

# Vapor–Liquid Equilibria in Binary Systems Formed by Cyclohexane with Alcohols

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The modified Świętosławski ebulliometer was used for the accurate determination of vapor–liquid equilibria in binary isothermal systems formed by cyclohexane with: 2-butanol at 313.15 K, 323.15 K, 333.15 K, and 343.15 K, 2-pentanol at 333.15 K, 343.15 K, and 353.15 K, 2-methyl-2-butanol at 313.15 K, 323.15 K, 333.15 K, and 343.15 K, and 1-hexanol at 323.15 K, 333.15 K, 343.15 K, and 353.15 K. The vapor pressures of the pure substances are also given. The experimental data have been compared with literature data (if available) of those systems and correlated by means of the Redlich–Kister, NRTL, and Wilson equations.

## Introduction

Reliable and accurate vapor–liquid equilibrium (VLE) data are always needed for both better understanding of the behavior of liquid mixtures and process engineering design. The literature data are not always consistent and are usually measured only at one or two different pressures (isobaric data) or temperatures (isothermal data). For many systems, there are simply the lack of the experimental data.

This work is a part of a big project concerning accurate measurement of binary isothermal VLE data for systems formed by hydrocarbons (aliphatic, cyclic, aromatic) and organic compounds containing oxygen, nitrogen, and sulfur. The aim of the project is to deliver very reliable, accurate VLE isothermal data at many different temperatures for systems which are not available in the literature as well as systems for which only one or two isotherms were measured or measured VLE are not reliable (small number of experimental points, lack of information about the purity of pure components, inconsistent data).

The purpose of this paper is to provide reliable and accurate binary VLE data for systems formed by cyclohexane with the following alcohols:

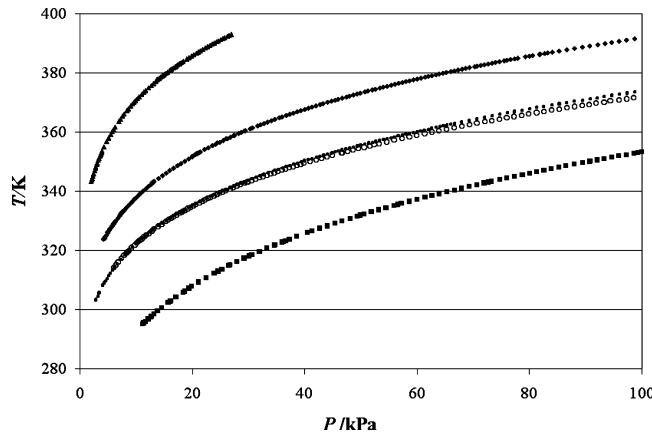
- (a) 2-butanol at 313.15 K, 323.15 K, 333.15 K, and 343.15 K;
- (b) 2-pentanol at 333.15 K, 343.15 K, and 353.15 K;
- (c) 2-methyl-2-butanol at 313.15 K, 323.15 K, 333.15 K, and 343.15 K;
- (d) 1-hexanol at 323.15 K, 333.15 K, 343.15 K, and 353.15 K.

Nineteen VLE data for the cyclohexane + 2-butanol system have already been reported in the literature. The main sources<sup>1–4</sup> consist both of isobaric (from (8 to 101) kPa) and of isothermal [(323.15 to 372.15) K] data. Much less (only two publications<sup>5,6</sup>) VLE data can be found for the cyclohexane + 2-methyl-2-butanol system, and the VLE for the cyclohexane + 1-hexanol system have been measured only in one laboratory by Svoboda et al.<sup>7</sup> In the literature, there are the lack of VLE data for the cyclohexane + 2-pentanol system.

