



LETTERS TO THE EDITOR



SUPPRESSION OF VIBRATION IN THE AXIALLY MOVING KIRCHHOFF STRING BY BOUNDARY CONTROL

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1. INTRODUCTION

Axially moving string-like continua such as threads, wires, magnetic tapes, belts, band-saws, chains, and cables have been subjects of the study of researchers in recent years; see survey papers [1–3] for extensive lists of references. Researchers have derived and studied different linear and non-linear mathematical models which describe the dynamics of such systems; see, e.g., references [4–28]. Recently, the important problem of designing stabilizing controllers to suppress the vibration of axially moving string-like continua has received attention by researchers; see, e.g., references [29–35]. Controllers in these references, except those in references [32] and [35], are designed for the linear models of axially moving strings. One way to describe the dynamics of an axially moving string is to model it as the moving Kirchhoff string; see, e.g., references [9] and [26]. The axially moving Kirchhoff string is represented by a non-linear partial differential equation. Our goal in this note is to show that the linear boundary control is a stabilizing controller for the axially moving Kirchhoff string. We achieve this goal by using an approach analogous to that in reference [35]. To the best of our knowledge, this note is the first to present the application of the boundary control to the moving Kirchhoff string.

We consider the axially moving string in Figure 1. The string is pulled at a constant speed through two eyelets which are distanced from each other by 1. One of the eyelets is fixed and the other one can move freely in the direction of the Y -axis. A control input force, denoted by u in Figure 1, can be applied to the free-to-move eyelet transversally. By transversal we mean in the direction of Y .

The dynamics of the string in Figure 1 can be represented by the following nonlinear partial differential equation (see, e.g., references [9] and [26]):

$$y_{tt}(x, t) + 2vy_{xt}(x, t) = \left(1 - v^2 + b \int_0^1 y_x^2(x, t) dx\right) y_{xx}(x, t), \quad (1a)$$

for all $x \in (0, 1)$ and $t \geq 0$. In equation (1a), $y(\cdot, \cdot) \in \mathbb{R}$ denotes the transversal displacement of the string, $y_x := \partial y / \partial x$, $y_{xx} := \partial^2 y / \partial x^2$, $y_{tt} := \partial^2 y / \partial t^2$, $y_{xt} := \partial^2 y / \partial x \partial t$, and $b > 0$ is a constant real number, and $v \geq 0$ is proportional to the speed of the string through the eyelets. In realistic physical situations, $v < 1$.

The tension in the string represented by equation (1a) is *not* constant and is given by

$$T(t) = 1 + b \int_0^1 y_x^2(x, t) dx,$$

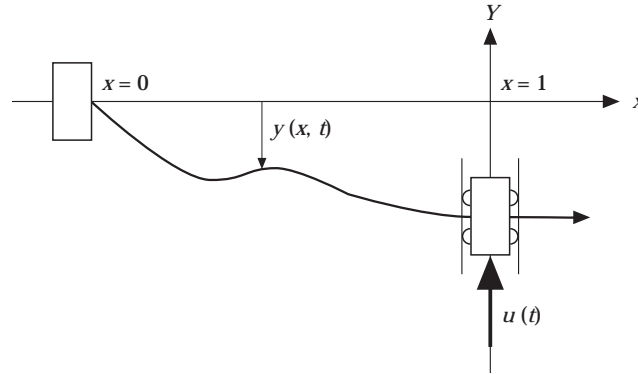


Figure 1. The string is pulled at a constant speed through two eyelets. The eyelet at $x = 0$ is fixed and the one at $x = 1$ can move freely in the direction of the axis Y . The control input force $u(t) = -ky_t(1, t)$ for all $t \geq 0$, where $k > 0$ is a constant real number, is applied to the free-to-move eyelet in the direction of Y .

for all $t \geq 0$ (see reference [36]). Having the tension T , we have the following boundary conditions:

$$y(0, t) = 0, \quad \left(1 - v^2 + b \int_0^1 y_x^2(x, t) dx\right) y_x(1, t) = u(t), \quad (1b, c)$$

for all $t \geq 0$. The boundary condition in equation (1b) states that the string is fixed at $x = 0$. The boundary condition in equation (1c) represents the balance of forces applied to the string at $x = 1$ in the direction of Y .

