



THE EFFECT OF THE POISSON RATIO ON THE VIBRATION OF HOLLOW CIRCULAR FINITE-LENGTH CYLINDERS

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1. INTRODUCTION

A recent report by Leissa and So [1] recorded results for the frequencies of vibration for solid circular cylinders with free-free boundary conditions. That report included the results concerning the effect of the Poisson ratio on the frequency of vibration for free-free cylinders. The present study is intended to extend those results to include hollow cylinders. An investigation of the frequency of vibration for hollow cylinders with free-free boundary conditions was reported by So and Leissa [2] and included several different hollow cylinder sizes with the Poisson ratio of $\nu = 0.3$. The results given in reference [2] serve to validate the current analysis.

2. ANALYSIS

A finite element analysis [3] was developed to facilitate computing frequencies for solid cylinders. Frequencies and mode shapes were reported for a variety of solid cylinders with various boundary conditions. In this report, the analysis that was developed in reference [3] is used to analyze hollow cylinders with free-free and fixed-fixed boundary conditions. The finite element will not be discussed here since the development of the basic element is available [3]. It is useful to note that the element is based upon three-dimensional elasticity in cylindrical co-ordinates. The element-co-ordinate system is rendered axisymmetrically two-dimensional by assuming a solution that satisfies the governing equations in the circumferential θ direction [3]:

$$\begin{aligned} u(r, z, \theta, t) &= U(r, z) \cos m\theta \cos \omega t, & v(r, z, \theta, t) &= V(r, z) \sin m\theta \cos \omega t, \\ w(r, z, \theta, t) &= W(r, z) \cos m\theta \cos \omega t, \end{aligned} \quad (1)$$

where m is the circumferential wave number and ω is the circular frequency. Solutions are computed for integer values of m . The final form of the eigenvalue problem is written as

$$[\mathbf{K}] \{\mathbf{u}\} - \omega^2 [\mathbf{M}] \{\mathbf{u}\} = 0, \quad (2)$$

where $[\mathbf{K}]$ is the stiffness matrix, $[\mathbf{M}]$ is the mass matrix and $\{\mathbf{u}\}$ is the eigenvector.

TABLE 1

Non-dimensional frequency Ω for free-free hollow cylinder with $L/a = 2$ and $b/a = 0.2$

| m | Mode | $v = 0.0$ | $v = 0.1$ | $v = 0.2$ | $v = 0.3$ | $v = 0.4$ |
|----------------|------|-----------|-----------|-----------|-----------|-----------|
| 0^{\dagger} | 1 | 1.981(6) | 2.271(7) | 2.283(6) | 2.285(6) | 2.287(6) |
| | 2 | 2.223(8) | 2.362(8) | 2.530(8) | 2.695(8) | 2.853(8) |
| | 3 | 2.258(9) | 2.505(9) | 2.683(9) | 2.870(10) | 3.066 |
| | 4 | 2.404(10) | 2.680(10) | 3.056 | 3.478 | 3.557 |
| | 5 | 3.162 | 3.285 | 3.390 | 3.537 | 4.086 |
| 0^{\ddagger} | 1 | 1.571(1) | 1.571(1) | 1.571(1) | 1.571(1) | 1.571(1) |
| | 2 | 3.142 | 3.142 | 3.142 | 3.142 | 3.142 |
| | 3 | 4.715 | 4.715 | 4.715 | 4.715 | 4.715 |
| | 4 | 5.223 | 5.223 | 5.223 | 5.223 | 5.223 |
| | 5 | 5.454 | 5.454 | 5.454 | 5.454 | 5.454 |
| 1 | 1 | 1.793(4) | 1.871(4) | 1.935(4) | 1.986(4) | 2.015(4) |
| | 2 | 1.950(5) | 1.972(5) | 1.990(5) | 2.003(5) | 2.028(5) |
| | 3 | 2.501 | 2.614 | 2.720(10) | 2.813(9) | 2.887(9) |
| | 4 | 2.860 | 2.936 | 3.001 | 3.056 | 3.102 |
| | 5 | 2.947 | 3.026 | 3.117 | 3.222 | 3.333 |
| 2 | 1 | 1.665(2) | 1.690(2) | 1.714(2) | 1.737(2) | 1.760(2) |
| | 2 | 1.775(3) | 1.817(3) | 1.860(3) | 1.904(3) | 1.950(3) |
| | 3 | 2.187(7) | 2.245(6) | 2.298(7) | 2.347(7) | 2.392(7) |
| | 4 | 2.822 | 2.895 | 2.956 | 3.009 | 3.056(10) |
| | 5 | 3.724 | 3.817 | 3.876 | 3.928 | 3.957 |
| 3 | 1 | 3.129 | 3.139 | 3.148 | 3.155 | 3.162 |
| | 2 | 3.224 | 3.262 | 3.288 | 3.307 | 3.322 |
| | 3 | 3.421 | 3.462 | 3.505 | 3.547 | 3.588 |
| | 4 | 3.815 | 3.923 | 4.013 | 4.087 | 4.150 |
| | 5 | 4.613 | 4.736 | 4.775 | 4.805 | 4.829 |
| 4 | 1 | 4.233 | 4.246 | 4.253 | 4.258 | 4.262 |
| | 2 | 4.234 | 4.265 | 4.286 | 4.299 | 4.310 |
| | 3 | 4.557 | 4.617 | 4.674 | 4.726 | 4.773 |
| | 4 | 4.752 | 4.878 | 4.985 | 5.074 | 5.149 |
| | 5 | 5.397 | 5.550 | 5.677 | 5.731 | 5.751 |

