

A Table of Fundamental Pairs of Units in Totally Real Cubic Fields

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In honor of Daniel Shanks' 70th birthday

Abstract. We apply a method of Cusick [5] to tabulate data on the first 250 totally real cubic fields F having discriminant $D \leq 6,885$. Apart from D , we list the class number H and the regulator R of F . Also given are the integer coefficients A, B, C of a defining polynomial $g(x) = x^3 - Ax^2 + Bx - C$, its index I , and its largest zero R_0 . For $j = 1, 2$, we also tabulate both the integer coefficients X_j, Y_j, Z_j for the two units $E_j = (X_j + R_0 Y_j + R_0^2 Z_j)/I$ with norm $+1$, forming a fundamental pair, as well as the E_j and the integers $F_j = \text{trace}(E_j^2)$.

1. Introduction. The first author [4], [5] recently gave a new method for finding a fundamental pair of units in totally real cubic fields. This method is an improvement of one due to Godwin [8]. The earlier version [4] of the main theorem contained some possible exceptional cases (presumed not to exist) for which the determination of the fundamental pair was less simple. Godwin [10] gave a clever and very short argument which proved that the exceptional cases do not exist. The later paper [5] provided a much simpler proof of the main theorem in which there are no longer any exceptional cases.

The purpose of the present paper is to apply the algorithm of [5] to the actual computation of units and to tabulate the fundamental pairs of units E_1 and E_2 and other information for all the 250 totally real fields F with field discriminant $D \leq 6,885$. The resulting table has been photographically reproduced from the computer output.

The fundamental pairs of units are standardized so as to have a norm of $+1$; in common with all integers in F , they have a representation

$$(1) \quad E_j = (X_j + R_0 Y_j + R_0^2 Z_j)/I \quad (j = 1, 2).$$

Here X_j, Y_j, Z_j are rational integers, R_0 is the largest zero of a certain irreducible, monic defining polynomial $g(x)$ with rational integer coefficients and polynomial discriminant D_g , and $I = I_g$, the index of $g(x)$, is the positive integer $(D_g/D)^{1/2}$.

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The table lists the coefficients A, B, C in

$$(2) \quad \begin{aligned} g(x) &= x^3 - Ax^2 + Bx - C \\ &= (x - R_0)(x - R_1)(x - R_2), \quad R_0 > R_1 > R_2 > 0, \end{aligned}$$

as well as the index I of $g(x)$ and an approximation to the largest zero R_0 of $g(x)$. In addition, the coefficients X_j, Y_j, Z_j in (1) and approximations to the units E_j are given; also tabulated are the quantities

$$(3) \quad F_j = \text{trace}(E_j^2) \quad (j = 1, 2),$$

which play an important role in our determination of the E_j . Of course, $g(x)$ is not unique but, as we explain in Section 3, we have tried to pick it so that I is minimal.

The table also lists the discriminant D and class number H of the field F as well as an approximation to its regulator R defined by

$$(4) \quad R = \left| \det \begin{pmatrix} \log|E_1| & \log|E'_1| \\ \log|E_2| & \log|E'_2| \end{pmatrix} \right|,$$

where E'_1, E'_2 are the conjugates of E_1, E_2 obtained by replacing R_0 in (1) by R_1 . The values for D and H have been copied from the table of Angell [1], as have most of the triples A, B, C . For $D < 20,000$, a list of discriminants and class numbers has been computed independently by Godwin [9] and others.

In Section 3 we give some of the details of the computer program which determined the X_j, Y_j, Z_j of (1). Here we give a brief outline of Cusick's algorithm on which the program is based. If F is a totally real cubic field with a defining integer r , then any integer λ in F is of the form

$$(5) \quad \lambda = x + yr + zQ(r),$$

where $Q(r)$ is a fixed quadratic in r with rational coefficients and x, y, z are rational integers determined by λ . For any α in F , we define

$$(6) \quad T(\alpha) = \text{trace}(\alpha^2) = \alpha^2 + \alpha'^2 + \alpha''^2, \quad \text{norm}(\alpha) = \alpha\alpha'\alpha'',$$

where $\alpha, \alpha', \alpha''$ denote the conjugates of $\alpha = \alpha^{(0)}$. As the function $T(\lambda)$ is a positive-definite ternary quadratic form in x, y, z whose values are rational integers, we can systematically change x, y, z and seek a minimal value of $T(\lambda)$ for λ 's which are units. The minimizing unit λ is denoted by ε_1 . We then continue computing $T(\lambda)$, if necessary, until another minimizing unit $\varepsilon_2 \neq \pm \varepsilon_1^m$, m a rational integer, is obtained. Cusick's result [5, Theorem 1] is:

THEOREM. *The units $\varepsilon_1, \varepsilon_2$ are a fundamental pair of units for the totally real cubic field.*

In the table, the defining integer r of F is called R_0 and the units $\varepsilon_1, \varepsilon_2$ are called E_1, E_2 .

It is a consequence of (3) and $|E_j E'_j E''_j| = 1$ that, for example, $F_j \geq E_j'^2 = 1/(E_j^2 E_j'^2) \geq 1/(F_j F_j)$ for $j = 1, 2$; more generally, for $i = 0, 1, 2$, we have $1/F_j \leq |E_j^{(i)}| \leq F_j^{1/2}$. As F_j is minimal, $|E_j^{(i)}|$ is not too small, and the relative error in computing $|E_j^{(i)}|$ should be good; the same is true of the absolute error in calculating $\log|E_j^{(i)}|$. Hence, the absolute error in finding the regulator R in (4) should be satisfactory.