The initial displacement and velocity of the string are, respectively,

$$y(x, 0) = f(x), \quad y_t(x, 0) = g(x), \quad (1d)$$

for all $x \in (0, 1)$, where $y_t := \partial y / \partial t$. We assume that $f \in C^1[0, 1]$, and that at least one of the functions f or g is not identically zero over $[0, 1]$.

When the string does not move ($v = 0$), the system (1) represents the dynamics of a string known as the Kirchhoff string, which was originally studied by Kirchhoff in reference [37]. The Kirchhoff string has been studied by many researchers from the physical and mathematical points of view; see, e.g., references [38, pp. 220–254], [39], and [40] for extensive lists of references.

The control input u in equation (1c) is commonly known as the *boundary control*. In this note, we study the stabilization of the string in equation (1a) by u . More precisely, we study a u that results in $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$. As a stabilizing control input, the following is proposed:

$$u(t) = -ky_t(1, t), \quad (2)$$

for all $t \geq 0$, where $k > 0$ is a constant real number. With this choice of u , the boundary control is the negative feedback of the transversal velocity of the string at $x = 1$, with the gain k . It is known that fixed *linear* strings represented by equation (1), in which $v = 0$ and $b = 0$, can be stabilized by the control law in equation (2); see, e.g., references [41–47]. Also, it is known that axially moving *linear* strings represented by equation (1), in which $v > 0$ and $b = 0$, can be stabilized by the control law in equation (2); see references [31] and [33]. Roughly speaking, the boundary control in equation (2) provides a dissipative

effect in linear strings, because it is of the form of negative velocity feedback. This is in accordance with the well known fact that the negative velocity feedback increases damping in most finite dimensional inertial systems, such as, large flexible systems and robotic manipulators.

Our goal in this note is to show that the boundary control u in equation (2) stabilizes the non-linear axially moving non-linear string in equation (1), i.e., u results in $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for $x \in [0, 1]$.

2. STABILIZATION BY BOUNDARY CONTROL

Our plan to establish the stability of the non-linear string represented by equations (1) and (2) is as follows. We define an energy like (Lyapunov) function of time for the string and denote it by $t \mapsto V(t)$. We show that V tends to zero exponentially.

The scalar-valued function V is defined as

$$V(t) := E(t) + \gamma \int_0^1 [xy_t(x, t)y_x(x, t) + vxy_x^2(x, t)] dx, \quad (3)$$

for all $t \geq 0$, where γ is a constant real number satisfying

$$0 < \gamma < \min \left\{ \frac{1 - v^2}{1 + 2v}, \frac{2(1 - v^2)(k + v)}{1 - v^2 + k^2} \right\}, \quad (4)$$

and

$$E(t) := \frac{1}{2} \int_0^1 [y_t^2(x, t) + (1 - v^2)y_x^2(x, t)] dx + \frac{b}{4} \left(\int_0^1 y_x^2(x, t) dx \right)^2, \quad (5)$$

and $y(\cdot, \cdot)$ satisfies equations (1) and (2). From equations (3), (5), and (1d), we obtain

$$E(0) = \frac{1}{2} \int_0^1 [g^2(x) + (1 - v^2)f_x^2(x)] dx + \frac{b}{4} \left(\int_0^1 f_x^2(x) dx \right)^2, \quad (6a)$$

$$V(0) = E(0) + \gamma \int_0^1 [xg(x)f_x(x) + vxf_x^2(x)] dx, \quad (6b)$$

where $f_x(x) := df(x)/dx$. Recall that at least one of the functions f or g is not identically equal to zero over $[0, 1]$. Furthermore, the function f , for which $f(0) = 0$ by equation (1b), cannot assume a non-zero constant value over $[0, 1]$. Thus, $E(0) > 0$.

