

# Phase Compositions of Aqueous Two-Phase Systems Formed by L35 and Salts at Different Temperatures

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The phase compositions in liquid–liquid equilibria of aqueous two-phase systems (ATPS) composed of the poly(ethylene oxide)–poly(propylene oxide)–poly(ethylene oxide) (PEO–PPO–PEO) triblock copolymer L35 and various salt solutions (sodium carbonate, sodium succinate, sodium acetate, ammonium citrate, and ammonium sulfate) at several temperatures, (283.15, 298.15, and 313.15) K, are presented. The influence of temperature in the binodal position was pronounced for almost all of the ATPS's, with the phase-separation process being endothermic. Additionally, the slopes of the tie-lines (STL) tended to increase with increasing temperature. The capability of the various salts to induce formation of the biphasic system was evaluated and followed the order sodium carbonate > ammonium sulfate > sodium succinate > ammonium citrate > sodium acetate. The consistencies of the tie-line experimental compositions were confirmed by applying the Othmer–Tobias correlation, with excellent results, as shown by the regression coefficients acquired. The liquid–liquid equilibrium data of ternary systems have been correlated using the nonrandom two-liquid (NRTL) model for the activity coefficient. The results were considered very satisfactory with global root-mean-square deviations as low as 1.49 %.

## Introduction

Since 1956, when Albertsson showed the potential of aqueous two-phase systems (ATPS) as a separation technique,<sup>1</sup> several works have developed these systems for application in determination, preconcentration, purification, and separation of different solutes, such as phenol,<sup>2</sup> cell organelles,<sup>3,4</sup> proteins,<sup>5</sup> membranes,<sup>6</sup> DNA,<sup>7</sup> antibodies,<sup>8</sup> nanoparticles,<sup>9</sup> dye molecules,<sup>10</sup> and ions.<sup>11–15</sup>

ATPS are formed under specific thermodynamic conditions<sup>16</sup> when two mutually incompatible water-soluble polymers,<sup>17</sup> one polymer and one salt<sup>18,19</sup> or two salts,<sup>20</sup> are mixed. The phase split results in a polymer-enriched top phase and a salt-enriched bottom phase (or one enriched with the other polymer) or the converse. Additionally, these systems present a higher water content in both phases.

This biphase nature provides several advantages for using an ATPS in separation techniques, such as (i) a suitable environment for the preservation of biological activity of some solutes;<sup>21,22</sup> (ii) low interfacial tensions, which improve the migration process through the interface;<sup>23</sup> and (iii) the possibility of linear scale-up.<sup>24</sup>

The liquid–liquid equilibrium (LLE) behavior of various ATPS composed of poly(ethylene oxide) (PEO) have been reported in the literature,<sup>18,25–27</sup> with the influences of the nature of the electrolyte and temperature in the phase-separation process being evaluated. However, changes in the thermodynamic properties of both phases are limited if the ATPS are restricted to PEO/salt/water systems.

As an alternative to this limitation, ATPS formed by triblock copolymers are excellent options for the extraction of hydro-

phobic solutes into the polymer-enriched phase.<sup>28</sup> Owing to their amphiphilic character, triblock copolymers in aqueous solution and at critical temperature and concentration conditions form micelles via a self-assembly process. These aggregates have a crown of hydrophilic units of PEO and a core of hydrophobic units of poly(propylene oxide) (PPO),<sup>29</sup> which is capable of interacting with hydrophobic compounds.

Therefore, LLE data for ATPS composed of triblock copolymers can provide important information for potential applications such as chemical separation and extraction. However, LLE data for systems constituted by these polymers are scarce to date.<sup>16,30,31</sup> In this work, biphasic systems composed of (EO)<sub>11</sub>(PO)<sub>16</sub>(EO)<sub>11</sub>, denoted L35 (50 % EO), plus salt and water were prepared and the phase compositions determined. To study the effect of the electrolyte type, the salts used were sodium carbonate, sodium succinate, sodium acetate, ammonium citrate, and ammonium sulfate. Equilibrium data at (283.15, 298.15, and 313.15) K were determined to evaluate the influence of temperature on the binodal position.

The tie-line data were used in the Othmer–Tobias<sup>32</sup> correlation and were processed using the nonrandom two-liquid (NRTL)<sup>33</sup> model to find the corresponding fitting parameters.

## Experimental Section

**Materials.** L35, an (EO)<sub>11</sub>(PO)<sub>16</sub>(EO)<sub>11</sub> copolymer, with an average molar mass ( $M_w$ ) of 1900 g·mol<sup>-1</sup>, containing 50 % ethylene glycol, was purchased from Aldrich (USA). The analytical grade reagents Na<sub>2</sub>CO<sub>3</sub> (sodium carbonate), Na<sub>2</sub>C<sub>4</sub>H<sub>4</sub>O<sub>4</sub> (sodium succinate), Na(CH<sub>3</sub>COO) (sodium acetate), (NH<sub>4</sub>)<sub>2</sub>C<sub>6</sub>H<sub>5</sub>O<sub>7</sub> (ammonium citrate), and (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> (ammonium sulfate) were obtained from Vetec (Brazil). Milli-Q II water (Millipore, USA) was used to prepare all aqueous solutions.

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**Table 1. Equilibrium Data for L35 ( $w_{L35}$ ) + Sodium Carbonate ( $w_S$ ) + Water ( $w_w$ ) System from (283.15 to 313.15) K**

system	overall			top phase			bottom phase			TLL
	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	
$T = 283.15$ K										
1	19.02	5.51	75.47	29.38	2.54	68.08	2.54	12.07	85.39	28.48
2	22.54	6.67	70.79	37.39	1.57	61.04	3.70	14.72	81.58	36.17
3	26.08	7.60	66.32	43.82	1.12	55.06	3.22	18.05	78.73	43.99
4	29.44	8.86	61.70	49.90	0.82	49.28	3.68	21.22	75.10	50.52
5	32.16	10.39	57.45	56.55	0.51	42.94	3.33	25.05	71.62	58.61
$T = 298.15$ K										
1	19.02	5.51	75.47	36.95	1.94	61.11	3.38	9.77	86.85	34.46
2	24.40	5.36	70.24	40.88	1.67	57.45	2.55	11.67	85.78	39.61
3	29.91	5.86	64.23	49.04	1.00	49.96	2.14	14.20	83.66	48.73
4	35.42	6.36	58.22	55.34	0.70	43.96	2.86	17.02	80.12	54.96
5	40.93	6.86	52.21	60.91	0.51	38.58	2.88	20.27	76.85	61.31
$T = 313.15$ K										
1	19.02	5.51	75.47	42.07	1.34	56.59	1.49	9.53	88.98	33.51
2	22.55	6.67	70.78	51.94	0.89	47.17	1.37	11.84	86.79	41.54
3	26.09	7.60	66.31	59.17	0.54	40.29	2.65	13.94	83.41	48.66
4	29.45	8.86	61.69	64.37	0.41	35.22	2.66	17.39	79.95	54.63
5	32.15	10.39	57.46	64.75	0.40	34.85	3.32	20.66	76.02	62.14