Case No.	Field F			Fundamental Pair of Units							$E_j = (X_1 + R_0 Y_1 + R_0^2 Z_1) / I$							
	D	H	R	A	B	C	I	R_0	E_1	X_1	Y_1	Z_1	F_1	E_2	X_2	Y_2	Z_2	F_2
1	49	1	53	7	14	7	1	3.801938	1.247E+0	2	-4	1	5	-4.450E-1	-5	5	-1	5
2	81	1	85	6	9	1	1	3.532089	1.879E+0	0	-3	1	6	-3.473E-1	-2	4	-1	6
3	148	1	166	8	18	10	1	4.481194	1.481E+0	-3	-1	0	7	-1.939E-1	-7	6	-1	11
4	169	1	137	8	17	5	1	4.377203	2.651E+0	1	-4	1	8	-2.739E-1	-3	5	0	9
5	229	1	236	9	23	14	1	4.840803	-1.841E+0	3	-1	0	8	1.392E-1	3	-1	0	20
6	257	1	197	7	12	1	1	4.198491	1.199E+0	-3	-1	0	10	1.987E-1	-4	1	0	17
7	316	1	391	7	12	2	1	4.349233	-1.446E-1	-3	5	1	15	1.854E+0	1	-5	1	31
8	321	1	257	8	17	7	1	4.056428	1.709E+0	-3	1	0	13	1.135E-1	6	-6	1	16
9	361	1	195	10	27	11	1	5.283142	3.507E+0	2	-5	1	14	-2.219E-1	-4	6	-1	14
10	404	1	376	8	16	2	1	4.655442	-1.655E+0	3	-1	0	11	5.137E-2	-3	-4	1	43
11	469	1	385	10	28	17	1	5.391382	1.391E+0	-4	1	0	12	-6.406E-2	14	-8	1	68
12	473	1	284	9	22	11	1	5.128419	-2.128E+0	3	-1	0	10	-3.659E+0	-3	5	-1	21
13	564	1	540	10	28	18	1	5.514137	-4.514E+0	1	-1	0	27	-7.859E+0	-5	5	-1	63
14	568	1	609	11	34	22	1	5.761557	-1.354E-1	7	-7	1	23	-6.252E+0	-9	12	-2	67
15	621	1	540	9	21	6	1	5.145103	1.451E-1	-5	1	0	24	-3.290E+0	7	-2	0	51
16	697	1	271	9	20	1	1	5.164013	1.166E+0	-4	1	0	17	1.640E-1	-5	1	0	26
17	733	1	531	10	26	7	1	5.518199	-1.518E+0	4	-1	0	16	3.640E-2	-11	2	0	115
18	756	1	569	9	21	7	1	5.261802	-1.157E-1	-4	6	-1	27	1.493E+0	4	-11	2	111
19	761	1	353	11	34	23	1	5.891954	-1.892E+0	4	-1	0	13	1.080E-1	6	-1	0	29
20	785	1	410	10	27	13	1	5.575773	1.576E+0	-4	1	0	14	-5.884E-2	-8	7	-1	34
21	788	1	599	11	33	17	1	5.877404	1.226E-1	6	-1	0	31	2.755E+0	-9	2	0	67
22	837	1	680	9	21	8	1	5.361469	-2.361E+0	3	-1	0	12	-6.667E-3	-21	20	-3	300
23	892	1	832	10	25	2	1	5.597335	6.346E+0	-5	5	1	47	-3.504E+0	1	-12	2	195
24	940	1	891	9	20	2	1	5.292402	-6.548E+0	-5	-5	-1	63	-3.730E-2	9	-7	1	179
25	961	1	1220	13	46	32	2	7.297071	-2.741E+0	-26	32	-4	323	1.776E+1	2	-10	2	323
26	985	1	372	8	15	1	1	5.093763	2.094E+0	-3	1	0	13	9.376E-2	-5	1	0	29
27	993	1	555	10	27	15	1	5.733387	-2.692E+0	-4	6	-1	30	-8.171E-2	7	-7	1	33
28	1016	1	1013	8	15	2	1	5.177410	8.148E-2	1	5	-1	55	-8.436E+0	1	-7	1	183
29	1076	1	693	12	40	24	1	6.328872	1.329E+0	-5	1	0	19	1.338E-2	19	-3	0	291
30	1101	1	918	13	47	32	1	6.687400	7.577E+0	3	-6	1	60	-1.819E+1	-9	12	-2	339
31	1129	1	673	9	20	3	1	5.397462	-2.251E+0	1	-6	1	66	9.544E+0	-2	-4	1	93
32	1229	1	823	10	26	9	1	5.751532	1.752E+0	-4	1	0	16	4.128E-3	-23	4	0	515
33	1257	1	620	10	25	3	1	5.723956	-1.724E+0	-4	-1	0	18	-2.797E-2	13	-8	1	153
34	1300	1	655	12	38	14	1	6.423622	-1.424E+0	5	-1	0	23	1.875E-2	1	-13	2	183
35	1304	1	1195	10	25	2	1	10.022117	-2.800E+0	7	-11	0	23	2.267E-5	-49	55	-5	1303
36	1345	1	492	9	20	5	1	5.571201	-2.571E+0	3	-1	0	14	-3.988E-2	-8	7	-1	54
37	1369	1	313	14	53	29	1	7.187101	5.345E+0	4	-7	1	30	-1.576E-1	-6	8	1	30
38	1373	1	942	12	40	27	1	6.493932	-4.976E-2	10	-8	1	44	-3.779E+0	-1	14	-2	131
39	1384	1	1038	13	46	26	1	6.785667	-2.571E+0	11	-2	0	99	-2.573E-2	15	-9	1	103
40	1396	1	815	10	26	10	1	5.843404	8.495E-2	1	-6	1	59	3.758E+0	-3	7	-1	99
41	1425	1	668	11	32	13	1	6.113538	1.135E-1	-6	1	0	33	-7.694E+0	-7	6	-1	78
42	1436	1	1270	12	37	8	1	6.483612	3.278E-2	13	-2	0	163	1.624E+1	-3	-10	2	291
43	1489	1	336	11	30	1	1	6.142495	1.442E+0	-5	1	0	26	1.425E-1	-6	1	0	37
44	1492	1	765	11	31	7	1	6.126552	1.266E-1	-6	-1	0	35	5.649E+0	11	-7	1	119
45	1509	1	1130	10	26	11	1	5.925423	7.458E-2	6	-1	0	36	-5.994E+0	30	-12	1	612
46	1524	1	1045	11	33	21	1	6.273540	2.273E+0	-4	1	0	15	-1.161E-3	-65	48	-6	1731
47	1556	1	838	13	47	33	1	6.809786	-1.051E-1	8	-8	1	43	3.210E+0	-13	16	-2	259
48	1573	1	844	11	33	22	1	6.346462	-5.346E+0	1	-1	0	36	-1.177E-2	-21	16	-2	179
49	1593	1	633	12	39	21	1	6.487051	1.487E+0	-5	1	0	21	2.590E-2	13	-2	0	147
50	1620	1	1017	12	36	2	1	6.552475	-6.760E-2	-3	7	-1	39	1.186E+1	1	-18	3	219

