right] \\
{\left[\frac{\left(c_{1}+c_{2} p\right)^{2}}{\left(c_{1}+c_{2} p\right)-c_{2}\left(c_{3}-c_{4} / T-c_{5} / T^{1 / 3}+p\right)}\right]} \tag{16}
\end{gather*}
$$

Even when the expressions given in eqs 5 and 7 have no explicit dependence on density, the quantities are sensitive to the experimental uncertainty.

The calculated isothermal compressibilities and isobaric thermal expansivities of hexan-2-ol, octan-1-ol, and decan-2ol calculated with the 5-parameter equation are reported in Tables 6 to 8 . The isothermal compresibilities for hexan-2-ol, octan-1-ol, and decan-1-ol are plotted in Figures 11 to $13 . K_{\mathrm{T}}$ increases as the temperature was increased at constant pressure; on the other hand, $K_{\mathrm{T}}$ decreases as the pressure was increased at constant temperature. These two effects can be seen in Figures 11 to 13 for the three alcohols studied here. The alcohols studied in this work become more compressible with increasing temperatures. In contrast, the alcohols become less compressible with increasing pressure. For hexan-2-ol, the isothermal compressibilities range from $1.021 \mathrm{GPa}^{-1}$ at 313.13 K to 1.455 $\mathrm{GPa}^{-1}$ at 362.73 K at approximately 1 MPa . For octan-1-ol, the isothermal compressibilities range from $0.850 \mathrm{GPa}^{-1}$ at 313.14 K to $1.084 \mathrm{GPa}^{-1}$ at 362.77 K at approximately 1 MPa . Meanwhile, for decan-1-ol the isothermal compressibilities range from $0.811 \mathrm{GPa}^{-1}$ at 313.12 K to $1.069 \mathrm{GPa}^{-1}$ at 362.89 K at approximately 1 MPa .

The isobaric thermal expansivities for hexan-2-ol, octan-1ol, and decan-1-ol are plotted in Figures 14 to 16. The isobaric thermal expansivity follows similar behavior of $K_{\mathrm{T}}$. $\alpha_{\mathrm{p}}$ increases as the temperature was increased at constant pressure. On the other hand, $\alpha_{p}$ decreases as the pressure was increased at constant temperature, as is depicted in Figures 14 to 16 for hexan-2-ol, octan-1-ol, and decan-1-ol. For hexan-2-ol, the isobaric thermal expansivities range from $0.967 \mathrm{~K}^{-1}$ at 313.13

Table 8. Calculated Values of Isothermal Compressibility, $K_{T}$, and Isobaric Thermal Expansivity, $\boldsymbol{\alpha}_{\mathrm{p}}$, for Decan-1-ol