Now, we prove a property of V .

Lemma 2.1. The function V satisfies

$$0 \leq K_1 E(t) \leq V(t) \leq K_2 E(t), \quad (7)$$

for all $t \geq 0$, where $K_1 > 0$ and $K_2 > 0$ are constant real numbers given by

$$K_1 = 1 - \gamma(1 + 2v)/(1 - v^2), \quad K_2 = 1 + \gamma(1 + 2v)/(1 - v^2). \quad (8a, b)$$

Proof. For the integral terms in equation (3), whose coefficient is γ , we have (the argument (x, t) of the functions is deleted)

$$\int_0^1 xy_t y_x \, dx \leq \int_0^1 x|y_t| |y_x| \, dx \leq \frac{1}{2} \int_0^1 y_t^2 \, dx + \frac{1}{2} \int_0^1 y_x^2 \, dx, \quad (9a)$$

$$\int_0^1 vxy_x^2 \, dx \leq v \int_0^1 y_x^2 \, dx, \quad (9b)$$

for all $t \geq 0$. Adding equations (9a) and (9b), we obtain

$$\int_0^1 (xy_t y_x + vxy_x^2) \, dx \leq \frac{1}{2} \int_0^1 y_t^2 \, dx + \frac{1+2v}{2(1-v^2)} \int_0^1 (1-v^2)y_x^2 \, dx, \quad (10)$$

for all $t \geq 0$. Since

$$(1+2v)/(1-v^2) \geq 1, \quad (11)$$

for all $0 \leq v < 1$, we conclude that

$$\int_0^1 (xy_t y_x + vxy_x^2) \, dx \leq \frac{1+2v}{1-v^2} \left(\frac{1}{2} \int_0^1 [y_t^2 + (1-v^2)y_x^2] \, dx \right) \leq \frac{1+2v}{1-v^2} E(t), \quad (12a)$$

for all $t \geq 0$. Similarly, we obtain

$$\int_0^1 (xy_t y_x + vxy_x^2) \, dx \geq -\frac{1+2v}{1-v^2} E(t), \quad (12b)$$

for all $t \geq 0$. Using inequalities (12) in equation (3), we obtain inequality (7). Note that $\gamma < (1-v^2)/(1+2v)$ by inequality (4). Therefore, K_1 and K_2 in equation (8) are positive real numbers. \square

Remarks. (1) Since $(1+2v)/(1-v^2) \geq 1$ for all $0 \leq v < 1$, then γ in inequality (4) is at least less than 1.

(2) By inequality (7) and the fact that $E(0) > 0$, it is concluded that $V(0) > 0$. \square

Next, we use equation (2) in equation (1c) and rewrites the boundary conditions as

$$y(0, t) = 0, \quad y_x(1, t) = -ky_t(1, t) \left/ \left(1 - v^2 + b \int_0^1 y_x^2(x, t) \, dx \right) \right., \quad (13a, b)$$

for all $t \geq 0$. We now prove some identities for the functions satisfying equation (13).

Lemma 2.2. Let $y(\cdot, \cdot)$ satisfy the boundary conditions in equation (13). Then,

$$2 \int_0^1 y_{xt} y_t \, dx = y_t^2(1, t), \quad (14a)$$

$$\int_0^1 (y_{xx} y_t + y_{xt} y_x) \, dx = -ky_t^2(1, t) \left/ \left(1 - v^2 + b \int_0^1 y_x^2 \, dx \right) \right., \quad (14b)$$

$$\int_0^1 xy_{xt}y_t \, dx = \frac{1}{2}y_t^2(1, t) - \frac{1}{2}\int_0^1 y_t^2 \, dx, \quad (14c)$$

$$\int_0^1 xy_{xx}y_x \, dx = k^2y_t^2(1, t) / 2 \left(1 - v^2 + b \int_0^1 y_x^2 \, dx \right)^2 - \frac{1}{2}\int_0^1 y_x^2 \, dx, \quad (14d)$$

for all $t \geq 0$.