Case No.	Field F				$g(x) = x^3 - Ax^2 + Bx - C$				Fundamental Pair of Units				$E_j = (X_j + R_0 Y_j + R_0^2 Z_j) / I$						
	D	H	R		A	B	C	I	R ₀	E ₁	X ₁	Y ₁	Z ₁	F ₁	E ₂	X ₂	Y ₂	Z ₂	F ₂
51	1708	1	12.87		11	32	14	1	6.210184	-9.510E-2	-5	7	-1	47	1.532E+1	15	-31	5	927
52	1765	1	9.44		13	45	20	1	6.890547	1.095E-1	-7	-1	0	44	-1.814E+1	1	11	-2	368
53	1772	1	15.37		43	32	6	1	42.245892	2.202E+0	77	-213	5	31	-4.028E-4	-1399	3793	-89	4687
54	1825	1	4.49		10	25	5	1	5.919089	1.919E+0	-4	1	0	18	8.091E-2	6	18	-2	38
55	1849	1	18.92		14	51	22	2	7.888236	6.615E-3	-14	-14	2	323	-1.023E+1	-38	-8	-2	323
56	1901	1	10.66		11	31	8	1	6.230725	3.461E+0	-9	2	0	83	-2.386E-2	11	-8	1	100
57	1929	1	8.22		13	46	27	1	6.902223	9.778E-2	7	-1	0	42	1.113E+1	-2	-5	1	150
58	1937	1	6.54		11	32	15	1	6.295540	-2.295E+0	4	-1	0	17	-2.648E-2	17	-9	1	137
59	1940	1	11.09		9	19	1	1	5.693995	5.694E+0	0	1	-1	183	-9.776E+0	13	-4	0	259
60	1944	1	15.60		12	39	22	1	6.584225	-1.134E+1	-3	5	-1	183	-1.236E+1	-31	16	-2	379
61	1957	2	4.55		13	47	34	1	6.911503	-1.912E+0	5	-1	0	20	8.850E-2	7	-1	0	40
62	2021	1	11.52		9	19	2	1	5.763724	-2.764E+0	3	-1	0	16	-5.087E+1	1	-9	0	3324
63	2024	1	15.77		11	30	2	1	6.254820	-1.870E+1	-3	10	-2	355	2.455E+1	1	-15	3	615
64	2057	1	6.78		12	37	9	1	6.602581	-1.603E+0	5	-1	0	25	2.141E-2	4	6	-1	102
65	2089	1	20.76		12	35	8	2	7.440552	2.116E+1	-6	-10	2	451	-2.874E+1	2	-8	0	1091
66	2101	1	8.54		14	54	37	1	7.283186	1.283E+0	-6	1	0	28	-7.751E-3	25	-18	2	259
67	2177	1	7.52		10	25	7	1	6.073562	7.356E-2	-6	1	0	38	-1.152E+1	-5	5	-1	145
68	2213	1	12.68		14	52	23	1	7.355968	-1.356E+0	6	-1	0	32	1.013E-3	1	44	-6	2515
69	2228	1	11.09		15	41	37	1	7.714645	-8.513E+0	-3	7	-1	75	5.480E+0	22	-33	4	535
70	2233	1	5.52		11	32	17	1	6.442683	2.443E+0	-4	1	0	17	-3.330E-2	10	-8	1	61
71	2241	1	8.26		12	39	23	1	6.669464	-8.466E+0	-4	6	-1	78	-1.314E+1	-2	5	-1	174
72	2292	1	14.36		13	43	3	1	11.931522	3.183E+0	4	-12	1	27	6.447E+1	-47	69	-5	4707
73	2296	1	14.27		14	51	16	1	7.401976	2.188E-2	3	7	-1	87	-8.829E+0	3	-9	1	279
74	2300	1	18.12		11	32	18	1	6.507903	1.581E-2	-13	2	0	163	-5.447E+1	1	11	-3	3023
75	2349	1	11.92		12	36	3	1	6.670622	8.473E+0	4	-6	1	84	9.947E+0	-10	-12	2	147
76	2429	1	13.28		14	50	9	1	7.453204	-6.157E-2	4	-8	1	48	3.521E+0	-10	54	-7	2560
77	2505	1	10.68		11	30	3	1	6.349967	-1.057E+1	-2	5	-1	116	1.814E+1	1	-10	2	339
78	2557	1	10.72		11	31	10	1	6.401222	1.437E+1	-1	-4	1	212	-3.658E-2	23	-10	1	380
79	2589	1	16.29		26	180	141	1	12.739724	-5.557E-2	16	-14	1	36	2.853E+1	10	-75	6	3540
80	2597	3	4.80		10	24	1	1	6.079119	2.079E+0	-4	1	0	20	7.912E-2	-15	1	0	40
81	2636	1	18.38		14	49	2	1	7.515853	3.171E-2	-15	2	0	227	-2.669E+1	15	17	-3	959
82	2673	1	7.76		12	39	25	1	6.816914	-6.500E-2	8	-8	1	66	2.068E+0	-6	8	-1	102
83	2677	1	11.16		12	38	17	1	6.726235	1.088E+1	-6	-6	1	128	-4.568E+0	4	-8	-1	152
84	2700	1	20.37		15	60	30	1	7.805603	-4.066E+0	-29	11	-1	543	-3.744E+0	31	-43	5	1285
85	2708	1	12.95		14	54	38	1	7.383185	-1.666E+1	-11	14	-2	291	-1.204E+1	-9	13	-2	487
86	2713	1	12.34		15	62	45	1	7.745141	2.608E-2	2	-8	1	93	-9.052E+0	-13	16	-2	147
87	2777	2	3.95		13	42	1	1	7.124784	1.125E+0	-6	1	0	37	1.248E-1	-7	1	0	50
88	2804	1	15.24		11	31	11	1	6.474194	-2.474E+0	4	-1	0	19	-2.124E-4	-170	91	-10	19219
89	2808	1	20.31		12	39	26	1	6.882021	-2.714E+1	-15	12	-2	771	-4.986E+1	-11	15	-3	2487
90	2836	1	9.69		10	24	2	1	6.151148	7.026E-2	1	6	-1	91	2.859E+0	-11	-12	2	259
91	2857	1	4.87		13	46	29	1	7.085532	-2.086E+0	5	-1	0	22	8.553E-2	-7	1	0	42
92	2917	1	11.93		13	43	6	1	7.112228	1.122E-1	-7	1	0	48	1.536E+1	-21	-2	1	692
93	2920	1	17.94		12	31	2	1	11.018119	-1.284E+1	9	-13	1	199	1.809E-3	1	55	-5	1703
94	2941	1	13.72		17	79	58	1	8.583487	-2.167E+0	15	-2	0	179	1.018E-2	-5	-8	1	204
95	2981	1	14.63		13	43	22	1	7.095000	9.300E-2	-7	1	0	44	2.550E+1	-39	2	1	2056
96	2993	1	7.51		13	44	13	1	7.101785	1.018E-1	-7	1	0	46	-3.204E+0	11	-2	0	115
97	3021	1	17.40		10	24	3	1	6.217581	2.858E+1	1	-9	2	819	-3.253E+0	50	-21	2	2244
98	3028	1	20.35		12	38	18	1	6.805342	9.665E+0	11	-7	1	147	-1.554E+1	17	-32	4	2307
99	3124	1	19.56		15	59	33	2	8.552799	-4.864E+0	-5	6	0	39	1.530E+2	-5	76	-13	23799
100	3132	1	22.49		15	57	15	2	8.506642	-1.328E-2	-34	4	0	291	-5.250E+0	134	-34	-2	3903

Case No. Field F $g(x) = x^3 - Hx^2 + Bx - C$ Fundamental Pair of Units $E_j = (X_j + R_0 Y_j + R_1 Z_j) / I$

