Articles

Measurements of the Surface Tension for the R290 + R32 Mixture^{\dagger}

Katsuyuki Tanaka* and Yukihiro Higashi

Department of Mechanical Systems and Design Engineering, Iwaki Meisei University, Iwaki, Fukushima 970-8551, Japan

There were no data of the surface tension for the R290 + R32 mixture which is expected as one of the new refrigerant mixtures, and its prediction is considered to be difficult because it is a mixture of a very polar molecule with a nonpolar molecule. In this work, the surface tension measurements for the R290 + R32 mixture were carried out by the differential capillary-rise method modified for measuring mixtures. Thirty-one, thirty-five, and thirty-three data points were obtained with changing the composition of the mixture at T = 280 K, 290 K, and 300 K, respectively. The experimental uncertainties of temperature and surface tension are estimated to be within 20 mK and 0.2 mN·m⁻¹, respectively. The excess molar surface tension is also calculated by the present data, and its uncertainty was estimated to be 0.3 mN·m⁻¹. The excess molar surface tension was correlated as a function of composition. The deviation of the present data from the present correlation was within the experimental uncertainty.

Introduction

Regarding the working fluids of refrigerators and heat pump systems, hydrofluorocarbons and their mixtures are shifting toward hydrocarbons such as R290 (propane: C_3H_8) and R600a (isobutane: *i*- C_4H_{10}) from viewpoints of ozone depletion and global warming. Although hydrocarbons have no ozone depletion potential and no global warming potential, their applications in home refrigerator and air-conditioning are problematic because of their flammability. Whereas R32 (difluoromethane: CH_2F_2) is a kind of hydrofluorocarbon, it has a low global warming potential and is superior as a refrigerant. The mixing of R32 with hydrocarbons is effective in their applications.

In recent years, thermophysical properties for mixtures composed of R290, R600a, and R32 have been measured in our laboratory. Vapor–liquid equilibrium measurements of their three binary mixtures,^{1–3} critical parameters, and saturated density measurements of their three binary mixtures,^{4–6} and surface tension measurement of the R290 + R600a mixture⁷ were conducted.

The surface tension, which is one of the important thermophysical properties of fluids, is required for the heat transfer solutions with boiling and condensation states. Its experimental data are necessary to refine the model for evaluating refrigerant mixtures and for designing refrigeration cycles. However, there were no data for this mixture.

In the present study, the surface tension of the R290 + R32 mixture has been measured by the differential capillary-rise method modified for measuring the mixture. Measurements are conducted at T = 280 K, 290 K, and 300 K with changing the composition of the mixture, and the excess molar surface tensions are calculated and correlated as a function of composition.

[†] Part of the special section "2008 European Conference on Thermophysical Properties".

1

Apparatus

The surface tension measurement for fluid mixtures was already conducted for the R290 + R600a system in our laboratory, and the apparatus and procedure are described in detail there.⁷ The apparatus was designed to measure the surface tension of the fluid mixture by the differential capillary-rise method. Two glass capillaries are placed vertically in a pressure vessel composed of a thick-walled Pyrex glass tube. Their inner radii of capillaries determined by means of a mercury thread are (0.4222 ± 0.0009) mm and (1.0050 ± 0.0012) mm. The sample is put in the pressure vessel whose temperature is kept constant to be within 10 mK by the thermostat. Temperature was measured with a 100 Ω platinum resistance thermometer with the thermometer bridge [ASL F250A] installed in the thermostat. It is calibrated against ITS-90 using a 25 Ω standard platinum resistance thermometer with the thermometer bridge [ASL F17A]. The experimental uncertainty of the temperature measurement is estimated to be within 20 mK. The second component of the mixture can be added to the pressure vessel for measurements at other compositions of the mixture. The pressure of the sample was measured by the precise digital pressure gauge [Paroscientific 2400A] to determine the composition of the sample from the vapor-liquid equilibrium relation. REFPROP⁸ ver.8.0 was used for calculations of vapor-liquid equilibrium relation. The experimental uncertainty of the pressure measurement is estimated to be within 0.02 %. The location of the bottom of the meniscus of the sample in each capillary is measured by the traveling microscope through the window of the thermostat. Measured values of the location of the meniscus were corrected by the Rayleigh equation.⁹ The corrected values were used for the difference of rise heights in the capillaries. The surface tension is determined by the following relation