**Preparation of ATPS Assays.** Previously, stock solutions of L35 and salt were prepared by weighing appropriate amounts of reagents on an analytical balance (Shimadzu, AG 220 with an uncertainty of  $\pm 0.0001$  g). ATPS were prepared by mixing appropriate quantities of the stock solutions of copolymer, salt and water, in glass vessels, according to the global compositions desired. In a typical experiment, 10 g of each system was prepared. After being vigorously stirred, the system became turbid and was allowed to settle for (24 to 72) h at the operation temperature of (283.15, 298.15, or 313.15) K in a temperature-controlled bath (Microquímica, MQBTC 99-20, with an uncertainty of  $\pm 0.1$  K). The equilibrium state was characterized by the absence of turbidity in both top and bottom phases. Aliquots of the top and bottom phases were collected with a syringe for analysis.

**Construction of Phase Diagrams.** The salt and L35 concentrations in the separated phases were determined in two steps. First, after separating the two phases from each other and after suitable dilution, the salt concentration in both phases was determined by conductometry (Schott CG853, Germany) in the mass percentage range of ( $1.00 \cdot 10^{-3}$  to  $2.50 \cdot 10^{-2}$ ) %. The salt solutions showed the same conductivity in water or diluted polymer solution. The uncertainty of the salt composition by this method was  $\pm 0.10$  %. Second, the copolymer concentration in the phases was after suitable dilution then determined by measuring the total refractive index of the solutions and then subtracting the refractive index of salt. To do this, standard curves were established for aqueous solutions of L35 and salt. The validity of refractive index additivity was also confirmed. The refractive index measurements were performed by a refractometer (Analytic Jena AG Abbe, model 09-2001, Germany) at 289.15 K.<sup>22</sup> The uncertainty of the copolymer mass percentage was  $\pm 0.006$  %. The water content was determined by difference of mass (percentage mass) of each component ( $w_{H_2O} = w_{total} - w_S - w_{L35}$ ), where  $w_{total} = 100$  % (w/w). All analytical measurements were performed in triplicate.

## Results and Discussion

For ATPS, the decrease in the system free energy occurs at specific thermodynamic conditions by an exclusion process between the water-soluble polymer and the salt, leading to the formation of two aqueous phases. At lower polymer concentrations, the other polymer or salt is miscible, and they are codissolved as a single phase. Above a critical concentration,

they will separate into two phases, where each phase is enriched in one of the polymer or salt components.<sup>34</sup> Tables 1, 2, 3, 4, and 5 show LLE data, expressed in mass percent, for L35 + sodium carbonate + water, L35 + sodium succinate + water, L35 + sodium acetate + water, L35 + ammonium citrate + water, and L35 + ammonium sulfate + water ATPS at (283.15, 298.15, and 313.15) K. These results show that the overall polymer and salt concentrations necessary to obtain phase separations are similar to those for systems containing PEO (MW 2000 or 6000) + salt (sodium carbonate, sodium succinate, ammonium citrate, and ammonium sulfate).<sup>34–36</sup>

Depending on the system, five to six tie lines (TL) were determined. The tie-line length (TLL) is a thermodynamic parameter that at constant pressure and temperature expresses the difference in intensive thermodynamic functions between the top and the bottom phases.<sup>14</sup> TLL is expressed as the difference between polymer and salt concentrations present in the phases and is calculated by the following equation:

$$TLL = [(C_P^T - C_P^B)^2 + (C_S^T - C_S^B)^2]^{1/2} \quad (1)$$

where  $C_P^T$  and  $C_P^B$  are the polymer concentrations in the top and bottom phases, respectively, while  $C_S^T$  and  $C_S^B$  are those of the salt. The TLs were obtained by linear regression of the corresponding sets of overall, bottom-phase, and top-phase concentrations. An increase in copolymer and salt segregation with an increase in global composition and consequently an increase in the TLL were noted. This behavior is in agreement with the reported results for other ATPS.<sup>28</sup> Nevertheless, as a consequence of the hydrophobic contribution of the PO segments,<sup>37</sup> the top-phase water content is markedly lower than the water concentration observed in the top phase of PEO–salt ATPS.<sup>34–36</sup>

The influence of temperature on the binodal positions of the ATPS is presented in Figures 1, 2, 3, 4, and 5. Except in the phase diagram of the L35 + ammonium sulfate + water system, temperature had a remarkable effect on the phase equilibrium compositions of the ATPS. As can be seen in the figures, the biphasic area increased along with the temperature. This behavior shows that the phase-separation process is endothermic. This entropic phase separation is a general feature of the ATPS process, as has been related in previous studies.<sup>38</sup>

The temperature effect on the phase-equilibrium compositions can be analyzed through the slope of the tie line (STL) values,

