# Densities, Viscosities, and Speeds of Sound of Binary Liquid Mixtures of Sulfolane with Ethyl Acetate, *n*-Propyl Acetate, and *n*-Butyl Acetate at Temperature of (303.15, 308.15, and 313.15) K

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Density, viscosity, and speed of sound data for (sulfolane + ethyl acetate (EA)), (sulfolane + *n*-propyl acetate (PA)), and (sulfolane + *n*-butyl acetate (BA)) were determined at T = (303.15 to 313.15) K. From this data, excess molar volume and deviation in isentropic compressibility,  $\Delta \kappa_s$ , have been calculated. The computed properties were fit to a Redlich–Kister polynomial.

### Introduction

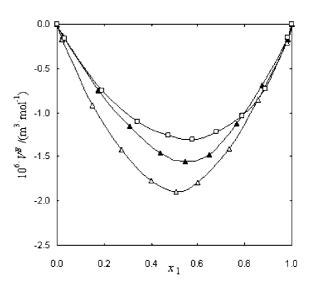
Physical properties of liquid mixtures are required in most of the engineering calculations where fluid flow or mixing is an important factor in many practical problems concerning mass transport applications. Sulfolane is an important industrial solvent that has several advantageous physicochemical properties and the ability to extract monocyclic aromatic hydrocarbons from petroleum products. Mixtures of sulfolane with other solvents are also of particular interest. An understanding of the mixing behavior of sulfolane with esters is therefore important and has applications in many engineering areas. To the best of our knowledge, no extensive studies have been made on the mixtures of sulfolane with esters. In a continuation of our ongoing program of research,<sup>1–3</sup> we now report the results of density, viscosity, and speed of sound for the binary mixtures of sulfolane with ethyl acetate, *n*-propyl acetate, and *n*-butyl acetate over the entire range of composition at T = (303.15 to 313.15) K. With this data, the excess molar volume and deviation in isentropic compressibility have been computed. These results have been fitted to the Redlich-Kister polynomial equation using a multiparametric nonlinear regression analysis technique to derive the binary coefficients and to estimate the standard deviation ( $\sigma$ ) between experimental and calculated data.

# **Experimental Procedure**

*Materials.* Ethyl acetate, *n*-propyl acetate, and *n*-butyl acetate that were all supplied by Sigma-Aldrich with stated purities of better than 99 % were stored over molecular sieves (0.3 nm Merck, India). Sulfolane with a purity of 99 % was provided by Sigma-Aldrich Chemicals and was used without further purification. To minimize the contact of this deliquescent reagent with moist air, the product was kept in sealed bottles in a desiccator. The purity of the substances was determined by GLC. Densities and viscosities of pure substances and their comparison with literature values are listed in Table 1.<sup>4-14</sup>

Apparatus and Procedure. Binary mixtures were prepared by mass in airtight bottles. The mass measurements were performed on a Dhona 100 DS (India) single-pan analytical

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**Figure 1.** Plots of excess molar volume,  $V^{\text{E}}$ , of the sulfolane (1) + esters (2) system as a function of mole fraction at T = 308.15 K:  $\triangle$ , ethyl acetate;  $\blacktriangle$ , *n*-propyl acetate;  $\square$ , *n*-butyl acetate. The symbols represent experimental values.

balance with a resolution of  $\pm 0.01 \cdot 10^{-6}$  kg. The required properties of the mixture were measured on the same day. The uncertainty in mole fraction was estimated to be less than  $\pm 1 \cdot 10^{-4}$ . The detailed procedures for measuring density and viscosity have been described in our previous publication.<sup>15</sup>

The speed of sound was measured with a single-crystal variable-path interferometer (Mittal Enterprises, India) operating at a frequency of 2 MHz that had been calibrated with water and benzene. The detailed procedure was described in our previous papers.<sup>2,3</sup> The uncertainty in speed of sound was found to be  $\pm 0.2$  %. In all property measurements, the temperature was controlled within  $\pm 0.01$  K using a constant temperature bath (INSREF model IRI-016 C, India) by circulating water from the thermostat.