Proof. From equation (13a), we have $y_t(0, t) = 0$ for all $t \geq 0$. Thus, we obtain

$$2 \int_0^1 y_{xt}y_t \, dx = \int_0^1 (y_t^2)_x \, dx = y_t^2(1, t), \quad (15)$$

for all $t \geq 0$. That is, equation (14a) holds.

Having $y_t(0, t) = 0$ for all $t \geq 0$, we next obtain

$$\int_0^1 (y_{xx}y_t + y_{xt}y_x) \, dx = \int_0^1 (y_x y_t)_x \, dx = y_x(1, t)y_t(1, t), \quad (16)$$

for all $t \geq 0$. Using equation (13b) in equation (16), we obtain equation (14b).

Next, we write

$$\int_0^1 xy_{xt}y_t \, dx = \frac{1}{2} \int_0^1 (xy_t^2)_x \, dx - \frac{1}{2} \int_0^1 y_t^2 \, dx, \quad (17)$$

for all $t \geq 0$. Thus, equation (14c) follows.

Finally, we write

$$\int_0^1 xy_{xx}y_x \, dx = \frac{1}{2} \int_0^1 (xy_x^2)_x \, dx - \frac{1}{2} \int_0^1 y_x^2 \, dx = \frac{1}{2}y_x^2(1, t) - \frac{1}{2} \int_0^1 y_x^2 \, dx, \quad (18)$$

for all $t \geq 0$. Using equation (13b) in equation (18), we obtain equation (14d). \square

Next, we compute the time-derivative of the function E .

Lemma 2.3. The time-derivative of the function E in equation (5), along the solution of the system (1a), (1d), and (13) (equivalently, the system (1) and (2)) satisfies

$$\dot{E}(t) = -(k + v)y_t^2(1, t) \leq 0, \quad (19)$$

for all $t \geq 0$.

Proof. From equation (5), we obtain

$$\dot{E}(t) = \int_0^1 [y_{tt}y_t + (1 - v^2)y_{xt}y_x] \, dx + b \int_0^1 y_x^2 \, dx \int_0^1 y_{xt}y_x \, dx, \quad (20)$$

for all $t \geq 0$. Substituting y_{tt} from equation (1a) into equation (20), we obtain

$$\dot{E}(t) = -2v \int_0^1 y_{xt}y_t \, dx + \left(1 - v^2 + b \int_0^1 y_x^2 \, dx \right) \int_0^1 (y_{xx}y_t + y_{xt}y_x) \, dx, \quad (21)$$

for all $t \geq 0$. Using equations (14a) and (14b) in equation (21), we obtain inequality (19). \square

Using the preliminary results obtained thus far, we next prove that the functions V and E tend to zero exponentially.

Theorem 2.4. The functions V and E , along the solution of the system (1a), (1d), and (13) (equivalently, the system (1) and (2)) satisfy

$$0 \leq V(t) \leq V(0) e^{-\gamma t/K_2}, \quad 0 \leq E(t) \leq (V(0)/K_1) e^{-\gamma t/K_2}, \quad (22a, b)$$

for all $t \geq 0$, where K_1 and K_2 are given in equation (8).

Proof. From equation (3) we obtain

$$\dot{V}(t) = \dot{E}(t) + \gamma \int_0^1 (xy_{tt}y_x + xy_t y_{xt} + 2vxy_{xt}y_x) dx, \quad (23)$$

for all $t \geq 0$. Substituting y_{tt} from equation (1a) into equation (23), we obtain

$$\dot{V}(t) = \dot{E}(t) + \gamma \int_0^1 xy_{xt}y_t dx + \gamma \left(1 - v^2 + b \int_0^1 y_x^2 dx \right) \int_0^1 xy_{xx}y_x dx, \quad (24)$$

for all $t \geq 0$. Using equations (19), (14c), and (14d) in equation (24), we obtain