**Table 2. Equilibrium Data for the L35 ( $w_{L35}$ ) + Sodium Succinate ( $w_S$ ) + Water ( $w_w$ ) System from (283.15 to 313.15) K**

system	overall			top phase			bottom phase			TLL
	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	
$T = 283.15$ K										
1	29.15	7.31	63.54	42.28	3.64	54.08	0.92	15.40	83.68	43.00
2	32.90	7.48	59.62	50.75	2.93	46.32	0.68	17.06	82.26	52.03
3	35.82	8.17	56.01	56.55	2.26	41.19	0.20	18.88	80.92	58.76
4	39.48	8.66	51.86	60.69	1.72	37.59	0.19	21.01	78.80	63.50
5	41.54	9.00	49.46	62.02	1.66	36.32	0.01	21.74	78.25	65.18
$T = 298.15$ K										
1	29.97	7.63	62.40	49.11	3.30	47.59	2.97	15.21	81.82	47.65
2	33.16	8.05	58.79	53.74	2.35	43.91	2.78	17.96	79.26	53.29
3	36.17	8.54	55.29	62.21	1.94	35.85	2.71	18.41	78.88	61.73
4	39.74	8.93	51.33	66.80	1.53	31.67	2.44	19.15	78.41	66.72
5	41.79	9.58	48.63	68.82	1.23	29.95	2.07	20.97	76.96	69.60
$T = 313.15$ K										
1	29.83	7.52	62.65	55.41	1.87	42.72	1.82	13.30	84.88	54.79
2	33.73	8.05	58.22	61.65	1.35	37.00	1.47	15.95	82.58	61.93
3	36.03	8.45	55.52	66.29	1.04	32.67	1.07	17.09	81.84	67.17
4	40.25	8.97	50.78	71.28	0.70	28.02	0.57	19.41	80.02	73.15
5	42.80	9.68	47.52	76.54	0.43	23.03	0.12	21.71	78.17	79.33

**Table 3. Equilibrium Data for L35 ( $w_{L35}$ ) + Sodium Acetate ( $w_S$ ) + Water ( $w_w$ ) System from (283.15 to 313.15) K**

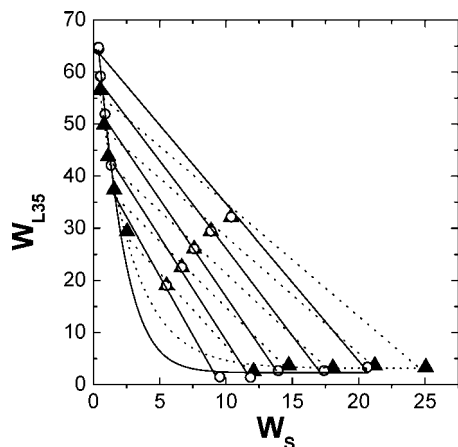
system	overall			top phase			bottom phase			TLL
	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	
$T = 283.15$ K										
1	13.73	18.47	67.80	23.21	15.58	61.21	0.43	23.22	76.35	28.48
2	20.89	17.62	61.49	30.25	14.92	54.83	0.29	25.11	74.60	36.17
3	26.43	17.31	56.26	38.09	13.31	48.60	0.01	27.69	72.30	43.99
4	32.43	17.03	50.54	51.13	9.14	39.73	0.01	30.83	69.16	50.52
5	35.73	16.93	47.34	59.67	6.97	33.36	0.01	31.38	68.61	58.61
$T = 298.15$ K										
1	19.55	16.18	64.27	26.05	14.26	59.69	0.91	22.68	76.41	26.51
2	22.07	16.68	61.25	40.44	11.19	48.37	0.65	24.06	75.29	41.82
3	24.59	17.18	58.23	51.77	8.92	39.31	0.69	25.72	73.59	53.77
4	27.11	17.68	55.21	64.31	6.58	29.11	0.56	27.48	71.96	67.09
5	29.63	18.18	52.19	70.76	5.01	24.23	0.67	28.85	70.48	74.03
$T = 313.15$ K										
1	24.50	10.39	65.11	30.08	9.11	60.81	2.44	15.68	81.88	28.41
2	30.06	10.22	59.72	42.39	7.31	50.30	1.98	17.38	80.64	41.64
3	33.11	10.16	56.73	49.46	6.25	44.29	2.01	18.28	79.71	48.95
4	32.43	17.03	50.55	77.84	1.57	20.59	2.46	27.84	69.70	79.82
5	35.73	16.93	47.35	83.12	0.64	16.24	3.14	28.87	67.99	84.82
6	50.36	8.72	40.91	66.11	3.51	30.38	1.95	22.84	75.21	67.01

**Table 4. Equilibrium Data for the L35 ( $w_{L35}$ ) + Ammonium Citrate ( $w_S$ ) + Water ( $w_w$ ) System from (283.15 to 313.15) K**

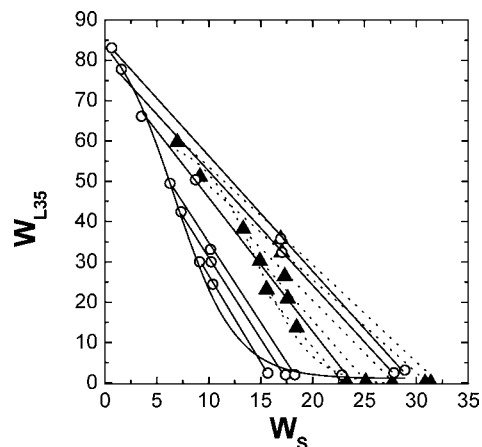
system	overall			top phase			bottom phase			TLL
	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	
$T = 283.15$ K										
1	19.94	16.28	63.78	33.21	8.13	58.66	0.93	28.02	71.05	37.92
2	22.80	16.76	60.44	39.45	6.78	53.77	0.40	30.63	68.97	45.75
3	25.73	18.24	56.03	46.77	5.52	47.71	0.13	34.45	65.42	54.88
4	27.94	18.66	53.40	50.25	4.93	44.82	0.08	36.21	63.71	59.12
5	30.08	20.27	49.65	55.96	4.19	39.85	0.04	39.61	60.35	66.20
$T = 298.15$ K										
1	23.26	14.16	62.58	39.06	7.48	53.46	0.81	25.09	74.10	42.11
2	25.90	14.84	59.26	45.54	6.18	48.28	0.33	27.52	72.15	50.00
3	28.50	15.65	55.85	51.18	5.25	43.57	0.35	31.29	68.36	57.11
4	31.20	16.32	52.48	55.51	4.53	39.96	0.39	32.79	66.82	61.94
5	33.94	16.95	49.11	59.51	4.06	36.43	0.72	36.46	62.82	67.13
$T = 313.15$ K										
1	19.92	16.28	63.80	48.84	4.27	46.89	0.28	24.46	75.26	52.59
2	23.02	16.84	60.14	54.89	4.02	41.09	0.07	26.92	73.01	59.42
3	25.79	18.26	55.95	60.38	3.31	36.31	0.05	30.72	69.23	66.26
4	27.95	18.67	53.38	64.90	2.98	32.12	0.02	33.12	66.86	71.54
5	30.07	20.30	49.63	68.10	2.71	29.19	0.04	35.43	64.53	75.52

which are reported in Table 6. The STL is defined as the ratio  $STL = (\Delta_{polymer}/\Delta_{salt})$ , in which  $\Delta_{polymer}$  and  $\Delta_{salt}$  are the differences between the compound concentrations in the two