# **Results and Discussion**

Experimental values of densities,  $\rho$ , viscosities,  $\eta$ , speeds of sound, u, and excess molar volumes,  $V^{\text{E}}$ , for the binary mixtures

Table 1. Comparison of Experimental Densities,  $\rho$ , Viscosities,  $\eta$ , and Speeds of Sound, u, of Pure Components with Available Literature at Different Temperatures

		$ ho \cdot 10^{-3} / \text{kg} \cdot \text{m}^{-3}$		$\eta \cdot 10^3$ /mPa · s		$u/m \cdot s^{-1}$	
component	<i>T</i> /K	exptl	lit.	exptl	lit.	exptl	lit.
sulfolane	298.15	1.2639	$1.2640^{14}$			1601	
	303.15	1.2618	$1.2618^4$	10.0304	$10.0742^{5}$	1588	1588.8 <sup>13</sup>
	313.15	1.2516	$1.2519^{5}$	7.8365		1558	
ethyl acetate	298.15	0.8951	$0.8946^{6}$	1.3716	$1.3710^{7}$	1142	
	303.15	0.8894	$0.8896^{11}$	0.3806		1122	$1119^{11}$
	308.15	0.8839	0.8832 <sup>9</sup>	0.3622		1101	
<i>n</i> -propyl acetate	298.15	0.8837	0.88317	1.3838	1.38357	1156	
<i>n</i> -butyl acetate	298.15	0.8756	$0.8759^{7}$	1.3934	1.39317	1203	120112
	303.15	0.8716	0.8713 <sup>8</sup>	0.6072	$0.6080^{10}$	1176	$1176^{11}$
	313.15	0.8620	$0.8618^{10}$	0.5340		1135	

of sulfolane with ethyl acetate, *n*-propyl acetate, and *n*-butyl acetate at T = (303.15 to 313.15) K are listed as a function of the mole fraction of sulfolane in Table 2.

The density values have been used to calculate excess molar volumes,  $V^{E}$ , using the following equation

$$V^{\rm E}/({\rm m}^3 \cdot {\rm mol}^{-1}) = (x_1 M_1 + x_2 M_2)/\rho_{\rm m} - (x_1 M_1/\rho_1 + x_2 M_2/\rho_2)$$
(1)

where  $\rho_{\rm m}$  is the density of the mixture and  $x_1$ ,  $M_1$ ,  $\rho_1$  and  $x_2$ ,  $M_2$ , and  $\rho_2$  are the mole fraction, molar mass, and density of pure components, respectively.

The speed of sound, u, was used to calculate the isentropic compressibility,  $\kappa_s$ , using

$$\kappa_{\rm s} = 1/u^2 \rho$$
 (2)

The deviation from isentropic compressibility,  $\Delta \kappa_s$ , has been evaluated using the equation

$$\Delta \kappa_{\rm s} / ({\rm m}^2 \cdot {\rm N}^{-1}) = \kappa_{\rm s} - (\Phi_1 \kappa_{\rm s1} + \Phi_2 \kappa_{\rm s2}) \tag{3}$$

where  $\kappa_{s1}$ ,  $\kappa_{s2}$ , and  $\kappa_s$  are the isentropic compressibility of the pure components and observed isentropic compressibility of liquid mixture, respectively. In eq 4,  $\Phi_i$  is the volume fraction and is calculated from the individual pure molar volumes,  $V_i$ , with the relation

$$\Phi_i = x_i V_i / (\Sigma x_i V_i) \tag{4}$$

The excess or deviation properties,  $Y^{\text{E}}$ , were fitted by the method of nonlinear least-squares to a Redlich-Kister-type polynomial<sup>16</sup>

$$Y^{\rm E} = x_1 x_2 \Sigma A_i (x_1 - x_2)^i \tag{5}$$

In each case, the optimum number of coefficients,  $A_i$ , was determined from an examination of the variation of standard deviation,  $\sigma$ , as calculated by

$$\sigma(Y^{\rm E}) = \left[\Sigma \left(Y_{\rm obsd}^{\rm E} - Y_{\rm calcd}^{\rm E}\right)^2 / (n-m)\right]^{1/2} \tag{6}$$

where *n* represents the number of experimental points and *m* is the number of coefficients. It is found that for the solution of the fifth degree polynomial, the agreement between the experimental values and the calculated values is satisfactory. The derived parameters,  $A_i$ , and the estimated standard deviation,  $\sigma$ , for  $V^{\rm E}$  and  $\Delta \kappa_s$  are given in Table 3.

*Excess Molar Volume.* Excess molar volumes of (sulfolane + esters) at T = 308.15 K are shown in Figure 1. The values of  $V^{\rm E}$  are negative for all (sulfolane + EA), (sulfolane +

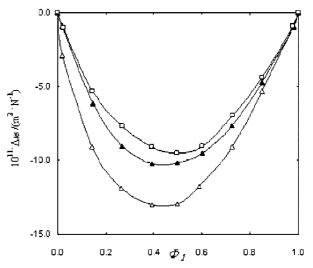
PA), and (sulfolane + BA) over the whole mole fraction range and are less negative with increasing chain length of the ester molecules. The negative values of  $V^{E}$  vary in the following order: EA < PA < BA < 0. The  $V^{E}$  values are less negative with increasing temperature in the case of BA, whereas no particular trend was observed in the case of EA and PA. These plots are not furnished to avoid overcrowding.