## Experimental Section

The modified Świętosławski ebulliometer<sup>8</sup> was used for determination of both VLE data of all investigated binary

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**Figure 1.** Experimental  $T$ – $P$  data of the all pure components investigated. ■, cyclohexane; ○, 2-butanol; ◆, 2-pentanol; ●, 2-methyl-2-butanol; ▲, 1-hexanol.

systems and the boiling points of the pure components. The selection of the method for VLE measurement was imposed by the physical properties of the mixtures investigated. First, the pure components were highly hygroscopic and even a small amount of water present in the sample could change considerably the results of the vapor pressure measurements. Second, the differences between the boiling temperatures of cyclohexane and other components of the investigated mixtures were big, and consequently the values of relative volatilities were high. Third, the experimental program was extensive, and due to this the method chosen should provide accurate results in a relatively short time. Moreover, the selected ebulliometric method has some other following advantages:<sup>8</sup>

- (a) it enables accurate determination of total pressure above the samples of known composition;
- (b) the measurement can be isolated from the surroundings to prevent the penetration of moisture into the sample being investigated;
- (c) the time for achieving a steady state operation is short.

Since using the ebulliometer requires rapid, reliable, and accurate methods for determining pressure and temperature, in our ebulliometer system, the Systemteknik AB Temperature Meter type S1228 was used for determination of the temperature and Pfeiffer vacuum manometer TPG 251A for measurement