| $T=313.12 \mathrm{~K}$ |  |  | $T=323.09 \mathrm{~K}$ |  |  | $T=333.04 \mathrm{~K}$ |  |  | $T=342.98 \mathrm{~K}$ |  |  | $T=352.86 \mathrm{~K}$ |  |  | $T=362.89 \mathrm{~K}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $p$ | $K_{\text {T }}$ | $\alpha_{\text {p }} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ | $p$ | K | $\alpha_{p} \cdot 10^{3}$ | $p$ | K | $\alpha_{p} \cdot 10^{3}$ | $p$ | $K_{\text {T }}$ | $\alpha_{p} \cdot 10^{3}$ |
| MPa | $\mathrm{GPa}^{-1}$ | K | MPa | $\mathrm{GPa}^{-1}$ | $\mathrm{K}^{-1}$ | MPa | $\mathrm{GPa}^{-1}$ | K | MPa | $\mathrm{GPa}^{-1}$ | K | MPa | $\mathrm{GPa}^{-1}$ | K | MPa | $\mathrm{GPa}^{-1}$ | $\mathrm{K}^{-1}$ |
| 1.025 | 0.811 | 0.840 | 002 | 0.860 | 0.867 | . 046 | 0.910 | . 890 | 1.058 | 0.961 | 0.910 | 1.069 | 1.014 | 0.926 | 1.077 | 1.069 | 0.941 |
| 2.002 | 0.803 | 0.835 | 2.011 | 0.851 | 0.862 | 2.018 | 0.900 | 0.885 | 2.045 | 0.951 | 0.905 | 2.043 | 1.004 | 0.921 | 2.027 | 1.058 | 0.936 |
| 2.995 | 0.795 | 0.831 | 3.019 | 0.842 | 0.857 | 3.008 | 0.891 | 0.880 | 3.022 | 0.941 | 0.900 | 3.040 | 0.993 | 0.916 | 3.089 | 1.046 | 0.930 |
| 4.013 | 0.786 | 0.826 | 4.014 | 0.833 | 0.853 | 4.012 | 0.882 | 0.875 | 4.035 | 0.931 | 0.894 | 4.048 | 0.982 | 0.911 | 4.047 | 1.036 | 0.925 |
| 5.004 | 0.778 | 0.822 | 5.006 | 0.825 | 0.848 | 5.059 | 0.872 | 0.870 | 5.028 | 0.922 | 0.889 | 5.038 | 0.972 | 0.905 | 5.061 | 1.025 | 0.919 |
| 5.994 | 0.770 | 0.817 | 6.012 | 0.816 | 0.843 | 6.016 | 0.863 | 0.865 | 6.030 | 0.912 | 0.884 | 6.043 | 0.962 | 0.900 | 6.060 | 1.014 | 0.914 |
| 7.003 | 0.762 | 0.813 | 7.002 | 0.808 | 0.839 | 7.022 | 0.855 | 0.861 | 7.023 | 0.903 | 0.879 | 7.038 | 0.952 | 0.895 | 7.041 | 1.004 | 0.909 |
| 7.997 | 0.755 | 0.808 | 8.003 | 0.800 | 0.834 | 8.014 | 0.846 | 0.856 | 8.028 | 0.894 | 0.874 | 8.039 | 0.942 | 0.890 | 8.049 | 0.993 | 0.904 |
| 9.000 | 0.747 | 0.804 | 9.008 | 0.791 | 0.829 | 9.015 | 0.837 | 0.851 | 9.062 | 0.884 | 0.869 | 9.040 | 0.933 | 0.885 | 9.049 | 0.983 | 0.899 |
| 9.994 | 0.740 | 0.799 | 10.006 | 0.783 | 0.825 | 10.015 | 0.829 | 0.846 | 10.035 | 0.875 | 0.865 | 10.038 | 0.923 | 0.880 | 10.052 | 0.973 | 0.893 |
| 10.995 | 0.732 | 0.795 | 11.000 | 0.776 | 0.820 | 11.019 | 0.820 | 0.842 | 11.029 | 0.867 | 0.860 | 11.032 | 0.914 | 0.875 | 11.045 | 0.963 | 0.888 |
| 11.995 | 0.725 | 0.791 | 12.002 | 0.768 | 0.816 | 12.007 | 0.812 | 0.837 | 12.064 | 0.858 | 0.855 | 12.032 | 0.905 | 0.870 | 12.044 | 0.953 | 0.884 |
| 12.997 | 0.718 | 0.787 | 13.002 | 0.760 | 0.812 | 13.019 | 0.804 | 0.833 | 13.023 | 0.849 | 0.851 | 13.040 | 0.896 | 0.866 | 13.054 | 0.944 | 0.879 |
| 13.996 | 0.711 | 0.783 | 14.000 | 0.753 | 0.807 | 14.019 | 0.796 | 0.828 | 14.042 | 0.841 | 0.846 | 14.046 | 0.887 | 0.861 | 14.053 | 0.934 | 0.874 |
| 14.998 | 0.704 | 0.778 | 15.017 | 0.745 | 0.803 | 15.014 | 0.788 | 0.824 | 15.022 | 0.833 | 0.841 | 15.043 | 0.878 | 0.856 | 15.052 | 0.925 | 0.869 |
| 15.990 | 0.697 | 0.774 | 16.003 | 0.738 | 0.799 | 16.021 | 0.781 | 0.819 | 16.022 | 0.824 | 0.837 | 16.037 | 0.869 | 0.852 | 16.056 | 0.916 | 0.864 |
| 16.995 | 0.690 | 0.770 | 17.015 | 0.731 | 0.795 | 17.026 | 0.773 | 0.815 | 17.021 | 0.816 | 0.833 | 17.040 | 0.861 | 0.847 | 17.063 | 0.906 | 0.860 |
| 17.986 | 0.684 | 0.766 | 18.006 | 0.724 | 0.790 | 18.023 | 0.765 | 0.811 | 18.034 | 0.808 | 0.828 | 18.046 | 0.852 | 0.843 | 18.062 | 0.898 | 0.855 |
| 18.992 | 0.677 | 0.762 | 19.007 | 0.717 | 0.786 | 19.018 | 0.758 | 0.807 | 19.025 | 0.801 | 0.824 | 19.040 | 0.844 | 0.838 | 19.062 | 0.889 | 0.850 |
| 19.993 | 0.671 | 0.759 | 20.007 | 0.710 | 0.782 | 20.025 | 0.751 | 0.802 | 20.038 | 0.793 | 0.819 | 20.064 | 0.835 | 0.834 | 20.068 | 0.880 | 0.846 |
| 20.999 | 0.664 | 0.755 | 21.002 | 0.703 | 0.778 | 21.020 | 0.744 | 0.798 | 21.018 | 0.785 | 0.815 | 21.048 | 0.828 | 0.829 | 21.072 | 0.871 | 0.841 |
| 21.509 | 0.661 | 0.753 | 22.014 | 0.697 | 0.774 | 22.032 | 0.736 | 0.794 | 22.035 | 0.778 | 0.811 | 22.049 | 0.820 | 0.825 | 22.063 | 0.863 | 0.837 |