**Deviation in Isentropic Compressibility.** The  $\Delta \kappa_s$  values are negative over the whole composition range for all mixtures and become more negative at higher temperatures. It can be pointed out that the influence of the structure of the homologous series of esters on the isentropic compressibility behavior is very marked. An inspection of Figure 2 reveals that the  $\Delta \kappa_s$  values become more negative with decreasing chain length of the ester.

In the present study, the behavior of  $V^{\rm E}$  and  $\Delta \kappa_{\rm s}$  are similar in nature. The sign of  $\Delta \kappa_{\rm s}$  supports the postulates used to interpret the sign of excess molar volume. The negative  $V^{\rm E}$  and  $\Delta \kappa_{\rm s}$  values may result from dipole–dipole and dipole-induced dipole interactions<sup>13,17–19</sup> that enhance the solvent structure in the mixture, in turn making negative contributions to  $V^{\rm E}$  and  $\Delta \kappa_{\rm s}$ .

### Conclusions

The experimental values of density, viscosity, and speed of sound and calculated excess molar volume and deviation in



**Figure 2.** Plots of deviation in isentropic compressibility,  $\Delta \kappa_s$ , of the sulfolane (1) + esters (2) system as a function of volume fraction at T = 308.15 K:  $\triangle$ , ethyl acetate;  $\blacktriangle$ , *n*-propyl acetate;  $\square$ , *n*-butyl acetate. The symbols represent experimental values.

Table 2. Values of Density,  $\rho$ , Viscosity,  $\eta$ , Speed of Sound, u, and Excess Molar Volume,  $V^{E}$ , for the Binary Liquid Mixtures at Temperature T