Case No.	D	H	R	A	B	C	I	R ₀	E ₁	X ₁	Y ₁	Z ₁	F ₁	E ₂	X ₂	Y ₂	Z ₂	F ₂
101	3137	1	7.81	12	37	11	1	6.787759	1.788E+0	-5	1	0	25	-1.416E-2	15	9	1	173
102	3144	1	24.86	14	49	12	2	8.209050	-6.277E-3	-118	39	-3	2917	-2.412E+0	146	-43	3	4551
103	3173	1	15.47	15	61	38	1	7.825476	-1.669E-2	17	-10	1	136	5.983E+0	23	-10	1	272
104	3221	1	16.39	11	31	14	1	6.662465	7.414E+0	3	-6	1	84	2.849E+1	13	-11	2	868
105	3229	1	14.78	10	24	5	1	6.337317	1.681E+1	22	-4	1	284	-4.436E+0	6	-27	4	1384
106	3252	1	17.26	11	31	15	1	6.717741	-4.937E-2	2	-10	1	267	4.351E+0	-104	43	-4	6313
107	3261	1	18.76	14	54	39	1	7.469990	4.088E-2	4	-8	1	96	8.907E+1	50	-62	0	8160
108	3281	1	7.45	14	51	17	1	7.512680	-1.513E+0	6	-1	0	34	2.536E-2	-15	2	0	211
109	3305	1	9.53	11	30	5	1	6.509040	4.313E+0	1	-6	1	58	1.282E+1	3	-5	1	169
110	3316	1	9.43	15	59	23	1	7.901190	9.881E-2	8	-1	0	59	3.704E+0	-20	3	0	363
111	3325	1	13.26	12	38	19	1	6.874076	-4.748E+0	9	-2	0	83	8.461E-3	-6	-6	1	248
112	3356	1	21.93	14	50	24	2	8.366910	-3.367E+0	10	-2	0	31	-3.992E-5	-734	322	-28	86575
113	3368	1	23.05	17	78	50	1	8.658042	3.932E-2	3	-9	1	71	6.238E+1	-39	55	-5	12103
114	3496	1	17.20	15	62	46	1	7.841222	-8.624E-2	9	-9	1	71	5.564E+1	59	-71	9	4295
115	3508	1	10.04	13	45	23	1	7.174972	-8.045E-2	-6	-8	-1	75	2.416E+0	13	-23	3	651
116	3540	1	20.31	14	50	10	1	7.567030	1.443E-2	1	-15	2	303	-3.602E+1	-7	34	-5	1419
117	3569	1	7.79	13	46	31	1	7.232331	2.232E+0	-5	1	0	22	-1.670E-2	20	-10	1	169
118	3576	1	27.75	14	50	28	2	8.512976	9.367E+0	10	-16	2	195	-1.271E+2	2	38	-8	16311
119	3580	1	21.09	13	41	13	2	8.184732	1.988E+1	4	-12	2	419	-8.781E+0	94	-30	1	1823
120	3592	1	18.70	16	67	26	1	8.341806	-1.694E-2	-11	18	-2	227	-1.624E+1	45	1	-1	2311
121	3596	1	23.05	12	37	12	1	6.846885	7.248E-2	1	-7	1	95	-1.745E+2	-43	125	-21	36175
122	3604	1	9.32	16	68	34	1	8.305810	-1.704E+0	7	-1	0	43	8.384E-3	9	-26	3	603
123	3624	1	28.01	11	39	1	1	6.578921	1.398E+1	1	-5	1	135	1.762E+2	-91	-12	8	39747
124	3721	1	13.71	30	239	207	1	4.074980	4.008E+1	127	-138	9	1405	-2.434E-2	-131	141	-9	1605
125	3732	1	19.08	13	43	9	1	7.206330	4.952E+0	-5	23	-3	927	2.785E-2	7	-37	5	1935
126	3736	1	17.86	13	42	2	1	7.225800	5.895E+0	1	-21	3	471	-3.289E+1	1	17	-3	1079
127	3753	1	8.04	13	60	31	1	7.910752	8.929E-2	8	-1	0	57	2.822E+0	-13	12	0	147
128	3873	1	12.01	14	49	3	1	7.627161	1.041E+1	-2	-6	1	114	-4.687E+0	1	-16	2	435
129	3877	1	13.44	14	52	25	1	7.555673	1.556E+0	-6	1	0	32	1.055E-3	-68	9	0	4188
130	3887	1	7.03	11	30	7	1	6.641892	-2.642E+0	4	-1	0	21	-2.041E-2	9	-8	1	98
131	3892	1	13.04	12	38	22	1	7.057087	5.709E-2	-7	1	0	47	-1.429E+1	21	-5	0	503
132	3941	1	17.77	17	77	42	1	8.737949	-2.774E-2	11	-10	1	76	-2.600E+1	-31	53	-6	1252
133	3957	1	22.29	17	78	60	2	9.326577	-1.185E+1	-6	-9	-1	144	2.980E+1	154	-178	18	14067
134	3969	3	4.20	18	87	55	1	9.137763	7.259E+0	6	9	1	54	-1.211E-1	-8	10	-1	54
135	3973	3	12.59	18	87	62	2	9.651205	-1.328E+1	-14	18	-2	195	-1.750E-2	26	-22	2	195
136	3973	1	13.15	12	38	23	1	7.111039	-3.111E+0	4	-1	0	20	6.485E-4	64	-9	0	3972
137	3981	2	10.63	13	45	24	1	8.248898	-2.249E+0	5	-1	0	24	4.408E-3	29	-4	0	771
138	3988	1	11.49	11	19	7	1	8.968502	-1.494E+1	3	-2	0	227	1.694E+1	-1	2	0	291
139	4001	1	10.59	12	37	13	1	6.935152	6.485E-2	7	-1	0	49	6.805E+0	-14	3	0	210
140	4065	1	14.12	13	46	33	1	7.357463	-6.357E+0	4	-1	0	54	-2.962E+1	-17	13	-2	918
141	4104	1	23.76	15	57	19	2	8.697700	2.698E+0	-12	2	0	39	-2.497E-5	606	-348	32	85731
142	4193	1	11.10	14	53	33	1	7.589844	1.407E+1	-6	-6	1	202	-1.607E+1	-4	6	-1	262
143	4212	3	5.46	12	36	6	1	6.930454	1.930E+0	-5	2	0	27	6.955E-2	7	-1	0	51
144	4281	1	15.30	13	40	17	1	7.267567	-1.848E+1	-2	5	-1	354	-2.445E-2	14	-31	4	1449
145	4312	3	7.23	13	40	8	2	8.292951	6.182E+1	-6	9	-1	55	-1.932E+0	2	-9	1	87
146	4345	1	30.53	19	98	74	1	9.545803	1.267E-2	59	-73	7	2871	7.484E+0	207	-250	24	31203
147	4365	1	9.16	10	23	1	1	6.467859	8.468E+0	0	0	0	54	5.934E+0	-7	2	0	83
148	4360	1	23.57	11	30	10	1	6.810821	-2.679E+1	-1	3	-1	743	4.645E+0	37	15	-3	4359
149	4364	1	25.75	16	56	28	2	7.046483	4.648E-2	-18	1	0	79	-3.265E+1	-890	254	-18	150335
150	4409	1	9.62	11	50	11	2	6.861319	4.1847E-2	1	-7	1	129	-1.477E+1	-2	5	-1	226

