An Experimental and Kinetic Modeling Study of the Oxidation of the Four Isomers of Butanol

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Butanol, an alcohol which can be produced from biomass sources, has received recent interest as an alternative to gasoline for use in spark ignition engines and as a possible blending compound with fossil diesel or biodiesel. Therefore, the autoignition of the four isomers of butanol (1-butanol, 2-butanol, iso-butanol, and tert-butanol) has been experimentally studied at high temperatures in a shock tube, and a kinetic mechanism for description of their high-temperature oxidation has been developed. Ignition delay times for butanol/oxygen/argon mixtures have been measured behind reflected shock waves at temperatures and pressures ranging from approximately 1200 to 1800 K and 1 to 4 bar. Electronically excited OH emission and pressure measurements were used to determine ignition-delay times. The influence of temperature, pressure, and mixture composition on ignition delay has been characterized. A detailed kinetic mechanism has been developed to describe the oxidation of the butanol isomers and validated by comparison to the shock-tube measurements. Reaction flux and sensitivity analysis illustrates the relative importance of the three competing classes of consumption reactions during the oxidation of the four butanol isomers: dehydration, unimolecular decomposition, and H-atom abstraction. Kinetic modeling indicates that the consumption of 1-butanol and iso-butanol, the most reactive isomers, takes place primarily by H-atom abstraction resulting in the formation of radicals, the decomposition of which yields highly reactive branching agents, H atoms and OH radicals. Conversely, the consumption of tertbutanol and 2-butanol, the least reactive isomers, takes place primarily via dehydration, resulting in the formation of alkenes, which lead to resonance stabilized radicals with very low reactivity. To our knowledge, the ignitiondelay measurements and oxidation mechanism presented here for 2-butanol, iso-butanol, and tert-butanol are the first of their kind.

Introduction

Butanol derived from biomass sources, typically 1-butanol, has received recent attention as an alternative to gasoline and as a candidate for blending with diesel and biodiesel. Considerable research has been carried out aimed at production of butanol by using fermentation^{1,2} and nonfermentative biosynthesis.³ It has been shown that butanol can be produced via acetonebutanol—ethanol (ABE) fermentation by using starch- or sugarbased feedstocks (corn, wheat, sugar beets, sugar cane, sorghum)⁴ and nonedible lignocellulosic biomass.⁵ Because of the possibilities of butanol as an alternative transportation fuel, recently, the development and commercialization of butanol production processes has been undertaken by industrial corporations and startup companies. In partnership, Dupont and British Petroleum (BP) are converting a British Sugars ethanol plant in Wissington, England into a 1-butanol pilot plant to produce 9 million gallons yearly.⁶ The primary focus of synthesis research and commercial development has been on the production of 1-butanol, often called biobutanol, but there is also interest in processes to generate the higher octane rated 2-butanol and iso-butanol (2-methyl-1-propanol) isomers^{3,6} which may be used as neat fuels, in blended fuels, or as additives. Additionally, tert-butanol is currently used as a high-octane rated (RON = 105, MON = 89) oxygenated additive in gasoline. However, tert-butanol has a melting point of 25.5 $^{\circ}$ C and is not suitable as a neat fuel or as a high-concentration blending compound because of its propensity to gel.

Butanol has several advantages over methanol and ethanol as a transportation fuel. The butanol isomers have higher energy density than methanol and ethanol, see Table I. The volumetric energy density of 1-butanol is only 9% lower than that of gasoline. The butanols also have a much lower vapor pressure than ethanol and methanol, reducing evaporative emissions and chance of explosion. They are less hygroscopic than ethanol and methanol, making blending with gasoline and water contamination less problematic. 1-Butanol has also shown to be less corrosive to materials found in automotive fuel systems and existing pipelines than ethanol and is very close in octane rating to gasoline (Table I). In fact, 1-butanol can be used as a direct replacement for gasoline in spark ignition engines with few or no modifications.⁷

There have been few previous studies of the oxidation kinetics of the isomers of butanol. Rice et al.⁸ and Yacoub et al.⁹ have studied engine emissions and knock characteristics for a variety of butanol-gasoline blends. Hamins and Seshadri¹⁰ investigated the extinction of butanol diffusion flames. McEnally and Pfefferle¹¹ studied methane/air flames doped with the four butanol isomers. They measured temperature, C_1 – C_{12} hydrocarbons, and major species allowing investigation of the

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TABLE I: Properties of Gasoline, Methanol, Ethanol, and 1-Butanol

fuel	lower heating value [MJ/kg]	volumetric energy density [MJ/L]	research octane number, RON	motor octane number, MON	vapor pressure at 25 °C [Torr]
gasoline	42.5	32	92-98	82-88	
methanol	19.9	16	136	104	127
ethanol	28.9	20	129	102	59
1-butanol	33.1	29	96	78	6

decomposition kinetics of the butanol dopants and the emissions of toxic byproducts. Yang et al. 12 studied combustion intermediates in premixed, low-pressure (30 Torr, 1 Torr = 7.5 kPa), laminar, butanol-oxygen flames, for all four isomers, by using photoionization mass spectrometry. Shock-tube ignition-delay measurements for 1-butanol have been performed by Zhukov et al.¹³ for high-temperature, low-pressure (from 2.6 to 8.3 bar), argon-dilute mixtures. Dagaut and Togbé¹⁴ have recently investigated the oxidation of blends of 1-butanol with a gasoline surrogate mixture (iso-octane, toluene, and 1-hexene blends) in jet-stirred reactor experiments (temperatures range from 770 to 1220 K at 10 bar). They also developed a kinetic oxidation mechanism for 1-butanol which was combined with a mechanism for their gasoline surrogate and used to simulate their jetstirred reactor measurements with fairly good agreement between simulations and measurements. It has also been shown that the addition of oxygenated compounds, such as butanol, to traditional fuels can reduce engine-soot emissions. In the recent study of Pepiot-Desjardins et al.,15 this phenomenon was quantified for a variety of oxygenates, including butanol.

Because of the growing interest in butanol as an alternative fuel and the limited number and types of previous kinetic studies, here, we present shock tube ignition-delay measurements for 1-butanol, 2-butanol, iso-butanol, and tert-butanol at high temperatures and a newly developed kinetic mechanism to describe the oxidation of the four isomers at high temperatures. To our knowledge, the measurements and mechanism presented here are the first of their kind for 2-butanol, iso-butanol, and tert-butanol.

Experimental Method

Shock-tube ignition-delay times were measured in a newly constructed high-purity, low-pressure (P < 10 bar), stainless steel shock tube at Rensselaer Polytechnic Institute (RPI). The shock tube has a 12.3 cm inner diameter with 7.54 m long driven and 3.05 m long driver sections. The driver is separated from the driven by a single polycarbonate diaphragm prior to experiments. Diaphragms are burst by using a stationary mechanical cutter by pressurizing the driver with helium. At the diaphragm section, there is a round—square—round transition

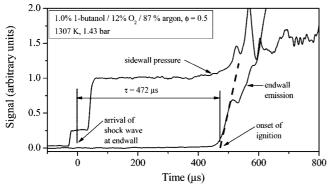


Figure 1. Example butanol ignition-delay time measurement (pressure and OH* emission).

which allows the diaphragm to separate into four petals upon rupture, minimizing the formation of small diaphragm particles which can contaminate the test section.

The driven section is evacuated with a Varian DS202 roughing pump, which can evacuate the shock tube to 2×10^{-3} Torr, and a Varian V70 turbomolecular pump coupled to a Varian DS202 backing pump, which can bring the shock tube to an ultimate pressure of 1×10^{-6} Torr with a leak rate of 3×10^{-6} Torr min⁻¹. Ultimate pressures are measured by using an ion gauge (Varian type 564 gauge). The driver is evacuated with another Varian DS202 vacuum pump to ultimate pressures of 2×10^{-3} Torr.

Reactant mixtures are made externally to the shock tube in a stainless steel mixing vessel with an internal, magnetically powered, vane stirrer. Gases are introduced to the mixing vessel from high-pressure gas cylinders (oxygen and argon) and via the vaporization of the liquid butanols from air-free glassware. The gases are introduced to the mixing vessel from the highpressure cylinders and glassware through a stainless steel mixing manifold; after mixing, the gas mixtures are introduced to the shock tube, located directly adjacent to the mixing vessel and manifold. The mixing vessel and manifold can be evacuated by using a Varian DS202 vacuum pump to an ultimate pressure of 2×10^{-3} Torr. Mixtures were made by using the method of partial pressures with measurements of pressure made by using a high-accuracy Baratron pressure manometer and a Setra diaphragm pressure gauge. Reactant mixtures were made by using high-purity oxygen (99.995%) and argon (99.999%) and 1-butanol (99.8+%), 2-butanol (99.5+%), iso-butanol (99.5+%), and tert-butanol (99.5+%) from Sigma Aldrich. The isomers of butanol were degassed prior to introduction into the evacuated mixing vessel via room-temperature evaporation. Atmospheric

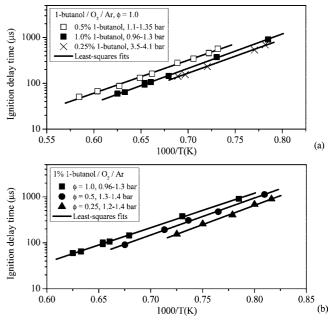


Figure 2. Raw 1-butanol ignition time measurements.

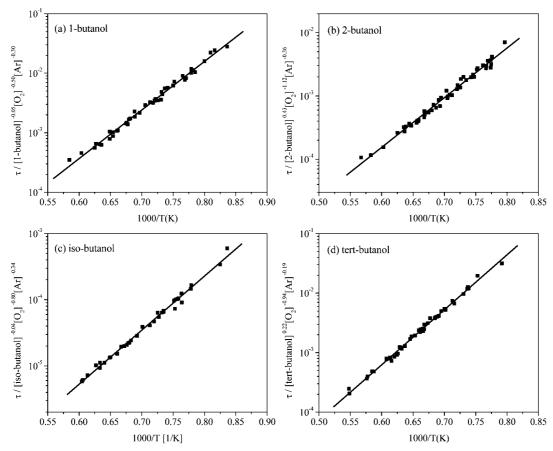


Figure 3. Correlated ignition times for all four butanol isomers.

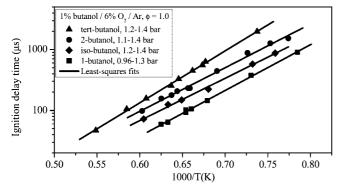


Figure 4. Ignition-time measurements for all four butanol isomers for a mixture composition of 1% butanol/6% O_2/Ar ($\Phi = 1.0$) and reflected-shock pressures near 1 bar.

water contamination was not an issue with 1-butanol, 2-butanol, and iso-butanol which are only slightly miscible in water. On the other hand, tert-butanol, which is soluble in water, was frozen at \sim 10-20 °C and pumped for a period of time to ensure that all atmospheric water introduced during transfer of the tertbutanol was removed. Mixtures were stirred by using the magnetically powered vane stirrer for two hours prior to experiments.