**Table 1.** Experimental P-T Data for Pure Cyclohexane, 2-Butanol, 2-Pentanol, 2-Methyl-2-butanol, and 1-Hexanol

experimental data															
P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)
cyclohexane															
11.15	295.42	22.47	310.98	46.59	330.05	72.6	343.15	13.81	299.77	34.69	321.99	58.63	336.7	87.93	349.19
11.16	295.45	23.89	312.48	48.07	330.94	73.25	343.43	14.52	300.85	35.95	322.94	59.96	337.36	89.43	349.72
11.17	295.46	24.56	313.15	49.32	331.68	74.73	344.05	15.71	302.63	36.27	323.15	61.39	338.06	90.64	350.18
11.33	295.72	25.25	313.84	49.89	332.02	75.96	344.55	16.03	303.03	36.59	323.44	61.4	338.07	90.87	350.25
11.35	295.75	26.47	315.01	50.6	332.41	77.27	345.09	16.11	303.15	37.23	323.89	62.63	338.66	92.07	350.67
11.63	296.22	26.67	315.26	51.87	333.11	78.76	345.69	17.04	304.38	37.33	323.95	62.64	338.67	93.27	351.1
12.15	297.08	27.88	316.32	51.92	333.15	80	346.18	17.05	304.4	38.56	324.83	63.95	339.29	94.63	351.57
12.16	297.13	29.23	317.52	53.15	333.83	81.25	346.67	17.07	304.42	40.45	326.13	65.29	339.92	95.92	352.01
12.17	297.14	30.09	318.32	53.19	333.86	82.56	347.18	18.33	306.05	41.25	326.68	66.63	340.54	97.23	352.45
12.61	297.86	30.56	318.67	54.47	334.53	82.57	347.18	18.60	306.4	42.68	327.61	67.95	341.12	98.57	352.91
12.71	297.99	31.93	319.82	55.85	335.27	83.89	347.69	19.40	307.45	43.97	328.43	69.29	341.72	99.31	353.15
13.23	298.84	33.27	320.87	56.56	335.64	85.23	348.19	19.91	308.06	45.4	329.33	70.65	342.32	99.95	353.36
13.8	299.75	34.59	321.91	57.19	335.96	86.49	348.66	21.12	309.5	45.43	329.35	71.93	342.88		
2-butanol															
6.08	314.47	18.68	333.65	35.32	346.86	63.97	360.61	11.84	325.27	26.79	340.95	47.65	353.60	84.03	367.47
6.43	315.36	19.24	334.23	36.01	347.28	65.29	361.10	12.31	325.92	27.36	341.40	48.61	354.06	85.39	367.89
6.81	316.21	19.71	334.69	36.63	347.65	66.71	361.64	12.81	326.66	27.99	341.87	49.61	354.53	86.71	368.27
7.45	317.61	20.20	335.19	37.31	348.06	67.99	362.10	13.16	327.32	28.63	342.34	50.63	355.00	88.05	368.68
7.92	318.57	20.71	335.69	37.99	348.46	69.43	362.63	14.03	328.28	29.37	342.89	51.63	355.46	89.41	369.08
8.35	319.37	21.33	336.28	38.64	348.85	70.69	363.08	14.61	329.05	29.76	343.15	52.39	355.81	90.67	369.43
8.45	319.58	21.85	336.77	39.29	349.21	72.12	363.58	15.31	329.91	29.97	343.32	53.33	356.23	91.91	369.79
8.77	320.18	22.35	337.23	39.95	349.59	73.36	364.00	15.79	330.49	30.67	343.81	54.63	356.80	93.33	370.20
9.23	321.05	22.87	337.72	40.97	350.16	74.72	364.48	16.31	331.11	31.31	344.25	55.96	357.37	94.44	370.56
9.80	322.03	23.28	338.08	42.05	350.75	76.00	364.90	16.71	331.58	31.99	344.71	57.41	357.99	96.00	370.94
10.19	322.68	23.87	338.60	43.03	351.26	77.31	365.33	17.25	332.17	32.63	345.15	58.67	358.50	97.35	371.32
10.48	323.15	24.43	339.07	43.96	351.74	78.65	365.76	17.87	332.81	33.33	345.60	60.03	359.06	98.59	371.65
10.64	323.41	24.95	339.50	44.97	352.27	79.95	366.18	18.20	333.15	33.99	346.03	61.41	359.62		
11.04	324.05	25.43	339.90	46.60	353.09	81.35	366.63	18.33	333.28	34.67	346.46	62.73	360.13		
11.47	324.72	25.97	340.34	46.75	353.15	82.63	367.04								
2-pentanol															
4.16	323.84	13.99	344.38	34.05	363.85	62.61	379.04	7.52	333.15	23.55	355.42	48.64	372.51	77.35	384.74