Case No.	Field F								Fundamental Pair of Units								$E_j = (X_j + R_0 Y_j + R_0^2 Z_j) / I$							
	D	H	R	A	B	C	I	R ₀	E ₁	X ₁	Y ₁	Z ₁	F ₁	E ₂	X ₂	Y ₂	Z ₂	F ₂						
151	4481	1	40-12	15	58	32	2	8,863876	-8,587E+0	-22	36	-4	835	1,-689E-4	-62	202	-22	37891						
152	4489	1	19-70	17	74	43	3	10,085427	-6,375E-3	-47	45	-4	714	2,403E+1	15	-34	3	714						
153	4493	1	20-11	13	43	10	1	7,288465	1,239E+1	0	-6	-1	156	9,753E+1	13	-54	9	9696						
154	4594	1	21-92	11	29	1	1	6,683060	6,683E+0	0	1	0	53	1,232E-4	91	-99	13	16947						
155	4597	1	15-31	14	50	11	1	7,640286	-2,640E+0	6	-1	0	36	5,347E-4	-74	2	1	6000						
156	4628	1	16-72	14	52	26	1	7,653249	-2,435E+1	-7	13	-2	593	-3,334E+1	-11	23	-4	2851						
157	4641	1	13-33	13	42	3	1	7,312360	-2,675E-2	5	-8	1	90	5,571E+0	1	-14	2	243						
158	4649	1	12-92	12	37	13	1	7,060432	6,043E-2	7	1	0	387	4,473E+1	-11	-2	1	749						
159	4684	1	18-88	17	64	34	1	8,822294	-1,975E+1	-5	16	-2	2	1,664E+1	-1	2	0	483						
160	4692	1	21-19	14	48	12	2	8,550309	3,353E+0	2	-8	1	51	-2,777E-4	94	-182	20	24891						
161	4729	1	4-49	15	56	1	1	8,110974	1,111E+0	-7	1	0	50	1,110E-1	-8	1	0	65						
162	4749	1	23-60	16	70	51	1	8,339652	1,415E-2	-11	18	-2	387	4,090E+0	76	-93	10	9216						
163	4764	1	32-10	14	53	34	1	7,661600	-1,007E+1	-5	7	-2	111	-4,359E+2	33	138	-26	206115						
164	4765	1	17-65	13	45	26	1	7,379390	2,379E+0	3	-4	0	24	-1,179E-4	-257	116	-11	34388						
165	4825	1	36-40	14	47	2	2	8,495135	9,730E-3	34	-4	0	323	4,299E+1	-826	140	-8	69443						
166	4841	1	9-11	16	69	43	1	8,370366	1,370E+0	-7	1	0	41	-1,100E-2	22	-11	1	246						
167	4844	1	28-52	13	44	18	1	7,338368	1,616E+1	-1	-5	1	271	-2,320E+2	-43	99	-17	53983						
168	4852	1	15-26	11	17	5	1	9,213847	-4,757E+0	-12	10	-1	91	-3,609E-3	27	-49	5	1083						
169	4853	1	19-96	14	14	3	1	12,935648	-3,768E+0	-10	-14	1	48	-2,168E-4	-151	348	-26	11827						
170	4857	1	14-15	17	78	51	1	8,763635	1,049E+1	4	-8	1	117	6,577E+0	-28	39	-4	1677						
171	4860	1	30-54	30	237	178	1	14,765898	-1,147E-2	-33	17	-1	399	1,995E+1	889	-1122	72	116643						
172	4892	1	30-19	12	37	16	1	7,117176	1,365E+0	29	-11	1	559	-1,074E-4	129	-132	16	24515						
173	4933	1	15-44	11	29	2	1	6,743614	1,465E-2	7	-6	1	188	-2,458E+0	1	-14	2	515						
174	5073	1	14-29	16	67	27	1	8,444316	-1,444E+0	7	-1	0	102	1,154E-3	74	-9	0	5322						
175	5081	1	9-90	12	37	17	1	7,170782	-5,384E-2	-6	8	-1	102	1,140E+1	3	-6	1	1449						
176	5089	1	11-65	14	51	19	1	7,684845	1,697E+0	-6	6	0	134	-2,389E-3	25	-34	4	1459						
177	5172	1	23-69	16	64	12	2	9,145480	-2,907E+0	2	-10	1	111	-3,937E-4	-70	218	-23	32943						
178	5204	1	22-71	14	48	20	2	8,688464	-1,537E+1	-6	6	-1	239	-4,754E+1	14	-30	2	3979						
179	5241	1	18-48	16	66	19	1	8,486250	2,350E-2	17	-2	0	275	-6,441E+0	36	-5	0	1228						
180	5281	1	9-94	14	65	35	1	7,727511	-3,894E+0	-6	8	-1	78	1,635E+1	3	-6	1	269						
181	5297	1	11-61	12	37	19	1	7,270200	-3,270E+0	4	-14	0	22	-1,825E-3	-45	28	-3	1177						
182	5300	1	17-89	28	208	166	1	13,775451	5,907E+0	9	-14	0	43	2,991E+1	297	-350	24	13233						
183	5325	1	27-47	16	61	32	1	7,708850	4,936E-3	97	-20	6	6483	1,331E+2	-28	-56	9	17208						
184	5327	1	19-25	14	52	1	3	9,818819	-2,571E+0	3	-60	2	2163	-4,644E+1	29	26	-4	2163						
185	5353	1	22-00	13	45	28	1	7,493311	1,338E-2	13	-2	0	211	1,945E+1	-33	7	0	1132						
186	5353	1	8-19	13	44	19	1	7,403519	-2,404E+0	5	-1	0	26	1,254E-2	3	7	-1	201						
187	5356	1	24-63	13	12	2	1	12,015112	-1,893E+0	-13	61	-5	999	1,258E-3	-71	78	-6	3171						
188	5368	1	24-46	18	83	20	1	9,367485	1,232E+0	-89	19	-1	7095	-5,059E-3	-143	34	-2	18083						
189	5369	1	11-04	15	58	17	1	8,092261	9,226E-2	-8	1	0	61	-2,159E+1	-12	15	-2	521						
190	5373	1	21-31	18	84	29	1	9,329348	1,196E-2	28	-3	0	732	-6,550E+1	-16	60	-7	4320						
191	5468	1	30-66	18	85	38	1	9,296159	-1,759E+1	1	-2	0	547	-4,417E+1	-49	47	-5	2671						
192	5472	1	22-72	12	22	9	1	9,861687	2,836E+1	10	-8	1	836	5,981E+1	2	-4	1	3580						
193	5497	1	39-31	16	67	44	2	9,313195	-2,454E+1	-10	14	-2	707	-7,514E+1	-3030	868	-60	1411907						
194	5521	1	5-71	12	35	1	1	7,068398	2,068E+0	-5	1	0	29	6,840E-2	-7	1	-0	53						
195	5529	1	13-78	16	65	11	1	8,537114	-4,829E-2	-4	9	-1	78	-4,895E+1	-5	29	-4	2433						
196	5556	1	21-74	17	77	43	1	8,389905	-2,678E+0	15	-2	0	195	-7,804E-4	63	-69	7	4083						
197	5613	1	28-27	17	79	60	1	8,783959	4,363E+0	-17	20	-2	531	9,614E-4	61	-86	9	7920						
198	5620	1	15-78	11	29	5	1	6,905030	2,905E+0	-4	1	0	23	9,524E+1	14	-78	13	17579						
199	5621	1	22-79	17	75	26	1	8,909973	9,003E-2	9	-1	0	76	-1,124E+1	175	39	-8	48254						
200	5624	1	29-64	17	72	8	2	9,543212	6,184E+0	2	-18	2	163	-2,1137E-4	82	-209	21	26519						