The shock tube is equipped with five piezoelectric pressure transducers (PCB transducer model 113A26 and amplifier model 498) with rise times of $\leq 1 \mu s$ spaced over the last 1.24 m of the driven section for the measurement of the incident shock velocity. The transducers are flush mounted in the shock-tube sidewall and coated with room-temperature-vulcanizing (RTV) silicone insulation to avoid signal decay due to heat transfer to the transducer from the shock-heated gases. The transducers

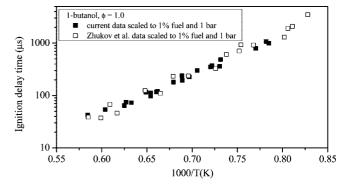


Figure 5. Comparison of the current ignition-time measurements for 1-butanol with the measurements of Zhukov et al.;13 all data scaled to a common condition: 1% butanol, $\Phi = 1.0$, and 1 bar.

are equally separated by 30.5 cm with the last transducer located 2 cm from the endwall. The signals from the five pressure transducers are sent to four Raycal Dana 1992 universal counters $(0.1 \,\mu s \text{ resolution})$, which provide the time intervals for incident shock passage allowing determination of the incident shock wave velocities at four locations over the last 1.1 m of the driven section. The four incident shock velocities are linearly extrapolated to the shock tube endwall to determine the incident shock velocity at the test location. Additionally, the pressure transducer located 2 cm from the shock-tube endwall can be used for quantitative pressure measurements at the test location.

The incident and reflected shock conditions (vibrationally equilibrated) are calculated by using the normal shock relations and the measured incident shock velocity at the test location, the measured initial temperature and pressure, and the thermodynamic properties of the reactant mixture. The initial temperature (room temperature) is measured by using a mercury

TABLE II: Primary Mechanism for the Oxidation of the Four Butanol Isomers at High Temperature^a

reactions	A A	n	E_{a}	no.
$C_4H_9OH-1 \Rightarrow H_2O + C_4H_8-1$	Intramolecular Dehydrations $2.0 \times 10^{+14}$	0.0	72000	(1)
	$1.5 \times 10^{+15}$	0.0	66000	(1)
$C_4H_9OH-2 \Rightarrow H_2O + C_4H_8-1$				(2)
$C_4H_9OH-2 \Rightarrow H_2O + C_4H_8-2$	$2.0 \times 10^{+14}$	0.0	67000	(3)
$isoC_4H_9OH \Rightarrow H_2O + iC_4H_8$	$2.0 \times 10^{+6}$	2.12	62000	(4)
$terC_4H_9OH \rightarrow H_2O + iC_4H_8$	$2.7 \times 10^{+15}$	0.0	72000	(5)
$C_4H_9OH-1 = \bullet OH + \bullet C_4H_9-1$	Unimolecular Initiations $1.16 \times 10^{+15}$	0.0	92320	(6)
$C_4H_9OH^{-1} = \bullet OH + C_3H_7CH_2O\bullet$	$1.51 \times 10^{+13}$			(6)
. ,		0.0	103620	(7)
$C_4H_9OH-1 = \bullet C_3H_7-1 + \bullet CH_2OH$	$1.47 \times 10^{+15}$	0.0	82930	(8)
$C_4H_9OH-1 = \bullet C_2H_5 + \bullet CH_2CH_2OH$	$2.23 \times 10^{+15}$	0.0	82760	(9)
$C_4H_9OH-1 = \bullet CH_3 + \bullet CH_2C_2H_4OH$	$5.82 \times 10^{+15}$	0.0	84870	(10)
$C_4H_9OH-2 = \bullet C_2H_5 \bullet CHOH + CH_3$	$1.58 \times 10^{+15}$	0.0	79770	(11)
$C_4H_9OH-2 = \bullet OH + \bullet C_4H_9-2$	$3.25 \times 10^{+14}$	0.0	92050	(12)
$C_4H_9OH-2 = \bullet H + C_2H_5CH(O\bullet)CH_3$	$1.24 \times 10^{+13}$	0.0	105460	(13)
$C_4H_9OH-2 = \bullet C_2H_5 + CH_3 \bullet CHOH$	$6.06 \times 10^{+14}$	0.0	82170	(14)
$C_4H_9OH-2 = \bullet CH_3 + \bullet CH_2CH(OH)CH_3$	$1.83 \times 10^{+15}$	0.0	85370	(15)
$isoC_4H_9OH = \bullet CH_3 + CH_3 \bullet CHCH_2OH$	$5.14 \times 10^{+15}$	0.0	80540	(16)
$isoC_4H_9OH = \bullet CH_2OH + \bullet C_3H_7-2$	$6.47 \times 10^{+14}$	0.0	79070	(17)
$isoC_4H_9OH = \bullet OH + \bullet iC_4H_9$	$1.40 \times 10^{+14}$	0.0	91720	(18)
$isoC_4H_9OH = \bullet H + \bullet CH_3CH(CH_3)CH_2O\bullet$	$5.24 \times 10^{+12}$	0.0	101860	(19)
$terC_4H_9OH = \bullet OH + \bullet tC_4H_9$	$1.00 \times 10^{+15}$	0.0	95639	(20)
$terC_4H_9OH = \bullet H + C(CH_3)_3O\bullet$	$2.39 \times 10^{+13}$	0.0	105630	(21)
$terC_4H_9OH = \bullet CH_3 + \bullet C(CH_3)_3OH$	$1.9 \times 10^{+16}$	0.0	83600	(22)
	Bimolecular Initiations			
$C_4H_9OH-1 + O_2 = \bullet HO_2 + C_3H_7\bullet CHOH$	$1.4 \times 10^{+13}$	0.0	46869	(23)
$C_4H_9OH-1 + O_2 = \bullet HO_2 + C_3H_7CH_2O\bullet$	$7.0 \times 10^{+12}$	0.0	55172	(24)
$C_4H_9OH-1 + O_2 = \bullet HO_2 + \bullet CH_2C_3H_6OH$	$2.1 \times 10^{+13}$	0.0	53033	(25)
$C_4H_9OH-1 + O_2 = \bullet HO_2 + CH_3 \bullet CHC_2H_4OH$	$1.4 \times 10^{+13}$	0.0	50588	(26)
$C_4H_9OH-1 + O_2 = \bullet HO_2 + C_2H_5 \bullet CHCH_2OH$	$1.4 \times 10^{+13}$	0.0	50652	(27)
$C_4H_9OH-2 + O_2 = \bullet HO_2 + C_2H_5CH(OH)\bullet CH_2$	$2.1 \times 10^{+13}$	0.0	52333	(28)
$C_4H_9OH-2 + O_2 = \bullet HO_2 + \bullet CH_2CH_2CH(OH)CH_3$	$2.1 \times 10^{+13}$	0.0	53033	(29)
$C_4H_9OH-2 + O_2 = \bullet HO_2 + CH_3 \bullet CHCH(OH)CH_3$	$1.4 \times 10^{+13}$	0.0	50588	(30)
$C_4H_9OH-2 + O_2 = \bullet HO_2 + C_2H_5CH(O\bullet)CH_3$	$7.0 \times 10^{+12}$	0.0	57272	(31)
$C_4H_9OH-2 + O_2 = \bullet HO_2 + C_2H_5C\bullet (OH)CH_3$	$7.0 \times 10^{+12}$	0.0	44726	(32)
$isoC_4H_9OH + O_2 = \bullet HO_2 + CH_3C\bullet (CH_3)CH_2OH$	$7.0 \times 10^{+12}$	0.0	47243	(33)
$isoC_4H_9OH + O_2 = \bullet HO_2 + \bullet CH_2CH(CH_3)CH_2OH$	$4.2 \times 10^{+13}$	0.0	52333	(34)
$isoC_4H_9OH + O_2 = \bullet HO_2 + CH_3CH(CH_3)CH_2O\bullet$	$7.0 \times 10^{+12}$	0.0	55172	(35)
$isoC_4H_9OH + O_2 = •HO_2 + CH_3CH(CH_3) •CHOH$	$1.4 \times 10^{+13}$	0.0	46869	(36)
$terC_4H_9OH + O_2 = \bullet HO_2 + C(CH_3)_3O\bullet$	$7.0 \times 10^{+12}$	0.0	56872	(37)
$terC_4H_9OH + O_2 = \bullet HO_2 + \bullet CH_2C(CH_3)_2OH$	$6.3 \times 10^{+13}$	0.0	53033	(38)
	Isomerizations			
$\bullet C_4 H_9 - 1 = \bullet C_4 H_9 - 2$	$3.3 \times 10^{+09}$	1.0	37000	(39)
C_3H_7 •CHOH = CH_3 •CHC ₂ H ₄ OH	$3.3 \times 10^{+09}$	1.0	43000	(40)
C_3H_7 •CHOH = •CH ₂ C ₃ H ₆ OH	$8.6 \times 10^{+08}$	1.0	25800	(41)
$\bullet CH_2C_3H_6OH = C_2H_5\bullet CHCH_2OH$	$3.3 \times 10^{+09}$	1.0	37000	(42)
$C_2H_5CH(OH) \bullet CH_2 = CH_3 \bullet CHCH(OH)CH_3$	$3.3 \times 10^{+09}$	1.0	37000	(43)
$C_2H_5CH(OH) \bullet CH_2 = \bullet CH_2CH_2CH(OH)CH_3$	$8.6 \times 10^{+08}$	1.0	19800	(44)
•CH ₂ CH ₂ CH(OH)CH ₃ = C_2H_3 C• (OH)CH ₃	$1.7 \times 10^{+09}$	1.0	33000	(45)
•CH ₂ CH(CH ₃)CH ₂ OH = CH ₃ CH(CH ₃) •CHOH	$3.3 \times 10^{+09}$	1.0	35000	(46)
	Beta-Scissions			
$ \bullet C_3H_{7}-1 \Rightarrow \bullet CH_3 + C_2H_4 $	$2.0 \times 10^{+13}$	0.0	31000	(47)
$\bullet C_3H_7-1 \Rightarrow \bullet H + C_3H_6$	$3.0 \times 10^{+13}$	0.0	38000	(48)
$\bullet C_4 H_9 - 1 \Rightarrow \bullet C_2 H_5 + C_2 H_4$	$2.0 \times 10^{+13}$	0.0	28700	(49)
$\bullet C_4H_9-1 \Rightarrow \bullet H + C_4H_8-1$	$3.0 \times 10^{+13}$	0.0	38000	(50)
C_3H_7 •CHOH \Rightarrow •H + C_4H_8 O-LY b,c	$3.0 \times 10^{+13}$	0.0	36400	(51)
C_3H_7 •CHOH \Rightarrow •H + C_4H_8 O-A d	$2.5 \times 10^{+13}$	0.0	29000	(52)
$C_3H_7CH_2O \bullet \Rightarrow \bullet C_3H_7-1 + HCHO$	$2.0 \times 10^{+13}$	0.0	24700	(53)
$C_3H_7CH_2O \Rightarrow \bullet H + C_4H_8O-A$	$3.0 \times 10^{+13}$	0.0	27800	(54)
$\bullet CH_2C_3H_6OH \Rightarrow \bullet CH_2CH_2OH + C_2H_4$	$2.0 \times 10^{+13}$	0.0	30700	(55)
$\bullet CH_2C_3H_6OH \rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	36500	(56)
$CH_3 \circ CH_2 \cup G_3 \cap G \circ CH_3 \circ CH_2 \cup G \cap G \circ CH_3 \circ CH_3 \circ CH_3 \circ CH_3 \cup G \cap G \cap G \circ CH_3 \cup G \cap G \cap G \circ CH_3 \cup G \cap G \cap G \cap G \circ CH_3 \cup G \cap G$	$2.0 \times 10^{+13}$	0.0	30500	(57)
	$3.0 \times 10^{+13}$			
$CH_3 \circ CHC_2H_4OH \Rightarrow \circ H + C_4H_8O-LY$ $CH_4 \circ CHC_4 \circ CHC_4 \Rightarrow \circ H + C_4H_8O-LY$	$3.0 \times 10^{+13}$ $3.0 \times 10^{+13}$	0.0	36900	(58)
$CH_3 \circ CHC_2H_4OH \rightarrow \circ H + C_4H_8O-LY$		0.0	38900	(59)
C_2H_5 •CHCH ₂ OH \Rightarrow •OH + C_4H_8 -1	$2.0 \times 10^{+13}$	0.0	26000	(60)
$C_2H_5 \circ CHCH_2OH \Rightarrow \circ H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	36900	(61)
C_2H_5 •CHCH ₂ OH \Rightarrow •H + C_4H_8 O-LY	$3.0 \times 10^{+13}$	0.0	31200	(62)
		0.0	20700	(62)
C_2H_5 •CHCH ₂ OH \Rightarrow •CH ₃ + C_3H_6 O-LY C_2H_5 CH(OH)•CH ₂ \Rightarrow •OH + C_4H_8 -1	$2.0 \times 10^{+13} \\ 2.0 \times 10^{+13}$	0.0 0.0	30600 26000	(63) (64)