4.39	324.55	14.65	345.27	34.64	364.28	63.39	379.39	7.76	333.36	24.12	355.92	49.31	372.91	77.93	384.95
4.41	324.20	15.31	346.15	35.47	364.84	63.91	379.60	7.99	333.88	24.44	356.39	49.87	373.16	79.27	385.42
4.67	325.09	15.96	347.02	35.95	365.13	64.60	379.89	8.33	334.61	24.84	356.55	50.71	373.58	80.00	385.65
4.89	326.22	16.63	347.80	36.71	365.63	65.20	380.13	8.77	335.52	25.47	357.15	51.25	373.88	80.56	385.87
4.93	325.99	17.32	348.68	37.32	366.02	65.99	380.47	9.17	336.34	26.00	357.79	52.03	374.25	81.79	386.24
5.20	327.15	17.95	349.38	37.95	366.40	66.63	380.71	9.19	336.37	26.2	357.76	52.55	374.47	81.88	386.32
5.27	326.99	18.63	350.16	38.64	366.86	67.31	381.00	9.59	337.20	26.75	358.23	53.37	374.85	82.68	386.54
5.43	327.64	19.31	350.93	39.31	367.24	68.01	381.26	9.95	337.85	27.32	358.88	53.95	375.15	83.23	386.77
5.64	328.23	19.96	351.64	39.97	367.65	68.67	381.53	10.43	338.74	27.45	358.83	54.67	375.45	84.05	386.96
5.71	328.19	20.00	351.88	40.64	368.06	69.31	381.77	10.81	339.44	27.45	359.01	55.37	375.83	85.27	387.37
5.91	329.05	20.43	352.34	41.27	368.44	70.21	382.08	11.21	340.10	28.19	359.53	56.01	376.13	86.61	387.79
5.95	329.11	20.65	352.60	41.96	368.85	70.63	382.28	11.67	340.82	28.67	359.91	56.71	376.47	88.00	388.23
6.04	329.11	20.72	352.70	42.73	369.32	71.31	382.55	12.11	341.54	29.25	360.35	57.36	376.74	89.39	388.66
6.16	329.66	20.83	352.77	43.23	369.58	71.95	382.78	12.52	342.20	29.41	360.49	58.00	377.07	90.69	389.07
6.33	329.90	20.96	352.90	44.05	370.05	72.65	383.05	12.77	342.83	30.29	361.13	58.64	377.33	92.16	389.51
6.71	330.86	21.12	353.05	44.75	370.46	73.35	383.29	12.97	342.88	30.68	361.45	59.32	377.65	93.44	389.90
7.08	331.78	21.19	353.10	45.40	370.74	73.93	383.53	13.00	343.15	31.59	362.10	59.97	377.91	94.61	390.26
7.17	332.29	21.20	353.15	45.91	371.08	74.63	383.77	13.07	343.26	32.13	362.49	60.67	378.22	95.95	390.66
7.31	332.61	21.40	353.35	46.64	371.47	75.48	384.09	13.11	343.30	32.73	362.93	61.40	378.56	97.27	391.05
7.40	332.55	22.16	354.12	47.45	371.82	75.99	384.26	13.16	343.38	33.35	363.38	61.97	378.81	98.71	391.46
7.43	332.92	22.83	354.72	47.93	372.15	76.63	384.50								
2-methyl-2-butanol															
2.81	303.29	17.29	332.46	39.32	350.08	61.27	360.83	8.61	319.86	27.97	342.4	49.95	355.74	78.63	367.53
2.85	303.47	17.87	333.15	39.96	350.49	61.99	361.11	8.84	320.32	28.67	342.92	50.75	356.09	79.97	368.02
3.16	304.67	17.99	333.26	40.64	350.83	62.61	361.40	9.36	321.32	28.95	343.15	51.36	356.45	81.28	368.44
3.40	305.75	18.65	333.99	41.31	351.20	63.35	361.72	9.99	322.44	29.31	343.42	52.00	356.69	82.53	368.83
3.43	305.90	19.32	334.70	42.08	351.67	64.04	362.01	10.41	323.15	30.01	343.94	52.61	356.99	83.93	369.31
4.08	308.35	20.03	335.46	42.65	351.95	64.67	362.24	10.49	323.28	30.67	344.47	53.32	357.35	85.28	369.73
4.31	309.12	20.67	336.05	43.35	352.30	65.35	362.54	11.03	324.11	31.35	344.91	54.03	357.67	86.63	370.15
4.55	309.86	21.31	336.68	44.00	352.73	66.00	362.84	11.51	324.91	32.07	345.39	54.67	357.96	87.97	370.56
4.80	310.61	21.96	337.31	44.65	353.02	66.71	363.07	12.03	325.71	32.67	345.78	55.35	358.25	89.39	370.99
5.15	311.64	22.63	337.97	44.87	353.15	67.92	363.56	12.55	326.45	33.48	346.35	55.95	358.47	90.76	371.39
5.43	312.47	23.47	338.69	45.35	353.44										