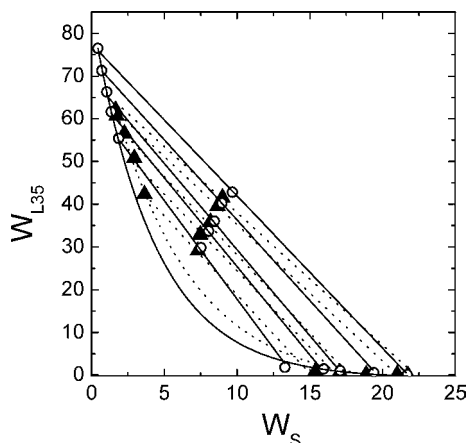
coexisting phases. The results indicate that an increase in the temperature promoted an increase in the STL for all ATPS. A possible explanation for this change is the spontaneous diffusion



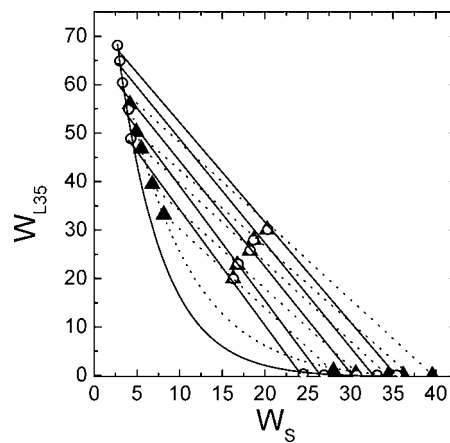
**Figure 1.** Temperature effect on the phase diagram for the L35 + sodium carbonate system.  $\blacktriangle$ , 283.15 K;  $\circ$ , 313.15 K.



**Figure 3.** Temperature effect on the phase diagram for the L35 + sodium acetate system.  $\blacktriangle$ , 283.15 K;  $\circ$ , 313.15 K.



**Figure 2.** Temperature effect on the phase diagram for the L35 + sodium succinate system.  $\blacktriangle$ , 283.15 K;  $\circ$ , 313.15 K.



**Figure 4.** Temperature effect on the phase diagram for the L35 + ammonium citrate system.  $\blacktriangle$ , 283.15 K;  $\circ$ , 313.15 K.

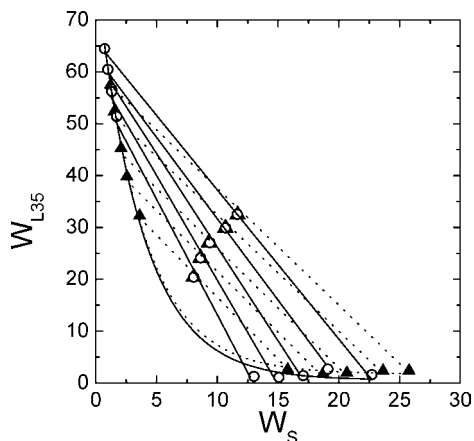
of water molecules from the top phase to the bottom phase, resulting in an increase in the copolymer concentration in the upper phase and a reduction in the salt concentration in the lower phase. This behavior has also been observed for the systems composed of PEO and salts (sodium carbonate, sodium succinate, ammonium citrate, and ammonium sulfate),<sup>34,35</sup> however, it is less pronounced than with the ATPS containing L35. Because of the higher hydrophobicity of PO segments, in the

copolymer ATPS, the diffusion of water molecules from the top phase to the top phase occurs to a larger extent than in the PEO ATPS.

Figure 6 presents the influence of the anion on the induction of phase segregation at 283.15 K. The formation of the ATPS clearly indicates the mutual exclusion between salt and copolymer and their affinity for water. This tendency is observed in all systems consisting of triblock copolymers or polymers and

**Table 5.** Equilibrium Data for the L35 ( $w_{L35}$ ) + Ammonium Sulfate ( $w_S$ ) + Water ( $w_w$ ) System from (283.15 to 313.15) K

system	overall			top phase			bottom phase			TLL
	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	100 $w_{L35}$	100 $w_S$	100 $w_w$	
$T = 283.15$ K										
1	20.40	8.05	71.55	32.26	3.60	64.14	2.60	15.79	81.61	32.06
2	24.12	8.62	67.26	39.81	2.55	57.64	1.81	18.71	79.48	41.29
3	27.10	9.31	63.59	45.27	2.08	52.65	1.94	20.67	77.39	47.15
4	29.92	10.66	59.42	52.30	1.51	46.19	2.33	23.64	74.03	54.65
5	32.48	11.66	55.86	57.49	1.21	41.30	2.38	25.78	71.84	60.33
$T = 298.15$ K										
1	25.20	6.20	68.60	37.86	3.14	59.00	2.94	12.95	84.11	36.27
2	29.54	6.69	63.77	45.98	2.19	51.83	2.31	15.05	82.64	45.52
3	33.98	7.20	58.82	51.38	1.65	46.97	2.84	17.06	80.10	50.93
4	38.37	7.70	53.93	57.16	1.21	41.63	2.68	20.11	77.21	57.67
5	42.75	8.21	49.04	61.64	0.94	37.42	3.40	22.36	74.24	62.06
$T = 313.15$ K										
1	20.42	8.04	71.54	51.40	1.71	46.89	1.26	13.01	85.73	51.40
2	24.12	8.62	67.26	56.69	1.29	42.02	1.08	15.07	83.85	57.30
3	27.03	9.38	63.59	56.23	1.32	42.45	1.42	17.07	81.51	57.02
4	29.92	10.67	59.41	60.47	0.99	38.54	2.65	19.09	78.26	60.58
5	32.52	11.64	55.84	64.49	0.72	34.79	1.60	22.71	75.69	66.62