TABLE II: Continued

reactions	A	n	E_{a}	no.
$C_2H_5CH(OH) \bullet CH_2 \Rightarrow \bullet H + C_4H_8O-LY$	$1.5 \times 10^{+13}$	0.0	35000	(65)
$CH_2CH_2CH(OH)CH_3 \Rightarrow CH_3 \bullet CHOH + C_2H_4$	$2.0 \times 10^{+13}$	0.0	29600	(66)
$CH_2CH_2CH(OH)CH_3 \Rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	36900	(67)
$CH_3 \bullet CHCH(OH)CH_3 \Rightarrow \bullet OH + C_4H_8-2$	$2.0 \times 10^{+13}$	0.0	26000	(68)
$CH_3 \bullet CHCH(OH)CH_3 \Rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	38100	(69)
$CH_3 \bullet CHCH(OH)CH_3 \Rightarrow \bullet CH_3 + C_3H_6O-LY$	$2.0 \times 10^{+13}$	0.0	29700	(70)
$CH_3 \bullet CHCH(OH)CH_3 \Rightarrow \bullet H + C_4H_8O-LY$	$1.5 \times 10^{+13}$	0.0	34800	(71)
$C_2H_5CH(O\bullet)CH_3 \rightarrow \bullet C_2H_5 + CH_3CHO$	$2.0 \times 10^{+13}$	0.0	21700	(72)
$C_2H_5CH(O\bullet)CH_3 \rightarrow \bullet CH_3 + C_2H_5CHO$	$2.0 \times 10^{+13}$	0.0	21900	(73)
$C_2H_5CH(O\bullet)CH_3 \rightarrow \bullet H + C_3H_8CO$	$1.5 \times 10^{+13}$	0.0	25000	(74)
$C_2H_5C\bullet(OH)CH_3 \Rightarrow \bullet H + C_3H_8CO$	$2.5 \times 10^{+13}$	0.0	29000	(75)
$C_2H_5C\bullet(OH)CH_3 \Rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	37800	(76)
$C_2H_5C\bullet(OH)CH_3 \Rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	39200	(77)
$C_2H_5C\bullet(OH)CH_3 \rightarrow \bullet CH_3 + C_3H_6O-LY$	$2.0 \times 10^{+13}$	0.0	32400	(78)
$CH_3C \bullet (CH_3)CH_2OH \Rightarrow \bullet OH + iC_4H_8$	$2.0 \times 10^{+13}$	0.0	26000	(79)
$CH_3C\bullet(CH_3)CH_2OH \Rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	39100	(80)
$CH_3C \bullet (CH_3)CH_2OH \rightarrow \bullet H + C_4H_8O-LY$	$6.0 \times 10^{+13}$	0.0	35100	(81)
${}^{\circ}\text{CH}_2\text{CH}(\text{CH}_3)\text{CH}_2\text{OH} \rightarrow {}^{\circ}\text{CH}_2\text{OH} + \text{C}_3\text{H}_6$	$2.0 \times 10^{+13}$	0.0	30600	(82)
$ \begin{array}{c} \text{CH}_2\text{CH}(\text{CH}_3)\text{CH}_2\text{OH} \Rightarrow \bullet \text{CH}_3 + \text{C}_3\text{H}_6\text{O-LY} \\ \text{CH}_2\text{CH}(\text{CH}_3)\text{CH}_2\text{OH} \Rightarrow \bullet \text{CH}_3 + \text{C}_3\text{H}_6\text{O-LY} \end{array} $	$2.0 \times 10^{+13}$	0.0	30600	(83)
	$1.5 \times 10^{+13}$	0.0	36700	(84)
$CH_3CH(CH_3)CH_2O\bullet \Rightarrow \bullet C_3H_7-2 + HCHO$	$2.0 \times 10^{+13}$	0.0	24200	(85)
$CH_3CH(CH_3)CH_2O \rightarrow H + C_4H_8O-A$	$3.0 \times 10^{+13}$	0.0	28600	(86)
$CH_3CH(CH_3)CH_2O^{\bullet} \rightarrow H + C_4H_8O-LY$ $CH_3CH(CH_3) \bullet CHOH \rightarrow \bullet H + C_4H_8O-LY$	$3.0 \times 10^{+13}$	0.0	35600	(87)
$CH_3CH(CH_3) \circ CHOH \Rightarrow \circ H + C_4H_8O-A$	$2.5 \times 10^{+13}$	0.0	29000	(88)
$CH_3CH(CH_3) \bullet CHOH \rightarrow \bullet CH_3 + C_3H_6O-LY$	$4.0 \times 10^{+13}$	0.0	30500	(89)
$C(CH_3)_3O \rightarrow CH_3 + C_2H_6CO$	$6.0 \times 10^{+13}$	0.0	22700	(90)
$C(CH_3)_3O^{\bullet} \rightarrow {}^{\bullet}CH_3 + C_2H_6CO$ $C(CH_2)_2OH \rightarrow {}^{\bullet}OH + iC_4H_8$	$4.0 \times 10^{+13}$	0.0	26000	(90)
$ \begin{array}{c} \text{CH}_2\text{C}(\text{CH}_3)_2\text{OH} \rightarrow \text{\bullet OH} + \text{IC}_4\text{H}_8\\ \text{CH}_2\text{C}(\text{CH}_3)_2\text{OH} \rightarrow \text{\bullet CH}_3 + \text{C}_3\text{H}_6\text{O-LY} \end{array} $	$4.0 \times 10^{+13}$ $4.0 \times 10^{+13}$	0.0	32500	(91)
- '	$2.0 \times 10^{+13}$	0.0	31000	. ,
${}^{\circ}C_4H_9-2 \Rightarrow {}^{\circ}CH_3 + C_3H_6$	$3.0 \times 10^{+13}$	0.0	38000	(93)
${}^{\circ}C_{4}H_{9}-2 \Rightarrow {}^{\circ}H + C_{4}H_{8}-1$				(94)
$C_4H_9-2 \Rightarrow \bullet H + C_4H_8-2$	$3.0 \times 10^{+13}$	0.0	39000	(95)
${}^{\circ}C_3H_{7^{-2}} \Rightarrow {}^{\circ}H + C_3H_6$	$6.0 \times 10^{+13}$	0.0	39000	(96)
${}^{\circ}\text{CH}_{2}\text{C}_{2}\text{H}_{4}\text{OH} \Rightarrow {}^{\circ}\text{CH}_{2}\text{OH} + \text{C}_{2}\text{H}_{4}$	$2.0 \times 10^{+13}$	0.0	31100	(97)
$\circ CH_2C_2H_4OH \Rightarrow \circ H + C_3H_6O-LY$	$3.0 \times 10^{+13}$	0.0	36500	(98)
C_2H_5 •CHOH \Rightarrow •H + C_2H_5 CHO	$2.5 \times 10^{+13}$	0.0	29000	(99)
$C_2H_5 \bullet CHOH \Rightarrow \bullet H + C_3H_6O-LY$	$3.0 \times 10^{+13}$	0.0	36800	(100)
$\bullet CH_2CH(OH)CH_3 \Rightarrow \bullet OH + C_3H_6$	$2.0 \times 10^{+13}$	0.0	26000	(101)
$\bullet CH_2CH(OH)CH_3 \Rightarrow \bullet H + C_3H_6O-LY$	$1.5 \times 10^{+13}$	0.0	35200	(102)
$CH_3 \bullet CHCH_2OH \Rightarrow \bullet OH + C_3H_6$	$2.0 \times 10^{+13}$	0.0	26000	(103)
$CH_3 \bullet CHCH_2OH \Rightarrow \bullet H + C_3H_6O-LY$	$3.0 \times 10^{+13}$	0.0	37700	(104)
$CH_3 \bullet CHCH_2OH \Rightarrow \bullet H + C_3H_6O-LY$	$3.0 \times 10^{+13}$	0.0	34700	(105)
$\bullet iC_4H_9 \Rightarrow \bullet CH_3 + C_3H_6$	$4.0 \times 10^{+13}$	0.0	31000	(106)
$\bullet iC_4H_9 \Rightarrow \bullet H + iC_4H_8$	$3.0 \times 10^{+13}$	0.0	37500	(107)
$\bullet tC_4H_9 \Rightarrow \bullet H + iC_4H_8$	$9.0 \times 10^{+13}$	0.0	39000	(108)
$\bullet C(CH_3)_3OH \Rightarrow \bullet H + C_2H_6CO$	$2.5 \times 10^{+13}$	0.0	29000	(109)
$\bullet C(CH_3)_3OH \Rightarrow \bullet H + C_3H_6O-LY$	$6.0 \times 10^{+13}$	0.0	39400	(110)
$C_3H_7 \bullet CHOH \Rightarrow CH_3CHO + \bullet C_2H_5$	$2.0 \times 10^{+13}$	0.0	28700	(111)
$C_2H_5CH(OH) \bullet CH_2 \Rightarrow CH_3CHO + \bullet C_2H_5$	$2.0 \times 10^{+13}$	0.0	28700	(112)
C_2H_5 •CHOH \Rightarrow CH ₃ CHO + •CH ₃	$2.0 \times 10^{+13}$	0.0	31000	(113)
$OCH_2CH(OH)CH_3 \Rightarrow CH_3CHO + OCH_3$	$2.0 \times 10^{+13}$	0.0	31000	(114)
				` '
	Oxidations	0.0	5000	/115\
C_3H_7 •CHOH + $O_2 \Rightarrow C_4H_8$ O-LY + •HO ₂	$1.3 \times 10^{+12}$	0.0	5000	(115)
$C_3H_7 \bullet CHOH + O_2 \Rightarrow C_4H_8O - A + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(116)
$C_3H_7CH_2O \bullet + O_2 \Rightarrow C_4H_8O - A + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(117)
$CH_2C_3H_6OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(118)
$CH_3 \bullet CHC_2H_4OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(119)
$CH_3 \bullet CHC_2H_4OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$5.3 \times 10^{+11}$	0.0	5000	(120)
$C_2H_5 \bullet CHCH_2OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(121)
$C_2H_5 \bullet CHCH_2OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(122)
$C_2H_5CH(OH) \bullet CH_2 + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(123)
$CH_2CH_2CH(OH)CH_3 + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(124)
$CH_3 \bullet CHCH(OH)CH_3 + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(125)
$CH_3 \bullet CHCH(OH)CH_3 + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$5.3 \times 10^{+11}$	0.0	5000	(126)
$C_2H_5CH(O\bullet)CH_3 + O_2 \Rightarrow C_3H_8CO + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(127)
$C_2H_5C_4OH)CH_3 + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(128)
$C_2H_5C_{\bullet}(OH)CH_3 + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$5.3 \times 10^{+11}$	0.0	5000	(129)
$C_2H_5C \bullet (OH)CH_3 + O_2 \Rightarrow C_3H_8CO + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(130)
$C_2H_3C \bullet (GH_3)CH_2OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.3 \times 10^{+12}$	0.0	5000	(131)
$CH_3C \bullet (CH_3)CH_2OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$ $CH_3C \bullet (CH_3)CH_2OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$1.0 \times 10^{+12}$	0.0	5000	(131)
	1.0 \ 10	0.0	5000	(134)
$\bullet CH_2CH(CH_3)CH_2OH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(133)

