

# The Structure of the Seven Layer Barium Niobium Silicon Oxide, $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ ( $x \approx 0.2$ )

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One of the products of reaction between  $\text{Nb}_2\text{O}_5$ , Nb, and BaO in a 1.6:1:2.4 mole ratio at 1250°C in an evacuated silica capsule is the complex oxide  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ . The compound has an hexagonal unit cell of dimensions  $a = 7.774 \pm 0.004 \text{ \AA}$ ,  $c = 16.765 \pm 0.007 \text{ \AA}$ , probable space group  $P\bar{3}$ ,  $Z = 1$ . Its structure has been determined from 4484 independent reflections measured by counter methods. Refinement by Fourier and least-squares methods was carried out to a weighted  $R$  value of 9.8% (conventional  $R = 12.4\%$ ).

The structure consists of a close-stacking of seven close-packed layers in the sequence  $\text{BaO}_6$ ,  $\text{O}_6$  (oxygen layer with 1/7 of the oxygen missing),  $\text{O}_7$ ,  $\text{BaO}_6$ ,  $\text{BaO}_6$ ,  $\text{O}_7$ ,  $\text{O}_6$ . Between two  $\text{BaO}_6$  layers there is one Nb in an octahedral site (population parameter  $\approx 0.8$ ); between  $\text{BaO}_6$  and  $\text{O}_7$  layers there are three Nb in octahedral sites; between  $\text{BaO}_6$  and  $\text{O}_6$  layers there are three Nb in sites coordinated by five O in a square pyramidal arrangement; and between  $\text{O}_6$  and  $\text{O}_7$  layers, there are three Nb in similar square pyramidal sites, one Nb in an octahedral site, and one Si in a tetrahedral site. The niobiums in square pyramidal sites form an octahedron about the oxygen vacancy of the  $\text{O}_6$  layer and engage in metal-metal bonding, the Nb-Nb distances ranging from 2.78 to 2.85 Å.

$\text{Nb}_6\text{O}_{18}$  clusters can be identified in which the  $\text{Nb}_6$  octahedron is surrounded by a cubooctahedron of oxygen atoms capped by oxygen atoms on the square faces. Alternatively, the oxygen array may be described as an octahedron of oxygens with oxygens also at the centers of the edges.

## Introduction

When  $\text{Nb}_2\text{O}_5$ , Nb, and BaO react in the presence of  $\text{SiO}_2$ , various complex oxides may be produced. The first such compound to be described was  $\text{Ba}_3\text{Nb}_6\text{Si}_4\text{O}_{26}$ , which Shannon determined to have a structure composed of strings of  $\text{NbO}_6$  octahedra joined by corner-sharing, both among each other and with  $\text{Si}_2\text{O}_7$  groups (two  $\text{SiO}_4$  tetrahedra sharing one vertex), with bariums occupying holes between the chains (1). The compound  $\text{Ba}_3\text{Nb}_7\text{Si}_2\text{O}_{25-x}$  ( $x \approx 0.5$ ) has a similar but somewhat more complex structure (2), in which some edge-sharing of  $\text{NbO}_6$  octahedra occurs. A third oxide,  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ , however, has an entirely different structure which will be described herein.

In it  $\text{Nb}_6\text{O}_{18}$  clusters can be identified. Professor Ward has always shown an interest in such clusters, so we are particularly pleased to be able to report on a compound which not only

represents a continuation of his work at the University of Connecticut, but which also has some features of special interest to him.

## Experimental

The reactants  $\text{Nb}_2\text{O}_5$  and Nb were obtained commercially. BaO was prepared by heating  $\text{BaO}_2$  in *vacuo* to 1000°C for one hour. These three reactants were mixed in a 1.6:1:2.4 mole ratio and triturated under petroleum ether. The resulting powder was placed in a silica capsule which was evacuated and sealed, the silica serving as both container and reactant. The sample was held at 1250°C for one week. Upon removal from the furnace, the capsule was in a partially collapsed state, and on cooling it became clouded and crazed on the inside.

When the capsule was opened, black, highly reflective crystals were observed, both loose and

embedded in the walls, many of the former aggregated into clusters that appeared to have been partially melted. The loose non-aggregated crystals occurred in two distinct habits: thick chunks only occasionally exhibiting flat faces, and very thin hexagonal plates, often broken but usually having at least one  $120^\circ$  angle visible. The chunks were eventually determined to be  $\text{Ba}_3\text{Nb}_7\text{Si}_2\text{O}_{25-x}$ . It is, however, the investigation of the thin plates that is of interest here.

A single crystal in the shape of a roughly triangular plate about 0.3 mm across and 0.05 mm thick was selected for study. X-ray precession photographs showed hexagonal (trigonal) symmetry, Laue group  $\bar{3}$ . There were no systematic absences, so the probable space group is either  $P\bar{3}$  or  $P\bar{3}1$ . Unit-cell dimensions of  $a = 7.78 \text{ \AA}$ ,  $c = 16.75 \text{ \AA}$  were determined from the photographs. Due to the extremely small quantity of sample, measurement of its density was not feasible.

Data for structure determination were collected on a Picker Nuclear computer-controlled single-crystal diffractometer, using  $\text{MoK}\alpha$  radiation and operating in the  $\theta-2\theta$  scan mode. The base scan width was  $3^\circ$  in  $2\theta$ ; a dispersion factor of 0.692 was used; background was counted for 20 seconds on each side of the peak; three standard reflections were measured every 40 reflections. Data were collected in the following range:  $h$  and  $k$ ,  $-3$  to  $10$ ;  $l$ ,  $-3$  to  $36$ ; and  $2\theta$ ,  $2^\circ$  to  $100^\circ$ . In all, 6260 intensities were measured. The standards showed considerable variation with time, which was later shown to be due to instrument instability. Partial correction for this variability was made by dividing the data into groups during whose collection the standards remained reasonably constant and applying scale factors to bring the standards of different groups into agreement. Twenty scale groups were used, containing from 80 to 920 reflections and with scale factors ranging from 0.928 to 1.071. After scaling, the three standards had standard deviations of 1.6%, 6.0%, and 3.6%. The data were corrected for background and absorption, and reflections related by the symmetry of the Laue group were averaged. The absorption correction was made using Prewitt's program ACACA (3), with a few modifications to compensate for errors presumably due to diffractometer alignment problems. Averaging reduced the data set to 4484 independent reflections.