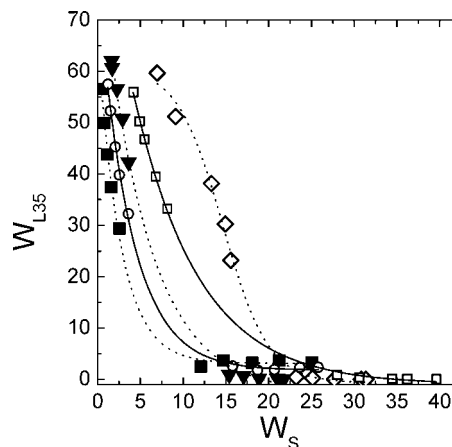


**Figure 5.** Temperature effect on the phase diagram for the L35 + ammonium sulfate system. ▲, 283.15 K; ○, 313.15 K.

**Table 6.** STL Value Systems at (283.15, 298.15, and 313.15) K

system	T/K		
	283.15	298.15	313.15
L35 + Sodium Carbonate + Water			
1	-2.76	-4.15	-4.63
2	-2.54	-3.83	-4.96
3	-2.38	-3.55	-4.23
4	-2.23	-3.22	-3.63
5	-2.15	-2.94	-3.03
L35 + Sodium Succinate + Water			
1	-3.51	-3.84	-4.68
2	-3.52	-3.24	-4.12
3	-3.38	-3.59	-4.06
4	-3.14	-3.65	-3.77
5	-3.11	-3.39	-3.59
L35 + Sodium Acetate + Water			
1	-2.96	-2.95	-4.2
2	-2.89	-3.08	-3.99
3	-2.63	-3.04	-3.93
4	-2.36	-3.06	-2.87
5	-2.45	-2.96	-2.84
6			-3.35
L35 + Ammonium Citrate + Water			
1	-1.62	-1.94	-2.41
2	-1.64	-1.95	-2.40
3	-1.61	-1.81	-2.20
4	-1.60	-2.16	-2.16
5	-1.58	-2.11	-2.08
L35 + Ammonium Sulfate + Water			
1	-2.42	-3.52	-4.46
2	-2.34	-3.38	-4.05
3	-2.32	-3.15	-3.48
4	-2.25	-2.88	-3.19
5	-2.24	-2.73	-2.86

inorganic salts. For salts in which the cation is  $\text{Na}^+$ , the ability of the three anions to promote the formation of ATPS followed the order carbonate > succinate > acetate. For ammonium salts, the system composed of  $(\text{NH}_4)_2\text{SO}_4$  had a larger biphasic area compared with the system containing ammonium citrate. Figure 6 also shows the results of a more general study, in which the effect of the particular salt on the binodal position is presented. The capability of the salts to induce phase segregation followed the order sodium carbonate > ammonium sulfate > sodium succinate > ammonium citrate > sodium acetate. The same behavior was observed for the other temperatures. These results are in agreement with the order shown for systems containing PEO, as reported in the literature.<sup>34–36</sup>



**Figure 6.** Influence of electrolyte on the phase diagram of the L35 + salt systems at 283.15 K. ■, sodium carbonate; ○, ammonium sulfate; ▼, sodium succinate; □, ammonium citrate; ◇, sodium acetate.

The reliability of the experimental tie-lines can be ascertained by applying the Othmer–Tobias<sup>32</sup> correlation. This correlation is given by eq 2:

$$\ln\left(\frac{100 - w_{sb}}{w_{sb}}\right) = A + B \ln\left(\frac{100 - w_{pt}}{w_{pt}}\right) \quad (2)$$

where  $w_{sb}$  and  $w_{pt}$  stand for mass percentages of salt in the bottom phase and the mass percentages of L35 in the top phase, respectively. The values of  $A$  and  $B$  depend on the individual systems.<sup>32</sup>

This is a well-known empirical procedure to ensure the consistency of experimental data by means of graphic linearity. This correlation was applied to our experimental data with eq 2, and the constants ( $A$  and  $B$ ) and the regression coefficients ( $R^2$ ) are given in Table 7. For all ternary systems, it is seen that the regression coefficients are close to 1, an indication of the high degree of consistency of the experimental data.

**Thermodynamic Modeling (NRTL) and Parameter Estimation.** When examining thermodynamic consistency, in this work we applied the NRTL thermodynamic model, which is based on local composition and is applicable to partially miscible systems. However, it has been proposed to use the modified NRTL model for multicomponent systems, for example, those that contain salts and polymers. In this case, the original NRTL model<sup>33</sup> was used to calculate the interaction parameters with the experimental TL data at several temperatures. Some authors<sup>39–41</sup> have shown that the original NRTL thermodynamic model approach is able to represent electrolyte systems, and all electrostatic contributions to the activity coefficient are accounted for in the binary interaction parameters.<sup>42</sup> In this case, the equations of the original NRTL model were adapted by Straghetich<sup>43</sup> for polymer and salt-containing systems, as expressed by the following set of equations:

$$\ln \gamma_i = \frac{\sum_j \frac{\tau_{ji} G_{ji} w_j}{M_j}}{\sum_k \frac{G_{ki} w_k}{M_k}} + \sum_j \left[ \frac{w_j G_{ij}}{M_j \sum_k \frac{G_{kj} w_k}{M_k}} \left( \tau_{ij} - \frac{\sum_k \frac{w_k \tau_{kj} G_{ki}}{M_k}}{\sum_k \frac{G_{kj} w_k}{M_k}} \right) \right] \quad (3)$$

$$\tau_{ij} = \frac{A_{ij}}{T} \quad (\tau_{ij} \neq \tau_{ji}) \quad (4)$$

$$G_{ij} = \exp(-\alpha_{ij} \tau_{ij}) \quad (\alpha_{ij} = \alpha_{ji}) \quad (5)$$

Table 7. Othmer–Tobias Constants and Regression Coefficients

system	$A_1$	$B_1$	$R^2$
L35 + sodium carbonate + water at 283.15 K	1.31344	0.79332	0.99816
L35 + sodium carbonate + water at 298.15 K	1.75224	0.84022	0.99741
L35 + sodium carbonate + water at 313.15 K	2.02847	0.87336	0.95590
L35 + sodium succinate + water at 283.15 K	1.56545	0.52847	0.98585
L35 + sodium succinate + water at 298.15 K	1.65470	0.37096	0.92034
L35 + sodium succinate + water at 313.15 K	1.98105	0.60209	0.99506
L35 + sodium acetate + water at 283.15 K	0.85384	0.27389	0.98644
L35 + sodium acetate + water at 298.15 K	1.06572	0.16898	0.99394
L35 + sodium acetate + water at 313.15 K	1.43665	0.34504	0.99243
L35 + ammonium citrate + water at 283.15 K	0.56618	0.55748	0.99858
L35 + ammonium citrate + water at 298.15 K	0.82822	0.63977	0.99208
L35 + ammonium citrate + water at 313.15 K	1.10722	0.66539	0.99781
L35 + ammonium sulfate + water at 283.15 K	1.23119	0.59075	0.99978
L35 + ammonium sulfate + water at 298.15 K	1.59070	0.69334	0.99484
L35 + ammonium sulfate + water at 313.15 K	1.97285	1.24282	0.97204