\dagger Pure radial/longitudinal.

\ddagger Pure torsional mode.

3. RESULTS FOR FREQUENCY

The hollow cylinder is assigned a length L , outside radius a and inside radius b . Results are given in terms of unit outside radius $a = 1$, unit shear modulus $G = 1$, unit mass density ρ and cylinder height $L = 2a$. The frequency is reported, similar to references [1, 3], using a non-dimensional frequency Ω defined as

$$\Omega = \omega a \sqrt{\rho/G}. \quad (3)$$

The results for free-free boundary conditions are tabulated in Tables 1–3 and results for fixed-fixed boundary conditions are given in Tables 4–6. Frequencies are tabulated for five different values of the Poisson ratio. Frequencies that correspond to the Poisson ratio of 0.3

TABLE 2

Non-dimensional frequency Ω for free-free hollow cylinder with $L/a = 2$ and $b/a = 0.5$

| m | Mode | $v = 0.0$ | $v = 0.1$ | $v = 0.2$ | $v = 0.3$ | $v = 0.3$ [2, 4] | $v = 0.4$ |
|----------------|------|-----------|-----------|-----------|-----------|------------------|-----------|
| 0^{\dagger} | 1 | 1.841(7) | 1.994(7) | 2.011(7) | 2.042(7) | 2.043 | 2.050(7) |
| | 2 | 1.913(8) | 2.014(8) | 2.030(8) | 2.148(8) | 2.151 | 2.200(8) |
| | 3 | 1.975(9) | 2.036(9) | 2.168(9) | 2.302(10) | 2.305 | 2.395(10) |
| | 4 | 2.221 | 2.378 | 2.606 | 2.893 | 2.893 | 3.220 |
| | 5 | 2.793 | 2.847 | 2.971 | 3.093 | 3.091 | 3.242 |
| 0^{\ddagger} | 1 | 1.571(4) | 1.571(4) | 1.571(3) | 1.571(3) | 1.571 | 1.571(3) |
| | 2 | 3.142 | 3.142 | 3.142 | 3.142 | 3.142 | 3.142 |
| | 3 | 4.715 | 4.715 | 4.715 | 4.715 | 4.712 | 4.715 |
| | 4 | 6.293 | 6.293 | 6.283 | 6.283 | 6.293 | 6.293 |
| | 5 | 6.815 | 6.815 | 6.815 | 6.815 | 6.814 | 6.815 |
| 1 | 1 | 1.544(3) | 1.568(3) | 1.588(4) | 1.604(4) | 1.604 | 1.618(4) |
| | 2 | 1.686(5) | 1.762(5) | 1.831(5) | 1.894(5) | 1.893 | 1.950(5) |
| | 3 | 2.440 | 2.456 | 2.467 | 2.481 | 2.481 | 2.497 |
| | 4 | 2.462 | 2.648 | 2.859 | 2.931 | 2.931 | 2.992 |