$$\begin{aligned} \dot{V}(t) = & -\gamma E(t) - (k+v)y_t^2(1, t) - \frac{\gamma b}{4} \left(\int_0^1 y_x^2 dx \right)^2 \\ & + \frac{\gamma}{2} y_t^2(1, t) + \gamma k^2 y_t^2(1, t) / 2 \left(1 - v^2 + b \int_0^1 y_x^2 dx \right), \end{aligned} \quad (25)$$

for all $t \geq 0$. Neglecting the third term of equation (25) and $\int_0^1 y_x^2 dx$ in the last term of this equation, we obtain

$$\dot{V}(t) \leq -\gamma E(t) - (k+v)y_t^2(1, t) + \gamma y_t^2(1, t)/2 + \gamma k^2 y_t^2(1, t)/2(1-v^2), \quad (26)$$

for all $t \geq 0$. Therefore,

$$\dot{V}(t) \leq -\gamma E(t) - F(t), \quad (27)$$

for all $t \geq 0$, where

$$F(t) := [(k+v) - \gamma(1-v^2+k^2)/2(1-v^2)] y_t^2(1, t). \quad (28)$$

Having γ satisfying inequality (4), we conclude that the coefficient of $y_t^2(1, \cdot)$ in equation (28) is positive, and hence $F(t) \geq 0$ for all $t \geq 0$. Using the non-negativeness of F in inequality (27), we obtain

$$\dot{V}(t) \leq -\gamma E(t), \quad (29)$$

for all $t \geq 0$. Using inequality (7) in inequality (29), we obtain the following differential inequality:

$$\dot{V}(t) \leq -(\gamma/K_2)V(t), \quad (30)$$

for all $t \geq 0$, with the initial condition $V(0) > 0$ given in equation (6b). By a comparison theorem given in reference [48, p. 3] or reference [49, p. 2], we conclude that V in inequality (30) satisfies $V(t) \leq V(0) e^{-\gamma t/K_2}$ for all $t \geq 0$. Note that by inequality (7), we have

$V(t) \geq 0$ for all $t \geq 0$. Thus, inequality (22a) holds. By inequalities (7) and (22a), we conclude that inequality (22b) holds. \square

Finally, we show that the boundary control u in equation (2) stabilizes the non-linear string in equation (1).

Corollary 2.5. The solution of the system (1a), (1d), and (13) (equivalently, the system (1) and (2)), $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$.

Proof. For the system (1a), (1d), and (13) we choose the Lyapunov function V in equation (3). Then, by Theorem 2.4, the function E tends to zero exponentially. From equation (5), we conclude that $y_x(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$. Since, $y(0, t) = 0$ for all $t \geq 0$, we conclude that $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$. \square

3. CONCLUSION

In this note, the Lyapunov technique has been used to prove that the non-linear axially moving Kirchhoff string represented by equation (1) can be stabilized by the linear boundary control in equation (2). The boundary control is the negative feedback of the transversal velocity of the string at one end.