Table 8. Estimated NRTL Parameters

i	j	$A_{ij}$	$A_{ji}$	$B_{ij}$	$B_{ji}$	$\alpha_{ij}$
L35	sodium carbonate	-671.72	287.27	0.75786	-18.457	0.29798
L35	water	2785.7	765.33	0.12446	19.960	0.46828
L35	sodium succinate	-0.26161	133.12	74.865	56.838	0.21323
L35	sodium acetate	428.20	2.6547	7.2282	1.6509	0.30769
L35	ammonium citrate	420.62	132.32	6.3831	54.735	0.23449
L35	ammonium sulfate	1270.5	-238.64	26.278	0.87984	0.24027
sodium carbonate	water	2018.7	-537.40	55.133	117.23	0.26365
water	sodium succinate	819.44	-365.10	-11.347	44.428	0.20004
water	sodium acetate	0.34847	1209.5	5.8643	-4.9735	0.22023
water	ammonium citrate	-0.63924	877.23	35.208	28.256	0.26643
water	ammonium sulfate	632.38	2708.0	0.36141	-2.8190	0.45715

$$A_{ij} = A_{0ij} + A_{1ij}T \quad (6)$$

$$A_{ji} = A_{0ji} + A_{1ji}T \quad (7)$$

This model has five adjustable parameters for each binary pair ( $A_{0ij}$ ,  $A_{0ji}$ ,  $A_{1ij}$ ,  $A_{1ji}$ , and  $\alpha_{ij}$ ). The parameters  $A_{0ij}$ ,  $A_{0ji}$ ,  $A_{1ij}$ , and  $A_{1ji}$  are related to the characteristic energy of interaction between the molecules of types  $i$  and  $j$ , while the parameter  $\alpha_{ij}$  is related to the nonrandomness of the mixture.

The software Fortran code WTML-LLE<sup>43</sup> was used to estimate the molecular energy binary interaction parameters with the NRTL model. The results are shown in Table 8. With these parameters, the experimental LLE data can be correlated. Comparisons between the experimental and the calculated composition of each component in both phases were made through root-mean-square ( $\partial w$ ) deviations, given by eq 8:

$$\partial w = 100 \sqrt{\frac{\sum_i^M \sum_j^{N-1} (w_{ij}^{\text{I,exp}} - w_{ij}^{\text{I,calc}})^2 + (w_{ij}^{\text{II,exp}} - w_{ij}^{\text{II,calc}})^2}{2MN}} \quad (8)$$

The correlation results are shown in Table 9 and indicate that it was possible to use the NRTL model because the global root-mean-square deviations, with 76 TLs, are as low as 1.49 %.

## Conclusions

LLE data for the ATPS L35 + sodium carbonate + water, L35 + sodium succinate + water, L35 + sodium acetate + water, L35 + ammonium citrate + water, and L35 + ammonium sulfate + water were obtained at (283.15 to 313.15) K. Except for the L35-(NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> system, increases in the temperature caused increases in the two-phase areas, showing that the ATPS formation process is entropy-driven. An increase in the STL with increasing temperature was also observed. The efficacy of the salts to induce phase segregation followed the

Table 9. Root-Mean-Square Deviations in Ternary Systems

system	NRTL $\partial w$ (%)
L35 + sodium carbonate + water at 283.15 K	1.46
L35 + sodium carbonate + water at 298.15 K	1.72
L35 + sodium carbonate + water at 313.15 K	2.01
L35 + sodium succinate + water at 283.15 K	0.73
L35 + sodium succinate + water at 298.15 K	0.81
L35 + sodium succinate + water at 313.15 K	0.83
L35 + sodium acetate + water at 283.15 K	1.51
L35 + sodium acetate + water at 298.15 K	1.90
L35 + sodium acetate + water at 313.15 K	2.13
L35 + ammonium citrate + water at 283.15 K	1.00
L35 + ammonium citrate + water at 298.15 K	0.50
L35 + ammonium citrate + water at 313.15 K	0.59
L35 + ammonium sulfate + water at 283.15 K	1.56
L35 + ammonium sulfate + water at 298.15 K	1.75
L35 + ammonium sulfate + water at 313.15 K	2.05
global (76 TLs)	1.49

order sodium carbonate > ammonium sulfate > sodium succinate > ammonium citrate > sodium acetate.

The consistency of the TL experimental data was assessed using the Othmer–Tobias correlation. The results are very satisfactory and show the consistency of the experiments carried out.

The energy parameters of binary interaction in the NRTL model were estimated, and the results from the correlation of the activity coefficient are very satisfactory, with root-mean-square deviations as low as 1.49 %. For that reason, this paper has shown that it is possible to use the original NRTL thermodynamic model in ATPS.

## Literature Cited

- (1) Albertsson, P. A. Chromatography and partition of cells and cell fragments. *Nature (London, U.K.)* **1956**, *177*, 771–774.
- (2) Rodrigues, G. D.; de Lemos, L. R.; da Silva, L. H. M.; da Silva, M. C. H.; Minim, L. A.; Coimbra, J. S. R. A green and sensitive method to determine phenols in water and wastewater samples using an aqueous two phase system. *Talanta* **2009**. DOI: 10.1016/j.talanta.2009.08.039.

