# New $P-\rho-T$ Data for Nitrogen at Temperatures from (265 to 400) K at Pressures up to $150 \mathrm{MPa}^{\dagger}$ 

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#### Abstract

This paper reports $P-\rho-T$ data for pure nitrogen measured with a high-pressure, single-sinker magnetic suspension densimeter (MSD) at (265, 293, 298.15, 350, and 400) K. The MSD yields data with less than $0.03 \%$ estimated error over the pressure range of $(10$ to 200$) \mathrm{MPa}$. A comparison of the experimental data to the equation of state (EoS) developed by Span et al. indicates they are consistent at pressures below 30 MPa . The EoS has a relative uncertainty with respect to density of $0.02 \%$ over this range. At higher pressures, the density predictions of this model agree with the experimental data reported in this paper within a 0.05 \% deviation band.


## Introduction

Nitrogen is an important reference fluid widely used for calibrating scientific equipment and testing physical models. Span et al. ${ }^{1}$ developed the most recent reference equation of state (EoS) for nitrogen. The relative uncertainty of its density predictions apparently is better than $0.02 \%$ between ( 240 and $523) \mathrm{K}$ at pressures below 30 MPa . At higher pressures, the uncertainty of the EoS increases to $0.6 \%$. This uncertainty reflects a lack of high-accuracy data at high pressures during its development.
This paper provides new density data for pure nitrogen collected with a high-pressure single-sinker magnetic suspension densimeter (MSD). This apparatus uses the Archimedes principle and yields high-accuracy data, with estimated errors less than $0.05 \%$. Patil et al. ${ }^{2}$ describe this specific MSD. The Experimental Section of this paper presents some details of the instrumentation, calibration data, and the methodology followed in collecting the data. Data tables and comparison plots appear in the Results Section.

## Experimental Section

The isothermal density data for nitrogen reported here cover the range of temperatures of ( $265,293,298.15,350$, and 400) K up to 150 MPa . The nitrogen came from Scott Specialty Gases with a mole fraction purity of 0.999995 . For the MSD, the mass of the titanium sinker, determined using the procedure described by McLinden and Splett, ${ }^{3}$ was 30.39159 g with a volume of $6.741043 \mathrm{~cm}^{3}$. A PRT (Minco Products model S1059PA5X6 platinum resistance thermometer) with fixed temperature points

[^0]defined by ITS-90 and calibrated by a PRT traceable to the National Institute of Standards and Technology (NIST) provides temperature measurements with an uncertainty of 2.5 mK and a stability of 5 mK . The pressure measurement instruments are two Digiquartz transducers ((40 and 200) MPa) from Paroscientific, Inc. with uncertainties of $\pm 0.01 \%$ of full scale.

The determination of the force transmission error (FTE), an inherent type of error resulting from forces altering the magnetic coupling within the apparatus, for this MSD system used the procedures suggested by McLinden et al. ${ }^{4}$ The correction of this error applies a factor $(\varphi)$ to the apparent sinker mass determined in each measurement cycle. This factor reflects the proportionality relation assumed between the force transmitted to the balance by the suspension coupling system and the suspended load. The comprehensive FTE analysis of the Texas A\&M University (TAMU) instrument recently has appeared. ${ }^{5}$

The coupling factors, expressed as $(\varphi-1)$, applied to the density values reported here are (193, 197, 207, 201, and 202) $\cdot 10^{-6}$ for ( $265,293,298.15,350$, and 400) K, respectively. The reproducibility of these values was always better than $\pm$ $2 \cdot 10^{-6}$ at each temperature.

Of particular importance are the high-pressure data (above 10 MPa ) for which the total relative uncertainty is less than $0.03 \%$. That uncertainty increases to $0.05 \%$ between ( 7 and 10) MPa and to more than $0.1 \%$ below 5 MPa .

## Results and Analysis

Table 1 contains the current isothermal data. Each $(T, P)$ set results from several density measurement cycles (raw data). After adjusting these raw data to nominal temperatures and pressures, the mean density point is selected as the most likely value to report. The table also contains density values predicted


Figure 1. Percent deviation of experimental data using Span et al. ${ }^{1}$ as the reference. A, this work; $O$, Klimeck et al.; ${ }^{7} \diamond$, Michels et al.; ${ }^{8} \square$, Wiebe and Gaddy. ${ }^{9}$


Figure 2. Absolute deviations of second virial coefficients using Span et al. ${ }^{1}$ as the reference. $\Delta B=B_{\text {exp }}-B_{\text {eos. }}$. , this work; $\bigcirc$, Nowak et al. ${ }^{13} \diamond$, Duschek et al.; ${ }^{10} \square$, Pieperbeck et al.; ${ }^{11} \triangle$, Ewing and Trusler; ${ }^{12}-$, Huff and Reed; ${ }^{15} \times$, Otto and Wouters; ${ }^{16} *$, Canfield et al.; ${ }^{17,18}+$, Pocock and Wormald. ${ }^{19}$
by Span et al. ${ }^{1}$ as implemented in REFPROP 8.0. ${ }^{6}$ The last column in the table is the percent difference between the data and the equation. Figure 1 depicts those relative deviations from Table 1 along with other sets of data used in the development of the reference EoS. ${ }^{7-9}$