$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$		$\rho \cdot 10^{-3}$	$\eta \cdot 10^3$	u	$V^{E} \cdot 10^{6}$		$\rho \cdot 10^{-3}$	$\eta \cdot 10^3$	<u> </u>	$V^{E} \cdot 10^{6}$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$x_1$	$kg \cdot m^{-3}$	mPa•s	$\overline{\mathbf{m} \cdot \mathbf{s}^{-1}}$	$\overline{m^3 \cdot mol^{-1}}$	$x_1$	$\overline{\text{kg} \cdot \text{m}^{-3}}$	mPa•s	$\overline{\mathbf{m} \cdot \mathbf{s}^{-1}}$	m <sup>3</sup> ·mol <sup>-</sup>
$\begin{array}{c c c c c c c c c c c c c c c c c c c $					Sulfolane (1) +	Ethyl Acetate				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $					T/K =	= 303.15				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.0000	0.8894	0.3806	1122			1.1276	2,0539	1408	-1.633
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0218									-1.300
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.1511									-0.757
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.2748									-0.114
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.4012									0.000
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.5068					1.0000	1.2010	10.0501	1500	0.000
$\begin{array}{c c c c c c c c c c c c c c c c c c c $					T/K =	308 15				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000	0.8839	0 3622	1101			1 1239	1 8819	1398	-1.787
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0218									-1.414
$\begin{array}{c} 748 & 0.9977 & 0.7300 & 1241 & -1.418 & 0.9799 & 1.2519 & 8.0778 & 1559 & -1.877 \\ 1012 & 1.0488 & 1.0424 & 1301 & -1.771 & 1.0000 & 1.2570 & 8.7947 & 1576 & 0.9968 \\ 1.0903 & 1.3942 & 1355 & -1.897 & & & & & & & & & & & & & & & & & & &$	0.1511									-0.856
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.2748									-0.207
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.4012									0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.5068									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					T/K =	313 15				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000	0.8758	0 3426	1082			1 1167	1 7516	1397	-1.789
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0218									-1.410
$\begin{array}{c} 748 \\ 0.9899 \\ 0.6874 \\ 0.12 \\ 1.0405 \\ 0.9781 \\ 1.2925 \\ 1.346 \\ -1.338 \\ \\ \hline Sulfolane (1) + n-Propyl Acetate (2) \\ \hline T/K = 303.15 \\ \hline T/K = 308.15 \\ \hline T/K = 303.15 \\ $	0.1511									-0.857
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.2748									-0.163
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.4012									0.000
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.5068									
$\begin{array}{c c c c c c c c c c c c c c c c c c c $					Sulfolane $(1) \pm n$	-Propyl Acetat	e (2)			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							C (2)			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000	0.0777	0.4070	1140			1 12 10	2 (211	1.410	1 457
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000									-1.457
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0247									-1.113
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										-0.671
1468       1.0846       1.9225       1368       -1.551         T/K = 308.15         T/K = 308.15         0.000       0.6489       1.1201       2.3752       1410       -1         1247       0.8819       0.4827       1147       -0.134       0.7639       1.1647       3.5015       1469       -1         746       0.9358       0.6764       1203       -0.745       0.8733       1.2510       8.1319       1573       -0         T/K = 313.15         T/K = 313.15         T/K = 308.15         00.8667       0.4329       1126       0.000       0.6489       1.1141       2.1758       1401       -1         T/K = 313.15         T/K = 303.15         0000       0.8667       0.4329       1126       0.000       1.2516       7.8365       1558       0         0.798       0.8733       1.2022       4.6616       1510       -(         1416       1.0324       1.2220       1301       -1.555       1.0000       1.2516       7.8365       1558       0       0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-0.140</td></t<>										-0.140
T/K = 308.15 $T/K = 308.15$ $T/K = 308.15$ $T/K = 308.15$ $T/K = 308.15$ $T/K = 313.15$ $T/K = 313.15$ $T/K = 308.15$ $T/K$						1.0000	1.2018	10.0304	1588	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.5408	1.0040	1.9223	1508						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000	0.0721	0.4505	1120			1 1201	0 0750	1.410	1 474
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000									-1.474
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0247									-1.127
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.1746									-0.692
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$										-0.175
T/K = 313.15 $T/K = 313.15$ $T/K = 313.15$ $T/K = 303.15$ $T/K = 308.15$ $T/K = 313.15$	0.4416					1.0000	1.2570	8.7947	1370	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.5408	1.0790	1.7017	1559						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000	0.0447	0.4220	1106			1 1 1 4 1	0 1750	1.40.1	1 400
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000									-1.498
$\begin{array}{cccccccccccccccccccccccccccccccccccc$										-1.191
$\begin{array}{cccccccccccccccccccccccccccccccccccc$										-0.724
5468       1.0740       1.6173       1352       -1.623         Sulfolane (1) + n-Butyl Acetate (2)         T/K = 303.15 $7/K = 303.15$ $7/K = 308.15$ $7/K = 30000$ $0.8876$	0.3110									-0.165
Sulfolane (1) + n-Butyl Acetate (2) $T/K = 303.15$ $T/K = 303.15$ $1.1205  3.0273  1424  -1$ $1.0808  0.6426  1182  -0.068  0.7887  1.1682  4.2748  1477  -1$ $1.903  0.9323  0.8950  1232  -0.624  0.8876  1.2122  6.1997  1528  -0$ $1.040  0.9836  1.2542  9.0492  1577  -0$ $1.0361  1.7220  1327  -1.291  1.0000  1.2618  10.0304  1588  0$ $1.0785  2.2995  1372  -1.396$ $T/K = 308.15$ $1.0000  0.8671  0.5687  1155  0.000  0.6793  1.1144  2.7172  1418  -1$ $1.0311  0.8769  0.6016  1164  -0.162  0.7887  1.1621  3.8367  1468  -1$ $1.903  0.9286  0.8248  1212  -0.746  0.8876  1.2071  5.4987  1520  -0$ $1.0000  0.9809  1.1452  1261  -1.100  0.9836  1.2501  7.9251  1572  -0$ $1.0000  1.2670  3.0916  1366  -1.258  1.0000  1.2570  8.7947  1576  0$ $T/K = 313.15$	0.4416					1.0000	1.2310	7.8303	1558	0.000
T/K = 303.15 $T/K = 303.15$ $T/K = 308.05$ $T/K = 308.05$ $T/K = 308.15$ $T/K = 313.15$	0.5400	1.0740	1.0175	1552						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						•	e (2)			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$										
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0000									-1.336
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0311									-1.131
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.1903									-0.750
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.3402									-0.098
T/K = 308.15 $T/K = 308.15$ $1155   0.000   0.6793   1.1144   2.7172   1418   -1$ $1418   -1$ $10311   0.8769   0.6016   1164   -0.162   0.7887   1.1621   3.8367   1468   -1$ $1903   0.9286   0.8248   1212   -0.746   0.8876   1.2071   5.4987   1520   -0$ $1.452   1261   -1.100   0.9836   1.2501   7.9251   1572   -0$ $1740   1.0309   1.5770   1316   -1.258   1.0000   1.2570   8.7947   1576   0$ $T/K = 313.15$	0.4740					1.0000	1.2618	10.0304	1588	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.5789	1.0785	2.2995	13/2						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$										
1903         0.9286         0.8248         1212 $-0.746$ 0.8876         1.2071         5.4987         1520 $-0.746$ 0402         0.9809         1.1452         1261 $-1.100$ 0.9836         1.2501         7.9251         1572 $-0.746$ 1740         1.0309         1.5770         1316 $-1.258$ 1.0000         1.2570         8.7947         1576 $0.7789$ 1.0727         2.0816         1366 $-1.303$ $T/K = 313.15$	0.0000									-1.224
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0311									-1.028
1740 $1.0309$ $1.5770$ $1316$ $-1.258$ $1.0000$ $1.2570$ $8.7947$ $1576$ $0.7789$ $1.0727$ $2.0816$ $1366$ $-1.303$ $T/K = 313.15$ $T/K = 313.15$	0.1903									-0.733
5789 1.0727 2.0816 1366 $-1.303$ T/K = 313.15	0.3402									-0.154
T/K = 313.15	0.4740					1.0000	1.2570	8.7947	1576	0.000
	0.5789	1.0/2/	2.0810	1300						
	0.0000	0.01751	0					··		
	0.0000	0.8620	0.5340	1135	0.000	0.6793	1.1088	2.4714	1408	-1.219
	0.0311									-1.033
	0.1903									-0.726
	0.3402									-0.164
	0.4740					1.0000	1.2516	1.8365	1558	0.000
5789 1.0671 1.9028 1354 -1.295	0.5789	1.06/1	1.9028	1354	-1.295					