- (3) Banik, R. M.; Santhiagu, A.; Kanari, B.; Sabarinath, C.; Upadhyay, S. N. Technological aspects of extractive fermentation using aqueous two-phase systems. *World J. Microbiol. Biotechnol.* **2003**, *19*, 337–348.
- (4) Santesson, S.; Ramirez, I. B. R.; Viberg, P.; Jergil, B.; Nilsson, S. Affinity two-phase partitioning in acoustically levitated drops. *Anal. Chem.* **2004**, *76*, 303–308.
- (5) Haghtalab, A.; Mokhtarian, B.; Maurer, G. Experimental results and thermodynamic modeling of the partitioning of lysozyme, bovine serum albumin, and  $\alpha$ -amylase in aqueous two-phase systems of PEG and ( $K_2HPO_4$  or  $Na_2SO_4$ ). *J. Chem. Eng. Data* **2003**, *48*, 1170–1177.
- (6) Everberg, H.; Clough, J.; Henderson, P.; Jergil, B.; Tjerneld, F.; Ramirez, I. B. R. Isolation of *Escherichia coli* inner membranes by metal affinity two-phase partitioning. *J. Chromatogr., A* **2006**, *1118*, 244–252.
- (7) Frerix, A.; Schonewald, M.; Geilenkirchen, P.; Muller, M.; Kula, M. R.; Hubbuch, J. Exploitation of the coil-globule plasmid DNA transition induced by small changes in temperature, pH salt, and poly(ethylene glycol) compositions for directed partitioning in aqueous two-phase systems. *Langmuir* **2006**, *22*, 4282–4290.
- (8) Azevedo, A. M.; Gomes, A. G.; Rosa, P. A. J.; Ferreira, I. F.; Pisco, A. M. M. O.; Aires-Barros, M. R. Partitioning of human antibodies in polyethylene glycol-sodium citrate aqueous two-phase systems. *Sep. Purif. Technol.* **2009**, *65*, 14–21.
- (9) Alejandro, N.; Ling, T. C.; Lyddiatt, A. Aqueous two-phase recovery of bio-nanoparticles: A miniaturization study for the recovery of bacteriophage T4. *J. Chromatogr., B* **2007**, *854*, 13–19.
- (10) Mageste, A. B.; de Lemos, L. R.; Ferreira, G. M. D.; da Silva, M. C. H.; da Silva, L. H. M.; Bonomo, R. C. F.; Minim, L. A. Aqueous two-phase systems: an efficient, environmentally safe and economically viable method for purification of natural dye carmine. *J. Chromatogr., A* **2009**, *1216*, 7623–7629.
- (11) Lacerda, V. G.; Mageste, A. B.; Santos, I. J. B.; da Silva, L. H. M.; da Silva, M. C. H. Separation of Cd and Ni from Ni-Cd batteries by an environmentally safe methodology employing aqueous two-phase systems. *J. Power Sources* **2009**, *193*, 908–913.
- (12) da Silva, L. H. M.; da Silva, M. C. H.; Junior, J. A.; Martins, J. P.; Coimbra, J. S. R.; Minim, L. A. Hydrophobic effect on the partitioning of  $[Fe(CN)_5(NO)]^{2-}$  and  $[Fe(CN)_6]^{3-}$  anions in aqueous two-phase systems formed by triblock copolymers and phosphate salts. *Sep. Purif. Technol.* **2008**, *60*, 103–112.
- (13) da Silva, L. H. M.; da Silva, M. C. H.; de Aquino, R. A. N.; Francisco, K. R.; Cardoso, M. V. C.; Minim, L. A.; Coimbra, J. S. R. Nitroprusside-PEO enthalpic interaction as driving force for partitioning of the  $[Fe(CN)_5NO]^{2-}$  anion in aqueous two-phase systems formed by poly(ethylene oxide) and sulfate salts. *J. Phys. Chem. B* **2006**, *110*, 23540–23546.
- (14) da Silva, L. H. M.; da Silva, M. C. H.; Francisco, K. R.; Cardoso, M. V. C.; Minim, L. A.; Coimbra, J. S. R. PEO- $[M(CN)_5NO]^{x-}$  ( $M = Fe, Mn$  or  $Cr$ ) Interaction as driving force in the partitioning of the pentacyanonitrosylmetallate anion in ATPS: The strong effect of the central atom. *J. Phys. Chem. B* **2008**, *112*, 11669–11678.
- (15) da Silva, M. D. H.; da Silva, L. H. M.; Paggioli, F. J.; Coimbra, J. S. R.; Minim, L. A. Sistema aquoso bifásico: uma alternativa eficiente para a extração de íons. *Quim. Nova* **2006**, *29*, 1332–1339.
- (16) da Silva, M. D. H.; da Silva, L. H. M.; Amim Junior, J.; Guimaraes, R. O.; Martins, J. P. Liquid-liquid equilibrium of aqueous mixture of triblock copolymers L35 and F68 with  $Na_2SO_4$  or  $Li_2SO_4$  or  $MgSO_4$ . *J. Chem. Eng. Data* **2006**, *51*, 2260–2264.
- (17) Zaslavsky, B. Y. *Aqueous two-phase partitioning, physical chemistry and bio-analytical applications*; Marcel Dekker: New York, 1995.
- (18) Martins, J. P.; Carvalho, P. C.; da Silva, L. H. M.; Coimbra, J. S. R.; da Silva, M. C. H.; Rodrigues, G. D.; Minim, L. A. Liquid-liquid equilibria of an aqueous two-phase system containing poly(ethylene glycol) 1500 and sulfate salts at different temperatures. *J. Chem. Eng. Data* **2008**, *53*, 238–241.
- (19) Zuniga, A. D. G.; Coimbra, J. S. R.; Arquete, D. A.; Minim, L. A.; da Silva, L. H. M.; Maffia, M. C. Interfacial tension and viscosity for poly(ethylene)glycol/maltodextrin aqueous two-phase systems. *J. Chem. Eng. Data* **2006**, *51*, 1144–1147.
- (20) Bridges, N. J.; Gutowski, K. E.; Rogers, R. D. Investigation of aqueous biphasic systems formed from solutions of chaotropic salts with kosmotropic salts (salt-salt ABS). *Green Chem.* **2007**, *9*, 177–183.
- (21) Haraguchi, L. H.; Mohamed, R. S.; Loh, W.; Pessoa Filho, P. A. Phase equilibrium and insulin partitioning in aqueous two-phase systems containing block copolymers and potassium phosphate. *Fluid Phase Equilib.* **2004**, *215*, 1–15.