REFERENCES

1. C. D. MOTE JR. 1972 *The Shock and Vibration Digest* **4**(4), 2–11. Dynamic stability of axially moving materials.
2. J. A. WICKERT and C. D. MOTE JR. 1988 *The Shock and Vibration Digest* **20**(5), 3–13. Current research on the vibration and stability of axially-moving materials.
3. A. ABRATE 1992 *Mechanism and Machine Theory* **27**, 645–659. Vibration of belts and belt drives.
4. C. D. MOTE JR. 1966 *Journal of Applied Mechanics* **33**, 463–464. On the nonlinear oscillation of an axially moving string.
5. V. A. BAPAT and P. SRINIVASAN 1967 *Journal of Applied Mechanics* **34**, 775–777. Nonlinear transverse oscillations in traveling strings by the method of harmonic balance.
6. A. L. THURMAN and C. D. MOTE JR. 1969 *Journal of Applied Mechanics* **36**, 83–91. Free, periodic, nonlinear oscillation of an axially moving strip.
7. K. R. KORDE 1985 *Journal of Applied Mechanics* **52**, 493–494. On nonlinear oscillation of moving string.
8. J. A. WICKERT and C. D. MOTE JR. 1990 *Journal of Applied Mechanics* **57**, 738–744. Classical vibration analysis of axially moving continua.
9. J. A. WICKERT 1992 *International Journal of Non-linear Mechanics* **27**, 503–517. Non-linear vibration of a traveling tensioned beam.
10. J. A. WICKERT 1993 *Journal of Sound and Vibration* **160**, 455–463. Analysis of self-excited longitudinal vibration of a moving tape.
11. J. A. WICKERT 1993 *Journal of Vibration and Acoustics* **115**, 145–151. Free linear vibration of self-pressurized foil bearings.
12. M. PAKDEMIRLI, A. G. ULSOY and A. CERANOGLU 1994 *Journal of Sound and Vibration* **169**, 179–196. Transverse vibration of an axially accelerating string.
13. W. D. ZHU and C. D. MOTE JR. 1994 *Journal of Sound and Vibration* **177**, 591–610. Free and forced response of an axially moving string transporting a damped linear oscillator.
14. W. D. ZHU and C. D. MOTE JR. 1995 *Journal of Applied Mechanics* **62**, 873–879. Propagation of boundary disturbances in an axially moving strip in contact with rigid and flexible constraints.
15. J.-S. HUNAG, R.-F. FUNG and C.-H. LIN 1995 *International Journal of Mechanical Sciences*, **37**, 145–160. Dynamic stability of a moving string undergoing three-dimensional vibration.
16. A. V. LAKSHMIKUMARAN and J. A. WICKERT 1996 *Journal of Vibration and Acoustics* **118**, 398–405. On the vibration of coupled traveling string and air bearing systems.
17. R. S. BEIKMANN, N. C. PERKINS and A. G. ULSOY 1996 *Journal of Vibration and Acoustics*, **118**, 406–413. Free vibration of serpentine belt drive systems.
18. R. S. BEIKMANN, N. C. PERKINS and A. G. ULSOY 1996 *Journal of Vibration and Acoustics*, **118**, 567–574. Nonlinear coupled vibration response of serpentine belt drive systems.