| | 5 | 2.715 | 2.791 | 2.862 | 3.079 | 3.079 | 3.301 |
| 2 | 1 | 0.849(1) | 0.887(1) | 0.927(1) | 0.971(1) | 0.970 | 1.018(1) |
| | 2 | 0.962(2) | 0.990(2) | 1.017(2) | 1.046(2) | 1.045 | 1.073(2) |
| | 3 | 1.774(6) | 1.829(6) | 1.883(6) | 1.936(6) | 1.935 | 1.990(6) |
| | 4 | 2.360 | 2.414 | 2.459 | 2.498 | 2.498 | 2.533 |
| | 5 | 3.142 | 3.206 | 3.254 | 3.294 | 3.293 | 3.330 |
| 3 | 1 | 2.056(10) | 2.131(10) | 2.208(10) | 2.288(9) | 2.287 | 2.370(9) |
| | 2 | 2.180 | 2.238 | 2.294 | 2.349 | 2.348 | 2.402 |
| | 3 | 2.614 | 2.677 | 2.740 | 2.805 | 2.803 | 2.873 |
| | 4 | 3.229 | 3.318 | 3.40 | 3.478 | 3.477 | 3.551 |
| | 5 | 3.951 | 4.048 | 4.130 | 4.201 | 4.199 | 4.266 |
| 4 | 1 | 3.370 | 3.469 | 3.568 | 3.662 | 3.659 | 3.740 |
| | 2 | 3.473 | 3.549 | 3.618 | 3.682 | 3.680 | 3.747 |
| | 3 | 3.735 | 3.806 | 3.877 | 3.952 | 3.950 | 4.038 |
| | 4 | 4.170 | 4.278 | 4.382 | 4.483 | 4.482 | 4.584 |
| | 5 | 4.804 | 4.936 | 5.055 | 5.162 | 5.158 | 5.261 |

\dagger Pure radial/longitudinal.

\ddagger Pure torsional mode.

are compared with the results obtained by Leissa and So [2] and So [4]. The inside radius of the cylinder is b and results are given for b/a ratios of 0.2, 0.5 and 0.9.

Finite element analysis can be sensitive to the aspect ratio of the element. Results for b/a of 0.2 and 0.5 were computed using a 50-element model with aspect ratios of 1.25 and 2.00 respectively. Tables 3 and 6 for b/a of 0.9 were developed using a 36-element model with an element aspect ratio of 5.00. A double-precision eigenvalue routine was used for the 36-element model.

The numbers in parentheses show the order of the frequencies and it can be seen that the wall thickness of the cylinder has a definite effect on the order of frequencies. The first frequency for free-free cylinders with inside radius $b = 0.2$ is the first pure torsional mode

TABLE 3

Non-dimensional frequency Ω for free-free hollow cylinder with $L/a = 2$ and $b/a = 0.9$