K to $1.277 \mathrm{~K}^{-1}$ at 362.73 K at approximately 1 MPa . The isobaric thermal expansivities for octan-1-ol range from 0.804 $\mathrm{K}^{-1}$ at 313.14 K to $0.984 \mathrm{~K}^{-1}$ at 362.77 K at approximately 1 MPa. Meanwhile, for decan-1-ol the isobaric thermal expansivities range from $0.840 \mathrm{~K}^{-1}$ at 313.12 K to $0.941 \mathrm{~K}^{-1}$ at 362.89 K at approximately 1 MPa .

## Conclusions

Compressed liquid densities of hexan-2-ol, octan-1-ol, and decan-1-ol were reported at temperatures from ( 313 to 363 ) K and pressures up to 22 MPa . New experimental liquid densities for hexan-2-ol were reported at high pressure. These sets of data represent the first reported in the literature for hexan-2-ol at pressures higher than 0.1 MPa . Two equations were used to successfully correlate the experimental density data. Both equations were capable to correlate the reported densities for each alcohol within the experimental uncertainty. The obtained densities (or correlations) of octan-1-ol and decan-1-ol were compared with literature data and available correlations. Good agreement was found with literature data in the ranges of temperature and pressure measured. The extrapolation at atmospheric pressure was in good agreement with selected data published in the literature for the three alcohols. The isothermal compresibilities and isobaric thermal expansivities were calculated with the 5-parameter equation. The uncertainties of these derived properties were estimated to be better than $\pm 1.6 \%$ and $\pm 0.8 \%$. The influence of temperature and pressure on these properties was discussed.