- (22) Svensson, M.; Linse, P.; Tjerneld, F. Phase behavior in aqueous two-phase system containing micelle-forming block copolymers. *Macromolecules* **1995**, *28*, 3597–3603.
- (23) da Silva, L. H. M.; da Silva, M. D. H.; de Sousa, R. C. S.; Martins, J. P.; Rodrigues, G. D.; Coimbra, J. S. R.; Minim, L. A. Surface excess enthalpy of PEO + salt + water and L35 + Salt + Water Aqueous Two Phase Systems. *J. Chem. Eng. Data* **2009**, *54*, 531–535.
- (24) Martins, J. P.; Mageste, A. B.; da Silva, M. C. H.; da Silva, L. H. M.; Patricio, P. R.; Coimbra, J. S. R.; Minim, L. A. Liquid-liquid equilibria of an aqueous two-phase system formed by a triblock copolymer and sodium salts at different temperatures. *J. Chem. Eng. Data* **2009**, *54*, 2891–2894.
- (25) Snyder, S. M.; Cole, K. D.; Sziag, D. C. Phase compositions, viscosities and densities for aqueous two-phase systems composed of poly(ethylene glycol) and various salts at 25 °C. *J. Chem. Eng. Data* **1992**, *37*, 268–274.
- (26) Amaresh, S. P.; Murugesan, S.; Regupathi, I.; Murugesan, T. Liquid-liquid equilibrium of poly(ethylene glycol) 4000 + diammonium hydrogen phosphate plus water at different temperatures. *J. Chem. Eng. Data* **2008**, *53*, 1574–1578.
- (27) Carvalho, C. P.; Coimbra, J. S. R.; Costa, I. A. F.; Minim, L. A.; da Silva, L. H. M.; Maffia, M. C. Equilibrium data for PEG 4000 + salt + water systems from (278.15 to 318.15) K. *J. Chem. Eng. Data* **2007**, *52*, 351–356.
- (28) Rodrigues, G. D.; da Silva, M. D. H.; da Silva, L. H. M.; Paggioli, F. J.; Minim, L. A.; Coimbra, J. S. R. Liquid-liquid extraction of metal ions without use of organic solvent. *Sep. Purif. Technol.* **2008**, *62*, 687–693.
- (29) Ma, J. H.; Guo, C.; Tang, Y. L.; Wang, J.; Zheng, L.; Liang, X. F.; Chen, S.; Liu, H. Z. Salt-induced micellization of a triblock copolymer in aqueous solution: a  $^1H$  nuclear magnetic resonance spectroscopy study. *Langmuir* **2007**, *23*, 3075–3083.
- (30) da Silva, L. H. M.; da Silva, M. C. H.; Mesquita, A. F.; Nascimento, K. S.; Coimbra, J. S. R.; Minim, L. A. Equilibrium phase behavior of triblock copolymer + salt + water two-phase systems at different temperatures and pH. *J. Chem. Eng. Data* **2005**, *50*, 1457–1461.
- (31) Rodrigues, G. D.; da Silva, M. C. H.; da Silva, L. H. M.; Teixeira, L. S.; de Andrade, V. M. Liquid-liquid phase equilibrium of triblock copolymer L64, poly(ethylene oxide-*b*-propylene oxide-*b*-ethylene oxide), with sulfate salts from (278.15 to 298.15) K. *J. Chem. Eng. Data* **2009**, *54*, 1894–1898.
- (32) Othmer, D. F.; Tobias, P. E. Liquid-Liquid Extraction Data - The Line Correlation. *Ind. Eng. Chem.* **1942**, *34*, 693–696.
- (33) Renon, H.; Prausnitz, J. M. Local Compositions in Thermodynamics Excess Functions for Liquid Mixtures. *AIChE J.* **1968**, *14*, 135–144.
- (34) Regupathi, I.; Murugesan, S.; Govindarajan, R.; Amaresh, S. P.; Thanapalan, M. Liquid-liquid equilibrium of poly(ethylene glycol) 6000 + triammonium citrate + water systems at different temperatures. *J. Chem. Eng. Data* **2009**, *54*, 1094–1097.
- (35) Voros, N.; Proust, P.; Fredenslund, A. Liquid-liquid equilibria of aqueous two-phase systems containing salts and polyethylene glycol. *Fluid Phase Equilib.* **1993**, *90*, 333–353.
- (36) Zafarani-Moattar, M. T.; Hamzehzadeh, S. Liquid-liquid equilibria of aqueous two-phase systems containing poly(ethylene glycol) and sodium succinate or sodium formate. *CALPHAD: Comput. Coupling Phase Thermochem. Diagrams* **2005**, *29*, 1–6.
- (37) De Lisi, R.; Lazzara, G.; Milioto, S.; Muratore, N. A. Thermodynamic study to evidence the alpha, omega-dichloroalkane/block copolymer mixed aggregates formation: effect of the copolymer architecture. *J. Colloid Interface Sci.* **2006**, *300*, 368–374.
- (38) da Silva, L. H. M.; Loh, W. Calorimetric investigation of the formation of aqueous two-phase systems in ternary mixtures of water, poly(ethylene oxide) and electrolytes (or dextran). *J. Phys. Chem. B* **2000**, *104*, 10069–10073.
- (39) Santos, F. S.; D'Ávila, S. G.; Aznar, M. Salt Effect on Liquid-Liquid Equilibrium of Water + 1-Butanol + Acetone System: Experimental Determination and Thermodynamic Modeling. *Fluid Phase Equilib.* **2001**, *187/188*, 265–274.
- (40) Sé, R. A. G.; Aznar, M. Thermodynamic modeling of phase equilibrium for water + poly(Ethylene glycol) + salt aqueous two-phase systems. *Braz. J. Chem. Eng.* **2002**, *19*, 255–266.
- (41) Sé, R. A. G.; Aznar, M. Liquid-Liquid Equilibrium of the Aqueous Two-Phase System Water + PEG 4000 + Potassium Phosphate at Four Temperatures: Experimental Determination and Thermodynamic Modeling. *J. Chem. Eng. Data* **2002**, *47*, 1401–1405.
- (42) Castro, C. B.; Aznar, M. Liquid-Liquid Equilibrium of Water + PEG 8000 + Magnesium Sulfate. *Braz. J. Chem. Eng.* **2005**, *22*, 463–470.
- (43) Stragevitch, L. Liquid-Liquid Equilibrium in Nonelectrolyte Systems (in Portuguese). D.Sc. Thesis, State University of Campinas: Campinas, Brazil, 1997.

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