19. R. S. BEIKMANN, N. C. PERKINS and A. G. ULSOY 1997 *Journal of Mechanical Design* **119**, 162–168. Design and analysis of automotive serpentine belt drive systems for steady state performance.
20. J.-S. CHEN 1997 *Journal of Vibration and Acoustics* **119**, 152–157. Natural frequencies and stability of an axially-traveling string in contact with a stationary load system.
21. R.-F. FUNG, J.-S. HUNAG and Y.-C. CHEN 1997 *Journal of Sound and Vibration* **201**, 153–167. The transient amplitude of the viscoelastic travelling string: an integral constitutive law.
22. R.-F. FUNG and J.-S. SHIEH 1997 *Journal of Sound and Vibration* **199**, 207–221. Vibration analysis of a non-linear coupled textile-rotor system with synchronous whirling.
23. R. F. FUNG and S. L. WU 1997 *Journal of Sound and Vibration* **204**, 171–179. Dynamic stability of a three-dimensional string subjected to both magnetic and tensioned excitations.
24. S.-Y. LEE and C. D. MOTE JR. 1997 *Journal of Sound and Vibration* **204**, 717–734. A generalized treatment of the energetics of translating continua, part I: strings and second order tensioned pipes.
25. S.-Y. LEE and C. D. MOTE JR. 1997 *Journal of Sound and Vibration* **204**, 735–753. A generalized treatment of the energetics of translating continua, part II: beams and fluid conveying pipes.
26. J. MOON and J. A. WICKERT 1997 *Journal of Sound and Vibration* **200**, 419–431. Non-linear vibration of power transmission belts.
27. M. PAKDEMIRLI and A. G. ULSOY 1997 *Journal of Sound and Vibration* **203**, 815–832. Stability analysis of an axially accelerating string.
28. C. A. TAN and S. YING 1997 *Journal of Applied Mechanics* **64**, 394–400. Dynamic analysis of the axially moving string based on wave propagation.
29. A. GALIP ULSOY 1984 *Journal of Dynamic Systems, Measurement and Control* **106**, 6–14. Vibration control in rotating or translating elastic systems.
30. B. YANG and C. D. MOTE JR. 1991 *Journal of Applied Mechanics* **58**, 189–196. Active vibration control of the axially moving string in the S -domain.
31. C. H. CHUNG and C. A. TAN 1995 *Journal of Vibration and Acoustics* **117**, 49–55. Active vibration control of the axially moving string by wave cancellation.
32. R.-F. FUNG and C.-C. LIAO 1995 *International Journal of Mechanical Sciences* **37**, 985–993. Application of variable structure control in the nonlinear string system.
33. S.-Y. LEE and C. D. MOTE JR. 1996 *Journal of Dynamic Systems, Measurement and Control* **118**, 66–74. Vibration control of an axially moving string by boundary control.
34. S. YING and C. A. TAN 1996 *Journal of Vibration Acoustics* **118**, 306–312. Active vibration control of the axially moving string using space feedforward and feedback controllers.
35. S. M. SHAHRUZ and D. A. KURMAJI 1997 *Journal of Sound and Vibration* **201**, 145–152. Vibration suppression of a non-linear axially moving string by boundary control.
36. D. W. OPLINGER 1960 *Journal of the Acoustical Society of America* **32**, 1529–1538. Frequency response of a nonlinear stretched string.
37. G. KIRCHHOFF 1877 *Vorlesungen über Mathematische Physik: Mechanik*. Leipzig: Druck und Verlag von B. G. Teubner.
38. A. AROSIO 1995 *Proceedings of the 2nd Workshop on the Functional Analytic Methods in Complex Analysis and Applications to Partial Differential Equations, Trieste, Italy, January 1993*, W. Tutschke and A. S. Mshimba (Editors). Singapore: World Scientific; Averaged evolution equations. The Kirchhoff string and its treatment in scales of Banach spaces.
39. S. M. SHAHRUZ 1996 *IEEE Transactions on Automatic Control* **41**, 1179–1182. Bounded-input bounded-output stability of a damped nonlinear string.
40. K. ONO 1997 *Journal of Differential Equations* **137**, 273–301. Global existence, decay, and blowup of solutions for some mildly degenerate non-linear Kirchhoff strings.
41. J. QUINN and D. L. RUSSELL 1977 *Proceedings of the Royal Society of Edinburgh* **77A**, 97–127. Asymptotic stability and energy decay rates for solutions of hyperbolic equations with boundary damping.
42. G. CHEN 1979 *Journal de Mathématiques Pures et Appliquées*, **58**, 249–273. Energy decay estimates and exact boundary value controllability for the wave equation in a bounded domain.
43. G. CHEN 1981 *SIAM Journal of Control and Optimization* **19**, 106–113. A note on boundary stabilization of the wave equation.
44. J. LAGNESE 1983 *Journal of Differential Equations* **50**, 163–182. Decay of solutions of wave equations in a bounded region with boundary dissipation.
45. J. E. LAGNESE 1988 *SIAM Journal of Control and Optimization* **26**, 1250–1256. Note on boundary stabilization of wave equations.

46. V. KOMONIK and E. ZUAZUA 1990 *Journal de Mathématiques Pures et Appliquées* **69**, 33–54. A direct method for the boundary stabilization of the wave equation.
47. S. COX and E. ZUAZUA 1995 *Indiana University Mathematics Journal* **44**, 545–573. The rate at which energy decays in a string damped at one end.
48. V. LAKSHMIKANTHAM, S. LEELEA and A. A. MARTYNYUK 1989 *Stability Analysis of Nonlinear Systems*. New York, NY: Marcel Dekker.
49. D. BAINOV and P. SIMEONOV 1992 *Integral Inequalities and Applications*. Dordrecht, The Netherlands: Kluwer Academic Publishers.