## Literature Cited

(1) Zéberg-Mikkelsen, C. K.; Andersen, S. I. Density Measurements under Pressure for the Binary System 1-Propanol + Toluene. J. Chem. Eng. Data 2005, 50, 524-528.
(2) Shahidzadeh, N.; Bonn, D.; Meunier, J.; Nabavi, M.; Airiau, M.; Morvan, M. Dynamics of Spontaneous Emulsification for Fabrication of Oil in Water Emulsions. Langmuir 2000, 16, 9703-9708.
(3) Fandary, M. S.; Aljimaz, A. S.; Alkandary, J. A.; Fahim, M. A. LiquidLiquid Equilibria of Water + Ethanol + Reformate at Different Temperatures. J. Chem. Eng. Data 2002, 47, 487-491.
(4) Graziano, G. Entropy Convergence in the Hydration Thermodynamics of $n$-Alcohols. J. Phys. Chem. B 2005, 109, 12160-12166.
(5) Baysal, T.; Ersus, S.; Starmans, D. A. J. Supercritical $\mathrm{CO}_{2}$ Extraction of $\beta$-Carotene and Lycopene from Tomato Paste Waste. J. Agric. Food Chem. 2000, 48, 5507-5511.
(6) Sovova, H. Solubility of Ferulic Acid in Supercritical Carbon Dioxide with Ethanol as Cosolvent. J. Chem. Eng. Data 2001, 46, 1255-1257.
(7) Leal, P. F.; Braga, M. E. M.; Sato, D. N.; Carvalho, J. E.; Marques, M. O. M.; Meireles, M. A. A. Functional Properties of Spice Extracts Obtained via Supercritical Fluid Extraction. J. Agric. Food Chem. 2003, 51, 2520-2525.
(8) Montero, O.; Macias-Sanchez, M. D.; Lama, C. M.; Lubian, L. M.; Mantell, C.; Rodriguez, M.; de la Ossa, E. M. Supercritical $\mathrm{CO}_{2}$ Extraction of $\beta$-Carotene from a Marine Strain of the Cyanobacterium Synechococcus Species. J. Agric. Food Chem. 2005, 53, 9701-9707.
(9) Mukhopadhya, M. Natural Extracts using Supercritical Carbon Dioxide; CRC Press: Boca Raton, FL, 2000.
(10) Zúñiga-Moreno, A.; Galicia-Luna, L. A. Densities of 1-Propanol and 2-Propanol via a Vibrating Tube Densimeter from 313 to 363 K and up to 25 MPa . J. Chem. Eng. Data 2002, 47, 155-160.
(11) Zúñiga-Moreno, A.; Galicia-Luna, L. A. Compressed Liquid Densities of Carbon Dioxide + Ethanol Mixtures at four Compositions via a Vibrating Tube Densimeter up to 363 K and 25 MPa . J. Chem. Eng. Data 2002, 47, 149-154.
(12) Zúñiga-Moreno, A.; Galicia-Luna, L. A.; Horstmann, S.; Ihmels, C.; Fischer, K. Compressed Liquid Densities and Excess Volumes for the binary Systems Carbon Dioxide + 1-Propanol and Carbon Dioxide + 2-Propanol Using a Vibrating Tube Densimeter up to $25 \mathrm{MPa} . J$. Chem. Eng. Data 2002, 47, 1418-1424.
(13) Zúñiga-Moreno, A.; Galicia-Luna, L. A.; Betancourt-Cárdenas, F. F.; Bernal-García, J. M. Compressed Liquid Densities and Excess Molar Volumes of $\mathrm{CO}_{2}+$ Hexan-1-ol Mixtures from (313 to 363) K and Pressures up to 25 MPa . J. Chem. Eng. Data 2006, 51, 1723-1730.
(14) Zúñiga-Moreno, A.; Galicia-Luna, L. A.; Camacho-Camacho, L. E. Compressed Liquid Densities of 1-Butanol and 2-Butanol at Temper-
atures from 313 K to 363 K and Pressures up to 25 MPa . J. Chem. Thermodyn. 2007, 39, 254-260.
(15) Zúñiga-Moreno, A.; Galicia-Luna, L. A.; Compressed Liquid Densities of 1-Pentanol and 2-Pentanol from 313 K to 363 K at Pressures to 25 MPa. Int. J. Thermophys. 2007, 28, 146-162.