$$\sigma = \frac{g(\rho' - \rho'')(h_1 - h_2)}{2(1/r_1 - 1/r_2)\cos\theta}$$
(1)

where the local gravitational acceleration g at Iwaki, Japan, is

^{*} To whom correspondence should be addressed. E-mail: ktanaka@iwakimu.ac.jp. Tel.: +81-246-29-7026. Fax: +81-246-29-0577.

Table 1. Experimental Surface Tensions for the R290 + R32 Mixture at T = 280.00 K

Table 2.	Experimental Surface	Tensions fo	or the	R290 +	R32
Mixture	at $T = 290.00 \text{ K}$				

290

Т	Р	$h_1 - h_2$	<i>x</i> _{R290}	σ	a^2
K	kPa	mm	$mol \cdot mol^{-1}$	$\overline{mN \cdot m^{-1}}$	$\overline{mm^2}$
280.00	1034.61	2.76	0.010	9.7	2.01
	1043.03	2.67	0.013	9.4	1.95
	1099.68	2.78	0.037	9.5	2.03
	1159.63	2.75	0.070	9.0	2.00
	1184.36	2.70	0.087	8.7	1.96
	1190.67	2.61	0.092	8.4	1.90
	1217.40	2.72	0.115	8.5	1.98
	1222.01	2.69	0.120	8.4	1.96
	1223.07	2.58	0.121	8.0	1.88
	1224.52	2.64	0.123	8.2	1.92
	1225.61	2.64	0.124	8.2	1.92
	1232.43	2.58	0.131	7.9	1.88
	1240.57	2.65	0.141	8.0	1.92
	1281.92	2.89	0.515	6.4	2.10
	1263.20	3.09	0.588	6.5	2.25
	1257.52	3.10	0.605	6.5	2.26
	1239.90	3.32	0.648	6.8	2.41
	1239.68	3.30	0.648	6.7	2.40
	1232.84	3.35	0.662	6.8	2.44
	1221.87	3.41	0.682	6.8	2.48
	1212.24	3.53	0.697	7.0	2.57
	1206.12	3.57	0.706	7.1	2.60
	1189.23	3.63	0.729	7.1	2.64
	1166.11	3.81	0.755	7.4	2.77
	1144.97	3.87	0.775	7.4	2.81
	1097.55	4.09	0.813	7.8	2.98
	1077.66	4.12	0.826	7.8	3.00
	935.20	4.56	0.898	8.4	3.31
	842.18	4.82	0.931	8.8	3.51
	807.51	4.86	0.942	8.9	3.54
	715.86	5.02	0.968	9.1	3.65

9.8002 m·s⁻². The contact angle θ is assumed to be zero based on the visual observation of the image magnified in the CRT monitor. Saturated densities ρ' and ρ'' are obtained from the calculations by the REFPROP ver.8.0. The experimental uncertainty of the surface tension measurement is estimated to be within 0.2 mN·m⁻¹.

The sample of R290 was supplied from Takachiho Chemical Industrial Co., Ltd., Japan. The purity of R290 was better than 99.9 mol %. The sample of R32 was supplied from Daikin Industrial Co., Ltd., Japan. The purity of R32 was better than 99.9999 mol %.