TABLE II: Continued

reactions	A	n	E_{a}	no.
$CH_3CH(CH_3) \bullet CHOH + O_2 \Rightarrow C_4H_8O-LY + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(135)
$CH_3CH(CH_3) \bullet CHOH + O_2 \Rightarrow C_4H_8O - A + \bullet HO_2$	$4.4 \times 10^{+11}$	0.0	5000	(136)
$\bullet C_3H_7-2 + O_2 \Rightarrow C_3H_6 + \bullet HO_2$	$2.3 \times 10^{+12}$	0.0	5000	(137)
$\bullet_1 C_4 H_9 + O_2 \Rightarrow i C_4 H_8 + \bullet_1 HO_2$	$1.6 \times 10^{+12}$	0.0	5000	(138)
104119 1 02 104118 1 1102		0.0	2000	(130)
$C_4H_9OH-1 + \bullet O \bullet \Rightarrow \bullet OH + C_3H_7 \bullet CHOH$	Metathesis $3.4 \times 10^{+08}$	1.5	1000	(139)
$C_4H_9OH-1 + \bullet H \Rightarrow H_2 + C_3H_7 \bullet CHOH$	$4.8 \times 10^{+09}$	1.5	3310	(140)
$C_4H_9OH^{-1} + •OH \Rightarrow H_2O + C_3H_7•CHOH$	$2.4 \times 10^{+06}$	2.0	-2200	(140)
$C_4H_9OH^{-1} + •OH \rightarrow H_2O_2 + C_3H_7•CHOH$ $C_4H_9OH^{-1} + •HO_2 \Rightarrow H_2O_2 + C_3H_7•CHOH$	$2.4 \times 10^{+04}$ $2.8 \times 10^{+04}$	2.7	14380	(141)
$C_4H_9OH^{-1} + {}^{\bullet}HO_2 \longrightarrow H_2O_2 + C_3H_7 {}^{\bullet}CHOH$	$1.6 \times 10^{+06}$	1.9	6840	(143)
$C_4H_9OH-2 + \bullet O \bullet \Rightarrow \bullet OH + C_2H_5C \bullet (OH)CH_3$	$1.7 \times 10^{+08}$	1.5	-350	(144)
$C_4H_9OH-2 + \bullet H \Rightarrow H_2 + C_2H_5C\bullet(OH)CH_3$	$2.4 \times 10^{+09}$	1.5	2140	(145)
$C_4H_9OH-2 + \bullet OH \Rightarrow H_2O + C_2H_5C \bullet (OH)CH_3$	$1.2 \times 10^{+06}$	2.0	-3100	(146)
$C_4H_9OH-2 + \bullet HO_2 \Rightarrow H_2O_2 + C_2H_5C\bullet(OH)CH_3$	$1.4 \times 10^{+04}$	2.7	13300	(147)
$C_4H_9OH-2 + \bullet CH_3 \Rightarrow CH_4 + C_2H_5C \bullet (OH)CH_3$	$8.1 \times 10^{+05}$	1.9	5670	(148)
$isoC_4H_9OH + \bullet O \bullet \Rightarrow \bullet OH + CH_3CH(CH_3) \bullet CHOH$	$3.4 \times 10^{+08}$	1.5	1000	(149)
$isoC_4H_9OH + \bullet H \Rightarrow H_2 + CH_3CH(CH_3)\bullet CHOH$	$4.8 \times 10^{+09}$	1.5	3310	(150)
$isoC_4H_9OH + \bullet OH \Rightarrow H_2O + CH_3CH(CH_3)\bullet CHOH$	$2.4 \times 10^{+06}$	2.0	-2200	(151)
$isoC_4H_9OH + \bullet HO_2 \Rightarrow H_2O_2 + CH_3CH(CH_3)\bullet CHOH$	$2.8 \times 10^{+04}$	2.7	14380	(152)
$isoC_4H_9OH + \bullet CH_3 \Rightarrow CH_4 + CH_3CH(CH_3)\bullet CHOH$	$1.6 \times 10^{+06}$	1.9	6840	(153)
$C_4H_9OH-1 + \bullet O \bullet \Rightarrow \bullet OH + C_3H_7CH_2O \bullet$	$1.7 \times 10^{+13}$	0.0	7850	(154)
$C_4H_9OH-1 + \bullet H \Rightarrow H_2 + C_3H_7CH_2O\bullet$	$9.5 \times 10^{+06}$	2.0	7700	(155)
$C_4H_9OH-1 + \bullet OH \Rightarrow H_2O + C_3H_7CH_2O\bullet$	$8.9 \times 10^{+05}$	2.0	450	(156)
$C_4H_9OH-1 + \bullet HO_2 \Rightarrow H_2O_2 + C_3H_7CH_2O\bullet$	$2.0 \times 10^{+11}$	0.0	17000	(157)
$C_4H_9OH-1 + \bullet CH_3 \Rightarrow CH_4 + C_3H_7CH_2O\bullet$	1.0×10^{-01}	4.0	8200	(158)
$C_4H_9OH-2 + \bullet O \bullet \Rightarrow \bullet OH + C_2H_5CH(O \bullet)CH_3$	$1.7 \times 10^{+13}$	0.0	7850	(159)
$C_4H_9OH-2 + \bullet H \Rightarrow H_2 + C_2H_5CH(O \bullet)CH_3$	$9.5 \times 10^{+06}$	2.0	7700	(160)
$C_4H_9OH-2 + \bullet OH \Rightarrow H_2O + C_2H_5CH(O\bullet)CH_3$	$8.9 \times 10^{+05}$	2.0	450	(161)
$C_4H_9OH-2 + \bullet HO_2 \Rightarrow H_2O_2 + C_2H_5CH(O\bullet)CH_3$	$2.0 \times 10^{+11}$	0.0	17000	(162)
$C_4H_9OH-2 + \bullet CH_3 \Rightarrow CH_4 + C_2H_5CH(O\bullet)CH_3$	1.0×10^{-01}	4.0	8200	(163)
$isoC_4H_9OH + \bullet O \bullet \Rightarrow \bullet OH + CH_3CH(CH_3)CH_2O \bullet$	$1.7 \times 10^{+13}$	0.0	7850 7700	(164)
$isoC_4H_9OH + \bullet H \Rightarrow H_2 + CH_3CH(CH_3)CH_2O\bullet$	$9.5 \times 10^{+06}$	2.0	7700	(165)
$isoC_4H_9OH + \bullet OH \Rightarrow H_2O + CH_3CH(CH_3)CH_2O \bullet$	$8.9 \times 10^{+05}$	2.0	450.0	(166)
$isoC_4H_9OH + \bullet HO_2 \Rightarrow H_2O_2 + CH_3CH(CH_3)CH_2O \bullet$	$2.0 \times 10^{+11} \\ 1.0 \times 10^{-01}$	0.0	17000	(167)
isoC ₄ H ₉ OH + •CH ₃ \Rightarrow CH ₄ + CH ₃ CH(CH ₃)CH ₂ O• terC ₄ H ₉ OH + •O• \Rightarrow •OH + C(CH ₃) ₃ O•	1.0×10^{-3} $1.7 \times 10^{+13}$	4.0 0.0	8200 7850	(168) (169)
$terC_4H_9OH + \bullet H \Rightarrow H_2 + C(CH_3)_3O\bullet$	$9.5 \times 10^{+06}$	2.0	7700	(170)
$terC_4H_9OH + \bullet OH \Rightarrow H_2O + C(CH_3)_3O\bullet$	$8.9 \times 10^{+05}$	2.0	450	(171)
$terC_4H_9OH + \bullet HO_2 \Rightarrow H_2O_2 + C(CH_3)_3O\bullet$	$2.0 \times 10^{+11}$	0.0	17000	(171)
$terC_4H_9OH + \bullet CH_3 \Rightarrow CH_4 + C(CH_3)_3O\bullet$	1.0×10^{-01}	4.0	8200	(173)
$C_4H_9OH-1 + \bullet O \bullet \Rightarrow \bullet OH + \bullet CH_2C_3H_6OH$	$5.1 \times 10^{+13}$	0.0	7850	(174)
$C_4H_9OH-1 + \bullet O \bullet \Rightarrow \bullet OH + CH_3 \bullet CHC_2H_4OH$	$2.6 \times 10^{+13}$	0.0	5200	(175)
$C_4H_9OH-1 + \bullet O \bullet \Rightarrow \bullet OH + C_2H_5 \bullet CHCH_2OH$	$2.6 \times 10^{+13}$	0.0	5200	(176)
$C_4H_9OH-1 + \bullet H \Rightarrow H_2 + \bullet CH_2C_3H_6OH$	$2.9 \times 10^{+07}$	2.0	7700	(177)
$C_4H_9OH-1 + \bullet H \Rightarrow H_2 + CH_3 \bullet CHC_2H_4OH$	$9.0 \times 10^{+06}$	2.0	5000	(178)
$C_4H_9OH-1 + \bullet H \Rightarrow H_2 + C_2H_5 \bullet CHCH_2OH$	$9.0 \times 10^{+06}$	2.0	5000	(179)
$C_4H_9OH-1 + \bullet OH \Rightarrow H_2O + \bullet CH_2C_3H_6OH$	$2.7 \times 10^{+06}$	2.0	450	(180)
$C_4H_9OH-1 + \bullet OH \Rightarrow H_2O + CH_3 \bullet CHC_2H_4OH$	$2.6 \times 10^{+06}$	2.0	-765	(181)
$C_4H_9OH-1 + \bullet OH \Rightarrow H_2O + C_2H_5 \bullet CHCH_2OH$	$2.6 \times 10^{+06}$	2.0	-765	(182)
$C_4H_9OH-1 + \bullet HO_2 \Rightarrow H_2O_2 + \bullet CH_2C_3H_6OH$	$6.0 \times 10^{+11}$	0.0	17000	(183)
$C_4H_9OH-1 + \bullet HO_2 \Rightarrow H_2O_2 + CH_3\bullet CHC_2H_4OH$	$4.0 \times 10^{+11}$	0.0	15500	(184)
$C_4H_9OH-1 + \bullet HO_2 \Rightarrow H_2O_2 + C_2H_5 \bullet CHCH_2OH$	$4.0 \times 10^{+11}$	0.0	15500	(185)
$C_4H_9OH-1 + \bullet CH_3 \Rightarrow CH_4 + \bullet CH_2C_3H_6OH$	3.0×10^{-01}	4.0	8200	(186)
$C_4H_9OH-1 + \bullet CH_3 \Rightarrow CH_4 + CH_3 \bullet CHC_2H_4OH$	$2.0 \times 10^{+11}$	0.0	9600	(187)
$C_4H_9OH-1 + \bullet CH_3 \Rightarrow CH_4 + C_2H_5 \bullet CHCH_2OH$	$2.0 \times 10^{+11}$	0.0	9600	(188)
$C_4H_9OH-2 + \bullet O \bullet \Rightarrow \bullet OH + C_2H_5CH(OH) \bullet CH_2$	$5.1 \times 10^{+13}$	0.0	7850	(189)
$C_4H_9OH-2 + \bullet O \bullet \Rightarrow \bullet OH + \bullet CH_2CH_2CH(OH)CH_3$	$5.1 \times 10^{+13}$	0.0	7850 5200	(190)
$C_4H_9OH-2 + \bullet O \bullet \Rightarrow \bullet OH + CH_3 \bullet CHCH(OH)CH_3$	$2.6 \times 10^{+13}$	0.0	5200	(191)
$C_4H_9OH-2 + \bullet H \Rightarrow H_2 + C_2H_3CH(OH) \bullet CH_2$ $C_4H_9OH-2 + \bullet H \Rightarrow H_2 + \bullet CH_2CH_2CH(OH)CH_3$	$2.9 \times 10^{+07} \\ 2.9 \times 10^{+07}$	2.0	7700 7700	(192)
	$9.0 \times 10^{+06}$	2.0 2.0		(193)
$C_4H_9OH-2 + \bullet H \Rightarrow H_2 + CH_3 \bullet CHCH(OH)CH_3$ $C_4H_9OH-2 + \bullet OH \Rightarrow H_2O + C_2H_5CH(OH) \bullet CH_2$	$2.7 \times 10^{+06}$	2.0	5000 450	(194) (195)
$C_4H_9OH-2 + \bullet OH \rightarrow H_2O + \bullet CH_2CH_2CH(OH)CH_3$	$2.7 \times 10^{+06}$ $2.7 \times 10^{+06}$	2.0	450	(196)
$C_4H_9OH-2 + \bullet OH \rightarrow H_2O + CH_2CH_2CH_1OH)CH_3$ $C_4H_9OH-2 + \bullet OH \rightarrow H_2O + CH_3\bullet CHCH(OH)CH_3$	$2.6 \times 10^{+06}$	2.0	-765	(190)
$C_4H_9OH-2 + \bullet HO_2 \Rightarrow H_2O_2 + C_2H_5CH(OH) \bullet CH_2$	$6.0 \times 10^{+11}$	0.0	17000	(197)
$C_4H_9OH-2 + \bullet HO_2 \rightarrow H_2O_2 + \bullet CH_2CH_2CH(OH)CH_3$	$6.0 \times 10^{+11}$	0.0	17000	(198)
$C_4H_9OH-2 + •HO_2 \rightarrow H_2O_2 + CH_3•CHCH(OH)CH_3$	$4.0 \times 10^{+11}$	0.0	15500	(200)
$C_4H_9OH-2 + \bullet CH_3 \Rightarrow CH_4 + C_2H_5CH(OH) \bullet CH_2$	3.0×10^{-01}	4.0	8200	(201)
$C_4H_9OH-2 + \bullet CH_3 \Rightarrow CH_4 + \bullet CH_2CH_2CH(OH)CH_3$	3.0×10^{-01}	4.0	8200	(202)
$C_4H_9OH-2 + \bullet CH_3 \Rightarrow CH_4 + CH_3 \bullet CHCH(OH)CH_3$	$2.0 \times 10^{+11}$	0.0	9600	(203)
$isoC_4H_9OH + \bullet O \rightarrow \bullet OH + CH_3C \bullet (CH_3)CH_2OH$	$1.0 \times 10^{+13}$	0.0	3280	(204)
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TABLE II: Continued