| m | Mode | $v = 0.0$ | $v = 0.1$ | $v = 0.2$ | $v = 0.3$ | $v = 0.3$ [2, 4] | $v = 0.4$ |
|----------------|------|-----------|-----------|-----------|-----------|------------------|-----------|
| 0^{\dagger} | 1 | 1.488 | 1.557 | 1.608 | 1.647 | 1.647 | 1.675 |
| | 2 | 1.490 | 1.560 | 1.627 | 1.691 | 1.691 | 1.750 |
| | 3 | 1.499 | 1.570 | 1.641 | 1.707 | 1.707 | 1.771 |
| | 4 | 1.600 | 1.675 | 1.750 | 1.824 | 1.823 | 1.899 |
| | 5 | 1.887 | 1.978 | 2.073 | 2.173 | 2.168 | 2.282 |
| 0^{\ddagger} | 1 | 1.571 | 1.571 | 1.571 | 1.571 | 1.571 | 1.571 |
| | 2 | 3.142 | 3.142 | 3.412 | 3.142 | 3.142 | 3.142 |
| | 3 | 4.714 | 4.714 | 4.714 | 4.714 | 4.712 | 4.714 |
| | 4 | 6.288 | 6.288 | 6.288 | 6.288 | 6.283 | 6.288 |
| | 5 | 7.869 | 7.869 | 7.869 | 7.869 | 7.854 | 7.869 |
| 1 | 1 | 1.223(12) | 1.251(12) | 1.274(12) | 1.294(12) | 1.294 | 1.312(11) |
| | 2 | 1.305(13) | 1.369(13) | 1.429(13) | 1.485(13) | 1.485 | 1.538(13) |
| | 3 | 1.555 | 1.628 | 1.699 | 1.770 | 1.769 | 1.843 |
| | 4 | 1.886 | 1.976 | 2.070 | 2.158 | 2.157 | 2.160 |
| | 5 | 2.088 | 2.148 | 2.156 | 2.170 | 2.165 | 2.280 |
| 2 | 1 | 0.122(1) | 0.128(1) | 0.134(1) | 0.146(1) | 0.143 | 0.152(1) |
| | 2 | 0.171(2) | 0.176(2) | 0.180(2) | 0.188(2) | 0.185 | 0.192(2) |
| | 3 | 0.964(8) | 1.007(8) | 1.049(8) | 1.091(8) | 1.090 | 1.131(8) |
| | 4 | 1.398(15) | 1.467 | 1.527 | 1.589 | 1.587 | 1.651(14) |
| | 5 | 1.853 | 1.907 | 1.941 | 1.972 | 1.971 | 2.001 |
| 3 | 1 | 0.339(3) | 0.357(3) | 0.377(3) | 0.401(3) | 0.400 | 0.427(3) |
| | 2 | 0.415(4) | 0.431(4) | 0.448(4) | 0.467(4) | 0.466 | 0.488(4) |
| | 3 | 0.859(7) | 0.893(7) | 0.928(7) | 0.966(7) | 0.964 | 1.006(7) |
| | 4 | 1.399 | 1.458(15) | 1.519(15) | 1.585(15) | 1.583 | 1.659(15) |
| | 5 | 1.978 | 2.063 | 2.155 | 2.258(6) | 2.250 | 2.376 |
| 4 | 1 | 0.644(5) | 0.677(5) | 0.715(5) | 0.758(5) | 0.757 | 0.808(5) |
| | 2 | 0.728(6) | 0.760(6) | 0.795(6) | 0.834(6) | 0.833 | 0.876(6) |
| | 3 | 1.039(10) | 1.080(9) | 1.124(9) | 1.174(9) | 1.172 | 1.230(9) |
| | 4 | 1.546 | 1.607 | 1.675 | 1.750 | 1.746 | 1.838 |
| | 5 | 2.157 | 2.244 | 2.342 | 2.454 | 2.445 | 2.584 |
| 5 | 1 | 1.028(9) | 1.108(10) | 1.139(10) | 1.207(10) | 1.207 | 1.285(10) |
| | 2 | 1.114(11) | 1.166(11) | 1.223(11) | 1.285(11) | 1.284 | 1.354(12) |
| | 3 | 1.386(14) | 1.444(14) | 1.507(14) | 1.579(14) | 1.577 | 1.662 |
| | 4 | 1.847 | 1.920 | 2.002 | 2.095 | 2.090 | 2.205 |
| | 5 | 2.449 | 2.546 | 2.655 | 2.782 | 2.772 | 2.931 |
| 6 | 1 | 1.485 | 1.560 | 1.644 | 1.740 | — | 1.850 |
| | 2 | 1.571 | 1.645 | 1.727 | 1.817 | — | 1.915 |
| | 3 | 1.829 | 1.909 | 1.996 | 2.095 | — | 2.210 |
| | 4 | 2.260 | 2.352 | 2.454 | 2.572 | — | 2.710 |
| | 5 | 2.841 | 2.953 | 3.080 | 3.226 | — | 3.401 |

[†]Pure radial/longitudinal.

[‡]Pure torsional mode.