Of these, 1148 had intensities less than twice the standard deviation of the background and

were labelled as unobserved. Upper bounds for these intensities were set equal to the observed intensities plus twice their standard deviation ( $I_0 + 2\sigma_{I_0}$ ). A standard deviation was calculated for each reflection according to the formula

$$\sigma_F = \frac{\sigma_g}{10\sqrt{Lp}} \left( \{N_T + BG + [0.02(N_T - BG)]^2\}/(N_T - BG) \right)^{1/2}$$

for observed reflections and

$$\sigma_F = \frac{\sigma_g}{10\sqrt{Lp}} (BG)^{1/2}$$

for unobserved reflections, where  $\sigma_g$  is the percentage standard deviation in a group of symmetry-related reflections (set to 10 for single reflections),  $Lp$  is the product of Lorentz and polarization factors,  $N_T$  is the total counts recorded on the scan through the peak, and  $BG$  is the background counts for the scan. These standard deviation are derived from counting statistics, the equation used being based on those given by Stout and Jensen (4).

Lorentz and polarization corrections were made using the program package "The X-ray System" (5), which was also used to calculate accurate cell dimensions of  $a = 7.774 \pm 0.004 \text{ \AA}$  and  $c = 16.765 \pm 0.007 \text{ \AA}$  from the 20 values of twelve individually centered reflections, and in all subsequent calculations of Fourier maps, least squares refinements, and so forth.

A rough determination of relative composition was made with a KEVEX-Quanta/Metric energy dispersive spectrometer, using  $\text{Ba}_3\text{Nb}_7\text{Si}_2\text{O}_{25-x}$  as the standard. This measurement indicated a Ba/Si ratio of about 3/2 and a Ba/N ratio of about 1/7. The statistical distribution of normalized structure factors indicated the presence of a center of symmetry, making the probable space group  $P\bar{3}$ .

### Structure Determination and Refinement

Examination of the  $hk0$  reflections revealed 140 and 630 to be very strong, suggesting that many of the heavy atoms lie on or near the intersections of the corresponding planes, i.e. a sites  $0, 0, z$ ;  $1/3, 2/3, z$ ;  $1/21, 5/21, z$ ;  $2/7, 3/7, z$ ;  $2/21, 10/21, z$  (and symmetry-related sites). Of these, only the first two are suitable for barium, since use of any of the other three would place symmetry-related bariums uncomfortably close together. All five sites are possible for

obium (and also for oxygen). A Patterson map was calculated and showed strong concentrations of peaks corresponding to the interatomic vectors among the above hypothesized locations.

One particularly large peak indicated the possible presence of a heavy atom at  $1/3, 2/3, 0.14$ . A difference Fourier map calculated from a model of just one barium at this location was used in conjunction with the Patterson to suggest niobium locations. Structure solution proceeded by trial and error, using  $\Delta F$  maps as the primary tool for revision of the model. In order to reduce calculation time, only observed reflections of

$\sin \theta \leq 0.5$  (1770 reflections) were used in this process. Although the initial barium had actually been wrongly placed, a reasonable model was eventually produced in this way, having parameters close to the final values shown in Table I. The ideal formula of the compound was determined from this model to be  $\text{Ba}_3\text{Nb}_{21}\text{Si}_2\text{O}_{44}$ . After refinement of isotropic thermal parameters, using a weighting function  $w = 1/\sigma_F^2$ , the weighted  $R$ -value was 0.115 and the conventional  $R$  was 0.119 for the restricted data set.

Anisotropic thermal parameters were introduced for barium and niobium and the full data

TABLE I  
ATOMIC PARAMETERS FOR  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$

Atom	Ba(1)	Ba(2)	Nb(1)	Nb(2)	Nb(3)	Nb(4)	Nb(5) <sup>a</sup>
Position	1a	2d	6g (general)	6g	6g	2c	1b
Initial coordinates	0, 0, 0	$\frac{1}{3}, \frac{2}{3}, \frac{2}{3}0$	$\frac{2}{21}, \frac{1}{21}, \frac{7}{100}$	$\frac{1}{7}, \frac{5}{7}, \frac{2}{100}$	$\frac{3}{7}, \frac{1}{7}, \frac{3}{100}$	$0, 0, \frac{2}{100}$	$0, 0, \frac{1}{2}$
Final							
<i>x</i>	0	$\frac{1}{3}$	0.1123(2)	0.1423(2)	0.3938(2)	0	0
<i>y</i>	0	$\frac{5}{3}$	0.4762(2)	0.6951(2)	0.1317(2)	0	0
<i>z</i>	0	0.4406(1)	0.0765(1)	0.2165(1)	0.3601(1)	0.2112(1)	$\frac{1}{2}$
$J_{11} \times 100$	1.582	2.623	0.801(52)	0.740(52)	1.757(68)	1.586	2.313
$J_{22} \times 100$	1.582	2.623	0.814(53)	0.851(53)	1.415(62)	1.586	2.313
$J_{33} \times 100$	0.738(52)	0.872(42)	0.248(28)	0.306(28)	0.383(30)	0.542(57)	1.197(145)
$J_{12} \times 100$	0.791(31)	1.311(29)	0.391(46)	0.461(45)	1.094(57)	0.793(35)	1.157(91)
$J_{13} \times 100$	0	0	0.042(35)	-0.100(34)	-0.185(39)	0	0
$J_{23} \times 100$	0	0	-0.045(35)	0.000(36)	-0.132(39)	0	0
Atom	Si(1)	O(1)	O(2)	O(3)	O(4)	O(5)	
Position	2d	6g	6g	6g	6g	6g	6g
Initial coordinates	$\frac{1}{3}, \frac{2}{3}, \frac{7}{100}$	$\frac{1}{7}, \frac{5}{7}, 0$	$\frac{1}{21}, \frac{5}{21}, \frac{7}{50}$	$\frac{1}{21}, \frac{8}{21}, \frac{7}{50}$	$\frac{5}{21}, \frac{4}{21}, \frac{14}{50}$	$\frac{2}{21}, \frac{1}{21}, \frac{14}{50}$	$\frac{2}{21}, \frac{1}{21}, \frac{14}{50}$
Final							
<i>x</i>	$\frac{1}{3}$	0.1265(14)	0.0715(14)	0.5202(14)	0.2358(16)	0.0992(15)	
<i>y</i>	$\frac{5}{3}$	0.7061(15)	0.2367(15)	0.4112(14)	0.1726(15)	0.4708(14)	
<i>z</i>	0.8199(3)	0.0080(5)	0.1453(5)	0.1487(5)	0.2784(5)	0.2915(5)	
$J \times 100$	0.727(107)	0.964(165)	0.918(162)	0.633(140)	0.996(162)	0.983(159)	
Atom	O(6)	O(7)	O(8)				
Position	6g	6g	2d				
Initial coordinates	$\frac{1}{21}, \frac{8}{21}, \frac{2}{50}$	$\frac{1}{21}, \frac{5}{21}, \frac{2}{50}$	$\frac{1}{3}, \frac{2}{3}, \frac{3}{50}$				
Final							
<i>x</i>	0.4975(18)	0.0274(16)	$\frac{1}{3}$				
<i>y</i>	0.3903(18)	0.2327(16)	$\frac{5}{3}$				
<i>z</i>	0.4107(7)	0.4298(5)	0.7247(8)				
$J \times 100$	2.159(237)	1.282(171)	0.697(258)				