Experimental Results and Discussion

Thirty-one, thirty-five, and thirty-three data points of the surface tension against compositions were obtained on three isotherms of T = 280.00 K, 290.00 K, and 300.00 K, respectively. These data are listed in Tables 1 to 3. The capillary constant a^2 as expressed in eq 2 is also listed in Tables 1 to 3.

$$a^{2} = \frac{(h_{1} - h_{2})}{[(1/r_{1} - 1/r_{2})]\cos\theta} \frac{g}{g_{n}} = \frac{2\sigma}{g_{n}(\rho' - \rho'')}$$
(2)

where g_n denotes the normal gravitational acceleration of 9.80665 m·s⁻². The surface tension for the R290 + R32 mixture with relation to mole fraction of R290 was shown in Figure 1. The data in the mole fraction range from 0.2 to 0.5 of R290 could not be obtained. In this range, this mixture shows a strong positive pressure azeotrope, and the pressure becomes flat against mole fraction. So it was difficult to blend the secondary sample into near azeotrope compositions. From the measurements in this work, it is revealed that the behavior of the composition dependence of the surface tension for the R290 + R32 mixture shows simply convex downward. Calculations by

Т	Р	$h_1 - h_2$	<i>x</i> _{R290}	σ	a^2
K	kPa	mm	$mol \cdot mol^{-1}$	$\overline{mN \cdot m^{-1}}$	mm ²
0.00	1355.46	2.39	0.002	8.1	1.74
	1359.27	2.35	0.003	8.0	1.71
	1363.25	2.35	0.004	8.0	1.71
	1467.28	2.34	0.005	7.9	1.70
	1461.54	2.32	0.039	7.5	1.69
	1517.47	2.30	0.065	7.2	1.67
	1542.83	2.25	0.078	7.0	1.64
	1547.85	2.34	0.081	7.2	1.70
	1561.57	2.32	0.090	7.1	1.69
	1569.39	2.27	0.095	6.9	1.65
	1572.52	2.27	0.097	6.9	1.65
	1593.54	2.22	0.114	6.6	1.62
	1627.26	2.29	0.143	6.5	1.66
	1639.45	2.23	0.156	6.3	1.63
	1653.88	2.14	0.175	5.9	1.56
	1660.57	2.17	0.185	5.9	1.58
	1668.21	2.24	0.198	6.0	1.63
	1673.93	2.12	0.209	5.7	1.54
	1678.30	2.39	0.485	5.0	1.74
	1672.01	2.38	0.506	4.9	1.73
	1665.23	2.44	0.525	5.0	1.77
	1659.83	2.53	0.539	5.1	1.84
	1641.39	2.55	0.580	5.1	1.86
	1633.21	2.60	0.596	5.1	1.89
	1628.53	2.68	0.604	5.2	1.95
	1599.99	2.92	0.648	5.6	2.13
	1564.36	3.11	0.691	5.9	2.27
	1475.11	3.33	0.768	6.1	2.42
	1414.83	3.54	0.805	6.4	2.58
	1199.39	3.97	0.896	7.0	2.89
	1131.63	4.17	0.917	7.3	3.03
	1102.98	4.22	0.925	7.4	3.07
	897.69	4.44	0.975	7.7	3.23
	841.43	4.55	0.986	7.9	3.31
	773 92	4 63	0 000	8.1	3 37



Figure 1. Surface tension results for the R290 + R32 mixture with relation to mole fraction of R290: \bigcirc , present data at T = 280.00 K; \triangle , present data at T = 290.00 K; \times , present data at T = 300.00 K; ---, REFPROP⁸ ver.8.0.

the REFPROP ver.8.0 are also plotted in Figure 1 as broken lines. The model of Moldover and Rainwater¹⁰ is used in the REFPROP. The REFPROP calculations also show similar behavior. The present data at the R32-rich compositions are in good agreement with the REFPROP calculations, but the REFPROP calculations are larger up to about 1 mN·m⁻¹ than the present data at the R290-rich compositions. The present data will be incorporated for improvement of the model of the surface tension mixture.

The excess molar surface tension σ_m^{E} was also calculated from eq 3 for the binary mixtures and shown in Figure 2.

$$\sigma_{\rm m}^{\rm E} = \sigma_{\rm m} - (x_1 \sigma_1 + x_2 \sigma_2) \tag{3}$$

where 1, 2, and m refer to R290 of a first pure component, R32 of a second pure component, and mixture, respectively. The



Figure 2. Excess molar surface tension for the R290 + R32 mixture with relation to mole fraction of R290: \bigcirc , present data at T = 280.00 K; \triangle , present data at T = 290.00 K; \times , present data at T = 300.00 K; -, eq 4.