(16) Elizalde-Solis, O.; Galicia-Luna, L. A. Solubilities and Densities of Capsaicin in Supercritical Carbon Dioxide at Temperatures from 313 to 333 K. Ind. Eng. Chem. Res. 2006, 45, 5404-5410.
(17) Cibulka, I.; Ziková, M. Liquid Densities at Elevated Pressures of 1-Alkanols from $\mathrm{C}_{1}$ to $\mathrm{C}_{10}$ : A Critical Evaluation of Experimental Data. J. Chem. Eng. Data 1994, 39, 876-886.
(18) Cibulka, I.; Hnedkovsky, L.; Takagi, T. P- $\rho-T$ Data of Liquids: Summarization and Evaluation. 4. Higher 1-Alkanols $\left(\mathrm{C}_{11}, \mathrm{C}_{12}, \mathrm{C}_{14}\right.$, $\mathrm{C}_{16}$ ), Secondary, Tertiary, and Branched Alkanols, Cycloalkanols, Alkanediols, Alkanetriols, Ether Alkanols, and Aromatic Hydroxy Derivatives. J. Chem. Eng. Data 1997, 42, 415-433.
(19) Apaev, T. A.; Gylmanov, A. A.; Akhmedova, G. S. Measurement of the Density of $n$-Octanol over a Wide Range of Temperatures and Pressures. Izv. Vyssh. Uchebn. Zaved., Neft Gaz 1987, 30 (10), 1932.
(20) Altunin, V. V.; Konikevich, E. I. Teplofiz. Svoistva Veshchestv Mater. 1980, 14, 97.
(21) Matsuo, S.; Makita, T. Volumetric Properties of 1-Alkanols at Temperatures in the Range 298 to 348 K and Pressures up to 40 MPa . Int. J. Thermophys. 1989, 10, 885-897.
(22) Uosaki, Y.; Kitaura, S.; Moryioshi, T. Compressions of 4-methyl-1,3-dioxolan-2-one and Some Alkanols at Pressures up to 200 MPa and at the Temperature 298.15 K. J. Chem. Thermodyn. 1992, 24, 559-560.
(23) Garg, S. K.; Banipal, T. S.; Ahluwalia, J. C. Densities, Molar Volumes, Cubic Expansion Coefficients, and Isothermal Compressibilities of 1-Alkanols from 323.15 to 373.15 K and at Pressures up to 10 MPa . J. Chem. Eng. Data 1993, 38, 227-230.
(24) Lee, M.-J.; Lo, C.-K.; Lin, H.-M. PVT Measurements for Mixtures of 1-Octanol with Oligomeric Poly(ethylene glycol) from 298 K to 338 K and Pressures up to 30 MPa . J. Chem. Eng. Data 1999, 44, 13791385.
(25) Dzida, M. Speeds of Sound, Densities, Isobaric Thermal Expansion, and Internal Pressures of Heptan-1-ol, Octan-1-ol, Nonan-1-ol, and Decan-1-ol at Temperatures from (293 to 318) K and Pressures up to 100 MPa . J. Chem. Eng. Data 2007, 52, 521-531.
(26) Kuss, E. Hochdruckunterschungen III: Die Viskosität von komprimierten Flüssigkeiten. (High-Pressure Investigation III: Viscosity of Compressed Liquids.) Z. Angew. Phys. 1955, 7, 372-378.
(27) Mamedov, I. A.; Aliev, A. M. VINITI 1980, 1-33.
(28) Shelkovenko, A. E.; Zolin, V. S.; Vasilkovskaya T. N.; Golubev I. F. VINITI 1983, 1-12.
(29) Apaev, T. A.; Gylmanov, A. A. Measurement of the Density of $n$-Decyl Alcohol over a Wide Range of Temperature and Pressure. Izv. Vyssh. Uchebn. Zaved. Neft Gaz 1990, 33, 22-39.
(30) Shakhverdiev, A. N.; Naziev, Ya. M.; Safarov, D. T.; Kechedzhiler, A. Thermodynamic Properties of n-Butanol-n-Decanol Solution at High Temperatures. Russ. J. Appl. Chem. 1996, 69, 1472-1476.
(31) Zúñiga-Moreno, A.; Galicia-Luna, L. A.; Camacho-Camacho, L. Compressed Liquid Densities and Excess Volumes of $\mathrm{CO}_{2}+$ Decane Mixtures from (313 to 363) K and Pressures up to 25 MPa . J. Chem. Eng. Data 2005, 50, 1030-1037.