<sup>a</sup> Population parameter 0.79(1).

Anisotropic thermal vibration expressed as:

$$\exp[-1/4(a^{*2}U_{11}h^2 + b^{*2}U_{22}k^2 + c^{*2}U_{33}l^2 + 2a^*b^*U_{12}hk + 2a^*c^*U_{13}hl + 2b^*c^*U_{23}kl)]$$

Errors in the last digit are given in parentheses; where no error is shown, the parameter is not independent.

Isotropic thermal motion expressed as:  $[\exp -8\pi^2 U \sin^2 \theta / \lambda^2]$

set was used for the final stages of refinement. Allowing population parameters to vary resulted in a significant change only for Nb(5), whose final refined occupancy factor is 0.79. The compound formula is thus  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$  ( $x \approx 0.2$ ). A correction for secondary extinction was made to the 118 reflections having intensities greater than 10,000 and  $\sin\theta/\lambda$  less than 0.40, using the empirical method described by Stout and Jensen (4). Anomalous dispersion was included in all structure factor calculations. Neutral atom scattering factors taken from the International Tables (6) were used throughout. The final weighted  $R$  was 0.098, the conventional  $R$  0.124. The maximum shift to error ratio in the final cycle of refinement was 0.084. A final  $\Delta F$  map showed no peak higher than one-third the height of the peak produced by deliberate omission of a single oxygen atom. Atomic parameters are listed in Table I.

## Discussion

The unit cell of  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$  is shown in stereo in Fig. 1. It may be conveniently described in terms of the layer structure diagrammed in Fig. 2. Considering each layer simply as a close-packing of equal spheres, the stacking sequence is *ABCBCBC*. The compositions of the seven layers are:  $\text{BaO}_6$ ,  $\text{O}_6$  (an oxygen layer with one-seventh of the oxygens missing),  $\text{O}_7$  (a complete oxygen layer),  $\text{BaO}_6$ ,  $\text{BaO}_6$ ,  $\text{O}_7$ ,  $\text{O}_6$ , respectively.

The  $\text{BaO}_6$  layer found here has not, to our knowledge, been reported previously. It is, however, analogous to the  $\text{KF}_6$  layer found in  $\text{KO}_\text{F}_6$  and similar compounds.  $\text{KO}_\text{F}_6$  has a structure based on a cubic stacking of approximately close-packed  $\text{KF}_6$  layers, with one Os occupying the only available octahedral site between each pair of layers (7). Between the two

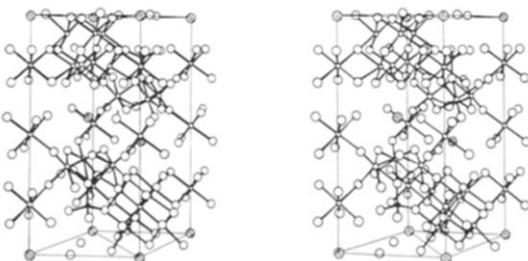


FIG. 1. Stereo view of the unit cell of  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ . Shaded circles are Ba, large open circles O, small open circles Nb, and small closed circles Si.

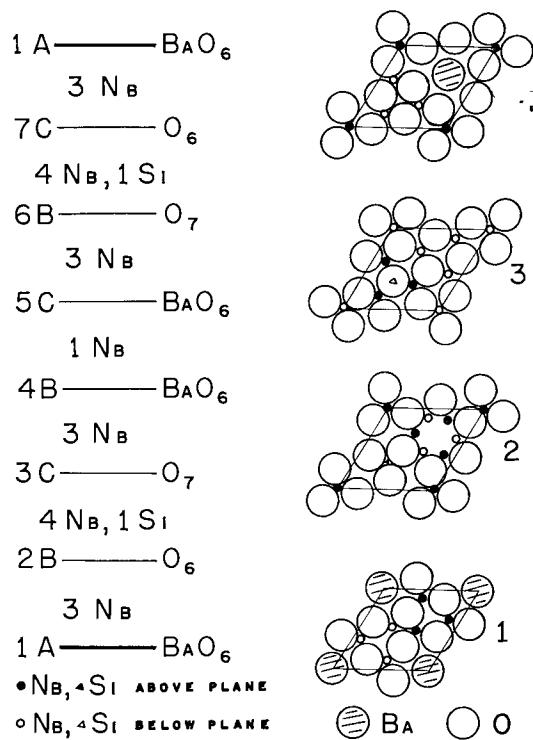


FIG. 2. Layer structure of  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ .

adjacent  $\text{BaO}_6$  layers in  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$  there is, similarly, a single niobium (Nb(5)) in the only available octahedral site, although here its population parameter is somewhat less than one.