reactions	A	n	E_{a}	no.
$isoC_4H_9OH + \bullet O \bullet \Rightarrow \bullet OH + \bullet CH_2CH(CH_3)CH_2OH$	$1.0 \times 10^{+14}$	0.0	7850	(205)
$isoC_4H_9OH + \bullet H \Rightarrow H_2 + CH_3C\bullet(CH_3)CH_2OH$	$4.2 \times 10^{+06}$	2.0	2400	(206)
$isoC_4H_9OH + \bullet H \Rightarrow H_2 + \bullet CH_2CH(CH_3)CH_2OH$	$5.7 \times 10^{+07}$	2.0	7700	(207)
$isoC_4H_9OH + \bullet OH \Rightarrow H_2O + CH_3C\bullet (CH_3)CH_2OH$	$1.1 \times 10^{+06}$	2.0	-1865	(208)
$isoC_4H_9OH + \bullet OH \Rightarrow H_2O + \bullet CH_2CH(CH_3)CH_2OH$	$5.4 \times 10^{+06}$	2.0	450	(209)
$isoC_4H_9OH + \bullet HO_2 \Rightarrow H_2O_2 + CH_3C\bullet (CH_3)CH_2OH$	$2.0 \times 10^{+11}$	0.0	14000	(210)
$isoC_4H_9OH + \bullet HO_2 \Rightarrow H_2O_2 + \bullet CH_2CH(CH_3)CH_2OH$	$1.2 \times 10^{+12}$	0.0	17000	(211)
$isoC_4H_9OH + \bullet CH_3 \Rightarrow CH_4 + CH_3C\bullet (CH_3)CH_2OH$	$1.0 \times 10^{+11}$	0.0	7900	(212)
$isoC_4H_9OH + \bullet CH_3 \Rightarrow CH_4 + \bullet CH_2CH(CH_3)CH_2OH$	6.0×10^{-01}	4.0	8200	(213)
$terC_4H_9OH + \bullet O \Rightarrow OH + \bullet CH_2C(CH_3)_2OH$	$1.5 \times 10^{+14}$	0.0	7850	(214)
$terC_4H_9OH + \bullet H \Rightarrow H_2 + \bullet CH_2C(CH_3)_2OH$	$8.6 \times 10^{+07}$	2.0	7700	(215)
$terC_4H_9OH + \bullet OH \Rightarrow H_2O + \bullet CH_2C(CH_3)_2OH$	$8.1 \times 10^{+06}$	2.0	450	(216)
$terC_4H_9OH + \bullet HO_2 \Rightarrow H_2O_2 + \bullet CH_2C(CH_3)_2OH$	$1.8 \times 10^{+12}$	0.0	17000	(217)
$terC_4H_9OH + \bullet CH_3 \Rightarrow CH_4 + \bullet CH_2C(CH_3)_2OH$	9.0×10^{-01}	4.0	8200	(218)
	Combinations			
$\bullet H + \bullet C_3 H_7 - 2 \Rightarrow C_3 H_8$	$8.3 \times 10^{+12}$	0.0	0	(219)
$\bullet H + \bullet tC_4H_9 \Rightarrow C_4H_{10}$	$8.3 \times 10^{+12}$	0.0	0	(220)
$\bullet OH + \bullet C_3H_7-2 \Rightarrow C_3H_7OH$	$5.9 \times 10^{+12}$	0.0	0	(221
$\bullet HO_2 + \bullet C_3H_7-2 \Rightarrow C_3H_7OOH$	$4.8 \times 10^{+12}$	0.0	0	(222)
$\bullet HO_2 + \bullet tC_4H_9 \Rightarrow C_4H_9OOH$	$4.5 \times 10^{+12}$	0.0	0	(223)
$\bullet CH_3 + \bullet C_3H_7-2 \Rightarrow C_4H_{10}$	$1.5 \times 10^{+13}$	0.0	0	(224)
$\bullet CH_3 + \bullet tC_4H_9 \Rightarrow C_5H_{12}$	$1.5 \times 10^{+13}$	0.0	0	(225)
•HCO + •C ₃ H ₇ -2=>C ₄ H ₈ O-A	$5.2 \times 10^{+12}$	0.0	0	(226)
•HCO + •tC ₄ H ₉ \Rightarrow C ₅ H ₁₀ O-A	$4.9 \times 10^{+12}$	0.0	0	(227)
$\bullet CH_2OH + \bullet tC_4H_9 \Rightarrow C_5H_{12}O-L$	$4.8 \times 10^{+12}$	0.0	0	(228)
$CH_3O \bullet + \bullet C_3H_7-2 \Rightarrow C_4H_{10}O-E^e$	$4.9 \times 10^{+12}$	0.0	0	(229)
$CH_3O \bullet + \bullet tC_4H_9 \Rightarrow C_5H_{12}O-E$	$4.6 \times 10^{+12}$	0.0	0	(230)
$CH_3OO \bullet + \bullet C_3H_{7}-2 \Rightarrow C_4H_{10}O_2-U^f$	$4.4 \times 10^{+12}$	0.0	0	(231)
$CH_3OO \bullet + \bullet tC_4H_9 \Rightarrow C_5H_{12}O_2 - U$	$4.1 \times 10^{+12}$	0.0	0	(232)
$\bullet C_2H_5 + \bullet C_3H_{7}-2 \Rightarrow C_5H_{12}$	$5.2 \times 10^{+12}$	0.0	0	(233)
$\bullet C_2H_5 + \bullet tC_4H_9 \Rightarrow C_6H_{14}$	$4.9 \times 10^{+12}$	0.0	0	(234)
$\bullet C_3 H_{7}-2 + \bullet C_3 H_{7}-2 \Rightarrow C_6 H_{14}$	$2.3 \times 10^{+12}$	0.0	0	(235)
$\bullet C_3H_7-2 + \bullet tC_4H_9 \Rightarrow C_7H_{16}$	$4.3 \times 10^{+12}$	0.0	0	(236)
$\bullet tC_4H_9 + \bullet tC_4H_9 \Rightarrow C_8H_{18}$	$2.0 \times 10^{+12}$	0.0	0	(237)

^a The rate constants are given at 1 bar $(k = AT^n \exp(-E_a/RT))$ in cm³, mol, s, cal units. ^b L indicates that the species is bearing an alcohol function. ^c Y indicates that the species is an unsaturated one. ^d A indicates that the species is bearing an aldehyde function. ^e E indicates that the species is bearing an ether function. f U indicates that the species is bearing an -O-O• function.

thermometer, and the initial pressure is measured by using the high-accuracy Baratron pressure manometer located on the mixing/gas filling manifold directly adjacent to the shock tube. Thermodynamic properties of the mixtures are calculated by using thermochemical polynomials from the Burcat and Ruscic database.¹⁶ The uncertainty in the resulting reflected shock conditions is estimated at <1 and <1.5% for temperature and pressure, respectively, on the basis of uncertainties in the measured incident shock velocity and initial conditions (temperature, pressure, and mixture composition). The uncertainty in measured incident shock velocity is the largest contributor to uncertainty in reflected shock conditions. The measured reflected shock pressures agreed well with calculated pressures when using vibrationally equilibrated incident and reflected shock conditions for all mixtures ($\pm 2\%$, within the uncertainty in measured reflected shock pressure).