(32) Zúñiga-Moreno, A.; Galicia-Luna, L. A. Compressed Liquid Densities and Excess Volumes for the Binary System $\mathrm{CO}_{2}+N$, $N$-Dimethylformamide (DMF) from ( 313 to 363 ) K and Pressures up to 25 MPa . J. Chem. Eng. Data 2005, 50, 1224-1233.
(33) Starling, R. B.; Han, M. S. Thermo Data Refined for LPG: Mixtures. Hydrocarbon Process. 1972, 51, 129-132.
(34) Zúñiga-Moreno, A.; Galicia-Luna, L. A.; Betancourt-Cárdenas, F. F. Compressed Liquid Densities and Excess Volumes of $\mathrm{CO}_{2}+$ Thiophene binary mixtures from 313 to 363 K and Pressures up to 25 MPa. Fluid Phase Equilib. 2005, 236, 193-204.
(35) Galicia-Luna, L. A.; Richon, D.; Renon, H. New Loading Technique for a Vibrating Tube Densimeter and Measurements of Liquid Densities up to 39.5 MPa for Binary and Ternary Mixtures of the Carbon Dioxide-Methanol-Propane System. J. Chem. Eng. Data 1994, 39, 424-431.
(36) Wagner, W.; Pruss, A. The IAPWS Formulation 1995 for the Thermodynamic Properties of Ordinary Water Substance for General and Scientific Use. J. Phys. Chem. Ref. Data 2002, 31, 387-535.
(37) Span, R.; Lemmon, E. W.; Jacobsen, R. T.; Wagner, W. A. Reference Quality Equation of State for Nitrogen. Int. J. Thermophys. 1998, 19, 1121-1132.
(38) Galicia-Luna, L. A.; Ortega-Rodríguez, A.; Richon, D. A. New Apparatus for the Fast Determination of High-Pressure Vapor-Liquid Equilibria of Mixtures and of Accurate Critical Pressures. J. Chem. Eng. Data 2000, 45, 265-271.
(39) Ortega, J. Densities and Thermal Expansivities of Hexanol Isomers at Moderate Temperatures. J. Chem. Eng. Data 1985, 30, 5-7.
(40) TRC Thermodynamic Tables, Non-Hydrocarbons; Thermodynamics Research Center, The Texas A\&M University System: College Station, TX, 1995.
(41) Iloukhani, H.; Parsa, J. B.; Saboury, A. A. Excess Molar Enthalpies of Binary Mixtures Containing $N, N$-Dimethylformamide + Six 2-Alkanols ( $\mathrm{C}_{3}$ to $\mathrm{C}_{8}$ ) at 300.15 K. J. Chem. Eng. Data 2000, 45, 10161018.
(42) Weng, W.-L.; Chen J.-T. Density and Viscosity Measurement of n-Butylamine with Hexyl Alcohol Isomer Binary Systems. J. Chem. Eng. Data 2004, 49, 1748-1751.
(43) Diaz-Peña, M.; Tardajos, G. Isothermal Compressibilities of n-1Alcohols from Methanol to 1-Dodecanol at 298.15, 308.15, 318.15, and 333.15 K. J. Chem. Thermodyn. 1979, 11, 441-445.
(44) Ortega, J. Densities and Refractive Indices of Pure Alcohols as a Function of Temperature. J. Chem. Eng. Data 1982, 27, 312-317.
(45) Rauf, M. A.; Stewart, G. H.; Farhataziz. Viscosities and Densities of Binary Mixtures of 1-Alkanols from 15 to $55^{\circ}$ C. J. Chem. Eng. Data 1983, 28, 324-328.
(46) Liew, K. Y.; Seng, C. E.; Ng, B. H. Viscosities of Long Chain $n$-Alcohols from 15 to $80{ }^{\circ} \mathrm{C}$. J. Solution Chem. 1993, 21, 10331040.
(47) Taylor, B. N.; Kuyatt, C. E. Guidelines for Evaluating and Expressing the Uncertainty of NIST Measurement Results; NIST Technical Note 1297; National Institute of Standards and Technology: Washington, DC, 1994; pp 1-24.

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