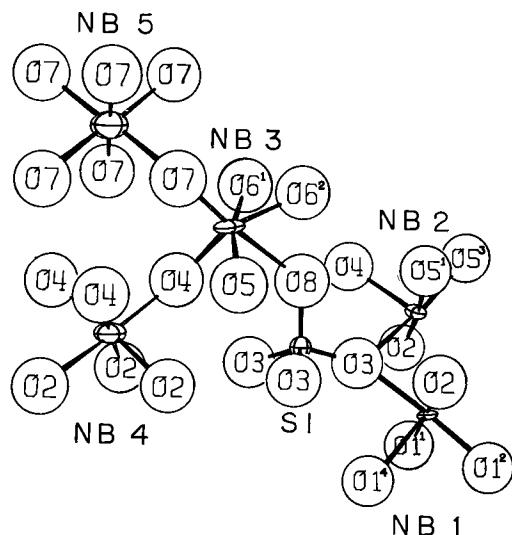
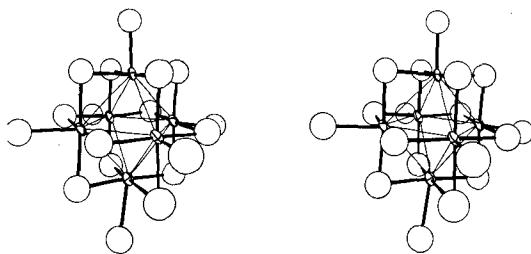


FIG. 3. Niobium and silicon coordination in  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ . See Table II for explanation of superscripts.

FIG. 4. Stereo view of  $\text{Nb}_6\text{O}_{18}$  cluster.

Between  $\text{BaO}_6$  and  $\text{O}_7$  layers there are three niobiums in octahedral sites; between  $\text{BaO}_6$  and  $\text{O}_6$  layers there are three niobiums in sites coordinated by square pyramids of oxygens with the niobiums in the pyramid bases; and between  $\text{O}_6$  and  $\text{O}_7$  layers there are three niobiums in square pyramidal sites, one niobium in a normal octahedral site, and one silicon in a tetrahedral site. The coordination of the various niobiums and of the silicon is shown in Fig. 3.

The square pyramidal sites mentioned above would be octahedral except for the oxygen vacancy in the  $\text{O}_6$  layer. The absence of an oxygen at the site is established by the lack of any peak on the final  $\Delta F$  map and by the fact that, when an oxygen atom was introduced there, upon refinement it quickly acquired a thermal parameter so large ( $U \approx 55$ ) as to indicate that the atom was not there at all. The six niobiums in square pyramidal sites surround the vacancy in an octahedral arrangement, as shown in Fig. 4. The Nb-O distances, as shown in Table II,

TABLE II—continued

Distances:	
$\text{Nb}(2)-\text{O}(3)$	$2.154 \pm 0.006$
$\text{Nb}(2)-\text{O}(4)$	$2.185 \pm 0.009$
$\text{Nb}(2)-\text{O}(5)^1$	$2.037 \pm 0.011$
$\text{Nb}(2)-\text{O}(5)^3$	$2.114 \pm 0.006$
$\text{Nb}(3)-\text{O}(4)$	$1.969 \pm 0.012$
$\text{Nb}(3)-\text{O}(5)$	$2.065 \pm 0.011$
$\text{Nb}(3)-\text{O}(6)^1$	$1.947 \pm 0.013$
$\text{Nb}(3)-\text{O}(6)^2$	$1.973 \pm 0.014$
$\text{Nb}(3)-\text{O}(7)$	$1.797 \pm 0.007$
$\text{Nb}(3)-\text{O}(8)$	$2.378 \pm 0.008$
$\text{Nb}(4)-\text{O}(2)$	$1.973 \pm 0.011$
$\text{Nb}(4)-\text{O}(4)$	$1.992 \pm 0.011$
$\text{Nb}(5)-\text{O}(7)$	$2.078 \pm 0.012$
$\text{Si}(1)-\text{O}(3)$	$1.622 \pm 0.013$
$\text{Si}(1)-\text{O}(8)$	$1.595 \pm 0.015$
Angles:	
$\text{O}(1)^1-\text{Nb}(1)-\text{O}(1)^4$	$97.3 \pm 0.4$
$\text{O}(1)^1-\text{Nb}(1)-\text{O}(1)^4$	$82.1 \pm 0.4$
$\text{O}(1)^2-\text{Nb}(1)-\text{O}(1)^4$	$87.2 \pm 0.4$
$\text{O}(1)^2-\text{Nb}(1)-\text{O}(2)^1$	$86.2 \pm 0.4$
$\text{O}(1)^4-\text{Nb}(1)-\text{O}(2)^1$	$94.5 \pm 0.4$
$\text{O}(1)^1-\text{Nb}(1)-\text{O}(3)^3$	$90.0 \pm 0.4$
$\text{O}(1)^4-\text{Nb}(1)-\text{O}(3)^3$	$87.0 \pm 0.4$
$\text{O}(2)-\text{Nb}(1)-\text{O}(3)$	$86.2 \pm 0.4$
$\text{O}(2)-\text{Nb}(2)-\text{O}(3)$	$91.3 \pm 0.3$
$\text{O}(2)-\text{Nb}(2)-\text{O}(4)$	$79.3 \pm 0.3$
$\text{O}(2)-\text{Nb}(2)-\text{O}(5)$	$90.5 \pm 0.3$
$\text{O}(3)-\text{Nb}(2)-\text{O}(4)$	$87.2 \pm 0.3$
$\text{O}(3)-\text{Nb}(2)-\text{O}(5)$	$87.9 \pm 0.4$
$\text{O}(4)^3-\text{Nb}(2)-\text{O}(5)^1$	$95.2 \pm 0.4$
$\text{O}(4)^3-\text{Nb}(2)-\text{O}(5)^3$	$88.6 \pm 0.3$
$\text{O}(4)-\text{Nb}(3)-\text{O}(5)$	$88.0 \pm 0.4$
$\text{O}(4)-\text{Nb}(3)-\text{O}(6)$	$96.1 \pm 0.6$
$\text{O}(4)-\text{Nb}(3)-\text{O}(7)$	$101.8 \pm 0.4$
$\text{O}(4)-\text{Nb}(3)-\text{O}(8)$	$84.3 \pm 0.4$
$\text{O}(5)-\text{Nb}(3)-\text{O}(6)$	$82.0 \pm 0.3$
$\text{O}(5)-\text{Nb}(3)-\text{O}(7)$	$94.5 \pm 0.4$
$\text{O}(5)-\text{Nb}(3)-\text{O}(8)$	$84.2 \pm 0.2$
$\text{O}(6)-\text{Nb}(3)-\text{O}(6)$	$88.8 \pm 0.5$
$\text{O}(6)^1-\text{Nb}(3)-\text{O}(7)^3$	$101.6 \pm 0.5$
$\text{O}(6)^2-\text{Nb}(3)-\text{O}(7)^3$	$95.4 \pm 0.4$
$\text{O}(6)-\text{Nb}(3)-\text{O}(8)$	$78.7 \pm 0.4$
$\text{O}(2)-\text{Nb}(4)-\text{O}(2)$	$91.7 \pm 0.5$
$\text{O}(2)^1-\text{Nb}(4)-\text{O}(4)^1$	$87.3 \pm 0.4$
$\text{O}(2)^1-\text{Nb}(4)-\text{O}(4)^2$	$89.8 \pm 0.4$
$\text{O}(4)-\text{Nb}(4)-\text{O}(4)$	$91.2 \pm 0.4$
$\text{O}(7)-\text{Nb}(5)-\text{O}(7)$ (O's in same layer)	$91.1 \pm 0.5^\circ$
$\text{O}(7)-\text{Nb}(5)-\text{O}(7)$ (O's in different layers)	$88.9 \pm 0.5$
$\text{O}(3)-\text{Si}(1)-\text{O}(3)$	$110.0 \pm 0.5$
$\text{O}(3)-\text{Si}(1)-\text{O}(8)$	$109.0 \pm 0.4$