It is clear that the density predictions of REFPROP 8.0 agree with the current experimental data within the uncertainties claimed for the reference $\operatorname{EoS}^{1}$ at low pressures (up to 30 MPa ). Figure 1 shows that the predictions at pressures greater than 30 MPa also have an uncertainty of $0.03 \%$, which means that, at


Figure 3. Absolute deviations of third virial coefficients using Span et al. ${ }^{1}$ as the reference. $\Delta C=\left(C_{\text {exp }}-C_{\text {eos }}\right)$. $\mathbf{\Delta}$, this work; $O$, Nowak et al.; ${ }^{13} \Delta$, Holborn and Otto; ${ }^{20} \square$, Kamerlingh and Urk; ${ }^{21} \diamond$, Michels et al.; ${ }^{8} \times$, Otto and Wouters; ${ }^{16} *$, Canfield et al.; ${ }^{17,18}+$, Roe and Saville. ${ }^{22}$

Table 1. New $\boldsymbol{P}-\boldsymbol{\rho}-\boldsymbol{T}$ Data Obtained for Nitrogen

| $P$ | $\rho(\exp )$ | $\rho$ (EoS) |  |
| :---: | :---: | :---: | :---: |
| MPa | $\mathrm{kg} \cdot \mathrm{m}^{-3}$ | $\mathrm{kg} \cdot \mathrm{m}^{-3}$ | $100 \cdot\left(\rho_{\text {exp }}-\rho_{\text {eos }}\right) / \rho_{\text {exp }}$ |
| $T / \mathrm{K}=265.000$ |  |  |  |
| 0.967 | 12.355 | 12.357 | -0.010 |
| 1.937 | 24.865 | 24.865 | -0.002 |
| 3.929 | 50.840 | 50.841 | -0.002 |
| 5.996 | 77.972 | 77.976 | -0.004 |
| 7.985 | 104.063 | 104.061 | 0.002 |
| 9.835 | 128.039 | 128.053 | -0.011 |
| 15.014 | 192.346 | 192.331 | 0.008 |
| 20.022 | 248.359 | 248.340 | 0.008 |
| 25.019 | 297.183 | 297.138 | 0.015 |
| 30.006 | 339.165 | 339.133 | 0.009 |
| 35.119 | 376.198 | 376.188 | 0.003 |
| 50.041 | 459.104 | 459.125 | -0.005 |
| 74.887 | 549.760 | 549.772 | -0.002 |
| 100.559 | 613.291 | 613.244 | 0.008 |
| $T / \mathrm{K}=293.000$ |  |  |  |
| 0.965 | 11.119 | 11.115 | 0.037 |
| 1.933 | 22.306 | 22.310 | -0.018 |
| 3.923 | 45.361 | 45.371 | -0.024 |
| 5.988 | 69.244 | 69.255 | -0.017 |
| 7.971 | 91.982 | 92.001 | -0.020 |
| 9.822 | 112.910 | 112.918 | -0.007 |
| 14.872 | 167.663 | 167.699 | -0.022 |
| 19.976 | 218.428 | 218.453 | -0.012 |
| 24.948 | 262.722 | 262.742 | -0.008 |
| 29.965 | 302.337 | 302.352 | -0.005 |
| 34.993 | 337.389 | 337.399 | -0.003 |
| 39.916 | 367.801 | 367.814 | -0.004 |
| 50.130 | 421.000 | 421.008 | -0.002 |
| 74.957 | 513.932 | 513.952 | -0.004 |
| 99.903 | 578.472 | 578.495 | -0.004 |
| 125.585 | 628.863 | 628.813 | 0.008 |
| 150.976 | 668.880 | 668.795 | 0.013 |
| $T / \mathrm{K}=298.150$ |  |  |  |
| 10.005 | 112.564 | 112.602 | -0.034 |
| 30.026 | 296.940 | 296.997 | -0.019 |
| 49.844 | 413.221 | 413.252 | -0.007 |
| 74.988 | 507.852 | 507.886 | -0.007 |
| 100.175 | 573.318 | 573.325 | -0.001 |
| 124.825 | 622.069 | 622.052 | 0.003 |
| 151.239 | 664.101 | 664.037 | 0.010 |