TABLE 4

Non-dimensional frequency Ω for fixed-fixed hollow cylinder with $L/a = 2$ and $b/a = 0.2$

| m | Mode | $v = 0.0$ | $v = 0.1$ | $v = 0.2$ | $v = 0.3$ | $v = 0.4$ |
|----------------|------|-----------|-----------|-----------|-----------|-----------|
| 0 [†] | 1 | 2.245(4) | 2.335(4) | 2.453(4) | 2.576(4) | 2.705(4) |
| | 2 | 2.584(6) | 2.794(6) | 3.031(6) | 3.342(10) | 3.767(10) |
| | 3 | 4.223 | 3.330 | 3.526 | 3.786 | 4.123 |
| | 4 | 4.444 | 4.342 | 4.450 | 4.591 | 4.862 |
| | 5 | 4.842 | 4.725 | 5.013 | 5.159 | 5.412 |
| 0 [‡] | 1 | 1.571(2) | 1.571(2) | 1.571(2) | 1.571(2) | 1.571(2) |
| | 2 | 3.142(10) | 3.142(10) | 3.142(10) | 3.142(7) | 3.142(6) |
| | 3 | 4.715 | 4.715 | 4.715 | 4.715 | 4.715 |
| | 4 | 5.454 | 5.454 | 5.454 | 5.454 | 5.454 |
| | 5 | 6.095 | 6.095 | 6.095 | 6.095 | 6.095 |
| 1 | 1 | 1.345(1) | 1.372(1) | 1.389(1) | 1.408(1) | 1.428(1) |
| | 2 | 2.438(5) | 2.511(5) | 2.581(5) | 2.647(5) | 2.710(5) |
| | 3 | 2.896(7) | 2.999(7) | 3.109(8) | 3.165(8) | 3.223(8) |
| | 4 | 3.045(9) | 3.079(9) | 3.119(9) | 3.226(9) | 3.352(9) |
| | 5 | 3.890 | 3.991 | 4.105 | 4.235 | 4.355 |
| 2 | 1 | 2.181(3) | 2.230(3) | 2.283(3) | 2.339(3) | 2.401(3) |
| | 2 | 2.972(8) | 3.029(8) | 3.085(7) | 3.140(6) | 3.194(7) |
| | 3 | 3.878 | 3.911 | 3.947 | 3.987 | 4.034 |
| | 4 | 3.958 | 4.062 | 4.168 | 4.278 | 4.390 |
| | 5 | 4.283 | 4.394 | 4.499 | 4.600 | 4.702 |
| 3 | 1 | 3.606 | 3.655 | 3.701 | 3.744 | 3.787 |
| | 2 | 4.043 | 4.092 | 4.144 | 4.192 | 4.235 |
| | 3 | 4.817 | 4.847 | 4.878 | 4.911 | 4.948 |
| | 4 | 4.907 | 4.500 | 5.085 | 5.162 | 5.234 |
| | 5 | 5.380 | 5.538 | 5.688 | 5.823 | 5.944 |
| 4 | 1 | 4.687 | 4.753 | 4.811 | 4.864 | 4.913 |
| | 2 | 5.025 | 5.097 | 5.159 | 5.213 | 5.260 |
| | 3 | 5.710 | 5.782 | 5.810 | 5.840 | 5.873 |
| | 4 | 5.755 | 5.802 | 5.896 | 5.947 | 6.042 |
| | 5 | 6.511 | 6.601 | 6.679 | 6.749 | 6.819 |

[†]Pure radial/longitudinal.

[‡]Pure torsional mode.

with the second and third frequency corresponding to $m = 2$. As the wall thickness decreases, the torsional mode is less dominant and the fundamental frequency corresponds to the circumferential wave number $m = 2$. The results in Tables 3 and 6 are extended to include additional circumferential wave numbers because the lower frequencies for thinner cylinders include larger circumferential wave numbers. The fixed-fixed cylinders show a behavior similar to that of free-free cylinders with the fundamental frequency corresponding to $m = 1$ for wall thickness of $b = 0.2$ and 0.5 . Table 6 shows that for $b = 0.9$ the first frequency corresponds to $m = 3$ except for $v = 0.4$ and $m = 2$ for that case. Additional results for hollow cylinders have been given by Yii [5].