Where necessary, symmetry-related atoms are distinguished by superscripts referring to the list of general position coordinates for space group  $P\bar{3}$  (No. 147) in the International Table (II).

TABLE II

INTERATOMIC DISTANCES AND ANGLES IN  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_x\text{O}_{44}$ 

Distances:	
$\text{Ba}(1)-\text{O}(1)$	$2.907 \pm 0.014 \text{ \AA}$
$\text{Ba}(1)-\text{O}(2)$	$2.933 \pm 0.009$
$\text{Ba}(2)-\text{O}(5)$	$3.018 \pm 0.008$
$\text{Ba}(2)-\text{O}(6)$ (same layer)	$3.039 \pm 0.017$
$\text{Ba}(2)-\text{O}(6)$ (different layers)	$2.953 \pm 0.013$
$\text{Ba}(2)-\text{O}(7)$	$3.008 \pm 0.012$
$\text{Nb}(1)-\text{Nb}(1)$	$2.793 \pm 0.002$
$\text{Nb}(1)-\text{Nb}(2)^1$	$2.840 \pm 0.002$
$\text{Nb}(1)-\text{Nb}(2)^2$	$2.854 \pm 0.002$
$\text{Nb}(1)-\text{O}(1)^1$	$2.080 \pm 0.012$
$\text{Nb}(1)-\text{O}(1)^2$	$2.028 \pm 0.011$
$\text{Nb}(1)-\text{O}(1)^4$	$2.197 \pm 0.008$
$\text{Nb}(1)-\text{O}(2)$	$2.076 \pm 0.011$
$\text{Nb}(1)-\text{O}(3)$	$2.115 \pm 0.007$
$\text{Nb}(2)-\text{Nb}(2)$	$2.783 \pm 0.002$
$\text{Nb}(2)-\text{O}(2)$	$2.104 \pm 0.010$

TABLE III  
ELECTROSTATIC BOND STRENGTHS TO OXYGEN IN  
 $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$

Assuming all niobium to be in average oxidation state (+3.56):

O(1): 1 Ba at 1/6 + 3 Nb at 0.71	= 2.30
O(2): 1 Ba at 1/6 + 2 Nb at 0.71 + 1 Nb at 0.59	= 2.18
O(3): 1 Si at 1 + 2 Nb at 0.71	= 2.42
O(4): 1 Nb at 0.71 + 2 Nb at 0.59	= 1.89
O(5): 1 Ba at 1/6 + 2 Nb at 0.71 + 1 Nb at 0.59	= 2.18
O(6): 2 Ba at 1/6 + 2 Nb at 0.59	= 1.51
O(7): 1 Ba at 1/6 + 1.8 Nb at 0.59	= 1.23
O(8): 1 Si at 1 + 3 Nb at 0.59	= 2.77

Assuming Nb(1) and Nb(2) to be in +2.5 oxidation state and  
Nb(3), Nb(4), and Nb(5) to be  $\text{Nb}^{\text{v}}$ :

O(1): 1 Ba at 1/6 + 3 Nb at 1/2	= 1.67
O(2): 1 Ba at 1/6 + 2 Nb at 1/2 + 1 Nb at 5/6	= 2.00
O(3): 1 Si at 1 + 2 Nb at 1/2	= 2.00
O(4): 1 Nb at 1/2 + 2 Nb at 5/6	= 2.17
O(5): 1 Ba at 1/6 + 2 Nb at 1/2 + 1 Nb at 5/6	= 2.00
O(6): 2 Ba at 1/6 + 2 Nb at 5/6	= 2.00
O(7): 1 Ba at 1/6 + 1.8 Nb at 5/6	= 1.67
O(8): 1 Si at 1 + 3 Nb at 5/6	= 3.50

range from 2.03 Å to 2.20 Å, well within the normal range for niobium oxides, but the Nb–Nb distances, averaging 2.81 Å, are extremely short.