Case No. Field F $g(x) = x^3 - Ax^2 + Bx - C$ E_1 X_1 Y_1 Z_1 F_1 E_2 X_2 Y_2 Z_2 F_2

$E_j = (X_j + R_0 Y_j + R_1 Z_j) / I_j$

201	5629	1	13.75	18	86	47	1	9.267435	-1.267E+0	8	-1	0	56	-1.404E-3	50	-61	6	2720
202	5637	1	27.21	17	17	4	1	15.949885	3.610E+1	5	-14	1	1320	2.102E-4	-63	-12	1	9528
203	5684	3	5.73	15	61	41	1	8.073185	-2.073E+0	6	-1	0	331	7.318E-2	-8	1	0	55
204	5685	1	29.72	13	45	30	1	7.595348	7.306E+1	17	-23	4	5364	-9.425E+1	-13	21	-4	7104
205	5697	1	12.18	15	60	33	1	8.078653	7.885E-2	-8	1	0	37	-3.808E-1	57	-112	12	1497
206	5724	1	29.55	12	21	8	1	9.975172	1.695E+1	-3	2	0	291	1.338E+2	15	-46	4	24771
207	5741	1	19.78	11	29	6	1	6.953570	4.634E-2	7	-10	0	56	-1.536E+1	125	-46	4	13315
208	5780	1	22.07	13	45	31	1	7.642840	1.540E-2	18	-10	0	139	-2.877E+1	40	-25	4	18319
209	5821	1	18.36	13	45	32	1	7.688338	-6.688E+0	1	-1	0	56	7.723E+1	33	-25	4	6128
210	5853	1	27.69	13	43	12	1	7.430084	-6.223E+1	-5	22	-4	3891	-1.151E+2	-11	38	-7	13272
211	5901	1	27.58	16	64	3	1	8.590936	-2.074E+1	-2	15	-2	432	3.383E+1	10	-212	25	39492
212	5912	1	31.96	14	51	20	1	7.759849	1.290E+1	7	-7	0	183	1.558E+2	63	-151	21	35671
213	5925	1	29.50	22	28	9	1	20.666204	-1.407E+2	4	-7	0	19788	-2.183E+0	694	-943	44	28768
214	5940	1	21.00	12	36	10	1	7.180140	-5.360E+0	9	-2	0	99	-9.574E+1	-27	31	-6	9243
215	5980	1	27.52	16	69	44	1	8.453029	-2.756E+1	3	14	-2	80	-5.460E+1	-27	39	-5	3039
216	6053	1	23.69	18	88	65	1	9.221237	1.221E+0	-8	1	0	52	-1.035E-2	-696	389	-34	207192
217	6088	1	26.75	12	35	2	1	7.131567	6.172E-2	1	7	-1	135	3.205E+2	9	-156	28	111491
218	6092	1	32.63	18	85	48	2	9.916692	2.038E+0	-86	19	-1	1375	3.017E-4	-238	24	0	13251
219	6108	1	40.49	34	49	18	1	32.509793	5.274E+0	535	-699	21	2703	-4.004E+2	583	-843	25	164367
220	6133	1	20.23	21	119	92	1	10.514049	2.810E-2	-21	2	0	371	-6.598E+0	67	-7	0	3716
221	6153	1	16.34	14	53	37	1	7.846027	-5.410E-2	9	-9	1	117	5.540E+1	21	-27	4	3177
222	6184	1	32.17	15	54	20	2	9.067092	-1.413E+1	-24	63	-7	3239	-5.018E-3	32	-67	7	3879
223	6185	1	12.42	13	49	5	1	7.800409	-1.801E+0	6	-1	0	38	3.047E-3	-39	5	0	1553
224	6209	1	13.38	13	44	21	1	7.520893	2.531E+0	-5	1	0	26	-1.148E-3	-34	-3	1	1858
225	6237	1	25.53	12	36	11	1	7.233194	-1.285E-2	20	-10	1	300	-1.396E+1	-74	30	-3	4296
226	6241	1	4.70	20	107	71	1	10.121309	8.230E+0	7	-10	1	69	-1.083E-1	-9	11	-1	69
227	6268	1	25.82	15	56	2	1	8.202724	4.046E+1	4	-28	4	1667	-1.042E+2	1	-61	9	11279
228	6289	1	11.30	13	42	5	1	7.459324	-3.308E-2	4	-8	1	109	-3.033E+0	1	-8	1	178
229	6396	1	40.03	16	65	26	2	9.336008	1.938E+1	-20	-3	1	485	-1.352E+2	22	-50	2	29475
230	6401	1	16.56	19	98	75	1	9.649566	-3.1110E-2	13	-11	1	89	-3.762E+0	-53	63	-6	2694
231	6420	1	28.31	19	95	47	1	9.757997	-3.077E-3	-34	23	-2	69	4.592E+0	43	-82	8	4323
232	6452	1	21.94	13	43	13	1	7.492505	1.499E-2	15	-2	0	227	-7.742E+0	55	-16	1	2635
233	6453	1	24.53	15	57	10	1	8.186658	1.795E+0	9	-50	6	3459	-2.974E-3	-85	27	-2	6756
234	6508	1	27.05	14	53	38	1	7.900053	2.379E+0	-15	18	-2	611	5.235E-4	97	10	0	5403
235	6549	1	27.17	14	50	13	1	7.814589	-1.799E+0	-6	1	0	36	-1.743E-6	1102	-774	81	1202848
236	6556	1	32.25	13	44	22	1	7.574473	2.970E+1	-2	-14	2	1059	5.546E-4	-39	-10	2	43619
237	6557	1	25.11	14	52	29	1	7.836919	4.674E+0	-11	2	0	115	-1.590E-4	-134	166	-19	28519
238	6584	1	31.18	15	58	18	1	8.172656	3.345E+0	-13	2	0	163	7.788E-5	505	-119	7	21265
239	6588	1	33.60	15	60	34	1	8.149602	-6.960E-2	9	-1	1	111	-4.750E+2	533	-849	89	1957503
240	6601	1	20.24	12	35	3	1	7.190470	-1.137E-2	13	-9	-1	201	4.134E+1	2	-23	4	2190
241	6616	1	48.49	15	56	24	2	9.191483	-5.922E-3	70	-26	2	867	-8.182E+1	1642	-463	29	511959
242	6637	1	16.63	15	59	26	1	8.160394	-1.191E-2	17	-10	1	172	-5.481E+0	19	-3	0	336
243	6669	1	21.97	12	36	13	1	7.331596	-1.233E+1	15	-4	0	387	5.213E-3	22	23	0	516
244	6681	1	25.56	14	51	21	1	7.826545	-1.064E-2	17	-10	1	213	5.184E+0	-4	9	-1	246
245	6685	1	22.20	16	70	51	1	8.491479	1.704E-2	17	-2	0	243	3.763E+1	68	-80	3	6264
246	6728	1	35.02	12	19	4	1	10.193875	5.795E+1	5	-5	1	3367	1.842E+2	5	-13	3	33991
247	6809	2	6.33	14	53	39	1	7.951255	-2.951E+0	5	-1	0	25	4.874E-2	8	-1	0	58
248	6856	1	31.05	23	4	2	1	22.378390	9.911E+0	-9	23	10	39	-1.452E+3	-3795	16978	-754	9988579
249	6886	1	12.95	17	79	61	1	8.863517	-7.334E-2	10	-10	1	107	4.220E+0	-26	30	-3	1227
250	6885	3	8.95	12	36	15	1	7.421656	-3.142E+0	4	-1	0	24	-1.384E+1	1	-2	0	243