Table 3.	Experimental S	urface Tei	nsions for	the R2	290 +	R32
Mixture a	at $T = 300.00 \text{ K}$					

Т	Р	$h_1 - h_2$	<i>x</i> _{R290}	σ	a^2
K	kPa	mm	$mol \cdot mol^{-1}$	$\overline{mN \cdot m^{-1}}$	$\overline{mm^2}$
300.00	1839.91	1.91	0.020	6.0	1.39
	1909.67	1.89	0.045	5.7	1.38
	1999.70	1.88	0.087	5.4	1.37
	2037.48	1.88	0.110	5.2	1.36
	2052.59	1.80	0.120	5.0	1.31
	2057.09	1.81	0.124	5.0	1.32
	2105.88	1.75	0.149	4.6	1.27
	2092.64	1.77	0.154	4.7	1.29
	2140.52	1.69	0.220	4.1	1.23
	2093.35	2.19	0.573	4.0	1.59
	1989.33	2.59	0.682	4.5	1.88
	1948.11	2.68	0.692	4.7	1.95
	1933.25	2.70	0.703	4.7	1.96
	1897.92	2.83	0.744	4.9	2.06
	1863.74	2.93	0.748	5.1	2.13
	1840.87	2.93	0.761	5.0	2.13
	1820.31	2.94	0.771	5.1	2.14
	1824.77	3.00	0.782	5.1	2.18
	1783.29	3.03	0.790	5.2	2.20
	1704.57	3.22	0.824	5.5	2.34
	1728.90	3.20	0.834	5.4	2.33
	1666.58	3.27	0.838	5.5	2.38
	1628.50	3.31	0.852	5.6	2.41
	1588.51	3.42	0.865	5.8	2.49
	1537.91	3.47	0.881	5.8	2.53
	1497.46	3.56	0.893	6.0	2.59
	1482.54	3.54	0.897	5.9	2.58
	1430.99	3.58	0.911	6.0	2.60
	1404.09	3.71	0.918	6.2	2.70
	1319.76	3.81	0.938	6.4	2.77
	1106.05	4.07	0.982	6.8	2.96
	1031.29	3.99	0.994	6.7	2.90
	1002.83	4.11	0.999	6.9	2.99

values of surface tension for pure R32 and R290 were obtained from our previous work.^{11,12} The uncertainty of the excess molar surface tension was estimated to be 0.3 mN·m⁻¹ in consideration of the uncertainty of the surface tension for pure components, 0.1 mN·m⁻¹. As shown in Figure 2, all of the σ_m^{E} values for this system are negative. At the R32-rich compositions, the σ_m^{E} values are almost the same at all temperatures. At the R290rich compositions, those absolute values decrease with increasing temperature. The present σ_m^{E} data were correlated with the following polynomial-type Redlich–Kister equation¹³

$$\sigma_{\rm m}^{\rm E} = x_1 x_2 \sum_{i=0}^{1} A_i (1 - 2x_1)^i \tag{4}$$

where A_i denotes the adjustable parameters determined by the present data. The parameters A_0 and A_1 and the standard deviations STD are given in Table 4. The solid lines in Figure 2 are calculations from eq 4. The deviations of the σ_m^E value



Figure 3. Deviation of the excess molar surface tension from eq 4 for the R290 + R32 mixture with relation to mole fraction of R290: \bigcirc , present data at T = 280.00 K; \triangle , present data at T = 290.00 K; \times , present data at T = 300.00 K.



Figure 4. Comparison of the composition dependence of the surface tension at 300 K from correlations for the R290 + R32 mixture and the R290 + R600a mixture⁷ with relation to mole fraction of R290: -, R290 + R32; ---, R290 + R600a.