In the ion  $\text{Nb}_6\text{O}_{19}^{8-}$ , for instance, the arrangement of niobium and oxygen is the same as in the present  $\text{Nb}_6\text{O}_{18}$  grouping except that an additional oxygen is present in the center of the group. The shortest Nb–Nb distance there, however, is about 3.2 Å (8). In that case, niobium is present as  $\text{Nb}^{\text{v}}$ . In  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$ , however, the average niobium oxidation state is +3.56, assuming  $x = 0.21$ . Moreover, Nb(3), Nb(4), and Nb(5) are found in the centers of simple  $\text{NbO}_6$  octahedra joined by corner- and edge-sharing and probably have oxidation numbers not much below +5. Hence Nb(1) and Nb(2), which make up the octahedral cluster, probably have oxidation states in the neighborhood of +2.5.

Thus a more appropriate analogy than the  $\text{Nb}_6\text{O}_{19}^{8-}$  group is found in the  $\text{Nb}_6\text{Cl}_{12}^{2+}$  ion, which consists of an octahedron of niobiums with chlorines placed some distance out from the midpoints of the edges. The niobium oxidation state is +2½, the average Nb–Nb distance 2.9 Å, and the shortest distance 2.85 Å, quite comparable to the values in  $\text{Ba}_3\text{Nb}_{21-x}\text{Si}_2\text{O}_{44}$  (9). An even more similar Nb–Nb distance is found

in  $\text{NbO}_2$ , in which edge-sharing  $\text{NbO}_6$  octahedra in a rutile-type chain are distorted so as to bring pairs of niobiums into metal–metal bonding range. The Nb–Nb distances along the chain are alternately 2.80 Å and 3.20 Å (10). The bonding distance of 2.80 Å is virtually identical to the 2.81 Å Nb–Nb distance found in the present compound.

Nb(1) and Nb(2), then, form an octahedral cluster of niobiums held together by metal–metal bonding, each niobium being coordinated to four others. The coordination sphere of each niobium consists of five oxygens in a square pyramidal arrangement, with the niobium in the base of the pyramid.  $\text{Nb}_6\text{O}_{18}$  clusters can be identified in which the  $\text{Nb}_6$  octahedron is surrounded by a cuboctahedron of oxygen atoms capped by oxygen atoms on the square faces. Alternatively, the oxygen array may be described as an octahedron with oxygens also at the centers of the edges. The remaining niobiums in the structure are in octahedral sites, having Nb–O distances of 1.95 to 2.08 Å, with the exception of the Nb(3)–O(8) distance of 2.38 Å. The extreme length of this bond relative to the normal Nb–O distance is due to the very poor local charge balance around O(8) shown in Table III. Electrostatic bond strengths are given first

TABLE IV

OBSERVED AND CALCULATED STRUCTURE FACTORS. COLUMNS ARE  $I$ ,  $10|F_0|$ ,  $10|F_c|$ . UNOBSERVED REFLECTIONS ARE MARKED WITH ASTERISKS.