Table 1.. Continued

experimental data															
P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)	P/(kPa)	T/(K)
2.47	346.17	7.27	364.61	14.40	378.72	20.79	386.84	3.89	353.32	11.05	373.00	17.21	382.56	25.13	391.40
2.67	347.27	7.64	365.59	14.65	379.10	21.15	387.23	3.96	353.82	11.43	373.67	17.44	382.85	25.51	391.76
2.79	348.10	7.92	366.29	14.91	379.46	21.48	387.63	4.31	355.21	11.73	374.19	17.69	383.18	25.83	392.06
2.85	348.35	8.40	367.45	15.12	379.75	21.91	388.10	4.79	357.02	12.27	375.14	17.84	383.34	26.31	392.51
3.04	349.38	8.67	368.05	15.37	380.06	22.37	388.59	5.15	358.22	12.73	375.93	18.09	383.67	26.59	392.78
3.11	349.75	9.08	368.99	15.61	380.41	22.79	389.05	5.51	359.42	13.15	376.59	18.43	384.08	27.00	393.15
3.32	350.75	9.40	369.67	15.95	380.87	23.20	389.48								

Table 2. Parameters of the Antoine Equation (Equation 5) Together with Calculated ( $T_b^c$ ) and Literature (NIST,  $T_b^l$ ) Values of Boiling Points for All Investigated Substances

compound	Antoine parameters			$T_b^c$ K	$T_b^l$ K	$\Delta T$ K	rmsd( $P$ ) kPa
	A	B	C				
cyclohexane	5.6641	1033.631	-71.351	353.89	$353.9 \pm 0.2$	-0.01	0.204
2-butanol	5.8479	928.321	-130.917	372.53	$372.0 \pm 1.0$	0.53	0.349
2-pentanol	5.6760	931.131	-139.043	392.74	$392.0 \pm 1.0$	0.74	1.011
2-methyl-2-butanol	5.3203	744.494	-150.173	374.79	$375.1 \pm 0.9$	-0.31	0.563
1-hexanol	5.3941	899.201	-166.275	431.65	$430.0 \pm 2.0$	1.65	0.125

of the total pressure. The accuracy of measurements in the case of the temperature was about 0.01 K (the thermometer resolution, 0.001 K) and in the case of pressure about 10 Pa (the pressure gauge resolution, 1 Pa). Both instruments are subject to drift to obtain the absolute values of temperature and pressure, which is why they were frequently recalibrated by the determination of the vapor pressure of water or benzene as a function of temperature.

The ebulliometric measurements have been carried out in the following ways:

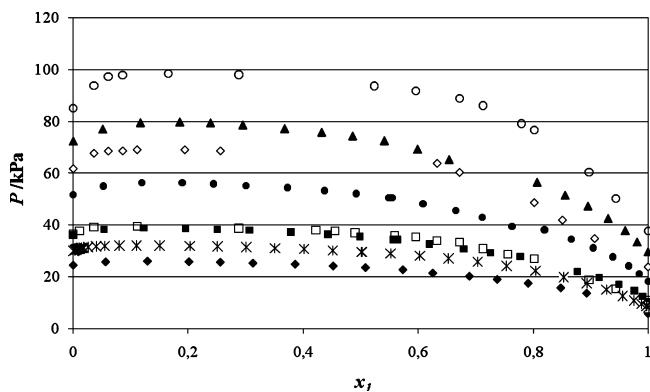


Figure 2. Comparison of the experimental isothermal  $P-x$  data with the literature data for the 2-butanol (1) + cyclohexane (2) system. This work: ♦,  $T = 313.15$  K; ■,  $T = 323.15$  K; ●,  $T = 333.15$  K; \*, ref 1,  $T = 318.15$  K; □, ref 2,  $T = 323.15$  K; ◇, ref 2,  $T = 338.15$  K; ○, ref 2,  $T = 348.15$  K.

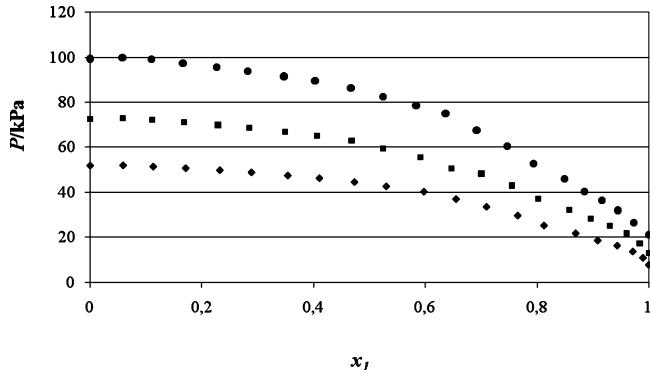


Figure 3. Experimental isothermal  $P-x$  data for the 2-pentanol (1) + cyclohexane (2) system. This work: ●,  $T = 333.15$  K; ▲,  $T = 343.15$  K; ○, ref 7,  $T = 323.15$  K; □, ref 7,  $T = 333.15$  K; ○, ref 7,  $T = 343.15$  K; \*, ref 7,  $T = 354.65$  K.