2. Other Tables and Methods. Most other tables of fundamental units use a method of Voronoï [15]. An account of this is given in the book of Delone and Faddeev [6, Chapter IV, Part A]. However, the Voronoï algorithm is very complicated, since it depends on a detailed consideration of sequences of points in various lattices.

We know of only two published tables of more than a few cases of fundamental pairs of units in general totally real cubic fields. The first of these, due to Billevich [2], lists the 33 fields (plus 7 duplications) with discriminant $D < 1,300$. He gives the field discriminant, an integral basis, a defining polynomial for the field, and the coefficients of the fundamental pair with respect to this basis. Billevich uses his own method for the calculation of the units. With this method, computational difficulties arise for discriminants larger than the small ones considered by Billevich (see Steiner and Rudman [14]). The second table, by Williams and Zarnke [16], gives fundamental pairs for various fields determined by irreducible cubic equations; for example, they list the coefficients of a fundamental pair with respect to the natural integral basis for all the totally real cubic fields defined by $x^3 - px - q = 0$ with $|p| \leq 15$, $|q| \leq 15$. The discriminants of the fields are not given, and no attempt is made to indicate different pairs p, q that give the same field. The Voronoï algorithm was used to compute the units, and an account of how this algorithm was implemented is given.

Among the unpublished tables is a large one of Angell who describes it in [1]. This was obtained by using the Voronoï procedure on the 4,804 fields with $D < 100,000$. The actual table gives the field discriminant, the class number of the field, a defining polynomial with its index, and the coefficients in a representation (1) of the fundamental units. It is known that about ten fields with $D > 30,000$ are missing from this table, and that some of the fundamental units are wrong (see Ennola and Turunen [7], and Llorente and Oneto [12]). There are other errors in [1], and apparently also in [12] (see Ennola and Turunen [7]). Some of these errors presumably result from mistakes in programming the Voronoï algorithm for the computer, but neither [1] nor [12] gives details about how this was done.

There is a still larger unpublished table of Ennola and Turunen [7] who applied Voronoï's method to the 26,440 fields with $D < 500,000$. No errors are known in this table, but 300-digit precision was used to handle the worst cases. The actual table gives the ordinal number for each field in the list, the field discriminant and class number, coefficients for an integral basis, a defining polynomial, and coefficients in a representation of two fundamental units with respect to the given integral basis.

The Voronoï procedure is certainly much faster than the method of the present paper for the worst cases (essentially those in which the fundamental units have at least one large conjugate). On the other hand, the necessary programming for the Voronoï algorithm is quite intricate, as is shown by the errors in previous tables produced by that method.

One advantage of the Cusick procedure [5] is its extreme simplicity. Another advantage of the procedure used here is that it makes easier the computation of the regulator R of the cubic fields. As noted in Section 1, for our units, the $|E_j^{(i)}|$ are not small, so that R can be computed with good accuracy. However, other algorithms, including Voronoï's, can perform badly in this respect. There is a good example of

this in the small table of units and regulators given by Pohst, Weiler and Zassenhaus [13, p. 301]. Even for as small a discriminant as 961, their method (which is based on the geometry of numbers, but is different from Voronoï's) gives a value for the regulator which is in error by 0.16% in spite of a machine precision of 14 digits. This happened, in part, because one of the units in their fundamental pair has a small conjugate.

Regulators are not given in the first four tables mentioned. However, the units in the table of Ennola and Turunen [7] can be used for the accurate computation of regulators. This is because the unit pairs given in their table are not the pairs produced by the Voronoï algorithm, but rather are normalized pairs derived from the Voronoï units. A comparison of Ennola and Turunen's normalized pairs with our pairs shows that in each of the 250 fields, our first unit E_1 agrees with one of their units, but this is not always the case for the unit E_2 .

We remark that in the special case of cyclic cubic fields, the discriminant is a square, and there always exists a fundamental pair made up of a unit and one of its conjugates. Cohn and Gorn [3] and Gras [11] use procedures simpler than Voronoï's to construct tables of units in the cyclic case, although Gras does not list the units. The method of the present paper becomes much simpler in the cyclic case and always gives a fundamental pair made up of two conjugate units [4, Theorem 2], but we have chosen not to make a separate table for the cyclic case.

3. The Computer Program. This was initially written for and tested on the HP-85 microcomputer and subsequently modified and run on the CDC 6400 mainframe which produced the table above. With the exception of R_0 , E_1 , E_2 , R and certain bounds, all computations were done in integer arithmetic.

For each of the totally real cubic fields F with discriminant $D \leq 6,885$, we used the table of Angell [1] to copy the value of D, H and the coefficients a, b, c of a polynomial

$$h(x) = x^3 - ax^2 + bx - c,$$

one of whose roots, say r , generates F . Let I_h be the index of $h(x)$ and let D_h be its discriminant, so that $D_h = -4a^3c + a^2b^2 + 18abc - (4b^3 + 27c^2)$.

If $D_h = D$, then $I_h = 1$ and $1, r, r^2$ form an integral basis for F , called a "power basis". In this case, the program takes $g(x)$ in (2) to be $h(x)$. Then, by Angell's choice of a, b, c , the smallest zero R_2 of $g(x)$ is in the interval $(0, 1)$ and $A, B, C > 0$.