TABLE IV—continued

3+-4-L	7 262 -196	3 56-L	2 372 +80	28 1762 -177	13 1819 -1113	3 136+ -27	31 267 -266	22 276+ -107	12 424 -249	1 386 -406	2 361
9 273 -226	0 351 387	6 364 364	4 412 27	28 228 -200	16 389 486	4 228 -304	22 313 293	24 299 187	14 269 187	2 1560 -1465	3 181
10 263 254	1 187 187	5 200 200	4 412 27	28 228 -200	16 389 486	4 228 -304	22 313 293	24 299 187	14 271 286	3 166+ -75	6 761
11 254 237	1 187 187	5 200 200	4 228 -304	28 228 -200	17 390 -65	3 279 331	7+2-L	25 256+ -63	14 351 384	4 385 -54	6 214
12 184+ -97	3 228+ -106	6 189+ 76	5 30 306 -66	18 265+ -157	9 1920 1927	1 1349 19	28 264+ -197	20 264+ -80	6 385 511	7 621	6 27
13 180+ -97	3 228+ -106	6 189+ 76	5 30 306 -66	18 265+ -157	9 1920 1927	1 1349 19	28 264+ -197	20 264+ -80	6 385 511	7 621	6 27
14 220+ -214	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100	10 361
15 200+ 71	15 645 365	3 234+ 409	10 356 570	33 297 240	21 244 249	11 1263 1084	3 230 212	20 289 176	10 2029 -100	10 1800 1642	10 361
16 233+ 168	7 337+ 321	11 676 676	12 264+ 100	28 234 250	13 264+ 250	12 333 -341	9 421 606	7+2-L	2 216+ -12	12 528 -482	12 201
17 226+ -30	9 1100 1048	13 164+ 93	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
18 246+ -30	9 1100 1048	13 164+ 93	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
19 216 164	10 94+ 954	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
20 142+ 162	11 111 111	17 385+ 712	1 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
21 212+ -165	12 313+ -166	16 201+ -57	2 915 833	28 228 -200	17 264+ -152	12 263+ -574	5 363 308	6 259+ -34	14 351 384	4 385 -54	6 214
22 294 249	13 323+ -153	17 211+ 269	4 162+ 403	28 228 -200	17 264+ -152	12 263+ -574	5 363 308	6 259+ -34	14 351 384	4 385 -54	6 214
23 184+ -97	3 228+ -106	6 189+ 76	5 30 306 -66	18 265+ -157	9 1920 1927	1 1349 19	28 264+ -197	20 264+ -80	6 385 511	7 621	6 27
24 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
25 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
26 200+ 71	15 645 365	3 234+ 409	10 356 570	33 297 240	21 244 249	11 1263 1084	3 230 212	20 289 176	10 2029 -100	10 1800 1642	10 361
27 226+ -30	15 645 365	3 234+ 409	10 356 570	33 297 240	21 244 249	11 1263 1084	3 230 212	20 289 176	10 2029 -100	10 1800 1642	10 361
28 246+ -30	9 1100 1048	13 164+ 93	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
29 216 164	10 94+ 954	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
30 214+ -97	21 212+ -165	16 201+ -57	2 915 833	28 228 -200	17 264+ -152	12 263+ -574	5 363 308	6 259+ -34	14 351 384	4 385 -54	6 214
31 705+ -730	21 212+ -165	16 201+ -57	2 915 833	28 228 -200	17 264+ -152	12 263+ -574	5 363 308	6 259+ -34	14 351 384	4 385 -54	6 214
32 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
33 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
34 200+ 71	15 645 365	3 234+ 409	10 356 570	33 297 240	21 244 249	11 1263 1084	3 230 212	20 289 176	10 2029 -100	10 1800 1642	10 361
35 216+ -30	9 1100 1048	13 164+ 93	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
36 233+ 168	7 337+ 321	11 676 676	12 264+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
37 226+ -30	9 1100 1048	13 164+ 93	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
38 216 164	10 94+ 954	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
39 215+ -97	21 212+ -165	16 201+ -57	2 915 833	28 228 -200	17 264+ -152	12 263+ -574	5 363 308	6 259+ -34	14 351 384	4 385 -54	6 214
40 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
41 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
42 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
43 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
44 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
45 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
46 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
47 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
48 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
49 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
50 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
51 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
52 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
53 183+ 214	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
54 223 422	23 184+ -97	4 200+ 213	5 197+ 107	3 231+ -55	28 231 -228	20 266 712	10 1268 1302	3 230 212	20 289 176	10 1268 1302	4 1000 -100
55 1+-4-L	7 262 -196	3 226+ 100	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
56 226+ -30	9 1100 1048	13 164+ 93	2 164+ 100	6+0-L	23 334 -518	13 264+ 250	9 213 -165	7+2-L	2 216+ -12	12 528 -482	12 201
57 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
58 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
59 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
60 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
61 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
62 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
63 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
64 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
65 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
66 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
67 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
68 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
69 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
70 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
71 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
72 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200	5 243+ -200
73 216+ -97	10 263 254	16 385+ 712	0 187+ 216	28 228 -200	15 363 496	4 365 262	5 243+ -200	5 243+ -200	5 243+ -2		