(1) for pure substances: simultaneous determination of pressure,  $P$ , and temperature,  $T$ ;

(2) for mixtures: simultaneous determination of  $P$ ,  $T$ , and  $x$  ( $P$ ,  $T$ ,  $x$  method).

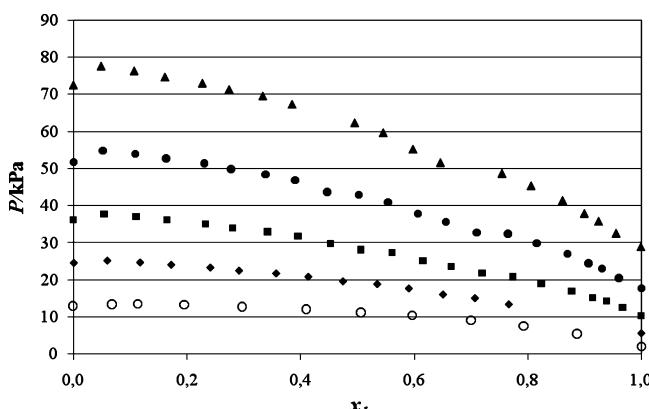


Figure 4. Comparison of the experimental isothermal  $P-x$  data with the literature data for the 2-methyl-2-butanol (1) + cyclohexane (2) system. This work: ♦,  $T = 313.15$  K; ■,  $T = 323.15$  K; ●,  $T = 333.15$  K; ▲,  $T = 343.15$  K; ○, ref 6,  $T = 298.15$  K.

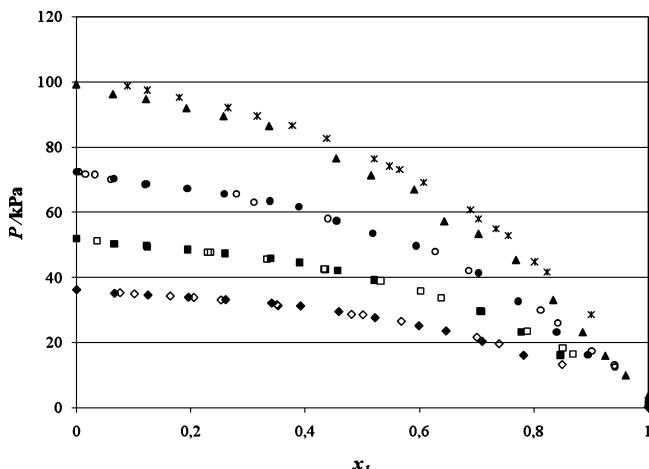


Figure 5. Comparison of the experimental isothermal  $P-x$  data with the literature data for the 1-hexanol (1) + cyclohexane (2) system. This work: ♦,  $T = 323.15$  K; ■,  $T = 333.15$  K; ●,  $T = 343.15$  K; ▲,  $T = 353.15$  K; ○, ref 7,  $T = 323.15$  K; □, ref 7,  $T = 333.15$  K; ○, ref 7,  $T = 343.15$  K; \*, ref 7,  $T = 354.65$  K.