TABLE 5

Non-dimensional frequency Ω for fixed-fixed hollow cylinder with $L/a = 2$ and $b/a = 0.5$

| m | Mode | $v = 0.0$ | $v = 0.1$ | $v = 0.2$ | $v = 0.3$ | $v = 0.4$ |
|----------------|------|-----------|-----------|-----------|-----------|-----------|
| 0 [†] | 1 | 2.084(4) | 2.197(4) | 2.325(4) | 2.478(4) | 2.627(4) |
| | 2 | 2.225(5) | 2.331(5) | 2.434(5) | 2.531(5) | 2.672(6) |
| | 3 | 2.702(10) | 2.822(10) | 2.979(10) | 3.193 | 3.492 |
| | 4 | 3.742 | 3.489 | 3.952 | 4.057 | 4.175 |
| | 5 | 4.566 | 4.692 | 5.000 | 5.364 | 5.500 |
| 0 [‡] | 1 | 1.571(3) | 1.571(3) | 1.571(3) | 1.571(2) | 1.571(2) |
| | 2 | 3.142 | 3.142 | 3.142 | 3.142(10) | 3.142(10) |
| | 3 | 4.715 | 4.715 | 4.715 | 4.715 | 4.715 |
| | 4 | 6.293 | 6.293 | 6.293 | 6.293 | 6.293 |
| | 5 | 6.993 | 6.993 | 6.993 | 6.993 | 6.993 |
| 1 | 1 | 1.240(1) | 1.262(1) | 1.285(1) | 1.308(1) | 1.334(1) |
| | 2 | 2.315(6) | 2.400(6) | 2.483(6) | 2.561(6) | 2.636(5) |
| | 3 | 2.673(9) | 2.716(9) | 2.765(9) | 2.8429(9) | 2.898(9) |
| | 4 | 2.785 | 2.892 | 3.014 | 3.157 | 3.331 |
| | 5 | 3.677 | 3.778 | 3.877 | 3.973 | 4.071 |
| 2 | 1 | 1.435(2) | 1.483(2) | 1.535(2) | 1.594(3) | 1.665(3) |
| | 2 | 2.485(8) | 2.537(8) | 2.602(8) | 2.671(8) | 2.744(8) |
| | 3 | 3.452 | 3.485 | 3.521 | 3.562 | 3.611 |
| | 4 | 3.776 | 3.868 | 3.961 | 4.055 | 4.153 |
| | 5 | 3.968 | 4.102 | 4.242 | 4.390 | 4.550 |
| 3 | 1 | 2.381(7) | 2.461(7) | 2.550(7) | 2.650(7) | 2.762(7) |
| | 2 | 3.167 | 3.252 | 3.342 | 3.439 | 3.542 |
| | 3 | 4.270 | 4.372 | 4.476 | 4.533 | 4.566 |
| | 4 | 4.463 | 4.484 | 4.507 | 4.584 | 4.694 |
| | 5 | 5.220 | 5.328 | 5.426 | 5.520 | 5.616 |
| 4 | 1 | 3.589 | 3.696 | 3.809 | 3.931 | 4.062 |
| | 2 | 4.180 | 4.289 | 4.403 | 4.521 | 4.645 |
| | 3 | 5.071 | 5.190 | 5.310 | 5.431 | 5.554 |
| | 4 | 5.533 | 5.550 | 5.567 | 5.587 | 5.612 |
| | 5 | 6.193 | 6.326 | 6.424 | 6.481 | 6.546 |

[†]Pure radial/longitudinal.

[‡]Pure torsional mode.

4. CONCLUDING REMARK

Finite-length hollow circular cylinders have been analyzed for free-free and fixed-fixed symmetrical boundary conditions with the Poisson ratio as the primary variable. A primary conclusion is that the frequencies increase as the Poisson ratio increases for all the cylinders that were studied.