Ignition delay times were determined behind reflected shock waves by using the emission from electronically excited OH radicals (OH*) observed through a UV fused silica optic flush mounted in the shock-tube endwall. The OH* emission was separated from other optical interference by using a UG-5 Schott glass filter and recorded with a Thorlabs PDA36A silicon photodetector. The ignition-delay time was defined as the time interval between shock arrival and reflection at the endwall and the onset of ignition at the endwall. The onset of ignition was determined by extrapolating the peak slope in OH* emission to the baseline, and the shock arrival and reflection at the endwall was determined from the measured incident shock

Figure 6. Example of intramolecular dehydration in the case of 1-butanol.

velocity and the measurement of the shock passage at a location 2 cm from the endwall, where a piezoelectric transducer is located. See figure 1 for an example ignition time measurement. The pressure transducer and emission signals were recorded by using a National Instruments PCI-6133 data acquisition card (3 MHz, 14-bit and eight analog input channels) interfaced to a desktop computer with LabVIEW software.

Prior to performing measurements for butanol ignition-delay times, measurements were made of ignition-delay times for propane and methanol behind reflected shock waves at the conditions of previous shock-tube studies published in the literature to validate the new shock-tube facility and experimental techniques. Measurements for ignition-delay times were made for propane/O₂/Ar mixtures at conditions previously investigated by Horning et al.,17 and measurements were made for methanol/O₂/Ar mixtures at conditions previously investigated by Shin et al.¹⁸ These compounds were chosen because of the confidence we have in these two previous data sets and because methanol, as a liquid-phase alcohol at room temperature, requires vaporization for mixture preparation, as do the butanol isomers. The validation measurements performed in the new shock tube are in excellent agreement (differences of at most

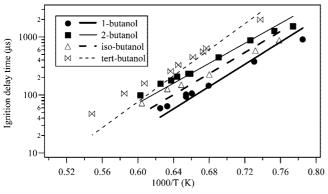


Figure 7. Comparison between simulations and experimental results for the ignition-delay times of the four isomers of butanol for stoichiometric mixtures containing 1% butanol.

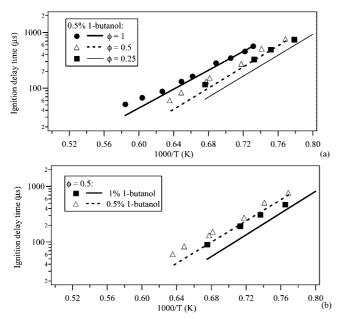


Figure 8. Comparison between simulations and experimental results for the ignition-delay times of 1-butanol (a) for mixtures containing 0.5% 1-butanol for three different equivalence ratios and (b) for mixtures with an equivalence ratio of 0.5 for two different concentrations of 1-butanol.

20%) with the previous studies, lending confidence to the new facility and methods used for determination of reflected shock conditions and ignition times.

Experimental Results

Ignition-delay measurements for 1-butanol, 2-butanol, isobutanol, and tert-butanol were carried out at a variety of conditions to determine the ignition-delay time dependence on concentration of the fuel, O_2 , and argon and temperature. Measurements were made for all butanol isomers by using mixtures (butanol/ O_2 /Ar molar %) with common composition at similar pressures: 1%/6%/93% ($\Phi=1$), 0.5%/3%/96.5% ($\Phi=1$), 1%/12%/87% ($\Phi=0.5$), 0.5%/6%/93.5% ($\Phi=0.5$), 1%/24%/75% ($\Phi=0.25$), and 0.5%/12%/87.5% ($\Phi=0.25$) mixtures, all at pressures near 1 bar, and 0.25%/1.5%/98.25% ($\Phi=1$) mixtures at pressures near 4 bar. Measurements were made for reflected shock temperatures ranging from 1196 to 1823 K with ignition times ranging from 47 to 1974 μ s.

In figure 2, raw ignition-delay results for 1-butanol are shown. As expected, the data exhibits clear Arrhenius exponential dependence on inverse temperature, with very little scatter about

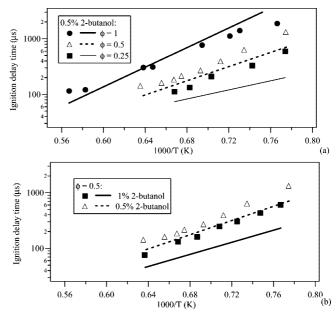


Figure 9. Comparison between simulations and experimental results for the ignition-delay times of 2-butanol (a) for mixtures containing 0.5% 2-butanol for three different equivalence ratios and (b) for mixtures with an equivalence ratio of 0.5 for two different concentrations of 2-butanol.

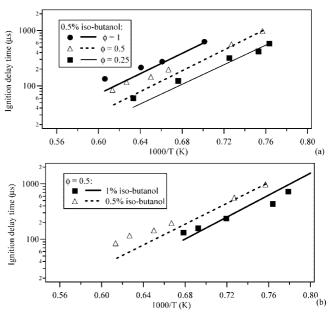


Figure 10. Comparison between simulations and experimental results for the ignition-delay times of iso-butanol (a) for mixtures containing 0.5% iso-butanol for three different equivalence ratios and (b) for mixtures with an equivalence ratio of 0.5 for two different concentrations of iso-butanol.

the linear least-squares fits for given data sets. We estimate the uncertainty in ignition-delay measurements at $\pm 15\%$ on the basis of uncertainties in reflected shock temperature and pressure and initial mixture composition and uncertainties in determining ignition times from the measured pressure and emission signals. The results for the three other isomers, not shown, have scatter similar to that of the 1-butanol data, with ignition times that vary in magnitude and slightly in overall activation energy. All of the data (177 experiments in total) is available in tabulated form in the Supporting Information.

A linear regression analysis was performed to determine the ignition time dependence on reactant concentrations and tem-

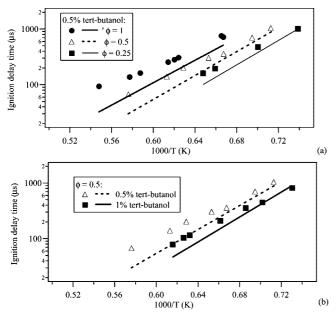


Figure 11. Comparison between simulations and experimental results for the ignition-delay times of tert-butanol (a) for mixtures containing 0.5% tert-butanol for three different equivalence ratios and (b) for mixtures with an equivalence ratio of 0.5 for two different concentrations of tert-butanol.

perature. The results of the regression analysis are four correlations for the butanol isomers

$$\begin{split} \text{1-butanol:} & \tau = 10^{-8.34(\pm 0.47)} [\text{1-butanol}]^{-0.05(\pm 0.06)} \times \\ & [\text{O}_2]^{-0.50(\pm 0.04)} [\text{Ar}]^{-0.30(\pm 0.05)} \exp(18800 \pm 400/T) \ (\mu\text{s}) \ \ (1) \\ \text{2-butanol:} & \tau = 10^{-8.53(\pm 0.57)} [\text{2-butanol}]^{-0.43(\pm 0.06)} \times \\ & [\text{O}_2]^{-1.12(\pm 0.04)} [\text{Ar}]^{-0.36(\pm 0.06)} \exp(18100 \pm 400/T) \ (\mu\text{s}) \ \ (2) \\ \text{iso-butanol:} & \tau = 10^{-10.19(\pm 0.62)} [\text{iso-butanol}]^{-0.04(\pm 0.06)} \times \\ & [\text{O}_2]^{-0.80(\pm 0.04)} [\text{Ar}]^{-0.34(\pm 0.05)} \exp(18800 \pm 450/T) \ (\mu\text{s}) \ \ (3) \\ \text{tert-butanol:} & \tau = \\ & 10^{-8.74(\pm 0.42)} [\text{tert-butanol}]^{-0.22(\pm 0.05)} [\text{O}_2]^{-0.94(\pm 0.03)} \times \\ & [\text{Ar}]^{-0.19(\pm 0.04)} \exp(21300 \pm 400/T) \ (\mu\text{s}) \ \ (4) \end{split}$$

where concentrations are in units of mol/cm³, temperature is in Kelvin, and the given uncertainties in the correlation parameters are the uncertainties in the regression analysis resulting from scatter in the data. The correlated ignition times are shown in Figure 3 and exhibit little deviation, with r^2 values of 98.7–99.5% for the four isomers. However, because of the relatively small range of conditions studied, extrapolating these correlations to conditions vastly different from those of the present study should be avoided.

The ignition times for the four butanol isomers are compared for a common mixture composition (1% butanol/6% O₂/93% Ar, $\Phi = 1$) and pressure (~ 1 bar) in Figure 4. The comparison shows that the ignition times vary from longest to shortest (least reactive to most reactive) in the order tert-butanol, 2-butanol, iso-butanol, and 1-butanol. The figure also shows that the apparent activation energy is similar for 1-butanol, 2-butanol, and iso-butanol but is somewhat greater for tert-butanol; the greater activation energy for tert-butanol is also exhibited in the correlations.

To our knowledge, there has been only one previous study of butanol ignition. Zhukov et al. 13 recently reported shocktube ignition-delay times for 1-butanol measured at pressures of 2.6, 4.4, and 8.3 bar and for three mixtures with $\Phi = 0.5$. 1.0, and 2.0. The majority of their measurements were made for $\Phi = 1.0$ mixtures with composition of 0.6% 1-butanol/3.6% $O_2/95.8\%$ Ar. In Figure 5, the current $\Phi = 1.0$ 1-butanol data is compared to the $\Phi = 1.0$ 1-butanol data of Zhukov et al., with both data sets scaled to 1% 1-butanol/6% O₂/93% Ar and 1 bar by using the correlations given previously. When scaled, the agreement between the two studies is quite good.

Mechanism Generation

A single mechanism has been generated for the four isomers of butanol by using the EXGAS software. This software has already been extensively described for the case of alkanes^{19–21} as well as for ethers.22

General Features of EXGAS. The software provides reaction mechanisms consisting of three parts:

- (1) A comprehensive primary mechanism, in which the only molecular reactants considered are the initial organic compounds and oxygen (see Table II).
- (2) A lumped secondary mechanism, containing reactions that consume the molecular products of the primary mechanism which do not react in the reaction bases. 19,20
- (3) A C₀-C₂ reaction base including all the reactions involving radicals or molecules containing less than three carbon atoms, 23 which is periodically updated and which is coupled with a reaction base for C₃-C₄ unsaturated hydrocarbons^{24,25} such as propyne, allene, butadiene, or butenes, including reactions leading to the formation of benzene. The pressuredependent rate constants follow the formalism proposed by Troe²⁶ and collision efficiency coefficients have been included.