Table 1. Continued

| $P$ |  |  |  |
| ---: | ---: | :---: | :---: |
| MPa |  | $\rho(\exp )$ | $\frac{\rho(\mathrm{EoS})}{\mathrm{kg} \cdot \mathrm{m}^{-3}}$ |
|  |  | $\mathrm{~kg} \cdot \mathrm{~m}^{-3}$ | $100 \cdot\left(\rho_{\text {exp }}-\rho_{\mathrm{eos}}\right) / \rho_{\text {exp }}$ |
|  |  | $T / \mathrm{K}=350.000$ |  |
| 2.974 | 28.486 | 28.490 | -0.014 |
| 4.917 | 46.878 | 46.888 | -0.020 |
| 5.971 | 56.772 | 56.770 | 0.003 |
| 7.481 | 70.762 | 70.787 | -0.035 |
| 9.976 | 93.531 | 93.525 | 0.007 |
| 13.786 | 127.029 | 127.042 | -0.010 |
| 17.230 | 155.891 | 155.899 | -0.006 |
| 20.677 | 183.287 | 183.290 | -0.002 |
| 24.132 | 209.197 | 209.197 | 0.000 |
| 27.582 | 233.510 | 233.524 | -0.006 |
| 29.848 | 248.687 | 248.686 | 0.000 |
| 34.691 | 279.018 | 279.022 | -0.002 |
| 49.978 | 358.872 | 358.864 | 0.002 |
| 74.999 | 452.980 | 452.998 | -0.004 |
| 99.994 | 520.331 | 520.368 | -0.007 |
| 124.395 | 571.157 | 571.212 | -0.010 |
| 150.364 | 614.997 | 615.056 | -0.010 |
|  |  | $T / \mathrm{K}=400.000$ |  |
| 1.004 | 8.432 | 8.433 | -0.005 |
| 1.999 | 16.747 | 16.739 | 0.048 |
| 2.999 | 25.040 | 25.031 | 0.036 |
| 4.000 | 33.281 | 33.272 | 0.028 |
| 5.001 | 41.463 | 41.448 | 0.037 |
| 7.000 | 57.573 | 57.567 | 0.010 |
| 8.004 | 65.564 | 65.551 | 0.019 |
| 10.000 | 81.202 | 81.186 | 0.021 |
| 14.997 | 118.841 | 118.820 | 0.018 |
| 19.991 | 154.143 | 154.112 | 0.020 |
| 24.998 | 187.116 | 187.081 | 0.018 |
| 29.991 | 217.621 | 217.580 | 0.019 |
| 35.015 | 246.029 | 245.981 | 0.019 |
| 40.004 | 272.126 | 272.072 | 0.020 |
| 49.964 | 318.659 | 318.571 | 0.028 |
| 59.948 | 358.969 | 358.864 | 0.029 |
| 69.931 | 394.143 | 394.046 | 0.025 |
| 79.958 | 425.322 | 425.232 | 0.021 |
| 89.963 | 453.061 | 452.976 | 0.019 |
| 99.951 | 477.982 | 477.911 | 0.015 |
| 110.031 | 500.804 | 500.751 | 0.011 |
| 120.573 | 522.585 | 522.543 | 0.008 |
|  |  |  |  |
|  |  |  |  |

Table 2. Second and Third Virial Coefficients for Nitrogen

| $\frac{T}{\mathrm{~K}}$ | $\frac{B}{\mathrm{~cm}^{3} \cdot \mathrm{~mol}^{-1}}$ | $\frac{C}{\left(\mathrm{~cm}^{3} \cdot \mathrm{~mol}^{-1}\right)^{2}}$ |
| :---: | :---: | :---: |
| 265.00 | -12.24 | 1538 |
| 293.00 | -5.76 | 1435 |
| 350.00 | 3.48 | 1364 |
| 400.00 | 8.71 | 1442 |

least for the temperature range studied here, the EoS has better predictive capabilities than originally claimed at these high pressures.

Extrapolation and analysis of the linear behavior of the ( $Z-$ 1) $/ \rho$ function to zero pressure determines the second and third virial coefficients as the intercept and slope, respectively. The procedure yields uncertainties less than $0.28 \mathrm{~cm}^{3} \cdot \mathrm{~mol}^{-1}$ and 200 $\left(\mathrm{cm}^{3} \cdot \mathrm{~mol}^{-1}\right)^{2}$ for $B$ and $C$, respectively. These values appear in Table 2.

Figure 2 presents the absolute deviation of second virial coefficients presented in Table 2 along with other sets of data from the literature. ${ }^{10-14}$ Figure 3 is a similar plot for the third virial coefficients. Although the reference equation does not include fits of virial coefficients, the current data agree with the EoS and other data within the experimental uncertainties quoted above.

## Conclusions

This paper contains new, accurate $P-\rho-T$ data for nitrogen measured using a high-pressure single-sinker MSD apparatus that yields an experimental uncertainty of $\pm 3 \cdot 10^{-4}$ in density for pressures greater than 7 MPa and up to $\pm 5 \cdot 10^{-4}$ for pressures between ( 5 and 7) MPa. The data validate the performance of the EoS developed by Span et al. ${ }^{1}$ up to 150 MPa with better predictive capabilities than expected.

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