TABLE 6

Non-dimensional frequency Ω for fixed-fixed hollow cylinder with $L/a = 2$ and $b/a = 0.9$

| m | mode | $v = 0.0$ | $v = 0.1$ | $v = 0.2$ | $v = 0.3$ | $v = 0.4$ |
|----------------|------|-----------|-----------|-----------|-----------|-----------|
| 0 [†] | 1 | 1.505(10) | 1.583(11) | 1.670(11) | 1.769(11) | 1.854(11) |
| | 2 | 1.605(14) | 1.678(13) | 1.742(13) | 1.799(12) | 1.883(12) |
| | 3 | 1.892 | 1.983 | 2.079 | 2.185 | 2.312 |
| | 4 | 2.221 | 2.343 | 2.484 | 2.642 | 2.820 |
| | 5 | 2.416 | 2.534 | 2.678 | 2.870 | 3.138 |
| 0 [‡] | 1 | 1.571(12) | 1.571(10) | 1.571(9) | 1.571(9) | 1.571(8) |
| | 2 | 3.142 | 3.142 | 3.142 | 3.142 | 3.142 |
| | 3 | 4.715 | 4.715 | 4.715 | 4.715 | 4.715 |
| | 4 | 6.292 | 6.292 | 6.292 | 6.292 | 6.292 |
| | 5 | 7.869 | 7.869 | 7.869 | 7.869 | 7.869 |
| 1 | 1 | 0.969(4) | 0.991(4) | 1.013(4) | 1.034(4) | 1.056(4) |
| | 2 | 1.449(9) | 1.518(9) | 1.584(10) | 1.649(10) | 1.716(10) |
| | 3 | 1.845 | 1.931 | 2.020 | 2.115 | 2.225 |
| | 4 | 2.384 | 2.475 | 2.552 | 2.633 | 2.723 |
| | 5 | 2.426 | 2.507 | 2.604 | 2.723 | 2.874 |
| 2 | 1 | 0.678(2) | 0.698(2) | 0.718(2) | 0.741(2) | 0.766(1) |
| | 2 | 1.227(7) | 1.280(7) | 1.335(7) | 1.395(7) | 1.463(7) |
| | 3 | 1.775(16) | 1.857(16) | 1.944(16) | 2.042(15) | 2.159(15) |
| | 4 | 2.415 | 2.526 | 2.649 | 2.790 | 2.964 |
| | 5 | 2.954 | 2.988 | 3.024 | 3.061 | 3.101 |
| 3 | 1 | 0.636(1) | 0.663(1) | 0.693(1) | 0.729(1) | 0.773(2) |
| | 2 | 1.156(5) | 1.206(5) | 1.262(5) | 1.326(5) | 1.404(5) |
| | 3 | 1.771(15) | 1.852(15) | 1.942(15) | 2.045(16) | 2.173(16) |
| | 4 | 2.477 | 2.590 | 2.716 | 2.863 | 3.046 |
| | 5 | 3.313 | 3.459 | 3.624 | 3.784 | 3.806 |
| 4 | 1 | 0.824(3) | 0.865(3) | 0.912(3) | 0.969(3) | 1.040(3) |
| | 2 | 1.273(8) | 1.333(8) | 1.401(8) | 1.484(8) | 1.581(9) |
| | 3 | 1.887 | 1.974 | 2.073 | 2.190 | 2.335 |
| | 4 | 2.620 | 2.739 | 2.874 | 3.032 | 3.230 |
| | 5 | 3.476 | 3.628 | 3.801 | 4.004 | 4.258 |
| 5 | 1 | 1.164(6) | 1.223(6) | 1.292(6) | 1.375(6) | 1.476(6) |
| | 2 | 1.550(11) | 1.625(12) | 1.712(12) | 1.816(13) | 1.945(13) |
| | 3 | 2.131 | 2.231 | 2.345 | 2.481 | 2.650 |
| | 4 | 2.858 | 2.988 | 3.136 | 3.311 | 3.528 |
| | 5 | 3.715 | 3.876 | 4.061 | 4.279 | 4.458 |
| 6 | 1 | 1.602(13) | 1.682(14) | 1.776(14) | 1.889(14) | 2.026(14) |
| | 2 | 1.946 | 2.040 | 2.150 | 2.281 | 2.442 |
| | 3 | 2.487 | 2.604 | 2.739 | 2.898 | 3.096 |
| | 4 | 3.190 | 3.334 | 3.500 | 3.695 | 3.937 |
| | 5 | 4.031 | 4.206 | 4.406 | 4.612 | 4.931 |

[†]Pure radial/longitudinal.

[‡]Pure torsional mode.

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