The examined samples were prepared by introducing a known mass of one substance to the ebulliometer and adding known masses of the other component. The equilibrium composition of the liquid phase in the ebulliometer can be calculated from the composition of the introduced sample by means of the material balance equation.<sup>8</sup> For one mole of the sample, the liquid,  $L$ , and vapor,  $V$ , streams leaving the equilibrium chamber fulfill the equation

$$V + L = 1 \quad (1)$$

The mole fraction of component  $i$  in the sample,  $q_i$ , is related to the mole fraction of this component in the liquid phase,  $x_i$ , and in the vapor phase,  $y_i$ , by the equation

$$q_i = Vy_i + Lx_i \quad (2)$$

If we define the coefficient of evaporation,  $f$

and compare eqs 1 and 2, the relation enabling the calculation of liquid phase composition by a iterative procedure is obtained

$$x_i = q_i \frac{1+f}{1 + (\gamma_i/x_i)f} \quad (4)$$

The coefficient  $f$  is fairly constant<sup>8</sup> over the range of temperatures and pressures applied in usual ebulliometric measurements. The above experimental procedures as well as a detailed description of the ebulliometer were reported previously.<sup>8</sup>

All reagents used in the investigations were supplied by Fluka with a guaranteed mass fraction greater than 0.9995 determined by GLC analysis. The remaining moisture was removed by sorption on molecular sieves AJ (Wolfen Zeosorb), and to prevent further contamination, each sample was introduced into

**Table 3.** Vapor–Liquid Equilibrium Measurements for the 2-Butanol (1) + Cyclohexane (2) System at (313.15 to 343.15) K, the 2-Pentanol (1) + Cyclohexane (2) System at (333.15 to 353.15) K, the 2-Methyl-2-butanol (1) + Cyclohexane (2) System at (313.15 to 343.15) K, and the 1-Hexanol (1) + Cyclohexane (2) System at (323.15 to 353.15) K

**Table 4.** Parameters for the Hayden–O’Connell Correlation<sup>a</sup>

compound	T <sub>c</sub> /K	P <sub>c</sub> /kPa	μ/D	RD/Å	η
cyclohexane	554.00	4000.70	0.00	3.561	0.00
2-butanol	536.00	4200.00	1.66	3.182	0.2580
2-pentanol	560.30	3700.10	1.70	3.634	0.2435
2-methyl-2-butanol	543.70	3700.10	1.68	3.641	0.2476
1-hexanol	611.00	4000.50	1.80	4.198	0.2496

<sup>a</sup> T<sub>c</sub>, critical temperature; P<sub>c</sub>, critical pressure; μ, dipole moment; RD, mean radius of gyration; η, association parameter.

the ebulliometer by direct distillation, made just before each measurement.

## Results and Discussion

Vapor pressures of the investigated five pure substances were determined as a function of temperatures, and the results are given in Table 1 and Figure 1. The obtained P-T data were further correlated by the Antoine equation<sup>9</sup> (eq 5), and the calculated normal boiling points were compared with the values given by NIST.<sup>10</sup>

$$\log P = A - \frac{B}{T + C} \quad (5)$$

where P is vapor pressure (kPa); T is temperature (K); and A, B, and C are Antoine’s constants.

The parameters of the Antoine equation (eq 5) together with calculated and literature values of boiling point for all investigated substances are given in Table 2. As seen from both tables, no discrepancies between data reported in the literature and measured in this work were found.

The simultaneous (P, T, x) method without withdrawal of samples<sup>8</sup> was applied in this experiment. The ebulliometer was filled with a known amount of one pure compound, and a sample of a second component was added after the steady state was reached. For each experimental determination, the temperature and pressure in the apparatus and the total concentration of the sample were recorded. This procedure was repeated until the concentration of the second component reached a value higher than 0.5 mol fraction. Then the ebulliometer was filled with a known amount of second pure compound, and the same procedure as for component one was repeated.

The vapor pressures of mixtures of different compositions were determined, and the equilibrium compositions of the liquid and vapor phases were calculated by the method described previously<sup>8</sup> using a value of 0.30 for f.

The obtained results, experimental data of temperature, pressure, and liquid phase composition, are given in Table 3 and Figures 2 to 5.