Thermochemical data for molecules or radicals are automatically computed by using the THERGAS software²⁷ based on group additivity²⁸ and stored as 14 polynomial coefficients, according to the CHEMKIN II formalism.29

The rate parameters for isomerizations, combinations of free radicals, and unimolecular decompositions are calculated by using the KINGAS software¹⁹ and based on thermochemical kinetics methods,²⁸ transition state theory, or modified collision theory. The kinetic data of other types of reactions are estimated from correlations, 20 which are based on quantitative structurereactivity relationships and obtained from the literature.

Mechanism Generation for Alcohol Reactants. The structure of the current butanol mechanism is similar to that of alkanes except for the addition of a new generic dehydration reaction. Many rate constants were also modified for reactions involving bonds in the vicinity of the OH group. Table II presents the comprehensive primary mechanism, which contains 237 reactions for 1-butanol, 2-butanol, iso-butanol, tert-butanol, and produced free radicals. Because the mechanism was built for modeling high-temperature conditions, the additions of alkyl free radicals to molecular oxygen are neglected. The generic reactions taken into account are then as follows.

Intramolecular Dehydration (Reactions 1–5 in Table II). Intramolecular dehydration must be considered for alcohols and, therefore, has been added for the four butanols. Figure 6 illustrates the occurrence of this reaction via the favored fourcenter cyclic transition state. By considering only the favored four-center cyclic transition state, there is one possible intramolecular dehydration reaction for 1-butanol, iso-butanol, and tertbutanol and two for 2-butanol. Few kinetic parameters have been published concerning these reactions, for example, by Tsang³⁰ in the case of ethanol ($A = 2.86 \times 10^{14} \text{ s}^{-1}$ (3 abstractable H atoms), $E_a = 68.9$ kcal/mol obtained by using a two parameters

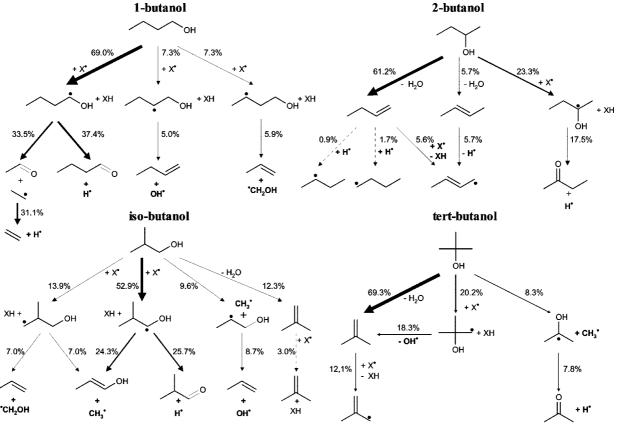


Figure 12. Reaction pathways analyses for the four isomers of butanol performed at 1450 K at atmospheric pressure for a stoichiometric mixtures containing 1% butanol and for 50% butanol conversion. The size of the arrows is proportional to the relative reaction flux. X• is H•, OH•, HO₂•, CH₃•, or •O• radicals and XH is H₂, H₂O, H₂O₂, or CH₄ molecules or OH• radicals.

fit), by Bui et al.31 from theoretical calculations for iso-propanol $(k_{\infty} = 2.0 \times 10^6 T^{2.12} \exp(-30700/T) \text{ s}^{-1} \text{ at the high-pressure}$ limit, for 6 abstractable H atoms) and by Newman³² for tertbutanol ($k = 7.7 \text{ x} 10^{14} \exp(-33145/T) \text{ s}^{-1}$, for 9 abstractable H atoms), but disagreements can be observed between all the proposed rate constants. For iso-butanol, we have used the isopropanol value proposed by Bui et al.³¹ For the other compounds, the rate parameters of these reactions which have large sensitivity coefficients, as it will be shown later in the text, have been fitted in order to obtain sufficient agreement with the experimental results. The starting point for this fit was taken from the recommendation of Tsang³⁰ for ethanol, by taking into account the change in the number of abstractable H atoms in the A factor for the case of the butanols. The required maximum adjustment in the rate parameters, from this starting point, was a factor 5 for the A factor (2-butanol) and adjustment to the activation energy of 3.1 kcal/mol (1-butanol and tert-butanol). The adjusted rate constant used for tert-butanol intramolecular dehydration is 3.75 times lower at 1200 K than that proposed by Newman.³² As shown by Tsang³⁰ in the case of the dehydration of ethanol, the falloff effect starts to have some influence above 1800 K; this effect has been neglected in the present work, which concerns the heavier butanols as opposed to ethanol, the subject of Tsang's work. The formation of the different butene isomers, namely, 1-butene, 2-butene, and isobutene, has been distinguished.

Unimolecular Initiations via C-C, C-O, or C-H Bond Fission (Reactions 6–22). The kinetic data for unimolecular decompositions were calculated by using the KINGAS software¹⁹ without considering falloff effects. The calculation was made for a temperature of 1400 K to reflect the range of experimental temperatures.

Bimolecular Initiations (Reactions 23–38). The rate constants for the bimolecular initiations between butanols and O_2 involving the abstraction of alkylic or alcoholic H atoms were estimated by using the correlation proposed by Ingham et al.³³ for hydrocarbons.

Intramolecular Radical Isomerizations (Reactions 39–46). The isomerizations involving the transfer of an alcoholic H atom were not considered. As in previous work, 19–21 the activation energy was set equal to the sum of the activation energy for H abstraction from the substrate by analogous radicals and the strain energy of the saturated cyclic transition state.

Decompositions of Radicals via β -Scission (Reactions 47–114). In order to maintain a mechanism of manageable size, molecules formed in the primary mechanism, with the same molecular formula and the same functional groups, are lumped into one unique species without distinction for the different isomers. Consequently, the molecules obtained via β -scission and oxidation reactions are lumped. This is the case, for example, for butenols (C₄H₈O-LY in Table II), butanals (C₄H₈O-A), pentanals $(C_5H_{10}O-A)$, pentanes (C_5H_{12}) , and hexanes (C₆H₁₄). The molecules contained in the reaction bases are not lumped, for example, allene, propyne, and butenes. Kinetic data for reactions involving radical decomposition via β -scission are the same as those used in the case of alkanes and ethers^{20,22} apart from the activation energy of the β -scissions involving the breaking of a C-C or a C-H bond in α-position of the alcohol function. Activation energies for these reactions were evaluated using Evans-Polanyi correlations between the activation energies for alkyl and alkenyl free radical decomposition^{20,34} and enthalpies of reaction obtained by using the THERGAS software.²⁷

Oxidations (Reactions 115-138). The oxidations of the involved radicals by O2 yield butenols or butanals. The rate constants are those used in previous work concerning alkanes²⁰ and alkenes.34

Metatheses Involving an H Abstraction by Small Radicals (Reactions 139-218). The small radicals taken into account are O and H atoms and OH, HO₂, and CH₃. All the abstractions involving alkylic and alcoholic H atoms have been considered. Kinetic data are generally those used for the alkanes.²⁰ Rate constants for the abstraction of an H atom from a carbon atom located in α -position of the alcohol function (reactions 139–153), the fastest of the H-atom abstraction reactions, have been evaluated by using an Evans-Polanyi-type correlation from Dean and Bozzelli,35 developed for the abstraction of H atoms from hydrocarbons

$$k = n_{\rm H} A T^n \exp(-\{E_0 - f(\Delta H_0 - \Delta H)\}/RT)$$
 (5)

where $n_{\rm H}$ is the number of abstractable H atoms, A, n, and E_0 are the rate parameters for the case of a metathesis by the considered radical from ethane, ΔH_0 is the enthalpy of the metathesis by the considered radical from ethane, ΔH is the enthalpy of the metathesis by the considered radical from the reacting molecule, f is a correlation factor, the values of which are given by Dean and Bozzelli35 for each considered radical, and R is the gas constant. According to Luo, 36 the bond energy of the O-H bond for the alcohol function is between 102 and 106 kcal⋅mol⁻¹, a value equal to that of a C−H bond in the case of an alkylic primary H atom. Therefore, the kinetic parameters for an H-atom abstraction from an alcohol function (reactions 154-173) are assumed equal to those for the abstraction of a primary alkylic H atom.

Termination Steps (Reactions 219–237). Termination steps include the combinations involving iso-propyl and tert-butyl radicals with rate constants calculated by using KINGAS software.19

Additional Reactions. Because butenes are important products of the oxidation of butanols under the present conditions, the mechanism for their consumption must be included. The reactions considered for the consumption of butenes (1-butene, 2-butene, and iso-butene) were the additions of H and O atoms and of OH, CH₃, and HO₂ radicals to the butene double bonds and the H abstractions by small radicals leading to resonance stabilized radicals. Additionally, two C₂ alcohol radicals, for which reactions were not considered in the C_0 – C_2 reaction base, must be taken into account. The consumption of these two radicals, namely, •CH2-CH2-OH and CH3-•CH-OH, was taken from the mechanism proposed by Konnov.³⁷

Discussion

Simulations were performed by using the SENKIN/CHEMKIN II software.²⁹ Figures 7–11 display a comparison between the experimental ignition-delay measurements and ignition-delay times computed by using the described mechanism, which globally contains 158 species and 1250 reactions; the complete mechanism is contained in the Supporting Information. The reflected shock environment was simulated by using a constantvolume adiabatic constraint, and the computed ignition times were defined as the time at which the OH concentration reached 10% of the maximum OH concentration occurring after ignition. The slight difference in experimental and computed ignitiontime definitions has a negligible influence on the results. The agreement between experiments and simulations is globally quite good, apart from disagreement for the more diluted mixtures at higher pressure (0.25% butanol, $\Phi = 1.0$, and pressures between 3.5 and 4.3 bar; simulations not presented here), for which ignition-delay times are underestimated by a up to a factor of 3 in the lower part of the studied temperature range. This disagreement is probably due to falloff effects which have been neglected in the mechanism.

The mechanism reproduces well the observed differences in reactivity for the four isomers under the different conditions studied as is illustrated in Figure 7 for the case of stoichiometric mixtures containing 1% butanol at pressures around 1.2 bar. The most reactive species is 1-butanol; the reactivity of isobutanol is just slightly lower. Longer ignition times were observed and predicted via simulation for 2-butanol and the least reactive isomer tert-butanol, for which the measured and simulated ignition times have a larger apparent activation energy compared to the three other isomers.

Figures 8a, 9a, 10a, and 11a exhibit that the experimentally observed increase in ignition-delay time as the equivalence ratio varies from 0.25 to 1.0 at pressures around 1.2 bar is mostly well represented by the mechanism. Figures 8b, 9b, 10b, and 11b illustrate that the experimentally observed acceleration in ignition with the increase in butanol concentration from 0.5 to 1.0% is captured by the simulations for the case of mixtures with an equivalence ratio of 0.5 at pressures around 1.2 bar. However, the influence of equivalence ratio and initial concentration on ignition times is stronger in the simulations than in experiments, especially in the case of linear butanols for mixtures with the highest butanol concentrations.