Table 3. Binary Coefficients  $(A_i)$  and Standard Errors  $(\sigma)$  of Sulfolane (1) + Esters (2)

function	<i>T</i> /K	$A_0$	$A_1$	$A_2$	$A_3$	$A_4$	σ			
Sulfolane $(1)$ + Ethyl Acetate $(2)$										
$V^{E} \cdot 10^{6}$	303.15	-6.824	-0.68	2.38	0.20	-0.4	0.021			
$m^3 \cdot mol^{-1}$	308.15	-7.556	-0.13	3.05	0.36	-4.4	0.024			
	313.15	-7.345	-0.42	1.08	1.62	-1.8	0.018			
$\Delta \kappa_{\rm s} \cdot 10^{11}$	303.15	-45.65	10.46	1.9	9.3	-10	0.070			
$m^2 \cdot N^{-1}$	308.15	-51.78	11.2	7.5	25.2	-43	0.30			
	313.15	-57.76	6.61	4.9	8.9	-11.7	0.083			
Sulfolane (1) + $n$ -Propyl Acetate (2)										
$V^{E} \cdot 10^{6}$	303.15	-6.216	-0.72	1.2	1.27	-2.0	0.022			
$m^3 \cdot mol^{-1}$	308.15	-6.166	-1.44	2.57	1.22	-3.5	0.027			
	313.15	-6.477	-1.06	2.44	0.66	-3.47	0.017			
$\Delta \kappa_{\rm s} \cdot 10^{11}$	303.15	-39.07	9	-10.1	-0.8	13	0.20			
$m^2 \cdot N^{-1}$	308.15	-40.96	8.38	-6	-1.3	3.4	0.096			
	313.15	-44.83	7.39	1.8	-0.7	-8.1	0.042			
Sulfolane $(1) + n$ -Butyl Acetate $(2)$										
$V^{\rm E} \cdot 10^{6}$	303.15	-5.293	-2.12	-0.99	-0.69	1.36	0.017			
$m^3 \cdot mol^{-1}$	308.15	-5.140	-0.913	-0.42	-0.95	-2.14	0.0088			
	313.15	-5.103	-0.94	-0.71	-0.6	-2.1	0.011			
$\Delta \kappa_s \cdot 10^{11}$	303.15	-32.81	3.8	-11.1	5.5	15.7	0.17			
$m^2 \cdot N^{-1}$	308.15	-38.20	2.63	8.1	6.1	-17.3	0.094			
	313.15	-42.80	-1	5.7	12.9	-16.5	0.10			

speed of sound for the binary mixtures of sulfolane + ethyl acetate, + n-propyl acetate, and + n-butyl acetate at T = (303.15 to 313.15) K are reported. The results are correlated using the Redlich-Kister polynomial equation.

### Acknowledgment

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