The obtained experimental data were compared with the available literature data<sup>1,2,6,7</sup> (see Figures 2 and 5) and correlated using the Redlich–Kister,<sup>11</sup> NRTL,<sup>12</sup> and Wilson<sup>13</sup> equations. The minimization objective function was defined as the difference between the measured and calculated total pressures, and for each equation the adjustable parameters were calculated using the Levenberg–Marquardt algorithm.<sup>14</sup> For computation of vapor phase nonideality, the Hayden–O’Connell correlation<sup>15</sup> was used. The necessary auxiliary data are given in Table 4.

The results of the correlation (D(P) and DR(P), the absolute and relative root mean square deviations of total pressure, respectively) for all investigated equations are shown in Table 5.

$$D(P) = \left[ \frac{\sum_{i=1}^n (P_i^{\text{exp}} - P_i^{\text{cal}})^2}{n - m} \right]^{0.5} \quad (6)$$

$$DR(P) = \left[ \frac{\sum_{i=1}^n \left( \frac{(P_i^{\text{exp}} - P_i^{\text{cal}})^2}{P_i^{\text{exp}}} \right)}{n - m} \right]^{0.5} \quad (7)$$

where P<sub>i</sub><sup>exp</sup> and P<sub>i</sub><sup>cal</sup> are the experimental and calculated total pressures, respectively; n is the number of experimental data points; and m is the number of adjustable parameters.

The experimental VLE data for 2-butanol + cyclohexane, 1-hexanol + cyclohexane, and 2-methyl-2-butanol + cyclohexane systems agree very well with the literature (Figures 2, 4, and 5).

The correlation results (Table 5) show that, depending on the equation used, the relative root mean square deviation of total pressure varied from 0.45 % to 3.52 %. The best correlation results, for all investigated systems (RD(P) = (0.45 to 2.63) %, Table 5), have been obtained for the Redlich–Kister<sup>11</sup> equation with four adjustable parameters. The worst (almost twice) results have been obtained for both the NRTL<sup>12</sup> and Wilson<sup>13</sup> equation. It is worth noticing that the difference between results given by these equations is very small which means that the equations based on the local composition concept can not be used for accurate correlation of these systems. The obtained results confirmed the opinion that in the case of highly

**Table 5.** Results of Correlation (D(P) and DR(P), the Absolute and Relative Root Mean Square Deviations of Total Pressure, Respectively) of the Experimental VLE Isothermal Data for All the Systems Investigated

system	T/K	equation					
		NRTL <sup>12</sup>		Wilson <sup>13</sup>		Redlich–Kister <sup>11</sup> (4 parameters)	
		D(P)/kPa	DR(P)/%	D(P)/kPa	DR(P)/%	D(P)/kPa	DR(P)/%
2-butanol + cyclohexane	313.15	0.172	0.745	0.221	0.956	0.106	0.459
	323.15	0.319	1.907	0.705	2.980	0.287	1.627
	333.15	0.537	1.360	0.838	2.554	0.343	0.837
	343.15	0.482	0.731	0.846	1.540	0.372	0.598
2-pentanol + cyclohexane	333.15	0.713	2.853	0.879	3.517	0.657	2.629
	343.15	0.660	2.395	0.926	3.011	0.629	2.045
	353.15	0.718	1.423	0.896	1.525	0.626	1.010
2-methyl-2-butanol + cyclohexane	313.15	0.291	1.351	0.498	2.268	0.217	1.017
	323.15	0.485	1.726	0.723	3.425	0.358	1.236
	333.15	0.858	2.256	0.994	3.106	0.658	1.568
	343.15	1.240	2.278	1.328	2.718	0.917	1.458
1-hexanol + cyclohexane	323.15	0.320	1.218	0.367	1.394	0.136	0.453
	333.15	0.638	2.274	0.663	2.380	0.171	0.471
	343.15	0.731	2.570	0.785	2.996	0.444	1.493
	353.15	1.291	2.562	1.296	2.572	0.909	1.804

associating systems the good correlation can be achieved only by the use of models providing an extra term and taking into account association (usually an extra adjustable parameter).<sup>16</sup>

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