Figure 12 displays a reaction flux rate analysis performed at 1450 K, for an equivalence ratio of 1.0, at atmospheric pressure, for mixtures containing 1% butanol and for 50% conversion of butanol. Figures 13 and 14 present the temporal evolution of some major species and a sensitivity analysis, respectively, computed under the same conditions.

1-Butanol and iso-butanol are mainly consumed by H abstractions by H atoms and hydroxyl radicals yielding radicals, the decomposition of which leads to the formation of highly reactive radicals, such as the branching agents, H atoms and OH radicals. The difference in reactivity between 1-butanol and iso-butanol is due to the fact that 69% of the consumption of 1-butanol leads to H atoms, whereas this number is only 29% in the case of iso-butanol, with 27% of its consumption leading to the less reactive methyl radical. As shown in Figure 13a,c, the autoignition of 1-butanol and iso-butanol occurs not too far after the total consumption of the reactant. The primary products obtained from 1-butanol are butanal, acetaldehyde, and ethylene (not shown in the figure) and, to a lesser extent, propene and 1-butene. The consumption of iso-butanol leads to similar amounts of propenol, iso-butanal, and iso-butene.

The reaction pathways are very different for 2-butanol and tert-butanol which react primarily (almost 70% of their consumption) by dehydration to form alkenes which are consumed by additions of H atoms or by H abstractions, reactions with very small flux, to give very nonreactive resonance stabilized radicals. Iso-butene obtained from tert-butanol by dehydration, as well a by H abstraction followed by a β -scission decomposition, yields only the very stable iso-butyl radical by H abstraction, explaining the low reactivity of this branched alcohol. As shown in Figures 13b,d, the autoignition of 2-butanol and tert-butanol occurs long after the total consumption of the reactant, and the main primary products are alkenes, 1-butene and iso-butene, respectively. The autoignition occurs only when the alkenes are totally consumed. Oxygenated species, such as butanone for 2-butanol and propanone for tert-butanol are produced only in much smaller concentrations.

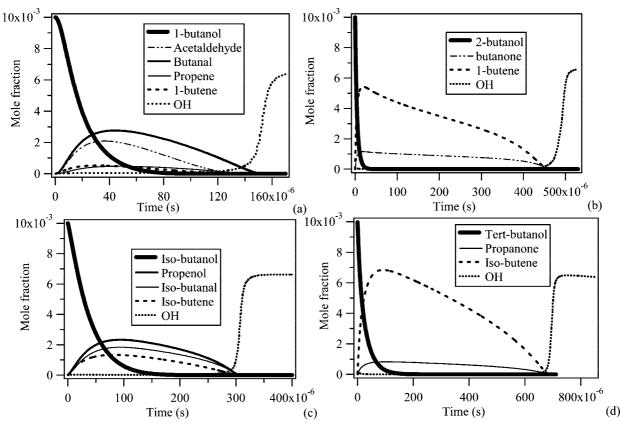


Figure 13. Time evolution of the mole fraction of the primary species formed during the oxidation of the four butanol isomers under the conditions of Figure 12.

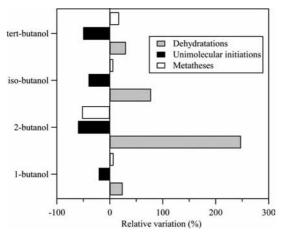


Figure 14. Sensitivity analysis for the main consumption reactions for the four butanol isomers under the conditions of Figure 12. Relative variations have been obtained by multiplying the rate constant of each generic reaction by a factor of 10.

The higher apparent activation energy (ignition-time slope) observed experimentally and predicted in the simulations for tert-butanol relative to the other isomers is due to the higher activation energies of all of the initiation reactions (dehydration, unimolecular decomposition, and H abstraction) for tert-butanol relative to the other isomers and the higher activation energies of the iso-butene consumption reactions relative to the consumption reactions for the primary products of the other butanol isomers (i.e., the relative stability of iso-butene compared to the other primary products).

The sensitivity analysis in Figure 14 shows that dehydration reactions for butanol have a large impact on the ignition delay times; the inhibiting effect of dehydration is particularly

important in the case of 2-butanol. Although the amount of butanol consumed through unimolecular initiations is relatively small (less than 10% of the butanol consumption for all of the isomers, as shown in Figure 12), these reactions, which are a source of radicals, have a promoting effect, especially in the case of the less reactive species (2-butanol and tert-butanol). Metatheses reactions, which consume reactive species such H atoms and OH radicals, have a slight inhibiting effect, apart from the case of 2-butanol for which metatheses have a promoting effect, because they are the main channels competing with dehydration.

Conclusions

Ignition-delay time measurements have been made, and a kinetic oxidation mechanism has been developed for the four butanol isomers: 1-butanol, 2-butanol, iso-butanol, and tertbutanol. The measurements and kinetic mechanism are the first of their kind for 2-butanol, iso-butanol, and tert-butanol. The mechanism predictions provide good agreement for the experimentally observed differences in reactivity of the four butanol isomers. Reaction flux and sensitivity analysis illustrates the relative importance of the three classes of butanol consumption reactions: dehydration, unimolecular decomposition, and H-atom abstraction. Uncertainties remain for the rate constants of dehydration reactions, which have the major influence on the reactivity. The less reactive butanols, tert-butanol and 2-butanol, are those for which the formation of alkenes through dehydration reaction is preponderant. Additional data in shock tubes at higher pressures would be of interest to give more information on falloff effects, as well as experiments in another type of apparatus involving analyses of the obtained products.

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Supporting Information Available: Experimental data in tabular form and kinetic mechanism in CHEMKIN format. This material is available free of charge via the Internet at http://pubs.acs.org.

References and Notes

- Ezeji, T. C.; Qureshi, N.; Blaschek, H. P. Curr. Opin. Biotechnol. 2007, 18, 220–227.
 - (2) Dürre, P. Biotechnol. J. 2007, 2, 771-780.
 - (3) Atsumi, S.; Hanai, T.; Laio, J. C. Nature 2008, 451, 86-89.
- (4) Lin, Y. L.; Blaschek, H. P. Appl. Environ. Microbiol. 1983, 45, 966-973.
- (5) Ezeji, T.; Qureshi, N.; Blaschek, H. P. Biotechnol. Bioeng. 2007, 97, 1460–1469.
- (6) Reardon, M. DuPont and BP Disclose Advanced Biofuels Partnership Targeting Multiple Butanol Molecules available at http://www.reuters. com/article/pressRelease/idUS177211+14-Feb-2008+PRN20080214; PRNewswire, 2/14/2008.
 - (7) ButylFuel LLC, www.butanol.com.
- (8) Rice, R. W.; Sanyal, A. K.; Elrod, A. C.; Bata, R. M. J. Eng. Gas Turbines Power 1991, 113, 377–381.
- (9) Yacoub, Y.; Bata, R.; Gautam, M. *Proc. I MECH E Part A: J. Power Energy* **1998**, *212*, 363–379.
 - (10) Hamins, A.; Seshadri, K. Combust. Flame 1986, 64, 43-54.
- (11) McEnally, C. S.; Pfefferle, L. D. Proc. Combust. Inst. 2005, 30, 1363–1370.
- (12) Yang, B.; Osswald, P.; Li, Y.; Wang, J.; Wei, L.; Tian, Z.; Qi, F.; Kohse-Höinghaus, K. Combust. Flame 2007, 148, 198–209.
- (13) Zhukov, V.; Simmie, J.; Curran, H.; Black, G.; Pichon, S. 21 st International Colloquium on the Dynamics of Explosions and Reactive Systems, Poitiers, France, 2007.
 - (14) Dagaut P.; Togbé, C. Fuel 2008, 87, 3313-3321.
- (15) Pepiot-Desjardins, P.; Pitsch, H.; Malhotra, R.; Kirby, S. R.; Boehman, A. L. Combust. Flame 2008, 154, 191–205.
- (16) Burcat A.;Ruscic, B. Ideal gas thermochemical database with updates from active thermochemical tables. available at http://garfield.chem.elte.hu/burcat/burcat.html.

- (17) Horning, D. C.; Davidson, D. F.; Hanson, R. K. J. Prop. Power **2002**, 18, 363–371.
- (18) Shin, K. S.; Bae, G. T.; Yoo, S. J. J. Korean Chem. Soc. 2004, 48, 99–102.
- (19) Warth, V.; Stef, N.; Glaude, P. A.; Battin-Leclerc, F.; Scacchi, G.; Côme, G. M. *Combust. Flame* **1998**, *114*, 81–102.
- (20) Buda, F.; Bounaceur, R.; Warth, V.; Glaude, P. A.; Fournet, R.; Battin-Leclerc, F. Combust. Flame 2005, 142, 170–186.
- (21) Biet, J.; Hakka, M. H.; Warth, V.; Glaude, P. A.; Battin-Leclerc, F. *Energy Fuels* **2008**, 22, 2258–2269.
- (22) Glaude, P. A.; Battin-Leclerc, F.; Judenherc, B.; Warth, V.; Fournet, R.; Côme, G. M.; Scacchi, G. Combust. Flame 2000, 121, 345–355.
- (23) Barbé, P.; Battin-Leclerc, F.; Côme, G. M. J. Chim. Phys. 1995, 92, 1666–1692.
- (24) Fournet, R.; Baugé, J. C; Battin-Leclerc, F. Int. J. Chem. Kin 1999, 31, 361–379.
- (25) Gueniche, H. A.; Glaude, P. A.; Fournet, R.; Battin-Leclerc, F. *Combust. Flame* **2008**, *152*, 245–261.
 - (26) Troe, J. Ber. Buns. Phys. Chem. 1974, 78, 478.
- (27) Muller, C.; Michel, V.; Scacchi, G.; Côme, G. M. J. Chim. Phys. 1995, 92, 1154–1178.
- (28) Benson, S. W. *Thermochemical Kinetics*, 2nd ed.; John Wiley: New York, 1976.
- (29) Kee, R. J.; Rupley, F. M.; Miller, J. A. Sandia Laboratories Report, SAND 89–8009B 1989.
 - (30) Tsang, W. Int. J. Chem. Kinet. 2004, 36, 456-465.
- (31) Bui, B. H.; Zhu, R. S.; Lin, M. C. J. Chem. Phys. 2002, 117, 11188–11195.
- (32) Newman, C. G.; O'Neal, H. E.; Ring, M. A.; Leska, F.; Shipley, N. Int. J. Chem. Kinet. 1979, 11, 1167–1182.
- (33) Ingham, T.; Walker, R. W.; Woolford, R. E. *Proc. Combust. Inst.* **1994**, 25, 767–774.
- (34) Touchard, S.; Fournet, R.; Glaude, P. A.; Warth, V.; Battin-Leclerc, F.; Vanhove, G.; Ribaucour, M.; Minetti, R. *Proc. Combust. Inst.* **2005**, *30*, 1073–1081.
- (35) Dean, A. M.; Bozzelli, J. W *Combustion Chemistry of Nitrogen, in Gas-phase Combustion Chemistry*; Gardiner, W. C., Ed.; Springer-Verlag: New York, 2000.
- (36) Luo, Y.-R. Comprehensive Handbook of Chemical Bond Energies, 1st ed; CRC Press; Boca Raton, FL; p 1688.
 - (37) Konnov, A. A. Proc. Combust. Inst. 2000, 28, 317.

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