Table 4. Parameters A_i of Equation 4 and Standard DeviationsSTD of the Excess Molar Surface Tension for Isotherms

T/K	A_0	A_1	$STD/mN \cdot m^{-1}$
280.00	-12.669	-2.2188	0.12
290.00	-12.239	-2.6270	0.10
300.00	-11.396	-4.0371	0.08

from the present correlation were within the experimental uncertainty as shown in Figure 3.

The composition dependence of the surface tension for the R290 + R32 mixture and the R290 + R600a mixture⁷ is shown in Figure 4. That for the R290 + R600a mixture could be represented as the simple linear function against mole fraction. However, that for the R290 + R32 mixture is not linear and became concave. These behaviors denote the same tendency of the critical temperature for these mixtures.⁶

Conclusion

The surface tension of the R290 + R32 mixture was measured on three isotherms of 280.00 K, 290.00 K, and 300.00 K. The composition dependence of the surface tension for this mixture was revealed. The correlation of the excess molar surface tension was formulated based on the present data and can be represented within the experimental uncertainty.

Acknowledgment

We thank Daikin Industrial Co., Ltd., Japan, for furnishing and analyzing the purity of R32.

Literature Cited

- Kayukawa, Y.; Fujii, K.; Higashi, Y. Vapor-Liquid Equilibrium (VLE) Properties for the Binary Systems Propane (1) + n-Butane (2) and Propane (1) + Isobutane (3). J. Chem. Eng. Data 2005, 50, 579–582.
- (2) Higashi, Y. Vapor-Liquid Equilibria For The Binary Difluoromethane (R-32) + Propane (R-290) Mixture. *Int. J. Thermophys.* **1999**, 20, 507–518.

- (3) Akasaka, R.; Higashi, Y.; Tanaka, K.; Kayukawa, Y.; Fujii, K. Vapor-liquid equilibrium measurements and correlations for the binary mixture of difluoromethane + isobutane and the ternary mixture of propane + isobutane + difluoromethane. *Fluid Phase Equilib.* 2007, 261, 286–291.
- (4) Higashi, Y. Measurements of saturated densities and critical parameters for the propane+isobutane system. Proc. IIR-Gustav Lorentzen Conf. 2004, 128–135.
- (5) Higashi, Y. Experimental Determination of the Critical Locus for the Difluoromethane (R32) and Propane (R290) System. *Fluid Phase Equilib.* 2004, 219, 99–103.
- (6) Higashi, Y. Composition dependence of the critical parameters for the binary mixtures of R32 + R290, R32 + R600a, and R290 + R600a system. Proc. IIR Int. Conf. 2005, 153–159.
- (7) Tanaka, K.; Higashi, Y. Measurements of the surface tension for R290, R600a and R290/R600a mixture. *Int. J. Refrig.* 2007, 20, 1368–1373.
- (8) Lemmon, E. W.; Huber, M. L.; McLinden, M. O. NIST Standard Reference Data 23 REFPROP, ver. 8.0, 2007.

- (9) Rayleigh, O. M. On the Theory of Capillary Tube. Proc. R. Soc. London 1916, A 92, 184–195.
- (10) Moldover, M. R.; Rainwater, J. C. Interfacial Tension and Vapor-Liquid Equilibria in the Critical Region of Mixtures. J. Chem. Phys. 1988, 88, 7772–7780.
- (11) Okada, M.; Higashi, Y. Experimental Surface Tensions for HFC-32, HCFC-124, HFC-125, HCFC-141b, HCFC-142b, and HFC-152a. Int. J. Thermophys. 1995, 16, 791–800.
- (12) Higashi, Y. Critical Parameters for HFC134a, HFC32 and HFC125. Int. J. Refrig. 1994, 17, 524–531.
- (13) Redlich, O.; Kister, A. T. Algebraic Representation of Thermodynamic Properties and the Classification of Solutions. *Ind. Eng. Chem.* 1948, 40, 345–348.

Received for review October 15, 2008. Accepted November 29, 2008.

JE800756R