If $D_h \neq D$, we attempted to reduce I_h so as to obtain a power basis. To this end, the program forms the irreducible monic polynomial $H(z) = (\gamma z + \delta)^3 h(\zeta) / \phi$, where $\zeta = (\alpha z + \beta) / (\gamma z + \delta)$ and $\phi = \gamma^3 h(\alpha / \gamma)$, for various rational integers $\alpha, \beta, \gamma, \delta$ in $[-10, 10]$ such that $\alpha\delta \neq \beta\gamma$ and $H(z)$ has integral coefficients; of course, $H(z)$ also generates F . If any $H(z)$ has $I_H = 1$, then we let $G(z) = H(z)$; otherwise, $G(z)$ was taken to be an $H(z)$ with the least index I_H that arose from this procedure. Letting ρ be the smallest zero of $G(z)$, we defined $g(x) = G(x + [\rho])$, guaranteeing that the smallest zero R_2 of $g(x)$ is in $(0, 1)$ and $A, B, C > 0$; also, $I_g = I_G$.

In the 250 cases we calculated, this algorithm resulted in 25 cases of index 2 compared with 45 cases in Angell's table [1] and 54 cases in the table of Ennola and Turunen [7]; we also had 2 cases of index 3, compared with 4 cases in the tables of

Angell and Ennola-Turunen. It is possible, of course, that further calculation would reduce the index in some, but not all, of these cases; e.g., in the case of $D = 961$, no polynomial has index 1.

Given the polynomial $g(x)$, the program computes its zeros $R_0 > R_1 > R_2$ in (2). Next the program finds an integral basis $1, R_0, S$ for the field F . If $I_g = 1$, the program takes $S = R_0^2 = Q(R_0)$. Otherwise, a standard algorithm of Voronoï (see Delone and Faddeev [6, pp. 108–112]) was used to determine

$$S = (u + vR_0 + R_0^2)/I = Q(R_0)$$

for suitable rational integers u, v , which are obtained from a solution of a simultaneous pair of congruences involving $g(x)$ and $g'(x)$.

For any integer λ in F , (6) and (5) with $r = R_0$ give $T(\lambda) = F(x, y, z)$, where

$$\begin{aligned} F(x, y, z) &= \sum_{k=0}^2 \{x + yR_k + zQ(R_k)\}^2 \\ &= a_0x^2 + b_0y^2 + c_0z^2 + 2(a_1yz + b_1xz + c_1xy) \end{aligned}$$

for suitable rational integers $a_0, b_0, c_0, a_1, b_1, c_1$; of course, $a_0 = 3$ and all these coefficients are expressible in terms of the power symmetric functions of the zeros R_k of $g(x)$ or, alternatively, in terms of A, B, C . The program calculates these six integers and also the ten integers occurring in $N(x, y, z) = \text{norm}(\lambda)$, where

$$\begin{aligned} (7) \quad N(x, y, z) &= \prod_{k=0}^2 \{x + yR_k + zQ(R_k)\} \\ &= a_2x^3 + b_2y^3 + c_2z^3 + a_3x^2y + b_3x^2z \\ &\quad + c_3xy^2 + d_3y^2z + e_3xz^2 + f_3yz^2 + g_3xyz. \end{aligned}$$

The last function is needed to test whether $N(x, y, z) = \pm 1$, i.e., whether λ is a unit of F .

To facilitate the search for the minima of the positive-definite quadratic form $F(x, y, z)$, the program next determines the real coefficients k_j appearing in the identity

$$(8) \quad F(x, y, z) = (k_1x + k_2y + k_3z)^2 + (k_4y + k_5z)^2 + (k_6z)^2,$$

where

$$\begin{aligned} k_1 &= a_0^{1/2}, \quad k_2 = c_1a_0^{-1/2}, \quad k_3 = b_1a_0^{-1/2}, \quad k_4 = (b_0 - k_2^2)^{1/2}, \\ k_5 &= (a_1 - k_2k_3)/k_4, \quad k_6 = (c_0 - k_3^2 - k_5^2)^{1/2} = (D/a_0)^{1/2}/k_4. \end{aligned}$$

The final step is to search the values of $F(x, y, z)$ until the fundamental units ϵ_1, ϵ_2 of the Theorem above are found. This is done by picking a number L (say $D^{1/2}$) and only considering x, y, z such that $F(x, y, z) \leq L$, a condition which imposes bounds on z, y, x , as we now explain. If the last inequality holds, then (8) shows that $|z| \leq L^{1/2}/k_6 \equiv Z_2$; as $F(x, y, -z) = F(-x, -y, z)$, it suffices to consider $z \geq 0 \equiv Z_1$. Thus, z must lie in the interval $[Z_1, Z_2]$. For a given z of this kind, (8) also gives $|k_4y + k_5z| \leq (L - k_6^2z^2)^{1/2}$, so that y is confined to some interval $[Y_1, Y_2]$ depending on z . Similarly, for given z, y , (8) implies that x must lie in some $[X'_1, X'_2]$. Finally, if we let $V_k = yR_k + zQ(R_k)$, then (7) shows that $N(x, y, z) < -1$ if

$x < X_1''$, and $N(x, y, z) > 1$ if $x > X_2''$, where

$$X_1'' = \min(-V_0, -V_1, -V_2) - 1, \quad X_2'' = \max(-V_0, -V_1, -V_2) + 1.$$

Hence, x can be restricted to $[X_1, X_2]$, where the bounds $X_1 = \max(X_1', X_1'')$ and $X_2 = \min(X_2', X_2'')$ depend on z, y . (Actually, x can be confined to the union of three subintervals of $[X_1, X_2]$.)

For given z, y, x in their respective ranges, the program checks the condition $N(x, y, z) = \pm 1$; if this is not satisfied, then the corresponding λ is not a unit and the next largest x is tried. Otherwise, the triple (x, y, z) is stored in a table for units after standardizing so that $N(x, y, z) = +1$. The value $F(x, y, z)$ is computed and compared with the previous minimum value for F , thereby keeping this minimum current. Once a unit λ_0 satisfying $T(\lambda_0) \leq L$ has been found, the program checks the condition $z > T(\lambda_0)^{1/2}/k_6$. If this holds, then $F(x, y, z) > T(\lambda_0)$, so that no additional z 's need be tried; i.e., the current minimum value for F is F_1 , and the z, y, x that produces F_1 defines $\varepsilon_1 = E_1$.

The program lets z, y, x run over their respective ranges. If no unit λ with $T(\lambda) \leq L$ is found, then L is doubled and the process is repeated.

Once ε_1 has been found, the program continues its search with the current value of L . Whenever it finds a unit λ , it checks that $\lambda \neq \pm \varepsilon_1^m$ for each integral m . If this is satisfied, then λ becomes a candidate for ε_2 ; the value $T(\lambda)$ is now used to replace L , and appropriate bounds on z, y, x are recomputed. If no independent unit λ is found after z, y, x have run through all their values, then L is doubled and the computation is started from the beginning. Ultimately, a unit $\lambda \neq \pm \varepsilon_1^m$ is found, and the minimum of $T(\lambda)$ for such λ is defined as F_2 with the associated λ defined as $\varepsilon_2 = E_2$.

In passing, we remark that our original HP-85 program reduced the positive-definite ternary form $F(x, y, z)$ to Gauss form. However, the running time for this search was no better than for the reduction in (8). We also tried changing the roles of x, y, z in (8), but here, also, we achieved no improvement.

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