## BARIUM NIOBIUM SILICON OXIDE

TABLE IV—continued

	8+L	20	266*	274	9+2-L	27	237*	17	9+4-L	10	346	290	11	205	298	10+1-L	6	195*	-12	10	317	205	12+5-L	14+7-L								
7	278	-195	22	294	121	1	151*	-72	28	379	238	0	657	481	12	301	-246	9	350	313	11+10-L	1	234*	-157	1	244*	108					
8	266*	-195	22	294	121	1	151*	-72	28	379	238	1	185*	-25	13	555	-567	1	284	872	10	711	573	12+2-L	1	228*	103	2	242*	40		
9	290*	156	24	457	429	3	992	-862	2	191*	122	14	312*	169	15	266*	166	2	261	-202	1	369	-307	3	1063	943						
0	260*	56	25	271	55	3	332	278	0	413	380	3	599	576	19	350*	371	6	405	546	4	355	228	13	235*	38						
1	330	121	21	281	109	5	324	1305	1	301	280	10	241	202	17	273	360	12	211	212	3	189*	-130	12+4-L	14+6-L							
2	27	253*	109	6	324	213	2	413	-79	5	235	71	17	274*	46	18	276	-245	6	121	1098	15	218	-60	14+6-L							
3	280*	20	226*	-21	7	236	215	3	314	-355	6	203*	-86	18	260	-7	15	639	624	7	404	298	16	260*	-210							
4	9+9-L	29	369	339	9	154	139	5	883	61	9	175	-77	20	251	-10	21	248*	18	1	297*	182	1	173	-104	2	437*	290				
5	2	160*	-63	30	228*	-65	10	154	124	10	154	81	10	219	-136	21	252	118	11	355*	-279	19	624	586	2	414	367					
6	459	644	11	162*	-557	6	151	154	10	219	-136	21	252	118	22	269	-114	11	355*	-279	19	624	586	2	414	367						
7	607	-607	9+6-L	12	489	-453	7	326	-354	11	194	192	20	295	-312	23	460	-427	12	220	-239	20	532*	-59	3	672	834					
8	511	512	13	271	232	13	1245	1109	13	267	90	24	238	134	25	301	359	14	274*	292	22	268	100	11+8-L	1	209*	-76	1	213*	43		
9	633	1	445	406	13	271	232	13	1245	1109	13	267	90	24	238	134	25	301	359	14	274*	292	22	268	100	11+8-L	1	209*	-76	1	213*	43
10	436	-517	2	172	-149	15	217*	26	11	230	-181	14	583	496	25	230*	88	17	276	-142	15	109%	920	23	314	201	1	209*	79	3	266*	42
11	187*	-136	4	460	487	17	727	-718	19	204*	58	16	316	197	27	249	197	28	219	-254	17	314	300	10+3-L	2	376	402	14+6-L				
12	249*	116	5	533	538	18	450	304	19	348	364	17	369	285	10	9+9-L	18	220	220	14	348*	-358	12+4-L	14+6-L								
13	505	557	6	539	562	19	279	-104	16	428	-815	19	272	47	1	465	421	21	287	-102	1	1310	-1202	21	287	145	2	360	-326			
14	250*	133	7	679	-704	20	278*	-104	16	428	-815	19	272	47	2	172*	-117	21	287	-102	1	1313	-292	3	189*	-9	3	1027	694			
15	253*	49	7	679	-704	20	278*	-104	16	428	-815	19	272	47	2	172*	-117	21	287	-102	1	1313	-292	3	189*	-9	3	1027	694			
16	245	-153	21	461	449	17	352	-270	20	272	-52	2	172*	-117	1	1310	-1202	21	287	-145	2	245*	121	2	360	-326						
17	505	613	8	640	668	23	252*	57	18	276	81	21	312	-148	3	265*	77	2	458	-427	22	746	-701	3	303*	-67	3	200*	119			
18	249*	133	10	640	668	23	252*	57	18	276	81	21	312	-148	3	265*	77	2	458	-427	22	746	-701	3	303*	-67	3	200*	119			
19	273*	-24	11	338	371	24	460	654	20	223	111	5	709	701	10+9-L	9	525	617	6	255*	-285	10+1-L	14+6-L									
20	489	413	12	159	35	25	402	-340	21	305	4	9+5-L	6	581	607	10+5-L	7	525	617	6	242*	-171	11+7-L	1	357	320	1	489	-381			
21	505	557	13	271	232	13	252	-124	23	253	37	0	389	275	1	200*	3	9	290	55	1	231	121	2	360	-326						
22	547	-201	14	197	167	25	212	-124	23	253	37	0	389	275	1	200*	3	9	290	55	1	231	121	2	360	-326						
23	284	254	15	277	148	27	227*	74	25	559	473	1	200	133	9	420	511	0	151	-3	10	340	211	1	453	472						
24	273*	-319	16	278	215	29	236*	-215	26	254	-148	14	200*	133	9	420	511	0	151	-3	10	340	211	1	453	472						
25	249*	-225	17	278	215	30	236*	-215	26	254	-148	14	200*	133	9	420	511	0	151	-3	10	340	211	1	453	472						
26	250*	35	16	269	306	27	226*	54	2	405	340	20	320	58	1	200*	133	9	420	511	0	151	-3	10	340	211	1	453	472			
27	322*	-25	17	278	215	30	236*	-215	26	254	-148	14	200*	133	9	420	511	0	151	-3	10	340	211	1	453	472						
28	271*	-33	21	695	766	1	544	-496	7	294	-160	15	437	399	2	535	-407	6	213	-208	7	237*	197	10+1-L	11+5-L							
29	271*	-33	21	695	766	1	544	-496	7	294	-160	15	437	399	2	535	-407	6	213	-208	7	237*	197	10+1-L	11+5-L							
30	265*	-106	22	258*	306	5	163*	-89	3	157	-413	29	19	655	400	20	256*	-50	1	467	792	1	249*	107	1	398	318					
31	384	359	27	279	587	13	1245	1109	5	981	-645	14	406	298	21	611	-557	1	279	-177	17	327	127	1	398	318						
32	2127	-1106	28	774	810	9	439	347	6	395	371	15	300*	168	22	272	-187	3	303	-275	14	221*	-86	10+4-L	11+5-L							
33	419	328*	12	218*	322	10	279	65	6	305	271	17	273	187	16	281	-183	4	868	729	15	269*	729	1	398	318						
34	519	528*	13	218*	322	10	279	65	6	305	271	17	273	187	16	281	-183	4	868	729	15	269*	729	1	398	318						
35	147	-55	12	188*	116	10	521	610	18	285*	194	25	318	-313	6	540	476	17	249	-103	8	849	687	13+5-L	15+5-L							
36	187*	18	9+5-L	13	351	377	11	760	798	19	355*	302	26	191	-232	7	211	-231	10	273	-228	9	378	318	13+5-L	15+5-L						
37	249*	-225	14	278	316	20	320	58	17	421	-416	9	521	460	10	273	-228	10	273	-228	9	378	318	13+5-L	15+5-L							
38	199*	-55	11	145	1012	15	216	-307	13	213	61	9	521	460	10	273	-228	10	273	-228	9	378	318	13+5-L	15+5-L							
39	970	845	3	276	360	16	262*	-165	14	476	414	0	205*	-50	11	254	-186	7	304	-216	9	378	318	13+5-L	15+5-L							
40	114	1012	16	271	324	16	262*	-165	14	476	414	0	205*	-50	11	254	-186	7	304	-216	9	378	318	13+5-L	15+5-L							
41	439	-646	18	313	284	18	268*	61	19	267	201	15	259	246	18	211	216	12	273*	249	7	430	-326	11+2-L	1	189*	-40	1	299	202		
42	350	418	19	280	185	20	232*	57	2	323	236	22	229	-183	14	201	87	6	217*	251	9	528	438	2	309*	331						
43	273*	-127	20	278	310	21	273	-127	20	278	310	21	273	-127	13	273	-127	14	273*	249	7	430	-326	11+2-L	1	189*	-787	3	216*	20		
44	251*	-60	21	272	323	20	278*	-323	27	275	311	21	272	-187	11	211	393	23	303	-178	3	869	758	13+5-L	16+10-L							
45	241*	-122	21	272	323	20	278*	-323	27	275	311	21	272	-187	11	211	393	23	303	-178	3	869	758	13+5-L	16+10-L							
46	241*	-122	21	272	323	20	278*	-323	27	275	311	21	272	-187	11	211	393	23	303	-178	3	869	758	13+5-L	16+10-L							
47	241*	-122	21	272	323	20	278*	-323	27	275	311	21	272	-187	11	211	393	23	303	-178	3	869	758	13+5-L	16+10-L							
48	291	576	29	224*	-17	22	280	-237	23	240	310	5	584	480	6	724	-725	20	484	-631	4	348	-356	12+6-L	1	512	482					
49	230*	-109	30	380	513	24	656	586	26	274	-175	16	521	466	24	731	-212	21	476	-494	3	427	-390	5	185	-156						
50	336	370	26	268*	124	10	206*	-77	15	231	-132	10	624	402	28	221	-57	11	316	262	21	236	-95	14	272	-205						
51	762	774	27	268*	124	10	206*	-77	15	231	-132	10	624	402	28	2																

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